



Theoretical Study of the Atomic Structure and the Radiative Parameters of Lowly and Moderately Ionized Heavy Elements

Applications to Cosmochronology and to the Spectral Analysis of Compact Astrophysical Objects

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Contents

General Introduction

1	\mathbf{Ast}	rophys	ical Context 5	
	1.1	The Li	ife of a Star	
		1.1.1	The Hertzprung-Russel Diagram	
		1.1.2	Evolution of a Low-Mass Star	
		1.1.3	Evolution of a High-Mass Star	
	1.2	Stellar	Nucleosynthesis	
		1.2.1	S-process	
		1.2.2	R-process	
	1.3	Cosmo	ochronology \ldots \ldots \ldots \ldots 12	
		1.3.1	Uranium-Thorium Cosmochronology	
	1.4	Study	of White Dwarfs Spectra	
		1.4.1	White Dwarfs	
		1.4.2	Radiative Levitation	
		1.4.3	RE0503-289	
ი	The	onotios	Nothoda 20	
4	2 1 2 1	Atomi	a Methods 20 a Physics Reminders 20	
	2.1	0.1.1	Finatein Coefficients	
		2.1.1	Padiative Transitions	
		2.1.2	Line Strength	
		2.1.3 2.1.4	Casillator Strength	
		2.1.4 2.1.5	Drenching Fraction	
		2.1.0	Drahching Fraction	
	იი	Z.1.0 Decud	Radiative Lifetime	
	2.2	r seudo	Solf consistent Field Method and Hertree Fock Fountions	
		2.2.1	Self-consistent Field Method and Hartree-Fock Equations 24	
		2.2.2	Core Delerization Connections (UED + CDOI)	,
		2.2.3	Core-Polarization Corrections ($\Pi F R + CPOL$)	
		2.2.4	Solving the Hamiltonian Eigenvalue Equation: Stater-Condon Method 28	
	<u></u>	2.2.3 E.ll., I	Semi-Empirical Process	
	2.3	Fully I	Relativistic Multiconnguration 20	
		Dirac-	Mathad's Desis Drinsinla	
		2.3.1	Divers Coulomb Hamiltonian and Atomic Wave Functions	
		2.3.2 9.2.2	Unrec-Coulomb Hamiltonian and Atomic wave Functions	
		2.3.3 9.2.4	Catting the Spin Orbitals through the MCDUE Equations 24	
		2.3.4 9.2.5	Getting the Spin-Orbitals through the MCDHF Equations 34	
		2.3.3	Solving the Eigenvalues Equation Using the Configuration Interac-	,
		0.0.0	tion Method 37 Overstein 37 Overstein 27	,
		2.3.0	Quantum Electrodynamics Corrections	
		2.3.7	GKASP2K - GKASP2018 Programs	

1

3	Ato	mic D	ata Calculations in U II and Th II for Cosmochronological	
	App	olicatio	ons 4	40
	3.1	U II		40
		3.1.1	HFR+CPOL Calculations	41
		3.1.2	Results	43
	3.2	Th II		49
		3.2.1	HFR+CPOL Calculations	50
		3.2.2	Results	51
	3.3	Summ	ary	61
4	Rad	liative	Parameter Computations in Moderately Charged Trans-Iron	
т	Ions	s for th	e Study of Hot White Dwarfs Spectra	32
	4.1	Cu IV	- VII	62
		4.1.1	Models Used	63
		4.1.2	Atomic Radial Parameters	64
		4.1.3	Radiative Transition Rates	69
	4.2	In IV -	- VII	73
		4.2.1	Models Used	73
		4.2.2	Atomic Radial Parameters	74
		4.2.3	Radiative Transition Rates	82
	4.3	Cs IV-	VII	86
	-	4.3.1	Models Used	86
		4.3.2	Atomic Radial Parameters	87
		4.3.3	Radiative Transition Rates	91
	4.4	Ag IV	-VII	92
		4.4.1	Models Used	92
		4.4.2	Atomic Radial Parameters	93
		4.4.3	Radiative Transition Rates	97
	4.5	Conclu	usion - Applications	99
5	Rad	liative	Decay Rates in Neutral and Singly Ionized Atoms for Stellar	~ ~
	Nuc	leosyn	thesis Analyses 10)0
	5.1	Lifetin	ne Measurements	
		5.1.1	TR-LIF Spectroscopy Technique	JL
	50	5.1.2	Experimental Setup	03
	5.2	Ir I-II	· · · · · · · · · · · · · · · · · · ·	J5
		5.2.1		J5
	F 0	5.2.2 D		J8 10
	5.3 E 4	Re I		12
	5.4			14
		5.4.1	HFR+CPOL Calculations	14
		5.4.2	MCDHF Calculations	10 10
		5.4.3 D I	Results	10
	5.5	Bal	L	28
	5.0	Rh I	· · · · · · · · · · · · · · · · · · ·	30
Ge	enera	al Cone	clusion 1:	32
Aı	open	dix	12	17
1	CuI	V-VII	- 1. 1.	48
	In IV	V-VII		88
	CsI	V-VII		22

Ag IV-VII

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General Introduction

For a little more than a century, some of the most important developments in astrophysics have been possible thanks to a better interpretation of the observed stellar spectra. In this context, atomic physics has always played an essential role insofar as this discipline is able to provide all the necessary tools for the detailed analysis of astrophysical spectra. From the latter, it is indeed possible to deduce the presence and abundance of the different chemical elements in celestial objects only through the accurate knowledge of the atomic structures and the radiative parameters characterizing these elements.

In recent years, astronomical observing instruments have improved dramatically with new space and ground-based telescopes providing spectra with unprecedented resolution and signal-to-noise ratio across the whole range of wavelengths, from X-rays to the far infrared, for a very large number of various cosmic sources. Consequently, the astrophysical spectra currently recorded are getting richer and richer and include many spectral lines that can be identified only by a sufficient knowledge of the atomic parameters, both in quality and quantity, of all the elements in their different ionization stages.

The work presented in this thesis is part of this context since it aims to make an original contribution to the determination of fundamental atomic parameters essential to the development of current astrophysical hot topics, in particular for studies related to cosmochronology, hot white dwarfs, and stellar nucleosynthesis.

In cosmochronology, heavy elements such as uranium and thorium are of paramount importance. More precisely, the abundance ratios of the long-lived isotopes ²³²Th and ²³⁸U can be used to determine the age of stars. To date, some spectral lines of singly ionized thorium and uranium have been identified on some stellar spectra. Unfortunately, the atomic data characterizing these two ions are still too incomplete and too unreliable to perform a sufficiently precise stellar dating. This motivated us to perform a detailed investigation of these two ions whose complex atomic structures make theoretical modeling very complicated. Both thorium and uranium belong to the actinide group of the periodic table, with atomic numbers Z = 90 and Z = 92, respectively.

We started this study with singly ionized uranium (U II). Before our work, we looked for previously available data in U II. We found that, Blaise and Wyart [1] listed some preliminary energy levels in U II for both parities in 1992. These data were preceded in the literature by the publications about emission lines by Steinhaus *et al.* [2] and Palmer [3] in 1971 and 1980, respectively and it provided an update to the previous estimations made by Brewer [4] en 1971. This database was later extended by Blaise *et al.* [5] in 1994. More recently, in 2017, the latest energy levels of U II were construed by Meftah [6] using the Racah-Slater parametric method with the Cowan codes [7]. Meftah *et al.* parametric study [6] allowed them to re-investigate the high resolution UV spectrum of uranium which was recorded in the late eighties at the Meudon Observatory and of which the analysis was unfinished. Unfortunately, Meftah *et al.* [6] were not able to put all the interacting configurations but we put them all in one calculation and we added the effects of the core-polarization. This will be discussed in Chapter 3.1.

As regards the radiative decay rates, the first measurements of relative line intensities in U II were obtained from emission arc spectra by Meggers et al. [8], Corliss and Bozman [9], Voigt [10] and Corliss [11] more than 40 years ago. In the atlas of uranium lines published by Palmer [3] in 1980, relative intensities measured from uranium hollow-cathode spectra were listed for 4928 U I and 431 U II emission spectral lines. The oscillator strengths of the lines at $\lambda = 3859.571$ Å and $\lambda = 4050.041$ Å were later determined by Chen and Borzileri [12] who combined experimental lifetime measurements of the upper levels with unpublished branching fractions. Oscillator strengths were also reported for about 100 U II lines by Henrion et al. [13] in 1987. In his database, Kurucz [14] listed transition probabilities and oscillator strengths for many U II lines based on the experimental data reported by Meggers et al. [8], Corliss and Bosmann [9], and Chen [12]. Finally, about 20 years ago, accurate radiative lifetimes were measured by Lundberg et al. [15], using laser-induced fluorescence technique. Experimental oscillator strengths for 57 U II lines in the region 3500 - 6700 A were then obtained by combining these radiative lifetimes with new branching fractions derived from the measured line intensities in the spectra emitted by a hollow cathode and analyzed using a Fourier transform spectrometer by Nilsson *et al.* [16].

Just after the calculation in U II, we started the calculations in Th II for those cosmochronological applications. The first investigation of the Th II spectrum was carried out by McNally et al. [17] in 1942. They identified 1091 lines of singly ionized thorium in a wavelength range from 2150 to 8140 Åallowing the classification of 219 levels. In order to link these two groups of energy levels, McNally [18] recorded the infrared spectrum of thorium in the region 8665 to 11230 Å in 1945. The separation between the ground leveland the first excited one was found to be only 4490.29 cm^{-1} . At the same period, independent experimental studies undertaken at the Zeeman laboratory of Amsterdam led to similar conclusions and the determination of additional levels [19, 20, 21]. All these published data, together with yet unpublished energy levels, were compiled in 1958 by Charles [22] in a list of 2850 classified lines of Th II from 165 odd and 191 even levels. McNally [18] pointed out that many of the strong transitions between low-lying Th II levels appear in the IR region and, although he observed some of them in the photographic infrared, the remaining lines were outside his region of observation. The majority of these lines were observed in the emission spectrum of thorium in the $1-2.5 \mu$ region recorded by Steers [23]. In this study, about 60 lines were attributed to Th II transitions. A few years later, Minski [24] discovered 28 energy levels through the first extensive parametric study of the Th II. The analysis of Th II was then extended with improved observations of the spectrum between 2000 and 25000 Å by Zalubas and Corliss [25]. They classified 6500 lines as transitions between 199 odd levels and 271 even levels. The emission spectrum of thorium from 2777 to 13500 Å in 1974.

Most of the Th II data obtained in the works mentioned hereabove were listed in three compilations: those of Blaise and Wyart [1], Sansonetti and Martin [26] and Redman *et al.* [27]. In the latter, the previously published thorium line lists were combined with new precise observations of a thorium-argon hollow cathode lamp emission spectrum in the region between 3500 and 11750 Å with a high-resolution Fourier transform spectrometer to refine the energy levels in Th I, Th II, and Th III. Using these refined level values, accurate Ritz wavelengths were also calculated for 19874 thorium lines between 2500 and 55000 Å while 102 new thorium energy levels, among which 9 belonging to Th II, were found. The list of Th II energy level values reported in the NIST database [28] is entirely based on the Redman *et al.* compilation [27].

Regarding the study of hot white dwarfs spectra, for about 15 years, the Atomic Physics and Astrophysics group of University of Mons has undertaken a systematic study of trans-iron elements in their ionization stages between 3+ and 6+¹ at the request of astrophysicists of University of Tübingen in Germany, the latter having identified numerous spectral lines of these heavy ions in the ultraviolet spectra of certain of those hot white dwarfs and deduced large overabundances of several orders of magnitude higher than the solar abundances. In order to best interpret the observed spectra, it is necessary to build non-local-thermodynamic-equilibrium (NLTE) synthetic models which requires to include the radiative parameters not only for the identified lines but also for all the transitions populating and depopulating the levels involved in the observed lines. The contribution we made in the framework of our thesis concerns the copper, indium, caesium and silver ions for which new semi-empirical calculations of radiative decay rates were determined, in their large majority for the first time.

The main source of atomic data related to the copper spectra is the paper published by Sugar & Musgrove [29] in which the available experimental energy levels of the copper atom, in all stages of ionization, have been compiled with ionization energies, either experimental or theoretical, experimental Landé *g*-factors, and leading components of calculated eigenvectors. This compilation is still being used as the standard reference database for the copper ions of interest at the National Institute of Standards and Technology [28]. For the fourth and fifth ionization stages of copper (Cu V and Cu VI), more recent data from Van Kleef *et al.* [30], and from Raassen and Van Kleef [31] have been used to perform the semi-empirical optimization of our HFR calculation. It is worth mentioning that our work is the first publication of radiative data in Cu IV,V and VII.

Using the most recent experimental data of Swapnil and Tauheed [32] and Ryabtsev and kononov [33], the radial parameters (average energies, Slater integrals, spin-orbit parameters and effective interaction parameters) were optimized during our fitting procedure included in the calculation for the third ionization stage of indium (In IV). We then compared our calculation including different configurations and core-polarization effects to theirs. When it came to the fourth ionization stage (In V), the fitting procedure aimed to minimize the differences between the calculated Hamiltonian eigenvalues and the experimental energy levels taken from Swapnil and Tauheed [34] and Ryabtsev [35]. Once again, we compared our calculation including different configurations and core-polarization effects to theirs. In the case of In VI, the experimental data from [36] and [37] were used for the fitting procedure. Finally, pertaining to In VII, we used experimental data of Ryabtsev *et al.* [38]. For all those ions, the goal was to consider the most complete and most recent set of experimental atomic data in order to have a more precise fit.

To perform our calculations in the caesium ions, we used the experimental energy levels from the compilation Sansonetti [39] and from Husain *et al.* [40]. Once again, those data are the most recent measured and compiled to our knowledge. Our work is the first one about radiative data in Cs IV, V and VI.

The last element studied in this framework of extreme overabundances in white dwarfs is silver. The experimental data used for the semi-empirical fits found in the literature, for the ions Ag IV, V, VI and VII ions are, respectively, Ankita and Tauheed [41] in Ag IV, Kildiyarova *et al.* [42] and Van Kleef *et al.* [43] in Ag V, Joshi *et al.* [44] in Ag VI and Ryabtsev and Kononov [45] in Ag VII.

Finally, it is important to mention that most of the studies published so far for the heavy elements were mainly focused on the lowest energy atomic states. However, highly excited states are of undeniable interest in astrophysics as they not only contribute to the construction of NLTE models, as mentioned above, but also involve radiative transitions that are increasingly observed in the spectra of celestial objects, in particular in the infrared range which is currently undergoing a considerable expansion with the recent launch

¹Noted IV to VII in our conventions.

of the James Webb Telescope. As a consequence, the radiative parameters characterizing the transitions between highly excited states are in great demand by the astrophysical community, particularly for neutral and singly ionized atoms heavier than iron for which the identification on the astrophysical spectra makes it possible to establish constraints on nucleosynthesis models worked out for the determination of abundances in chemically peculiar stars. In order to help fill these gaps, we have performed semi-empirical studies leading to the determination of radiative rates in some selected elements, namely neutral and singly ionized iridium, neutral rhenium, neutral lanthanum, neutral barium and neutral rhodium. In these cases, the methodology was to combine experimental radiative data measured by time-resolved laser-induced-fluorescence spectroscopy at University of Jilin in China with theoretical branching fractions to obtain the relevant transition probabilities.

The present thesis is written as follows. The first chapter is devoted to the astrophysical context in which our work was carried out, beginning with a general introduction about the life of stars and some reminders about the Hertzprung-Russel diagram. Next, the nucleosynthesis theory which explains how the heavy elements are created in the Universe, is described, as well as the uranium-thorium cosmochronology and the study of white dwarfs. In the second chapter we make some fundamental reminders of atomic physics by particularly insisting on the parameters considered in this thesis. The theoretical methods used in our different studies, namely the pseudo-relativistic Hartree-Fock (HFR) and the fully relativistic Multiconfiguration Dirac-Hartree-Fock (MCDHF) approaches, are presented in Chapter 2 while the results we have obtained are detailed in Chapters 3 to 5. These last three chapters are divided in such a way that they bring to the light the astrophysical applications of the atomic parameters determined in our work in three specific topics, namely cosmochronological investigations (Chapter 3), the study of hot white dwarfs (Chapter 4) and the analysis of chemically peculiar stars (Chapter 5). In addition, in Chapter 5, we briefly describe the experimental technique used in collaboration with University of Jilin in China, i.e. the time-resolved laser-induced-fluorescence technique.

Chapter 1

Astrophysical Context

1.1 The Life of a Star

1.1.1 The Hertzprung-Russel Diagram

The Hertzsprung-Russell (HR) diagram is a fundamental tool in astrophysics in which the intrinsic luminosity of a star is plotted as a function of its effective temperature¹ (and therefore its spectral type).

This allows to highlight that the stars are grouped according to certain regions of the graph, thus creating specific branches and sequences. The most important one is the main sequence, extending from the lower right corner (cold and faint stars) to the upper left corner of the diagram (the hot and highly luminous stars), which is the most important because this is the part of the diagram where stars spend most of their life. On the HR diagram shown in Figure 1.1, the region where the white dwarfs are located is also indicated. Since they are located in the lower left part of the diagram, we can deduce that they are hot and not very luminous. At the beginning of their life, most of stars are on the main sequence of the HR-Diagram once the nuclear fusion in them has been ignited. At that moment, the star has a stable core temperature and luminosity. Those stars are therefore called main-sequence stars. The exact position of the star on the main sequence depends on its mass [47]:

- the stars with the lowest masses and low surface temperatures and luminosities are situated in the right-bottom of the main-sequence;
- the massive stars with high temperatures and luminosities are located in the upperleft part of the sequence.

The latest continue their evolution further up in the diagram than the lower-mass stars. The time on the main sequence is the longest stage in the life of a star and depends of the mass of the star as shown in Table 1.1 using the data from Woosley *et al.* [48]. During

Table 1.1: Different stars' lifetimes on the main sequence compared to their total lifetimes depending on their mass - Source: [48]

1 0	L J		
Approximative initial mass	Time on the main sequence	Total lifetime	Percentage of life spent on the main sequence
M_{\odot}	Millions of years	Millions of years	%
0.8	2.0×10^{4}	3.2×10^{4}	62.5
1	9.2×10^3	$1.2 imes 10^4$	76.7
2	8.7×10^{2}	1.2×10^3	72.5
5	78	102	76.5
15	11	13	84.6
25	6.7	7.5	89.3

¹Defined as the surface temperature of a spherical black body with its luminosity and radius



Figure 1.1: Hertzprung-Russel Diagram - Credit: ESO [46]

their time on this main sequence, stars fuse hydrogen to helium in their core:

$$4^{1}H + 2e^{-} \rightarrow {}^{4}He + 6\gamma. \tag{1.1}$$

This is called the *proton-proton cycle*. It allows the transformation of hydrogen into ${}^{4}\text{He}^{2}$. This cycle is more complex than the simplified equation here above. It is actually divided into several reactions. The first reaction of this cycle allows the transformation of a proton and a neutron into deuterium. Then, depending on what is available in the core of the star (i.e. depending on the time of its evolution at which this reaction occurs), through the intermediary of tritium or helium 3 with which the deuterium atoms will fuse, the star generates helium 4. This proton-proton cycle occurs mainly in low-mass stars. The heavier stars can also perform what is called the CNO (Carbon-Nitrogen-Oxygen) cycle whose principal cycle³ is:

$${}^{12}_{6}C + {}^{1}_{1}H \rightarrow {}^{13}_{7}N + \gamma + E$$
 (1.2)

$${}^{13}_{7}N \to {}^{13}_{6}C + e^+ + \nu_e + E$$
 (1.3)

$${}^{13}_{6}C + {}^{1}_{1}H \to {}^{14}_{7}N + \gamma + E$$
 (1.4)

$${}^{14}_{7}N + {}^{1}_{1}H \to {}^{15}_{8}O + \gamma + E$$
 (1.5)

$${}^{15}_{8}O \rightarrow {}^{15}_{7}N + e^+ + \nu_e + E$$
 (1.6)

$${}^{15}_{7}N + {}^{1}_{1}H \to {}^{12}_{6}C + {}^{4}_{2}He + E$$
 (1.7)

In the course of these reactions, carbon is used as a catalyst, it is regenerated at the end of the cycle. A mix of proton-proton and CNO cycles can occur in stars. For example,

²Where γ represents photon emission.

³One should notice that secondary CNO cycles exist but are way less likely to happen.

in the case of the sun, it is estimated that the balance between those two phenomena is 99% (proton-proton) - 1% (CNO cycle)⁴ [49].

The stars that are less massive than the Sun (or around its mass) spend a substantially longer time on the main sequence because they live a lot longer, as highlighted in Table 1.1. Because of their much lower luminosities, they burn their core hydrogen very slowly. More massive and more luminous stars, in contrast, burn their hydrogen fuel much more rapidly and that is why they live much less time.

After that main-sequence life, stars begin to go through the red giant branch phase as shown in Figure 1.1. That time as a red giant is also quite long, for example one star with a mass around $1M_{\odot}$ will be a red giant for about 1 billion years and a star of a mass around $10M_{\odot}$ will spend only about 1 million years in that phase.

What will happen to the star after that red giant phase only depends on its initial mass and is explained in the two following subsections.

1.1.2 Evolution of a Low-Mass Star

In this section we will consider stars with a mass lower than 8 M_{\odot} . Once such a star has reached the main sequence, it sustains the fusion of hydrogen into helium in its core during around 75% of its (long) life, as mentioned in the previous section.

The temperatures are much higher in the stellar core, which implies that the fusion of hydrogen occurs first. This also means that hydrogen is consumed first. It all forms a burning layer above the core where hydrogen continues to fuse into helium. This phase is called *shell burning* [47]. Afterwards, the newly formed core region underneath the hydrogen-burning shell begins to contract (in the absence of thermonuclear reactions) and slowly heats up in the process (the pressure rises resulting in a rise in temperature). This heating process eventually causes the hydrogen burning in the shell to flare up. The layers above the burning shell then expand very rapidly and begin to cool down in such a way that the star moves to the lower end of the red giant zone in the HR Diagram.

Once there, the (still) inert helium core of the star slowly continues to contract itself and therefore heats up. At the same time, the hydrogen-burning shell becomes thinner and thinner as the expansion goes on. As a result, the surface area increases and therefore the luminosity of the star increases too. As for the surface temperature, it undergoes a huge decrease at this point.

At the red giant phase peaks, the helium in the center of the star becomes so dense and so hot that its fusion can be ignited. Helium then fuses into carbon and oxygen (see section 1.2 for more details). In low-mass stars that ignition of helium fusion is called *The Helium Flash*. The star therefore enters a new phase of its life: the helium burning phase. It lasts much less time than the hydrogen-burning phase (around 100 times less) but helium burning provides a new source of energy. This leads to a fast decrease in the luminosity of the star, the star contracts itself, leading to a much higher surface temperature. At that point the star fuses helium into carbon and oxygen in its hot core while hydrogen is still fusing into helium in the burning shell above it.

When the star has (almost) fused all the helium in its core, a change similar to what happened at the end of core hydrogen fusing takes place: an helium- burning shell forms at the outer edge of the newly created carbon-oxygen core.

The helium-burning shell gets thinner and thinner with time. That thinning leads to thermal instabilities: it reacts very quickly and violently to any change (addition or diminution) of heat. Therefore, any tiny rise in temperature caused by the core below, immediately leads to an uncontrolled rise in temperature in the helium-burning shell.

⁴This was discovered thanks to the observation of solar neutrino in 2020 by the Borexino collaboration.

Those thermal instabilities lead to a temperature increase in the helium-burning shell around the core despite its expansion. At the same time, the surface temperature goes down because of the expansion of the layers above the helium-burning shell. This also includes regions where the hydrogen burning-shell is still present. As a result, the luminosity of the hydrogen-burning shell drops drastically. After a very short time (several years), the helium-burning shell has expanded enough for it to regain thermal stability. At this point of the process, any further expansion leads, once again, to cooling and not to additional heating.

The overall contraction of the stellar envelope causes the temperature in the hydrogenburning shell to rise, therefore increasing the fusion rate in that shell. "Thermal pulses" originating from the bottom of the helium-burning shell occur at fairly regular intervals (around a few thousand years) in all stars with both helium and hydrogen burning shells (if the initial mass of the star is really too small, for example lower than 0.8 M_{\odot} , the process is stopped earlier as the fusion of the helium can never be ignited).

The helium-burning shell fuses ⁴He into ¹²C and ¹⁶O and the hydrogen-burning shell then converts ¹²C into ¹⁴N. That nitrogen remains under the hydrogen-burning shell even as the shell is bigger and bigger because of the pulses. In the pulse that follows its creation, the nitrogen is mixed down into the helium-burning shell (by a convection zone operating between the shells).

For the low- and intermediate-mass stars that are of interest in this section, this is the very last step before the end of their evolution. Indeed, the stars with an initial mass lower than 8 M_{\odot} do not have enough mass to cause a contraction and sufficient heating of the carbon-oxygen core to ignite carbon fusion. The remaining sources of energy are the helium- and hydrogen- burning shells. The smaller these two burning shells become, the closer they get to the stellar surface and the stronger the consequences of the thermal pulses become. The star will eject its outermost layers, layer by layer until the end. At this point, the entire material above the helium-burning shell has been blasted into the interstellar space. What is left of the initial star is its extremely hot and dense carbonoxygen core a white dwarf surrounded by a gaseous cloud called a planetary nebula [47].

This final state is of particular interest to us since the study of the spectrum of these white dwarfs constitutes an entire chapter of this thesis. We will discuss those peculiarly hot and very dense astrophysical objects in more detail in Section 1.4 and Chapter 4.

1.1.3 Evolution of a High-Mass Star

Even if in the context of this thesis the evolution of high-mass stars is less relevant, it is still worth briefly explain how this kind of star evolves.

Massive stars also spend most of their life on the main sequence (around 90%). This time is just much shorter than less massive stars because of their much shorter lifetime. Exactly as low- and intermediate-mass stars, during their time on the main sequence, massive stars fuse their hydrogen into helium. And, exactly as explained in the previous subsection, this newly formed helium core contracts while hydrogen-burning shell moves outward, layer by layer. Massive stars also go on the red giant branch just after helium fusion has begun. But the end of the story from now on is a little bit different for massive stars than what is was for lighter stars. Indeed, in this case, every step, even if quite similar, happens much more quickly and much more intensively. The conditions are extreme and additional thermonuclear fusion reactions can occur. Massive stars are able to form a carbon core which is large enough to reach temperatures of over 1 billion K during the contraction phase subsequent to helium burning.

At such intense temperatures and high densities, large numbers of neutrinos are created (due to the reactions) in the stellar interior. Those neutrinos, which have practically no interaction with matter, will leave the star without contributing any counteracting pressure to gravity in the way photons would do^5 . The stellar core therefore continues to contract itself and to heat up, causing the nuclear reactions to occur more and more rapidly. This creates an iterative cyclical phenomenon: the hotter the core region, the more neutrinos are generated, the more neutrinos are generated, the more the star will contract itself, and the more it does, the more the temperature increases. As a result, nuclear burning in the star accelerates.

The final stage occurs at about 3 billion K, where the fusion of silicon can be ignited. This process of conversion of silicon into iron and nickel is very quick.

During those very advanced and intense phenomena within the core of a massive star, the outer envelope of the star is not affected much by the processes because the envelope cannot react so quickly to any changes. The star just continues to move along the asymptotic giant branch in the Hertzsprung-Russell diagram.

When the final stage of fusion has occurred, the conditions are too extreme and the star explodes as a gigantic supernova.

In the end, the remnant of a low- (or intermediate-)mass star is a white dwarf as mentioned in the previous section. A massive star leaves behind a neutron-star or black hole [47]. Those three kinds of dead stars are called compact bodies.

1.2 Stellar Nucleosynthesis

The theory of nucleosynthesis describes the distribution of the abundances of the different elements found in our current Universe and aims to explain how they were formed. One of the channels of element formation is the nucleosynthesis in the core of stars during a long period of their quiet evolution as described in sections 1.1.2 and 1.1.3. As mentioned in those sections, when the temperature in the core of the star is sufficient, the fusion of helium can ignite itself. Afterwards, the higher the temperature can rise, the heavier elements the fusion process will be able to create.

However, this stellar channel is unable to explain the formation of elements much heavier than iron (which are exactly the ones we are interested in for this thesis). As a result, the concept of explosive nucleosynthesis was introduced. The latter implies that matter is irradiated under a flux of neutrons from highly energetic phenomena. Even if exposures to neutron fluxes are of limited duration, neutron-capture reactions are a very plausible explanation for the creation of heavy elements.

In neutron capture, a nucleus (for example, a carbon or iron nucleus) is bombarded with neutrons. Since the number of protons does not change, the nucleus remains of the same species as before the bombardment, but becomes unstable due to the additional neutrons. In order to reach stability, the nucleus realizes a beta decay, and is then transformed into an element with an higher atomic number.

This process repeated in an iterative way can lead to the creation of heavy elements. The heaviest one reachable is lead which is, as iron, very stable.

In order to create elements heavier than lead and bismuth, the neutronic irradiation must be more intense and the time scale must be shorter, leading to a more rapid process explained in section 1.2.2.

 $^{^{5}}$ With radiation pressure as explained in section 1.4.2

1.2.1 S-process

1.2.1.1 Neutron Sources

As mentioned in section 1.1.2, at the very end of its life, a star of a mass lower than $8M_{\odot}$ ejects all its gaseous layers planetary nebula to form a planetary nebula.

Spectroscopic analyses of those nebulae have shown that they contain many heavy s-process elements.

At some point, the low mass star will (generally) reach a state where a very hot dense carbon core is surrounded by two burning shells, one burning helium and the other one burning hydrogen, with a convection zone between them.

Located underneath the stellar envelope is the hydrogen-burning shell, and below that the helium- burning shell. The s-process takes place in the pulsating intershell between those two burning shells. A neutron source arises if carbon isotopes (13 C) or neon isotopes (22 Ne) capture a helium nucleus. A neutron is released at each capture. It generates quite a low but long-lasting neutron density, depending on the stellar mass. The neutrons are mainly available at the bottom of the convection zone, where they are repeatedly incorporated into the available seed nuclei. The total abundance of new elements not only depends on the neutron flux but also on the number of available seed nuclei inside a star which partly depends on the stellar environment in which it was first created⁶. The star can enrich the stellar environment in heavy elements through stellar winds or, in the end, through the expulsion of its outer layers.

1.2.1.2 S-Process Basic Principle

Under weak neutron irradiation, an unstable nuclide is formed from a stable nuclide that has captured a neutron. This unstable nuclide will undergo a β decay in order to stabilize itself (as much as possible) before absorbing another neutron. We are thus talking about a fairly slow process. In this regime, matter that undergoes neutron irradiation is enriched, by successive steps of one atomic mass at a time, to create heavy elements. Neutron capture immediately followed by a β decay (or several successive β decays) can only follow one path in the nuclide map. This way is shown on figure 1.2.

About half of all the isotopes heavier than iron are produced by this s-process [47] capable of synthesizing elements up to lead. For larger atomic masses, the neutron absorption is not followed by a β decay but by a α decay that moves the element back 4 atomic masses. That's why lead is a difficult boundary to cross for the s-process. Elements with a magic number of neutrons generate points of partial limitation of the process. Because these elements only have complete layers of neutrons, they have a small effective absorption cross section of a new neutron. The $^{208}_{82}$ Pb is doubly magic (82 protons and 126 neutrons).

1.2.2 R-process

1.2.2.1 Neutron sources

Unlike the s-process, the r-process needs much more intense neutron irradiation. The required conditions to provide that kind of neutronic irradiation can only be achieved in a supernova or during neutron star mergers [47]. For a long time, the first one was the preferred candidate by astrophysicists but in the last few years, the tendency has been reversed, launching many studies on the kilonovae, supposed to be the biggest source of intense neutron irradiation.

⁶It also depends on whether the star had a companion star from which it could have drawn neutrons and s-process elements.

1.2.2.2 R-Process Basic Principle

Under intense neutron irradiation, unstable nuclides do not have time to undergo the β decay before absorbing a new neutron. Unstable, neutron-rich nuclides, far enough away from the valley of nuclear stability, can then be temporarily created under neutron irradiation. Under a given neutron flux and for a given γ irradiation (influenced by temperature), there is, for each Z, a boundary nuclide that the r-process can create and maintain. After neutron irradiation (which can come from a supernova for example), these boundary nuclides, which are unstable when the neutron flux is no longer there to maintain them, tend to return to the valley of nuclear stability through successive β disintegrations. Once again, nuclides with a magic number of neutrons are favored to play the role of boundary nuclides (because of their small effective absorption cross section for a new neutron). This process explains the natural abundance of heavy elements.

As for the synthesis of super-heavy elements (whose mass amounts to about 300 a.m.u.), it is made possible by a 2-step r-process, the second operating on a gas that has already undergone a first r-episode.

An example of s-r-processes' path through the Mendeleev Table is shown in Figure 1.2.



Figure 1.2: Example of s-r-nucleosynthesis processes in the Mendeleev Table. Credit: [47] data from [50]

1.3 Cosmochronology

In principle, radioactive decay can lead to a very precise age-dating technique for a specific star if the half-lives of the decaying isotopes are known⁷ if the current isotopic abundance⁸, can be measured and if the production of that isotope is well understood (see section 1.3.1 for more details on the technique).

In the case of stars where elemental abundances can be measured, the element involved must be free of any stable isotope with a more important abundance than the radioactive isotope.

The most suitable isotopes identified for this purpose are all (super-)heavy r-process nuclei. These elements can only be made by neutron capture. They all lie beyond the last stable elements, lead and bismuth, and cannot be reached via the s-process of neutron capture as mentioned in section 1.2. Their production mechanisms and rates are therefore known and it is also understood that they decay to lead or bismuth. The isotopes matching that description are:

- 187 Re (half life: 45 Gyr)
- 232 Th (half life: 14 Gyr)
- 235 U (half life: 0.7 Gyr)
- 238 U (half life: 4.5 Gyr)

After about a Gyr, one can ignore the lighter U isotope assuming it entirely decayed. This leads to the conclusion that 232 Th and 238 U are very suitable candidates to perform stellar datation.

Since the initial abundances has to be known, and each star has a different initial metallicity, the technique generally used by the astrophysicists is to compare the abundance ratios of the unstable isotope (element) that they are interested in to either another unstable isotope or to a stable one. The most often used ratios are Rhenium/Osmium (Re/Os), Thorium/Europium (Th/Eu), and Uranium/Thorium (U/Th) [51, 52]. Europium has two stable isotopes (¹⁵¹Eu and ¹⁵³Eu) which are produced almost exclusively through the r-process neutron capture. The Th/Eu ratio cosmochronological study is the most used up to now but it is not ideal because of the high different atomic weight (151 or 153 versus 232 and atomic number Z = 63 versus 93). That means that there is a greater risk of error/uncertainty due to our current understanding of the r-process mechanisms. When it comes to predict the initial production ratios, the uncertainty is generally smaller when the two elements are as close in mass number as possible [52]. This is why U/Th ration seems a particularly good candidate.

1.3.1 Uranium-Thorium Cosmochronology

The U/Th (238 U/ 232 Th) ratio is, as mentioned above, of great significance in cosmochronology [53]:

$$R^{U/Th} = P^{U/Th} e^{\frac{T}{\tau_{Th}} - \frac{T}{\tau_U}}$$
(1.8)

where T is the age of the star studied, $R^{U/Th}$ is the Uranium/Thorium abundance ratio, $P^{U/Th}$ is the production rates ratio (supposedly known) and τ_U and τ_{Th} are the radioactive half-lives of the most abundant isotopes of Uranium (²³⁸U) and Thorium (²³²Th). For

⁷They are usually known based on experimental measurements.

⁸Or at least the abundance of the product of the decay.

example, in 2001, Cayrel $et\ al.$ [54] dated the CS31082-001 star (also known as Cayrel's star) at

 $12.5 \pm 3.0 \; \text{Gyr}$

According to the latter authors, the main sources of uncertainty were:

- the nuclear models;
- the lack of atomic data;
- the fact that only few lines were identified.

Within the scope of this thesis, we will act on the last two sources of uncertainties. Indeed, in the particular case of CS31082-001, only one U II line was identified (for the first time ever!) and its relatively weak intensity made the identification very difficult (see figure 1.3). The numerical value of the age of CS31082-001 was later refined (see e.g. [55])



Figure 1.3: CS31082-001 spectrum around the U II line at 385.959 nm. The U II line is shown in red. Source: [54]

but the uncertainties are still important with similar causes. This maintains and even reinforces our motivation to perform calculations in U II and Th II.

1.3.1.1 U II

Oscillator strengths for electric dipole (E1) radiative transitions in U II are supposed to be of a great interest in cosmochronology. Indeed, as mentioned above, the age of a star can be determined using a radioactive isotope of a sufficiently long lifetime. Up until a few years ago, the radioisotope ²³²Th, with a half-life of ≈ 14 Gyr, was used to date galactic stars (see e.g.[56]). As shown in [57], new accurate observations of heavy radioactive elements could improve the accuracy of those cosmochronometrical analyses. More particularly, the ²³⁸U isotope, which has a half-life of 4.5 Gyr, should represent a more precise age indicator. Furthermore, the U/Th ratio might be a much better cosmochronometer than both previously used Th/Eu and Th/Dy ratios because of the fact that the mass difference between Th and U is much smaller than between either one of these two actinides and the lighter lanthanides.

Unfortunately, uranium is very hard to detect in stars. In 2001, Cayrel (54) reported the first detection of a spectral line at a wavelength of 3859.57 Å, from singly ionized uranium, in the very metal-poor star BPS CS31082-001. This star, also called Cayrel's star, is more metal deficient than the globular clusters, and was thus probably born in the Galaxy's very early times. This measurement was made with the ESO/VLT telescope, and the UVES spectrograph. It was therefore possible to use the U/Th ratio in order to determine the age of formation of these elements in the early Galaxy for the very first time. The derived uranium abundance yielded an age of 12.5 ± 3 Gyr, which led to the best estimate of the age of the Galaxy and consequently provided a lower limit to the age of the Universe. However, as mentioned in [54], the accuracy of this uranium dating technique is still largely limited by the uncertainty of the abundance ratio which is derived from observation, and by the uncertainty of the theoretical estimation of the U/Th production ratio. The improvement of this situation not only depends on a better estimation of the U/Th production ratio, on refinements of the models in nuclear physics and on the possible discovery of other metal-deficient r-process-enhanced stars in which U and Th abundances can be measured, but also on a comprehensive knowledge of the radiative properties for the potentially observable spectral lines, notably for the strongest U II electric dipole transitions.

1.3.1.2 Th II

While uranium is extremely hard to detect in stars, making the U II line at 3859.57 Å the only one that could be used as a cosmochronometer so far, thorium is often detectable in r-process stars. For example, in the star CS31082-001, 14 individual Th II lines were identified, 10 of which being sufficiently unblended to allow for a precise determination of its abundance [54]. In CS22892-052, there were only three Th II lines at 3539.59, 4019.13, and 4086.52 Å that might be used for abundance measurements as mentioned by Sneden & Cowan [58]. Roederer et al. [59] observed the four Th II lines at 3539.59, 4019.13, 4086.52, and 4094.75 Å in 14 metal-poor stars whose very heavy element enrichment was only produced by the r-process. A detailed analysis of the blending features was performed in this work, confirming or supplementing the discussion previously started by Lawler et al. [60], Morell et al. [61], Sneden et al. [62], Norris et al. [63], and Johnson & Bolte [64] for different stars. Several Th II lines were detected by Frebel *et al.* [65] in the spectrum of the strongly r-process-enhanced metal-poor star HD1523-0901. However, most of them were severely blended with lines from other elements so that only the line at 4019.13 Å was selected to determine the age of the star. Based on this single line, Ren et al. [66] estimated thorium abundances for 17 stars, and upper limits for another 60 stars. Th II lines were also detected in several other stellar spectra, but it would be too tedious to list them all here. However, in all these studies, the number of observed thorium lines was very small, most of them being often blended with lines of other ions. It is therefore of paramount importance that astrophysicists have a list of strong transitions in Th II and U II ions at their disposal with radiative parameters sufficiently reliable to be used in uranium and thorium stellar abundance studies and, even more so, in cosmochronological analyses.

1.4 Study of White Dwarfs Spectra

1.4.1 White Dwarfs

White dwarfs (often referred to as WD) are objects of high density which are the result of the evolution of a low to moderate mass star ($M_{star} < 10 M_{\odot}$). They are very small in size (hence the name dwarf) and have a high surface temperature (hence the term white). Typically, for a mass of about $1M_{\odot}$, they have a volume of about V_{Earth} . Upon their formation, they populate the lower left part of the Hertzprung-Russel diagram and drift to the right as they cool down. Their T_{eff} is generally between around 10 000K and 150 000K and, unless there is an accretion of surrounding matter, their radiation only comes from stored (unrenewed) heat. For that kind of astrophysical objects, the cooling process is very slow [67].

1.4.1.1 Formation Process

As already mentioned in section 1.1.2, white dwarfs are the residual end-of-life form of low-mass main sequence stars with masses ranging between 0.13 and 10 M_{\odot} .

As a quick reminder of what has already been explained in section 1.1.2, at the end of their lives, these low-mass stars have burnt most of their hydrogen into helium. Deprived of their primary fuel, these stars collapse due to their own mass. At this point, the pressure and temperature of the core increases, causing the helium to fuse and produce heavier elements such as carbon. At this stage of the process, there is an increase in energy, the star has become a red giant. Once the helium is consumed, the contraction resumes. The low mass does not provide the required conditions for the carbon fusion to occur: the core collapses into a white dwarf and the outer layers are expelled in the form of a nebula. The final result is a very hot white dwarf (composed mainly of a hydrogen and helium, which were not consumed during the fusion, atmosphere and an inert carbon and oxygen core) surrounded by a cloud of gas. The final composition of the white dwarf depends on the composition of the initial star.

1.4.1.2 Chandrasekhar Limit

White dwarf masses range from $0.13M_{\odot}$ to $1.33M_{\odot}$. There is a mass limit of $1.44M_{\odot}$ above which white dwarfs would no longer be able to withstand their own gravitational collapse. This also set an upper mass limit for a star to become a white dwarf $(8-10M_{\odot})$. The mass distribution of white dwarfs has a peak around $0.6M_{\odot}$ and therefore, the majority of white dwarfs are such that they have a mass around $0.5M_{\odot}$. However, for the most part, their radius is between 0.008 and $0.02R_{\odot}$. That means that white dwarfs are among the densest bodies in the Universe.

Those very high densities lead to the degeneration of internal matter. Such densities are indeed possible because we are in the plasma state. But, given that the star undergoes a cooling process, we could intuitively think that the energy will also decrease strongly. If, at some point we'd reach 0K, by Pauli's principle of exclusion, not all electrons can be in the fundamental state. We would then have a state called the Fermi Sea and even when the temperature decreases, we can have a quite high energy. To have a better idea of what degeneration pressure is, we can also use Heisenberg's uncertainty principle. Indeed, if the density is very high, the uncertainty of the position of the electrons is very low, which implies a large variation of the possible momenta or, in other words, a lot of kinetic energy. The degenerative pressure prevents gravitational collapse. It only depends on density and not on temperature, i.e. the star can cool down without collapsing on itself. That means that there is a balance between degenerative pressure and gravitational forces. There is therefore a limit mass. If the limit is exceeded and new fusion reactions do not start, then the star collapses on itself. It should be noted that, since degenerated matter is relatively compressible, the density of a high-mass white dwarf is higher than that of a low-mass white dwarf. Therefore, the radius of the white dwarf decreases as its mass increases.

1.4.1.3 Spectral Classification

White dwarfs are objects with a very high surface gravity, they are thus almost opaque to radiation. Nevertheless, some absorption lines have been observed and they led to the spectroscopic classification of white dwarfs. For each white dwarf, the first letter of the denomination is a D (for *Degenerate*). The second letter is given according to the spectral lines that could be observed. White dwarfs are classified as follows [68]:

Spectral Type	Main Absorption Lines		
DA	Hydrogen		
DB	He I		
DO	He II		
DQ	Atomic or Molecular Carbon		
DZ	Other Element		
DC	No marked line (i.e. optical depth $\leq 5\%$ of radiation)		

Table 1.2: Spectral Classification of WD

If there are marked lines for more than one element, then the denomination will be D + the other appropriate letters. The general shape of the spectrum gives the effective surface temperature (in our case $T \neq T_{eff}$ because the star is not quite a black body). Consequently, a number is associated with the temperature in the spectral classification: $\frac{50400K}{T_{eff}}$. Other letters can be added such as E if we see emission lines or a letter associated with another parameter: the variability. For a given characteristic, if it is followed by an interrogation mark or two dots, it means that the characteristic is not yet certified. Most (75%) of the white dwarfs observed are of type DA.

1.4.2 Radiative Levitation

With a given mass and composition, the internal dynamics and structure of a star is determined by the balance between the gravitational and radiative forces within it. Radiative forces are caused by photon-atom interactions. Let us consider these photon-atom interactions for individual elements. Quite intuitively, we will say that the gravitational forces pull the particles down (i.e. towards the center of the star). If gravity dominates the kinetic forces, then the heaviest particles will be more attracted towards the center of the star and a segregation between heavy and light elements will be observed. However, when we add the radiation pressure to the gravitational forces (in addition to the gas pressures in the stellar interiors), we find that these radiation forces combined with the internal gas pressure are greater than the gravitational force. As a result, the elements are in *levitation* and rise to the surface [69]. Intuitively, one would tend to think that despite everything, the heavier elements will remain more attracted by the force of gravity, but if we add atomic physics into the mix, other conclusions can be drawn. Indeed, the radiative force depends on the absorption of the radiation by the element, which in turn depends strongly on the ionization state of the element (the ionization state itself depending on the local temperature and density conditions). As a matter of facts, some

states of ionization have a much higher absorption cross section than others. As a result, the balance between radiative and gravitational forces in a star fluctuates according to the local conditions of the star. Therefore, the closer one gets to the center of the star, the more likely one is to have high temperatures and densities, and thus higher ionization states and the higher the radiative levitation phenomenon will be. That said, the phenomenon of radiative levitation can also (quite intuitively) explain why quite heavy elements (in a certain state of ionization) can be seen in the photosphere of some stars.

1.4.3 RE0503-289

The white dwarf RE0503-289 is located in an interstellar region of very low H I density and is itself of low hydrogen density. Its estimated temperature is situated between 60000 and 80000K [70]. It has been noticed that the abundance of carbon is in the order of a few %. Balmer's lines in absorption that we see for most white dwarfs are not to be seen but we have a large absorption for the 468.6 nm line of He II. RE0503-289 is thus a white dwarf of type DO or a star PG1159⁹. Moreover, RE0503-289 is located at the limit of the wind limit¹⁰ (see Figure 1.4) which corroborates the hypothesis that it could be a transient state between a star of type PG1159 and a white dwarf.



Figure 1.4: Position of RE0503-289 towards the wind limit. Source: [71]

 $^{^{9}\}mathrm{Transient}$ state between a star and a white dwarf, i.e. a predegenerated star.

¹⁰The wind limit is a semi-empirical limit beyond which there can be no more stars of type PG1159 and therefore there can only be white dwarfs.

1.4.3.1 Peculiarities

RE0503-289 raises many interrogations due to its peculiarities:

- 1. A priori it looks like a DO type WD (see section 1.4.1.3) but its opacity model looks more like a DA type containing more heavy elements.
- 2. It is very close to another DA type WD: RE0457-281. This gives us a very rare occasion to study an interstellar space much smaller than usual. In addition, some interactions could occur between those two stars and can therefore be studied.
- 3. RE0503-289 has an overabundance (up to 4 orders of magnitude greater than solar abundances) of heavy elements as highlighted in Figure 1.5 [72, 73, 74, 75, 76]. Given the nature of these elements, their production is surely the result of a s-process nucleosynthesis (see section 1.2). However, their overabundance is a mystery. It could be partly explained by radiative levitation, but this is not sufficient. Also note that RE0503-289 has a carbon abundance of about 3-4% rather than the 1% expected.



Figure 1.5: Extreme overabundances of Trans-Iron Elements (TIEs) in the spectrum of RE0503-289 - Source: [77]

One can wonder if this kind of phenomenon is a unique or common one. Rauch *et al.* [74] performed diffusion calculations to demonstrate that the extreme TIEs overabundances in RE 0503-289 are the result of efficient radiative levitation. They also observed three related objects close to the location of R0503-289, namely PG0109+111, PG1707+427, and WD0111+002. While RE 0503-289 is located directly on the PG1159 wind limit as shown in Figure 1.4, PG1707+427 lies towards higher T_{eff} and PG0109+111 and

WD0111+002 towards higher log g^{11} even right of the full line that indicates where the photospheric carbon abundance is reduced by gravitational settling. The detailed spectral analysis presented by Hoyer *et al.* [78] showed equally high TIE abundance enhancements in PG0109+111 and WD0111+002 as in RE0503-289 and, thus, the TIE abundance enhancement due to radiative levitation. In contrast, no TIE line has been identified in the spectrum of PG1707+427. Their hypothesis was that in that star the stellar wind is too strong and prevents efficient diffusion of the TIEs. Later on, Löbling *et al.* [79] identified many TIEs lines in a DAO-type white dwarf (namely BD-22°3467). This research topic is therefore still ongoing and new observations could be added to the models and lead to a better understanding of those overabundances, of radiative levitation and of white dwarfs.

1.4.3.2 Need of Atomic Data

The discovery of TIE lines in the spectrum of RE0503-289 [80] and the lack of reliable atomic data in the literature initiated a campaign to calculate transition probabilities and oscillator strengths at the University of Tübingen through The Tübingen Oscillator Strengths Service (TOSS). The Atomic Physics and Astrophysics group at the University of Mons later joined this project to perform precise atomic calculations. With those newly calculated data, abundance determinations for all TIEs with heretofore identified lines became possible. The ultimate goal of this collaboration is to produce reliable atomic data in all the TIEs elements up to cerium in their third to sixth ionization states in order to be able to have an exhaustive analysis of the spectrum of RE0503-289. This analysis could lead to a better understanding of the phenomenon mentioned in the previous subsections.

In the context of this thesis, we participated in that effort by calculating atomic data for four of those TIE elements: Cu, In, Cs and Ag.

 $^{^{11}{\}rm where}~{\rm g}$ is the surface gravity

Chapter 2

Theoretical Methods

2.1 Atomic Physics Reminders

2.1.1 Einstein Coefficients

When an atom (or an ion) in a certain state $|i\rangle$ of energy E_i is put into an electromagnetic radiation with a spectral energy density $\omega_{\nu}(\nu)$, that atom (or ion) can absorb a photon $h\nu$ such that it finds itself in a higher energy state $E_k = E_i + h\nu$. The variation in the population of the level E_i is given by the following relation:

$$\frac{dN_i(t)}{dt} = -B_{ik}N_i(t)\omega_\nu(\nu_{ik})$$
(2.1)

where B_{ik} is the Einstein coefficient for absorption.

The radiation field can also cause atoms in an excited state E_k to de-excite to a lower state E_i by emitting a photon of energy $E_k - E_i$. In this case B_{ki} is the Einstein coefficient for induced emission (or stimulated emission). It is also possible that an atom in an excited state E_k spontaneously de-excites to an E_i state without a radiation field (or without the intervention of a field). In this case,

$$\frac{dN_k(t)}{dt} = -A_{ki}N_k(t) \tag{2.2}$$

where A_{ki} is the Einstein coefficient for spontaneous emission.

Quite intuitively, we can link these three processes. Indeed, at thermodynamic equilibrium (for a certain temperature T), the radiation density is given by:

$$\omega_{\nu}(\nu_{ik}) = \frac{8\pi h \nu_{ik}^3}{c^3} \frac{1}{e^{h\nu_{ik}/kT} - 1}$$
(2.3)

which is equivalent to

$$\omega_{\sigma}(\sigma_{ik}) = 8\pi h c \sigma_{ik}^3 \frac{1}{e^{h\sigma_{ik}/kT} - 1}$$
(2.4)

where $\sigma_{ik} = \frac{1}{\lambda_{ik}}$ is the wavenumber. By the assumption of thermodynamic equilibrium, the populations of the levels verify the Boltzmann law:

$$\frac{N_i}{N_k} = \frac{g_i}{g_k} e^{-\frac{E_i - E_k}{kT}} = \frac{g_i}{g_k} e^{-\frac{h\sigma_{ik}}{kT}}$$
(2.5)

with $g_j = 2J_j + 1$. If we suppose in addition that we are in the conditions of a stationary regime we can then write:

$$B_{ik}N_i\omega_\sigma(\sigma_{ik}) = A_{ki}N_k + B_{ki}N_k\omega_\sigma(\sigma_{ik})$$
(2.6)

From there, we can obtain:

$$g_i B_{ik} = g_k B_{ki} \tag{2.7}$$

and

$$A_{ki} = 8\pi h c \sigma_{ik}^3 B_{ki} \tag{2.8}$$

2.1.2 Radiative Transitions

For an electric dipole transition (E1) between a $|\gamma_k J_k M_k\rangle$ state of degeneracy¹ $g_k = 2J_k + 1$ and a $|\gamma_i J_i M_i\rangle$ state of degeneracy $g_i = 2J_i + 1$, making the analogy with the classical approach of the oscillating electric dipole, a spontaneous emission probability can be obtained (see e.g. [7]):

$$a(E1) = \frac{64\pi^4 e^2 a_0^2 \sigma^3}{3h} \sum_q |\langle \gamma_i J_i M_i| \ P_q^{(1)} |\gamma_k J_k M_k\rangle |^2$$
(2.9)

where $P_q^{(1)} = \sum_j r_q^{(1)}(j)$ is the q^{th} component of the dipole momentum. For the transition probability from a state $|\gamma_k J_k\rangle$ to a state $|\gamma_i J_i\rangle$, A_{ki} we have:

$$A_{ki}(E1) = \frac{64\pi^4 e^2 a_0^2 \sigma^3}{3hg_k} \sum_{M_i} \sum_{M_k} \sum_q |\langle \gamma_i J_i M_i| \ P_q^{(1)} |\gamma_k J_k M_k\rangle |^2$$
(2.10)

We will also use the notation gA(E1) such that $gA(E1) = g_k A_{ki}(E1)$. Associated to each type of transitions, there are selection rules, in particular for the electric dipole transitions, due to the fact that the multipole transition operators are irreducible tensor operators and that they obey the Wigner-Eckart theorem. For E1 transitions, we find:

$$\Delta J = J_i - J_k = 0, 1, -1 \tag{2.11}$$

with $J_i = J_k = 0$ not allowed and

$$\Delta M = M_i - M_k = 0, 1, -1 \tag{2.12}$$

$$\Delta S = 0 \tag{2.13}$$

and

$$\Delta L = 0, \pm 1(0 \leftrightarrow 0 \text{ not allowed}) \tag{2.14}$$

with a mandatory change of parity.

Remark

It is important to note that the selection rules mentioned above are only valid for pure LS coupling, which is rarely the case in practice (especially for the heaviest elements). It is nevertheless important to know them because the deviation from the pure LS coupling is treated using the configuration interaction methods as explained in sections 2.2.4 and 2.3.5.

¹i.e. its statistical weight.

2.1.3 Line Strength

It is usual in atomic physics to introduce a quantity that is symmetric², namely the line strength $S_{ik} = S_{ki}$ by writing

$$gA(E1) = \frac{64\pi^4 e^2 a_0^2 \sigma^3}{3h} S_{ik}(E1)$$
(2.15)

with

$$S_{ik} = |\langle \gamma_i J_i| \ ||P^{(1)}||\gamma_k J_k\rangle \ |^2 = |\sum_{M_i} \sum_{M_k} \sum_q \langle \gamma_i J_i M_i| \ |P_q^{(1)}||\gamma_k J_k M_k\rangle \ |^2$$
(2.16)

where $P^{(1)}$ is the dipole transition operator.

2.1.4 Oscillator Strength

The oscillator strength f_{ik} is a dimensionless quantity that is defined as the number of oscillators³ that it is necessary to associate with an atom in state i in order for the classical absorption coefficient to be equal to the Einstein coefficient B_{ik} . For an electric dipole transition,

$$f_{ik}(E1) = \frac{8\pi^2 mca_0^2 \sigma}{3hq_i} S_{ik}(E1)$$
(2.17)

The notation $gf(E1) = g_i f_{ik}(E1)$ is often used.

The transition probability, can therefore be written as:

$$gA(E1) = \frac{8\pi^2 e^2 \sigma^2}{mc} gf(E1)$$
(2.18)

These two quantities are directly proportional and that is why we will treat them almost indifferently in this manuscript.

2.1.5 Branching Fraction

The branching fraction, BF, is defined as:

$$BF_{ki} = \frac{A_{ki}}{\sum_{i} A_{ki}} \tag{2.19}$$

2.1.6 Radiative Lifetime

Let's suppose that a level k is only depopulated by spontaneous emissions to lower energy levels, we can then write:

$$\frac{dN_k(t)}{dt} = -\sum_{i < k} A_{ki} N_k(t) \tag{2.20}$$

which gives

$$N_k(t) = N_k(0)e^{-\sum_{i < k} A_{ki}t} = N_k(0)e^{-\frac{t}{\tau_k}}$$
(2.21)

where, for the level k, we define the radiative lifetime:

$$\tau_k = \frac{1}{\sum_{i < k} A_{ki}} \tag{2.22}$$

²The symmetry concerns the two levels considered: k and i.

 $^{^{3}}$ By analogy with the classical theory of an oscillating dipole that absorbs part of the energy when subjected to continuous radiation.

2.2 Pseudo-Relativistic Hartree-Fock Method

The first method used to calculate atomic parameters in the present work is the HFR method (HFR stands for Hartree-Fock + Relativistic corrections). Developed by Cowan [7], the relativistic Hartree-Fock method is based on an iterative resolution of the Hartree-Fock equations (using the self-consistent field method) which themselves are obtained by the application of a variational principle minimizing the average energy of an electronic configuration. Single-electron relativistic corrections (spin-orbit, mass-velocity and Darwin term) are perturbatively added to the model (HFR is therefore a pseudo-relativistic method). The solutions of these equations are the radial parts of the wave functions, which are eigenfunctions of the Hamiltonian describing an atomic or ionic system. The HFR method was improved about twenty years ago by the Atomic Physics and Astrophysics Department at UMONS ([81, 82]) to incorporate the effects of core polarization (CPOL), which are particularly important to model heavy atoms and ions. In this thesis we will use atomic units:

$$\hbar = m_e = \frac{e^2}{4\pi\epsilon_0} = 1$$
 (2.23)

Our goal is to determine the energy levels of a given atomic or ionic system and the parameters associated with the possible transitions, i.e. the wavelengths corresponding to these transitions, the transition probabilities and the oscillator strengths. To that end, we must solve the Schrödinger's equation for stationary states, i.e. the eigenvalue equation

$$H\psi_k = E_k\psi_k \tag{2.24}$$

in order to obtain the eigen energies E_k associated with the eigen wavefunctions ψ_k . The (still non-relativistic) Hamiltonian is given by:

$$H = \sum_{i=1}^{N} \left(-\frac{1}{2}\Delta_i - \frac{Z}{r_i}\right) + \sum_{i>j} \frac{1}{r_{ij}}$$
(2.25)

where N is the number of electrons considered, r_i is the distance between the i^{th} electron and the nucleus (considered here as a point charge), r_{ij} is the distance between the i^{th} and the j^{th} electron and Δ_i is the Laplacian operator acting on r_i .

Given that the problem is not analytically solvable for N > 1, we will use the central field approximation in which we suppose that each electron moves independently of the others in a potential with a spherical symmetry which is generated by the nucleus and the N - 1 other electrons. The Hamiltonian is therefore written:

$$H = \sum_{i=1}^{N} \left(-\frac{1}{2} \Delta_i - \frac{Z}{r_i} + V(r_i) \right)$$
(2.26)

where $V(r_i)$ is the spherically symmetrical potential where the electron *i* finds itself. In this case, the problem is reduced to the case of a single electron in a spherically symmetrical system, which is quite similar to the hydrogen atom (it differs from the latter only in the shape of the potential). Therefore, for each electron, we can write, the single-electron wave function by separating the radial variables from the angular variables, which gives for the *i*th electron:

$$\phi_i(r_i, \theta_i, \Phi_i, s_i) = \frac{1}{r_i} P_{n_i l_i}(r_i) Y_{l_i}^{m_i}(\theta_i, \Phi_i) \sigma_{m_{s_i}}(s_i)$$
(2.27)

where (r_i, θ_i, Φ_i) are the spherical coordinates (whose origin is the nucleus), $P_{nl}(r)$ is the radial part of the single electron wave function, Y_l^m is a spherical harmonic (cf hydrogenoïd

atom) and $\sigma_{m_s}(s)$ the spin wave function. From these single-electron wave functions, an antisymmetric atomic wave function can be constructed by using a Slater determinant:

$$\psi(q_1, ..., q_N) = \frac{1}{\sqrt{N!}} \begin{vmatrix} \phi_1(q_1) & \dots & \phi_1(q_N) \\ \dots & \dots & \dots \\ \phi_N(q_1) & \dots & \phi_N(q_N) \end{vmatrix}$$
(2.28)

where $q_i = (r_i, \theta_i, \Phi_i, s_i)$. The wave function obtained is an eigenfunction of the Hamiltonian (and satisfies Pauli's principle by its antisymmetry). It is therefore necessary to determine the monoelectronic radial parts (which depend on the shape of the potential) in order to obtain the atomic wave functions giving the (stationary) states of the system. The method used is the self-consistent field method described in the following section.

2.2.1 Self-consistent Field Method and Hartree-Fock Equations

In order to determine the radial parts of the single-electronic wave functions $P_{nl}(r)$, the Hartree-Fock (HF) equations are used. The latter are obtained by applying a variational principle of minimization of the mean energy of a configuration E_{av} to the radial parts $P_{nl}(r)$ to form a system of coupled integro-differential equations (i.e. the equation determining the radial part of the wave function for the electron i, $P_{n_i l_i}$ implies all the other radial functions $P_{n_i l_j} \forall j \neq i$). The mean energy of an electronic configuration is given by

$$E_{av} = \frac{\sum_{i} (2J_i + 1)E_i}{\sum_{i} (2J_i + 1)}$$
(2.29)

where all the energy levels of the configuration are summed. It can also be written as the sum over all the energy states of the Hamiltonian operator's (H) average in each state belonging to an electronic configuration $|i\rangle$

$$E_{av} = \sum_{i} \langle i | H | i \rangle \tag{2.30}$$

By developing this expression, Cowan [7] showed that the terms of electronic interactions that can be expressed from Slater integrals appear in this expression. The generalized Slater integral R^k , representing the electrostatic interaction between 2 electrons belonging to different configurations, is given⁴ as follows:

$$R^{k}(ij;tu) = \int_{0}^{\infty} \int_{0}^{\infty} \frac{2r_{min}^{k}}{r_{max}^{k+1}} P_{i}^{*}(r_{1})P_{j}^{*}(r_{2})P_{t}(r_{1})P_{u}(r_{2})dr_{1}dr_{2}$$
(2.31)

where r_{min} and r_{max} are respectively the smallest and largest values of r_1 and r_2 . The direct electrostatic interaction $F^k(ij) = R^k(ij;ij)$ and the exchange electrostatic interaction⁵ $G^k = R^k(ij;ji)$, which describe the interactions of electrons of a same configuration, are particular cases of the generalized Slater integrals. It can be shown that the latter only exist for given values of k: $F^k(ij)$ for $k = 0,2,4,...,\min(2l_i,2l_j)$ and $G^k(ij)$ for $k = |l_i - l_j|, |l_i - l_j| + 2, ..., l_i + l_j$. The HF equations are therefore obtained by minimizing E_{av} for a given configuration

$$(n_1 l_1)^{w_1} (n_2 l_2)^{w_2} \dots (n_q l_q)^{w_q}$$
 where $\sum_{i=1}^q w_i = N$ (2.32)

⁴Using the notation $i = n_i l_i$.

⁵Due to the indiscernability of the electrons.

written as:

$$\left[-\frac{d^2}{dr^2} + \frac{l_i(l_i+1)}{r^2} - \frac{2Z}{r} + \sum_{j=1}^q (g_j - \delta_{ij}) \int_0^\infty \frac{2}{r_{max}} P_j^2(r') dr' - (g_i - 1)A_i(r) \right] P_i(r) = \epsilon_i P_i(r) + \sum_{j=i, j \neq i}^q g_j [\delta_{ij}\epsilon_{ij} + B_{ij}(r)] P_j(r)$$
(2.33)

where

$$A_i(r) = \frac{2l_i + 1}{4l_i + 1} \sum_{k=1}^{\infty} \left(\begin{array}{cc} l_i & k & l_i \\ 0 & 0 & 0 \end{array} \right)^2 \int_0^\infty \frac{2r_{min}^k}{r_{max}^{k+1}} P_i^2(r') dr'$$
(2.34)

and

$$B_{ij}(r) = \frac{1}{2} \sum_{k=1}^{\infty} \left(\begin{array}{ccc} l_i & k & l_i \\ 0 & 0 & 0 \end{array} \right)^2 \int_0^\infty \frac{2r_{min}^k}{r_{max}^{k+1}} P_i^2(r') P_j^2(r') dr'$$
(2.35)

where the symbols in brackets are Wigner's 3-j symbols⁶ and r_{min} and r_{max} are respectively the smallest and the largest value of r. g_j is the statistical weight (*i.e.* degeneracy) of the subshell (n_j, l_j) and ϵ_i , ϵ_{ij} are Lagrange multipliers introduced into the variational problem to impose orthonormality constraints on P_i :

$$\int_{0}^{\infty} P_{i}^{2}(r)dr = 1 \text{ and } \int_{0}^{\infty} P_{i}^{*}(r)P_{j}(r)dr = \delta_{n_{i}n_{j}}$$
(2.36)

Since the HF equations are coupled equations, they can only be solved by an iterative procedure, called the Self Consistent Field Method. This method consists in choosing a certain set of starting radial wave functions and then calculating all terms appearing in each HF equation with this set of radial wave functions. The HF equations then have to be solved one by one to obtain a new set of radial wave functions and this process has to be repeated until a certain convergence criterion, set on radial wave functions and energies, has been reached.

2.2.2 Relativistic Corrections

To take into account relativistic effects, single-electronic corrections are added to the nonrelativistic HF equations in a perturbative way. The resulting equations are then called relativistic Hartree-Fock equations (HFR).

1. Spin-orbit:

The first correction made is the spin-orbit correction. It represents the interaction between the orbital angular momentum of an electron, $\vec{l_i}$, and its spin, $\vec{s_i}$. This interaction induces, firstly, a displacement of the sublevels and secondly a separation of these into several energy levels. This is called the fine structure. This correction is introduced in the Hamiltonian of the system through the addition of a term proportional to $\vec{l_i} \cdot \vec{s_i}$ (which translates the coupling between $\vec{l_i}$ and $\vec{s_i}$). The proportionality factor is noted $\zeta_{n_i l_i}$.

2. Mass-velocity:

The second correction is the so-called *mass-velocity* correction, which is due to the relativistic dependence of the electron's mass on its speed. To obtain this correction, the difference between the relativistic expression of the energy of an electron (which

⁶Linked with Clebsch-Gordan coefficients.

is developed in series at the second order in $\frac{p^2}{m_0^2 c^2}$) and the non-relativistic energy must be calculated. That is to say $E_r - E_{nr}$ where

$$E_r = c\sqrt{m_0^2 c^2 + p^2} - m_0 c^2 + E_{pot}$$
(2.37)

and

$$E_{nr} = \frac{p^2}{2m_0} + E_{pot}$$
(2.38)

The correction is obtained by applying the substitution $\vec{p} \to -i\hbar \vec{\nabla}$ and taking the average value of $E_r - E_{nr}$ (in which the Laplacian squared then intervenes) in a state characterized by the quantum numbers (n, l, m).

3. Darwin Term:

The third and final correction takes into account the fact that, as a result of Heisenberg's uncertainty principle, the charge of the electron is delocalized, *spread* over a certain volume, which induces modifications in its potential energy.

Indeed, the instantaneous position of an electron can only be precisely defined in a volume corresponding to λ_C^3 where $\lambda_C = \frac{\hbar}{m_e c}$ is the Compton wavelength. The potential energy of the electron in the Coulomb field of the nucleus can therefore be written:

$$E_{pot}(r) = \int f(\rho) E_{pot}(r+\rho) d^3\rho \qquad (2.39)$$

where the integral relates to the volume λ_C^3 around the point r. If we develop in Taylor series around the point $\rho = 0$ we have:

$$E_{pot}(r+\rho) = E_{pot}(r) + \left(\frac{dE_{pot}}{d\rho}\right)_{\rho \to 0}\rho + \frac{1}{2}\frac{d^2E_{pot}}{d\rho^2}\rho^2$$
(2.40)

The first term corresponds to the non-perturbed energy, the second is zero because of the spherical symmetry of the potential and the third one is the Darwin term. This term will be equal to around $\lambda_C^2 \Delta E_{pot}$ (where Δ is the Laplacian operator).

For
$$E_{pot} = \frac{-Ze^2}{4\pi\varepsilon_0 r}$$

$$\Delta E_{pot} = \frac{Ze^2}{\varepsilon_0} \delta(r). \tag{2.41}$$

The Darwin correction is therefore given by:

$$\Delta E_D = \frac{Z e^2 \hbar^2}{\varepsilon_0 m_e^2 c^2} \delta(r) \tag{2.42}$$

and the Darwin term is the average value of this Darwin correction:

$$\langle \Delta E_D \rangle = \frac{Ze^2\hbar^2}{\varepsilon_0 m_e^2 c^2} |\Psi(r=0)|^2 \tag{2.43}$$

where $\Psi(r=0)$ is the wave function at the origin. This is non-zero only for the ssubshells (i.e. l=0). This implies that the Darwin term only affects the s-electrons.

2.2.3 Core-Polarization Corrections (HFR + CPOL)

The spectroscopic properties of an atom (or an ion) are largely influenced by the valence electrons. The problem can therefore be simplified by replacing the HF Hamiltonian with a Hamiltonian that includes an approximate potential describing the core electrons. However, we must ensure that this simplification preserves the effects of the ionic core on the wave functions of the valence electrons (i.e. the screening effects and the orthogonality of the wave function of a valence electron to that of a core electron). Correlation effects can be separated into three types of interactions:

- 1. valence-valence;
- 2. core-valence;
- 3. core-core.

For heavy ions, Migdalek and Baylis [83] developed an approach according to which the correlation between valence electrons is represented by the interaction of configurations explicitly introduced in the model while the core-valence correlation is described by a core polarization model potential. For an ion with N valence electrons, the one-body part of the polarization potential is written [81, 82]:

$$V_{P1} = -\frac{1}{2} \alpha_d \sum_{i=1}^{N} \frac{r_i^2}{(r_i^2 + r_c^2)^3}$$
(2.44)

where α_d is the dipole polarizability of the ionic core and r_c is an adapted cut-off radius which is arbitrarily chosen to be a measure of the ionic core's size.

Additionally, the interaction between the modified electric fields undergone by the valence electrons generates a two-body contribution given by

$$V_{P2} = -\alpha_d \sum_{k>l} \frac{\vec{r_k} \cdot \vec{r_l}}{[(r_k^2 + r_c^2)(r_l^2 + r_c^2)]^{3/2}}$$
(2.45)

There is a corresponding change to the radial matrix element of the length form of the oscillator strength: the radial integral $\langle P_{nl} | r | P_{n'l'} \rangle$ has to be substituted by

$$< P_{nl} | r(1 - \frac{\alpha_d}{(r^2 + r_c^2)^{3/2}}) | P_{n'l'} >$$
 (2.46)

Moreover, in order to allow for a more accurate treatment of the penetration of the core by the valence electrons, a further correction has been included in our model. With this correction [84, 85], the penetration of the ionic core by the valence electrons⁷ can be taken into account in a more realistic way. When we introduce the polarization of the core and the effects of penetration in the Hamiltonian, the operator of the dipole momentum⁸ appearing in the transition matrix must be adjusted. Therefore, the dipole radial integral becomes:

$$\int_{0}^{\infty} P_{nl}(r)r\left(1 - \frac{\alpha_d}{(r^2 + r_c^2)^{\frac{3}{2}}}\right)P_{n'l'}(r) - \frac{\alpha_d}{r_c^3}\int_{0}^{r_c} P_{nl}(r)rP_{n'l'}(r)dr.$$
 (2.47)

An accurate knowledge of the static dipole polarizability of the core α_d and the value of the cut-off radius are therefore required for this model. The values of α_d can be obtained

⁷Indeed, their wave function, and thus their probability of presence is non-zero in the core.

⁸Without all these effects in a spherically symmetric potential, the operator of dipole transition between a state ψ_1 and a state ψ_2 is simply given by r and we have the transition which can be written $\langle \psi_1 | r | \psi_2 \rangle$.

from theoretical calculations or experimental measurements. By contrast, the values of r_c cannot be inferred from the experiment. It is therefore common to take the mean value $\langle r \rangle$ of the core's outermost orbital as value for r_c . Biémont *et al.* [86] showed that relativistic Hartree-Fock calculations with core polarization corrections (HFR + CPOL) gave results comparable to a fully relativistic calculation taking explicitly into account valence interactions as well as core-valence interactions.

2.2.4 Solving the Hamiltonian Eigenvalue Equation: Slater-Condon Method

The Slater-Condon method is a method used to solve the Schrödinger equation. To do so, we develop the atomic wave functions ψ_k , which are eigenfunctions of the Hamiltonian H on a set of basis wave functions ψ_b generally characterized by a pure electronic coupling scheme (LS or jj for example).

$$\Psi_k = \sum_b x_k^b \psi_b \qquad \text{with} \qquad \sum_b (x_k^b)^2 = 1 \tag{2.48}$$

They describe the so-called configuration interaction, i.e. the interaction between basis states belonging to different configurations where the atomic wave function does not correspond to a pure state but to a superposition of states (similar to interference effects). Generally, atomic wave functions are not pure (each atomic state is a superposition of basis states). The series corresponding to Ψ_k is generally an infinite series (in other words, the base consists of an infinity of basis functions) but, in practice, we truncate this series by cleverly choosing the electronic configurations that we will then explicitly introduce in the model and that will thus give a finite number of basic wave functions ψ_b . This truncature of the series introduces undesirable effects in the calculation of the transition probabilities. These effects are called cancellation effects and are comparable to destructive interference effects (but they do not correspond to any physical reality, they are only due to errors introduced in the calculations by truncating the series). These cancellation effects can result in a transition being calculated with a much lower intensity than its actual value. To evaluate the significance of these cancellation effects for a calculated transition (between a $|\psi_i\rangle$ state and a $|\psi_i\rangle$ state), the cancellation factor (CF) is used. It is defined from the line strength of the transition. The line strength (for an E1 dipole transition) is the square of the electric dipole transition matrix element of the operator $P^{(1)}$ between the states considered:

$$S_{ij} = |\langle \psi_i | P^{(1)} | \psi_j \rangle |^2$$
 (2.49)

We have shown in the previous chapter that the transition probabilities A_{ij} and the oscillator strengths f_{ij} are commensurated to line strength S_{ij} . We write:

$$\sqrt{S_{ij}} = \sum_{b} \sum_{c} x_j^b x_i^c \langle \psi_c | P^{(1)} | \psi_b \rangle$$
(2.50)

from which we can define:

$$CF_{ij} := \left(\frac{\sum_{b}\sum_{c} x_{j}^{b} x_{i}^{c} \langle \psi_{c} | P^{(1)} | \psi_{b} \rangle}{\sum_{b}\sum_{c} |x_{j}^{b} x_{i}^{c} \langle \psi_{c} | P^{(1)} | \psi_{b} \rangle |}\right)^{2}$$
(2.51)

The smaller the CF value is, the less reliable the corresponding values for transition probability and oscillator strength⁹ are. Using the serial development of Ψ_k (which has

⁹Which can be subject to a large error.

been truncated by only keeping n terms), the eigenvalue equation can be written as a matrix $(\forall k = 1, ..., n)$:

$$\begin{pmatrix} H_{11} & \dots & H_{1n} \\ \dots & \dots & \dots \\ H_{n1} & \dots & H_{nn} \end{pmatrix} \begin{pmatrix} x_k^1 \\ \dots \\ x_k^n \end{pmatrix} = E_k \begin{pmatrix} x_k^1 \\ \dots \\ x_k^n \end{pmatrix}$$
(2.52)

The Hamiltonian diagonalization will provide us with the eigen energies and the mixing coefficients x_k^b . The latter will give us the expression of the atomic wave function Ψ_k .

2.2.5 Semi-Empirical Process

Thanks to Cowan's code [7], it is possible to model atomic structures and to obtain the parameters associated with them. Those parameters are: the energy levels E_k , the eigenfunctions Ψ_k , as well as the various radiative parameters which are associated with the possible transitions between the various states, namely the transition probabilities between two levels *i* and *j*, A_{ij} , and the associated oscillator strength, f_{ij} , as well as the radiative lifetime of each level, τ_i^{10} . This procedure is based on the HFR method to obtain the radial parts of mono-electronic wave function, and determines the energy levels and wave functions of the atomic system by diagonalizing the Hamiltonian using the method outlined in section 2.2.4. Knowing the eigenstates, the radiative parameters are then calculated through the calculation of the line strengths. Cowan's radiative parameter calculation procedure consists of four programs, called RCN, RCN2, RCG and RCE. These can be run in two different sequences:

- 1. an *ab initio* sequence: RCN, RCN2 and RCG, allowing the calculation of atomic parameters without any introduction of the experimental values;
- 2. an adjustment sequence of the energy levels by a least-squares method, in order to optimize the radial energy parameters. The latter consists in reducing the difference between the calculated energy levels and the known experimental levels and thus gives energy levels, wave functions and radiative parameters that are *a priori* more precise than in an *ab initio* calculation. It is performed by executing the *ab initio* sequence and then calling the RCE (which performs the optimization) and RCG programs in series.

2.2.5.1 Ab initio Sequence

The first program to be run is the RCN program. It needs the input, in the file named in36, of the configurations explicitly taken into account in the model. Then, it calculates, via the HFR method, the $P_{nl}(r)$ radial parts of the mono-electronic wave functions by solving the HF equations by the self-consistent field method. It gives the single-configuration parameters, i.e. the average energy of each configuration E_{av} , the single configuration Slater electrostatic interaction parameters $F^k(ij)$ and $G^k(ij)$ and the spin-orbit parameters ζ_{nl} . Afterwards, the RCN2 program requests the introduction of the scaling factors via the in2 file. These factors are necessary because it was found that the values of the parameters F^k, G^k and R^k calculated *ab initio* were generally too high compared to their optimal values. This systematic error is due to the finite and limited number of configurations that are chosen to be explicitly introduced into the model, which do not allow the entire set of configuration interactions to be modeled. Scaling factors are therefore introduced in order to reduce these values to have a better agreement between the calculated and

¹⁰The radiative lifetime of a level p being defined as $\frac{1}{A(p\to)}$ corresponds to the inverse of the sum of the transition probabilities of all possible radiative decay channels from the upper level p.

experimentally observed energy levels. In general, according to Cowan [7], scaling factors between 0.8 and 0.9 should be introduced (but they can be lower, down to 0.7 or 0.6 for very heavy elements). The RCN2 program then calculates, from the single-electronic radial wave functions, the Slater R^k interaction parameters that reflect the interactions between configurations and the transition radial integrals $\langle P_{nl}/P^{(1)}/P_{nl} \rangle$ for transitions between configurations.

Finally, the RCG program is executed. First, the code solves the angular part and builds the Hamiltonian H of the system thanks to the different radial parameters provided by RCN and RCN2 ($E_{av}, F^k, G^k, R^k, \zeta_{nl}$). Then, the eigen values and the eigen vectors of the atomic system are calculated by diagonalizing this Hamiltonian H. The wavelengths corresponding to the different possible transitions are then obtained by calculating the differences between the energy levels that may involve transitions. Finally, the radiative parameters (transition probabilities, oscillator strengths and radiative lifetimes) relative to these transitions are calculated using the line strengths. Cancellation factors are also calculated by RCG. RCN and RCN2 have been modified to take the CPOL effects into account. They now also read a new input, a file called *polpar*, that contains the α_d and r_c core-polarization parameters values.

2.2.5.2 Least-Square Adjustment Method - Fitting Procedure

Firstly, an *ab initio* procedure is initiated as explained in the previous section. Next, the RCE program is run, whose input file is the ine20 file. In this file, experimental levels (classified by values of J and increasing energies) are introduced parity by parity. By minimizing the difference between the energy levels calculated by RCG and the experimental energy levels by a least-squares method, it then performs an optimization of the parameters E_{av} , F^k, G^k, R^k and ζ_{nl} . This program also adjusts the so-called effective interaction parameters (α, β, γ) , which were previously set to zero. These parameters are there to correct some of the errors made by only including a limited number of configurations in the model (therefore not modeling all the configuration interactions). They adjust the electrostatic interaction parameters for the p, d and f subshells that are filled by more than one electron. Indeed, the "space" between the energy levels for these subshells is so small that it is comparable with the standard deviation of the fit. Thus, the effective interaction parameters α , β and γ correct respectively the electrostatic interaction parameters between the equivalent electrons of the subshells p, d and f. The RCE program then relaunches the first step of the RCG to obtain the new clean energies and eigenfunctions of the Hamiltonian built this time using the adjusted parameters (but, unlike the RCG program, the diagonalization of the Hamiltonian is done parity by parity). The procedure ends with a new execution of the RCG program, which calculates the optimized atomic and radiative parameters $(E_i, \Psi_i, \lambda_{ij}, A_{ij}, f_{ji}, \tau_i)$, as well as the CF associated with each calculated transition by diagonalizing the constructed Hamiltonian with the adjusted parameters obtained from RCE.

2.3 Fully Relativistic Multiconfiguration Dirac-Hartree-Fock Method

The second theoretical method we used was the Multiconfiguration Dirac-Hartree-Fock (MCDF or MCDHF), which is the purely relativistic equivalent of the Hartree-Fock method. Here, the Dirac equation must be solved in an approximate way for each electron of the atom under consideration and this in the approximation of the central field (independent electrons in an effective potential with spherical symmetry taking into account
the shielding). In this *multiconfiguration* method [87], each atomic state is described as a linear combination of well-chosen basis states. Then, by forcing an energy functional to be stationary with respect to small variations of the radial parts of the spin-orbitals, we obtain a system of coupled integro-differential equations (called Dirac-Fock equations) that we will solve iteratively using the method of the self-consistent field. At each iteration, the Hamiltonian diagonalization, constructed from the different interaction operators, provides us with an evaluation of the energy levels and atomic states. It is worth noting that quantum electrodynamics (QED)-related corrections are perturbatively added to the Hamiltonian of the system, allowing these effects to be taken into account in the final energy levels and atomic states.

2.3.1 Method's Basic Principle

In relativistic quantum mechanics, the wave equation governing the behavior of a free electron is the Dirac equation:

$$(i\gamma^{\mu}\partial_{\mu} - c)\psi = 0, \qquad (2.53)$$

where γ^{μ} are given in the Dirac representation by:

$$\gamma^{0} = \begin{pmatrix} \mathbb{1} & 0\\ 0 & -\mathbb{1} \end{pmatrix}, \gamma^{i} = \begin{pmatrix} 0 & \sigma_{i}\\ -\sigma_{i} & 0 \end{pmatrix}, \qquad (2.54)$$

i = 1, 2, 3 and σ_i are Pauli matrices. The problem of the hydrogen atom (i.e. the search for the bound stationary states of an electron in a Coulomb potential (potential with spherical symmetry) generated by the nucleus), is to search for the eigenstates of Dirac Hamiltonian¹¹.

$$h_D = c\vec{\alpha}.\vec{p} + (\beta - 1)c^2 + V_{nucl}(r), \qquad (2.55)$$

where α^i , i = 1, 2, 3, and β are defined, from Dirac matrices, as:

$$\alpha^{i} = \gamma^{0} \gamma^{i}, \qquad \beta = \gamma^{0}. \tag{2.56}$$

Assuming that the nucleus is punctual of infinite mass and of charge Z, we take, for the nuclear potential, a Coulomb potential $V_{nucl}(r) = -\frac{Z}{r}$.

The eigenvectors of the Hamiltonian h_D (2.55), which we will call later *spin-orbitals* (or *relativistic orbitals*), can then be written, in spherical coordinates:

$$\psi(r,\theta,\phi) = \frac{1}{r} \begin{pmatrix} cP_{nk}(r)\chi_{\kappa,m}(\theta,\phi) \\ -iQ_{n\kappa}(r)\chi_{-\kappa,m}(\theta,\phi) \end{pmatrix},$$
(2.57)

where $P_{n\kappa}(r)$ et $Q_{n\kappa}(r)$ are respectively the large and the small radial component which are solutions of the radial equations system:

$$\begin{pmatrix} (c^2 - \frac{Z}{r} - E_{n,\kappa}) & c(-\frac{d}{dr} + \frac{\kappa}{r}) \\ c(\frac{d}{dr} + \frac{\kappa}{r}) & (-c^2 - \frac{Z}{r} - E_{n,\kappa}) \end{pmatrix} \begin{pmatrix} P_{n\kappa}(r) \\ Q_{n\kappa}(r) \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix},$$
(2.58)

where *n* is the principal quantum number and κ is a quantum number that will be defined later. The two-component spinors $\chi_{\kappa,m}$ are eigenvectors of the operators \vec{j}^2 , j_3 , \vec{l}^2 and \vec{s}^2 (\vec{l}, \vec{s} and \vec{j} being respectively the operators of orbital angular momentum, of spin and of total angular momentum acting on a two-dimensional spinner space with $\vec{j} = \vec{l} + \vec{s}$) having as eigenvalues j(j+1), m, l(l+1) and s(s+1) where j is an half-integer. We

¹¹The electron's rest energy c^2 is subtracted to shift the state of zero energy and thus coincide with the usual non-relativistic conventions used in atomic physics.

have in addition: $-j \leq m \leq j$, l = j + 1/2, j - 1/2 and s = 1/2. The spinors $\chi_{\kappa,m}$ are also eigenvectors of the operator

$$K = -(1 + \vec{\sigma}.\vec{l}), \tag{2.59}$$

with eigenvalues

$$\kappa = (j + \frac{1}{2})\eta \text{ when } l = j + \frac{1}{2}\eta \text{ with } \eta = \pm 1,$$
(2.60)

The spinnors $\chi_{k,m}$ can be developped as

$$\chi_{k,m}(\theta,\phi) = \sum_{\sigma=-\frac{1}{2}} (l,m,-\sigma,1/2,\sigma|l,1/2,j,m) Y_l^{m-\sigma}(\theta,\phi) \Phi_{\sigma},$$
(2.61)

where Φ_{σ} are two basis two-components spinnors.

$$\Phi_{\frac{1}{2}} = \begin{pmatrix} 1\\ 0 \end{pmatrix} \text{ et } \Phi_{-\frac{1}{2}} = \begin{pmatrix} 0\\ 1 \end{pmatrix}.$$
(2.62)

2.3.2 Dirac-Coulomb Hamiltonian and Atomic Wave Functions

The relativistic Hamiltonian for an N-electron atom is given by the Dirac-Coulomb Hamiltonian:

$$H_{DC} = \sum_{i=1}^{N} h_{D_i} + \sum_{i>j} \frac{1}{r_{ij}},$$
(2.63)

where h_{D_i} is the mono-electronic Dirac Hamiltonian for the ith electron.

In the central field approximation, the hypothesis is that each electron moves independently from the other in a (spherical symmetry) effective potential V(r). This potential is generated by the nucleus and the N-1 other electrons as already explained in section 2.2. This allows us to write (2.55) as

$$h_D = c\vec{\alpha}.\vec{p} + (\beta - 1)c^2 + V(r), \qquad (2.64)$$

where

$$V(r) = \frac{-Z}{r} + U(r),$$
 (2.65)

and thus to approximate (2.63) by

$$H = \sum_{i=1}^{N} h_{D_i}.$$
 (2.66)

Given the spherical symmetry, this allows the spin-orbitals to be expressed as (2.57). Therefore, only the radial parts P(r) and Q(r) remain to be determined in order to fully know the electronic spin-orbitals.

The starting point of the MCDHF method is the development of each atomic state wave function (ASF) $\Psi(P, J, M)$ describing an atomic state of parity P, characterized by the quantum number of total angular momentum J of projection M, as a combination of configuration state functions (CSF) with the same parity and the same angular momentum $\Phi(\gamma, P, J, M)$ where γ contains all the information to define the CSF in a unique way (the coupling scheme, the orbital occupancy numbers, ...):

$$\Psi(P, J, M) = \sum_{r=1}^{n_c} c_r \Phi(\gamma_r, P, J, M),$$
(2.67)

where the c_r are the mixing coefficients and where n_c is the number of CSF introduced in the model. The mixing coefficients obviously have to be normalized:

$$\sum_{r=1}^{n_c} |c_r|^2 = 1.$$
 (2.68)

Each CSF is expressed as a linear combination of Slater determinants¹² constructed from spin-orbitals (2.57) whose radial parts are self-consistently optimized by solving the MCDHF equations (see section 2.3.4).

2.3.3 Hamiltonian Matrix in the Chosen CSF Basis

The first step is to build the Hamiltonian to be implemented in the method. The elements of the Hamiltonian matrix can be expressed [87] from angular coefficients that only depend on the angular parts of the selected CSFs and single and bielectronic radial integrals. The expression of the single-electron radial integral for an electron initially on an orbital a^{13} , is given by:

$$I(ab) = \delta_{\kappa_a \kappa_b} \int_0^\infty \left[cQ_a^*(r) \left(\frac{d}{dr} + \frac{\kappa_b}{r} \right) P_b(r) - cP_a^*(r) \left(\frac{d}{dr} + \frac{\kappa_b}{r} \right) Q(r) \right) - 2c^2 Q_a^*(r) Q_b(r) + V_{nucl}(r) \left[P_a^*(r) P_b(r) + Q_a^*(r) Q_b(r) \right] \right] dr.$$
(2.69)

The radial bi-electronic integral is given under the form of a generalized relativistic Slater-Integral, $R^k(abcd)$,

$$R^{k}(abcd) = \int_{0}^{\infty} \left[\left(P_{a}^{*}(r)P_{c}(r) + Q_{a}^{*}(r)Q_{c}(r) \right) \frac{1}{r} Y^{k}(bd,r) \right] dr, \qquad (2.70)$$

with Y Hartree-function defined as:

$$Y^{k}(bd,r) = r \int_{0}^{\infty} U^{k}(r,s) \left(P_{b}^{*}(s)P_{d}(s) + Q_{b}^{*}(s)Q_{d}(s) \right) ds, \qquad (2.71)$$

with

$$U^{k}(r,s) = \begin{cases} \frac{r^{k}}{s^{k}+1} & \text{if } r \leq s \\ \frac{s^{k}}{r^{k}+1} & \text{if } s < r \end{cases}$$
(2.72)

This bielectronic integral describes the electrostatic interaction between two electrons that may belong to different configurations (which reflects the configuration interaction). The direct radial integral, $F^k(ab)$, and the exchange integral, $G^k(ab)$, are two special cases of Slater integral in a monoconfigurational case. They respectively reflect the direct electrostatic and exchange interaction (due to the indistinguishability of the particles) between two electrons of the same configuration. Their expressions are given by:

$$F^{k}(ab) = R^{k}(abab),$$

$$G^{k}(ab) = R^{k}(abba).$$
(2.73)

¹²A Slater determinant allows the wave function of an atomic state to be written as an antisymmetric product of single-electron spin-orbitals, thus ensuring the antisymmetry of the wave function with respect to the exchange of two electrons as imposed by Pauli's exclusion principle.

¹³Characterized by quantum numbers (n_a, κ_a) .

The diagonal matrix elements in the chosen CSF basis can be written as [87]:

$$H_{rr} = \sum_{a=1}^{n_0} \left(q_r(a)I(aa) + \sum_{b\leq a}^{n_0} \left[\sum_{k=0,2,\dots}^{k_0} f_r^k(ab)F^k(ab) + \sum_{k=k_1,k_1+2,\dots}^{k_2} g_r^k(ab)G^k(ab) \right] \right),$$
(2.74)

where n_0 is the number of orbitals, $q_r(a)$ is the number of occupancy of orbital a (i.e. the number of electrons in the quantum number subshell (n_a, κ_a)) of the CSFr and where $f_r^k(ab)$ and $g_r^k(ab)$ are angular coefficients whose general expressions have been defined by [87]. These depend on the coupling scheme between equivalent (on the same subshell) and non-equivalent (on different subshells) electrons and, therefore, depend on the number of occupancy of each subshell. The standard coupling scheme used in the MCDHF method to construct CSFs is a jj coupling defined as follows:

- 1. the electrons from the same subshell a, with an occupation number $q(a) \leq 2j_a+1$ are coupled following a jj-coupling and thus give to each subshell an angular momentum J_a ;
- 2. T-the angular momenta J_a and J_b from successive subshell a and b are also jj-coupled in order to give an intermediate angular momentum X_1 which is itself coupled with the angular momentum of the subshell c, J_c , to get a new intermediate angular momentum X_2 . And so on until all the angular momenta from all the subshells have been coupled to give a total angular momentum J. This can be schematized as:

$$(...(J_a J_b) X_1 J_c) X_2 ...) J. (2.75)$$

The summation limits appearing in (2.74) are given by:

$$k_0 = (2j_a - 1)\delta_a b, (2.76)$$

$$k_1 = \begin{cases} |j_a - j_b| \text{ if } \kappa_a \kappa_b > 0\\ |j_a - j_b| + 1 \text{ if } \kappa_a \kappa_b < 0, \end{cases}$$
(2.77)

$$k_2 = \begin{cases} j_a + j_b \text{ if } j_a + j_b + \kappa \text{ is even} \\ j_a + j_b - 1 \text{ otherwise} \end{cases}$$
(2.78)

The off-diagonal elements $(r \neq s)$ of the Hamiltonian matrix in the chosen CSF basis, reflecting the configuration interactions between the different CSFs, can be expressed in the general form [87].

$$H_{rs} = \sum_{a,b} t_{rs}(ab)I(ab)\delta_{\kappa_a\kappa_b} + \sum_k \sum_{a,b,c,d} v_{rs}^k(abcd)R^k(abcd), \qquad (2.79)$$

where $t_{rs}(ab)$ and $v_{rs}^k(abcd)$ are angular coupling coefficients of the same type as those appearing in (2.74), also depending on the coupling scheme and the subshells a, b, c and dcontributing to H_{rs} . The expressions of these coefficients in the different cases¹⁴ are given by [87].

2.3.4 Getting the Spin-Orbitals through the MCDHF Equations

In order to optimize the radial parts P(r) and Q(r) of the spin-orbitals (2.57), a system of integro-differential equations obtained by applying a variational principle to an energy functional is solved to make it stationary with respect to the variations of the radial

¹⁴Sub-layer complete or not, electrons equivalent or not, etc.

parts of the spin-orbitals. The method of Lagrange multipliers is used to account for orthogonality constraints on spin-orbitals. Let us consider the energy functional as:

$$\mathcal{E} = \sum_{r=1}^{n_C} \sum_{s=1}^{n_C} d_{rs} H_{rs} + \sum_a \sum_b (1 - \delta_{ab}) \overline{q}(a) \epsilon_{ab}(a|b), \qquad (2.80)$$

where ϵ_{ab} are Lagrange multipliers in order to guarantee the orthonormality of radial parts of the spin-orbitals, where $\overline{q}(a)$ is the generalized occupation number and is defined as:

$$\overline{q}(a) = \sum_{r=1}^{n_C} d_{rr} q_r(a), \qquad (2.81)$$

and where

$$(a|b) = \int_0^\infty \left(P_a^*(r) P_b(r) + Q_a^*(r) Q_b(r) \right) dr.$$
(2.82)

The coefficients d_{rs} are generalized weights that can be expressed in different ways leading to several variants of the energy functional:

• OL Mode (*Optimal Level*): In this mode, optimization is done on only one ASF at a time, so each ASF is optimized independently of the others. For an atomic state *i*, the generalized weights are then given by

$$d_{rs} = c_{ri}c_{si}.\tag{2.83}$$

The spin-orbitals obtained with this method may vary from one ASF to another.

• EOL Mode (*Extended Optimal Level*): This option allows optimization to be performed on a set of energy levels. The generalized weights are then written as:

$$d_{rs} = \frac{1}{n_L} \sum_{i=1}^{n_L} c_{ri} c_{si}, \qquad (2.84)$$

where n_L is the number of levels chosen $(n_L \leq n_C)$. In this case, the same set of spin-orbitals is used to describe the set of ASFs corresponding to the energy levels chosen to construct \mathcal{E} .

• AL Mode (*Average Level*): In this option, we optimize the trace of the Hamiltonian matrix. The generalized weights are then independent of the mixing coefficients and each CSF is weighted by its statistical weight:

$$d_{rs} = \delta_{rs} \frac{2J_r + 1}{\sum_{t=1}^{n_C} (2J_t + 1)}.$$
(2.85)

Unlike the OL and EOL modes, this option allows a global optimization on all energy levels.

• EAL Mode (*Extended Average Level*): This option optimizes a weighted trace of the Hamiltonian matrix. The weights, independent of the mixing coefficients, can then be chosen by the user.

Applying the variational principle to the energy functional for a relativistic orbital, we obtain a system of coupled interdifferential equations called the MCDHF equations. They are given by:

$$\begin{cases} -\frac{Z - Y(a;r)}{r} P_a(r) + c\Big(-\frac{d}{dr} + \frac{\kappa_a}{r}\Big)Q_a(r) - \epsilon_{aa}P_a(r) = -X_{+1}(a;r) \\ c\Big(\frac{d}{dr} + \frac{\kappa_a}{r}\Big)P_a(r) + \Big(-2c^2 - \frac{Z - Y(a;r)}{r}\Big)Q_a(r) - \epsilon_{aa}Q_a(r) = -X_{-1}(a;r), \end{cases}$$
(2.86)

with the normalization condition:

$$\int_{0}^{\infty} \left(P_{a}^{*}(r)P_{a}(r) + Q_{a}^{*}(r)Q_{a}(r) \right) dr = 1,$$
(2.87)

where Y(a; r) is the direct interaction potential and $X_{\beta}(a; r)$, with $\beta = \pm 1$, is the exchange interaction potential. They can be written as:

$$Y(a;r) = \sum_{k} \sum_{b=1}^{n_0} \left[y^k(ab) Y^k(bb;r) - \sum_{c=1}^{n_0} y^k(abac) Y^k(bc;r) \right],$$
(2.88)

for Y(a; r) where Y^k is the Hartree function (see 2.71)

$$y^{k}(ab) = \frac{1+\delta_{ab}}{\overline{q}(a)} \sum_{r=1}^{n_{C}} d_{rr} f_{r}^{k}(ab), \qquad (2.89)$$

$$y^{k}(abac) = \frac{1}{\overline{q}(a)} \sum_{r=1}^{n_{C}} \sum_{s=1}^{n_{C}} d_{rs} v_{rs}^{k}(abac), \qquad (2.90)$$

and as

$$X_{\beta}(a;r) = -\sum_{b \neq a} \delta_{\kappa_{a}\kappa_{b}} \epsilon_{ab} R_{\gamma_{b}\beta_{\kappa_{b}}}(r) + \sum_{k} \left[\sum_{b \neq a} x^{k}(ab) \frac{Y^{k}(ba;r)}{r} R_{\gamma_{b}\beta_{\kappa_{b}}}(r) - \sum_{bcd} \left(1 - \delta_{ac} x^{k}(abcd) \frac{Y^{k}(bd;r)}{r} R_{\gamma_{b}\beta_{\kappa_{b}}}(r) \right) \right],$$

$$(2.91)$$

for $X_{\beta}(a; r)$

$$R_{\gamma_b\beta_{\kappa_b}}(r) = \begin{cases} P_{\gamma,\kappa}(r) \text{ if } \beta = +1\\ Q_{\gamma,\kappa}(r) \text{ if } \beta = -1, \end{cases}$$
(2.92)

and where

$$x^{k}(ab) = \frac{1}{\overline{q}(a)} \sum_{r=1}^{n_{C}} d_{rr} g_{r}^{k}(ab), \qquad (2.93)$$

$$x^{k}(abcd) = \frac{1}{\overline{q}(a)} \sum_{r=1}^{n_{C}} \sum_{s=1}^{n_{C}} d_{rs} v_{rs}^{k}(abcd).$$
(2.94)

Solving this system of coupled equations can only be done iteratively. It is thus the method of the self-consistent field which is used to obtain the radial parts P(r) and Q(r) of each spin-orbital (2.57). This method entails:

- 1. the selection of a set of starting radial functions P(r) and Q(r) (e.g. the radial parts of screened hydrogenic spin-orbitals);
- 2. the calculation of all the terms appearing in the MCDHF equations with the starting radial parts;
- 3. the resolution of the MCDHF equations to obtain new radial functions.

Steps 1, 2 and 3 are then repeated iteratively until a certain convergence criterion is reached. It should be noted, however, that the increase in the number of radial parts of relativistic orbitals relative to non-relativistic radial wave functions makes the optimization process much longer and more complex than in the non-relativistic (Hartree-Fock) case.

2.3.5 Solving the Eigenvalues Equation Using the Configuration Interaction Method

Once the orbitals are optimized, the mixing coefficients can be obtained with the interaction configuration method. An atom's energy in a state Γ described by an ASF is given by:

$$E_{\Gamma} = \vec{c_{\Gamma}}^{\dagger} H \vec{c_{\Gamma}}, \qquad (2.95)$$

Where H is the Hamiltonian matrix in the chosen CSF basis and where $\vec{c_{\Gamma}}$ is a column vector with, as components, the mixing coefficients of the ASF describing the atomic $\begin{pmatrix} c_{\Gamma,1} \end{pmatrix}$

state $\Gamma : \begin{pmatrix} c_{\Gamma,1} \\ \dots \\ c_{\Gamma,n_C} \end{pmatrix}$ with the normalizing condition (2.67) which can be written $\vec{c_{\Gamma}}^{\dagger} \vec{c_{\Gamma}} = 1$.

Looking for stationary states of the system, i.e. eigenstates of the Hamiltonian, entails the resolution of the secular equation

$$H\vec{c_{\Gamma}} = E_{\Gamma}\vec{c_{\Gamma}}.$$
(2.96)

Eigenvalues and eigenvectors obtained by diagonalizing the Hamiltonian correspond to the atomic energy levels and to the mixing coefficient of the ASF. This allows us to write and describe the atomic states.

2.3.6 Quantum Electrodynamics Corrections

To describe the interactions between the bound electrons in an atom, the Coulomb interaction term is no longer sufficient. Indeed, it is necessary, in a relativistic context, to add some corrections coming from quantum electrodynamics (QED). The most important corrections are the electron-electron scattering, also called transverse interaction and corresponding to a first-order correction, as well as the vacuum polarization and the electron self-energy correction, both corresponding to second-order corrections. All these corrections are perturbatively added to the Hamiltonian when solving the secular equation by the configuration interaction method in order to correct energy levels and ASF.

2.3.6.1 Transverse interaction

In QED, electron-electron scattering is described by the exchange of a virtual photon¹⁵. The correction to the instantaneous Coulomb interaction term between two bound electrons of the atom that is due to this virtual photon exchange is called the transverse interaction. It is described by a Hamiltonian operator that is added to the Dirac-Coulomb Hamiltonian describing the system. Its expression is obtained by assuming that the energy of the photon exchanged between an electron of an orbital i and an electron of an orbital j is equal to the difference of the binding energies of the two orbitals. The expression of this transverse interaction operator is given by [87]:

$$B_{ij}^{T} = -\vec{\alpha_{i}}.\vec{\alpha_{j}}\frac{e^{i\omega_{ij}r_{ij}/c}}{r_{ij}} - (\vec{\alpha_{i}}.\vec{\nabla_{i}})(\vec{\alpha_{j}}.\vec{\nabla_{j}})\frac{e^{i\omega_{ij}r_{ij}/c} - 1}{\omega_{ij}^{2}r_{ij}/c^{2}},$$
(2.97)

where $\vec{\alpha_i} = (\alpha_i^1, \alpha_i^2, \alpha_i^3)$ is a vector with the three Dirac matrices as components α^k acting on an electron from orbital i, $r_{ij} = |\vec{r_i} - \vec{r_j}|$, and where ω_{ij} is the emitted photon frequency i.e. $\hbar \omega_{ij} = |E_i - E_j|$ where E_i et E_j are the binding energies of electrons from orbitals iand j. The Feynman diagram of this interaction is given in Figure 2.1.

¹⁵Electromagnetic Interaction Gauge Boson



Figure 2.1: Feynman Diagram of the Transverse Interaction

2.3.6.2 Vacuum Polarization

The QED theory predicts that a fluctuation in vacuum energy ΔE can result in the creation of an electron-positron pair that annihilates after a time Δt so that Heisenberg's uncertainty principle $\Delta E.\Delta t \geq \hbar$ is satisfied. That way, dipoles spontaneously emerge from the vacuum for very short periods of time, changing the surrounding electromagnetic field. Indeed, an electron interacting with these dipoles modifies the spatial distribution of the latter, which gives rise to a polarization of the vacuum as well as a modification of the electromagnetic field generated by the electron (shielding of its charge). The electronic structure of the atoms is therefore also affected. The correction due to vacuum polarization is taken into account in the MCDHF method via an effective vacuum polarization potential in the vicinity of a point charge. This potential, called the Uehling potential [88], is perturbatively added to the Hamiltonian of the system. The vacuum polarization's Feynman diagram is given in Figure 2.2



Figure 2.2: Feynman Diagram of the Vacuum Polarization

2.3.6.3 Self-Energy

The electron self-energy is another correction from the QED theory which is taken into account in the MCDHF method. It is the phenomenon by which an electron spontaneously emits a virtual photon of energy ΔE and reabsorbs it after a time Δt such that $\Delta E.\Delta t \geq \hbar$. This phenomenon contributes in particular to the mass-energy of the electrons (hence its name) because the electron interacts with its own electromagnetic field, thus also modifying the electronic structure of the atoms. The electron's self-energy can be calculated as part of the renormalization of quantum electrodynamics. Figure 2.3.6.3 shows the Feynman diagram of this interaction.



Figure 2.3: Feynman Diagram of the Self Energy

2.3.7 GRASP2K - GRASP2018 Programs

In our work, the MCDHF method was implemented using two recent versions of GRASP (General Relativistic Atomic Structure Package) namely GRASP2K [89] and GRASP2018 [90]. In these codes, a sequence of routines is executed as follows:

- 1. *rnucleus*: defines the nuclear data and generates the radial coordinates grid;
- 2. *rcsfgenerate*: generates the CSF list on the basis of excitation rules from the reference configurations;
- 3. rangular: generates the angular parts of the wavefunctions ;
- 4. *rwfnestimate*: generates the radial parts of the initial radial wavefunctions;
- 5. *rmcdhf*: solves the MCDHF equations using the self-consistent field method;
- 6. *rci*: solves the secular equation by diagonalizing the Hamiltonian matrix while taking into acount the QED corrections;
- 7. *rtransition*: determines all the possible transitions between the previously calculated levels.

Chapter 3

Atomic Data Calculations in U II and Th II for Cosmochronological Applications

In view of their potential use in cosmochronological investigations as mentioned in section 1.3.1, only the strongest spectral lines in singly ionized thorium and singly ionized uranium were considered in the present study. More precisely, we limited our study to the Th II and U II electric dipole transitions for which the HFR+CPOL log gf-values were found to be larger than -1. Such strong transitions are among the only ones likely to be observed in astrophysical spectra and they could therefore be of primary importance in cosmochronology. They also have the great advantage of not being too much affected by significant cancellation effects when calculating the line strengths, which suggests that the corresponding oscillator strengths can be expected to be fairly reliable (see [7]).

3.1 U II

Uranium is the heaviest natural element (Z = 92). Among uranium isotopes, ²³⁸U is the most stable with a half-life of 4.5 billion years. This element was discovered in 1789 by the Prussian chemist Martin Heinrich Klaproth when he analyzed a piece of rock brought to him from the Saint Joachimstal mine [91]. He suggested the name *uran* or *uranite* for the compound he had just identified, in reference to the discovery of the planet Uranus made by William Herschel in 1781. This oxide, renamed uranium in 1790, had the property of giving a fine fluorescence to glass and a greenish yellow color to glasses. Henri Becquerel actually discovered the radioactivity of uranium much later, in 1896. He noticed that photographic plates placed next to uranium salts had been printed without having been exposed to light. The plates had been blackened by the radiation emitted by the salts; this was the manifestation of natural radioactivity [92, 93].

We started this study with singly ionized uranium (U II). Before our work, we looked for previously available data in U II. We found that, in their compilation of the energy levels and the spectra of actinides, Blaise and Wyart [1] listed, some preliminary energy levels in U II for both parities. These data were preceded in the literature by the publications about emission lines by Steinhaus *et al.* [2] and Palmer *et al.* [3]. Energy values of the lowest levels of configurations including 5f, 6d, 7s, 7p electrons were the main ones reported. It thus provided an update to the previous estimations made by Brewer [4]. This database was later extended by Blaise *et al.* [5] who measured uranium hollowcathode Fourier-transform spectra between 1800 and 42000 cm⁻¹ which, when combined with earlier visible and UV spectra, led to the determination of numerical values for 354 and 809 energy levels belonging to the four odd configurations $5f^37s^2$, $5f^36d7s$, $5f^36d^2$, $5f^47p$, and to the six even configurations $5f^47s$, $5f^46d$, $5f^26d^27s$, $5f^26d7s^2$, $5f^37s7p$, $5f^36d7p$, respectively.

More recently, the latest energy levels of U II were construed by Meftah *et al.* [6] using the Racah-Slater parametric method with the Cowan codes [7]. In this work, 253 levels of the interacting odd-parity configurations $5f^37s^2 + 5f^36d7s + 5f^36d^2 + 5f^47p + 5f^5$ were represented by 24 free radial parameters and 64 constrained ones. The root mean square (rms) deviation found was 60 cm⁻¹. In the even parity, 125 levels were classified using a multiconfiguration basis including $5f^47s + 5f^46d + 5f^26d^27s + 5f^26d7s^2 + 5f^26d^3$ by 22 free parameters with a rms deviation of 84 cm⁻¹. Moreover, a separate semi-empirical model, including only the higher even configurations $5f^37s7p$ and $5f^36d7p$, led to the tentative classification of 12 energy levels within these configurations.

Unfortunately, for these two configurations, the semi-empirical method of parametric fitting was limited by the optimization of average energies and spin-orbit ζ_{5f} integrals, the quantitative evaluation of configuration interaction effects within the whole group 5f⁴(7s + 6d) + 5f²(6d + 7s)³ + 5f³7s7p + 5f³6d7p having been tried unsuccessfully. Finally, Meftah *et al.* parametric study [6] allowed them to re-investigate the high resolution UV spectrum of uranium which was recorded in the late eighties at the Meudon Observatory and of which the analysis was unfinished. In the context of this study, 451 lines of U II were classified in the region 2344 – 2955 Å and a new level belonging to 5f³6d7p was established at 39115.98 cm⁻¹ with J = 11/2.

As regards the radiative decay rates, the first measurements of relative line intensities in U II were obtained from emission arc spectra by Meggers et al. [8], Corliss and Bozman [9], Voigt [10] and Corliss [11]. In the atlas of uranium lines published by Palmer [3], relative intensities measured from uranium hollow-cathode spectra recorded with a Fourier transform spectrometer (FTS) were listed for 4928 U I and 431 U II emission spectral lines between 11000 and 26000 cm⁻¹. The oscillator strengths of the lines at λ = 3859.571 Å and λ = 4050.041 Å were later determined by Chen and Borzileri [12] who combined experimental lifetime measurements of the upper levels with unpublished branching fractions. Oscillator strengths were also reported for about 100 U II lines by Henrion et al. [13] from relative intensities measured on a hollow-cathode lamp spectrum. In his database, Kurucz [14] listed transition probabilities and oscillator strengths for many U II lines based on the experimental data reported by Meggers et al. [8], Corliss and Bosmann [9], and Chen [12]. Finally, about 20 years ago, accurate radiative lifetimes were measured by Lundberg et al. [15], using laser-induced fluorescence technique, for six even-parity energy levels of singly ionized uranium located at 23315.090 cm⁻¹ (J = 9/2), 24684.132 cm⁻¹ (J = 9/2), 25714.049 cm⁻¹ (J = 13/2), 26191.309 cm⁻¹ (J = 13/2), $28154.450 \text{ cm}^{-1}$ (J = 11/2) and $30341.675 \text{ cm}^{-1}$ (J = 15/2). Experimental oscillator strengths for 57 U II lines in the region 3500 – 6700 Å were then obtained by combining these latter radiative lifetimes with new branching fractions derived from the measured line intensities in the spectra emitted by a hollow cathode and analyzed using a Fourier transform spectrometer by Nilsson *et al.* [16].

3.1.1 HFR+CPOL Calculations

In the present study, the configurations retained in the calculations were those presented by Meftah *et al.* [6] as being the most interacting ones in the lowest part of the energy level spectrum, namely $5f^37s^2$, $5f^36d7s$, $5f^36d^2$, $5f^47p$, $5f^5$ for the odd parity, and $5f^47s$, $5f^46d$, $5f^26d^27s$, $5f^26d7s^2$, $5f^26d^3$, $5f^37s7p$, $5f^36d7p$ for the even parity. This represents a total of 3237 and 6039 energy levels in each parity, respectively.

Since the configurations mentioned hereabove explicitly include part of the correlation effects out of the $5f^2$ ionic core, core-polarization effects were considered using the dipole

polarizability, α_d , equal to 9.79 a_0^3 as tabulated by Fraga *et al.* [94] for the U V ion. In the present work, we used $r_c = 0.75 a_0$, which depicts the distance at which the total probability density of the ionic core orbitals equates to 10% of its maximum value, as suggested by Hameed [84].

This is illustrated in Figure 3.1. This Figure shows the calculated probability density of the core in the ground configuration, together with the r_c value that we considered in our computations. We noticed that, when using these core-polarization parameters, electric dipole transition radial integrals were reduced by around 20-25%.



Figure 3.1: Electron probability density of the ionic core in the ground configuration $(5f^37s^2)$ of U II. The cut-off radius is marked by a dash vertical line where the probability density fall to 10% of its maximum value.

However, for singly ionized uranium, the analytical core-polarization correction to the dipole operator introduced in section 2.2 is no longer valid for transitions involving 5f electrons. The latter are indeed too deeply interlocked inside the $6s^26p^6$ closed subshells as highlighted in Figure 3.2.

In order to take polarization effects more realistically into account for the 5f-6d transitions, the corresponding radial integrals were scaled down by a factor 0.80, in a similar way to that used for computing the 4f-5d transitions in lowly ionized lanthanides (Biemont *et al.* [86]).

In order to reduce as much as possible the differences between calculated and available experimental energy levels, we adopted the fitted radial parameters reported by Meftah *et al.* [6] for the five odd- and the seven even-parity configurations that we included in our physical model. As a reminder, for the odd configurations, they were able to fit up



Figure 3.2: Electron probability densities of the outermost ionic core orbitals in U II, showing the overlap between 5f subshell and $6s^26p^6$ closed subshells

to 253 experimental energy levels with a final rms deviation of 60 $\rm cm^{-1}$ using 22 free and 64 constrained parameters among which the average energies (E_{av}) , the electrostatic Slater integrals (F^k, G^k, R^k) , the spin-orbit parameters (ζ_{nl}) and the effective interaction operators (α, β, γ) . Their semi-empirical fitting procedure was less satisfactory in the even parity. Indeed, they were forced to separate their parametric analysis into two groups of configurations, i.e. $5f^47s + 5f^46d + 5f^26d^27s + 5f^26d^7s^2 + 5f^26d^3$, on the one hand, and $5f^{3}7s7p + 5f^{3}6d7p$, on the other hand. For the first group of configurations, they found a rms deviation of 84 $\rm cm^{-1}$ for 125 energy levels which were fitted with 22 radial parameters. However, the interpretation of the second group's energy level structure with the same parametric method could only be carried out by only adjusting the average energies E_{av} and spin-orbit ζ_{5f} integrals. This led to a rms deviation of 441 cm⁻¹ for 12 energy levels. In our work, we gathered all these 7 even configurations together in the same model with the fitted parameters taken from Meftah et al. [6] as a starting point. After a rather similar fitting procedure but with all the configuration interactions explicitly taken into account, we found a rather good average energy deviation of 280 cm^{-1} for the levels of interest, i.e. those involved in the strongest transitions reported in Table 3.1.

3.1.2 Results

In view of their potential future use in cosmochronological studies, only the strongest spectral lines (log gf > -1) were considered in our study. These transitions, involving

energy levels up to 30342 cm^{-1} , are reported in Table 3.1. This corresponds to 38 U II spectral lines appearing in the wavelength range from 3337 to 4627 Å. For these lines, log qf-values obtained by our calculations are compared with the older data deduced from emission line intensity measurements by Corliss [11], Chen and Borzileri [12], Henrion et al. [13] and Kurucz [14], as well as with the more recent and more accurate experimental values obtained by Nilsson *et al.* [16]. It can be observed, from Table 3.1, that our calculated oscillator strengths are in reasonable agreement with the latter measurements, the mean relative difference between both sets of gf-values being found to be equal to 25%if we exclude four lines at 3670.068, 3865.916, 4155.409 and 4241.664 Å, for which our HFR+CPOL results are around twice as small as the experimental oscillator strengths of Nilsson *et al.* [16]. It is worth noting, however, that three of these transitions are characterized by the same upper even-parity level at $28154.451 \text{ cm}^{-1}$, which was found to be extremely mixed, and thus very sensitive to small changes in the eigenvector composition. Indeed, for this level, our calculations led to a main LS component, i.e. $5f^{3}(^{4}I)6d7p$ ${}^{6}L_{11/2}$, as weak as 7%, to be compared with the 18% obtained by Meftah *et al.* [6] using a more limited physical model.

For four other spectral lines, at $\lambda = 3337.785$, 3623.057, 4172.973 and 4178.995 Å, our computed log gf-values are given between square brackets in Table 3.1 to indicate that the corresponding results are more likely to be affected by larger uncertainties. This is because of the fact that, for the two upper even-parity levels involved in these transitions, it was extremely difficult to establish a trustworthy correspondence between the experimental values, i.e. E = 28507.894 and 30240.416 cm⁻¹, and the calculated ones, the retained theoretical levels being, moreover, very strongly mixed, with main LS components not exceeding 5% according to our calculations. For that matter, these two levels were not classified in the recent parametric analysis of the U II spectrum by Meftah *et al.*

Figure 3.3 shows the density of the energy levels distribution in U II and seen that proximity between the different levels, very high mixing effects due to very important configuration interaction are to be suspected.

Those effects have indeed been observed in our results as highlighted in Table 3.2 where the main LS-components of the most important levels (from our work) involved in the intense transitions displayed in Table 3.1 are given in percentages.

This also illustrates the strong intermediate coupling and configuration interaction characterizing heavy ions like U II. It is clear, as mentioned above, that the majority of levels appears to be extremely mixed, preventing any reliable spectroscopic designation. This is even more obvious in the even parity in which many levels were found to be the mixture of numerous (sometimes up to 20) significant contributions of comparable amplitudes and with the main component being often smaller than 10%.

Fortunately, the most intense transitions, more likely to be of use for the astrophysicists, are less affected by those cancellation effects. This can be seen in Table 3.1, because none of the most intense transitions is marked as affected by a high uncertainty. This is shown in Figure 3.4, where it is clear that the transitions with log gf > -1 are much less likely to be affected by those cancellation effects¹.

The line 3859.571 Å is also of high interest because it was used as cosmochronometer by Cayrel *et al.* [54], as mentioned in section 1.3. For this transition, our gf-value of 0.875 is in excellent agreement with the accurate experimental result reported by Nilsson *et al.*, i.e. gf = 0.857, whereas all the previous data were very scattered between gf-values so different as 0.240 ([11]), 0.625 ([12]), 0.190 ([13] and 0.785 ([14]).

Finally, it appeared that the core-polarization effects that we included in our physical model have a major influence on the final oscillator strengths, the mean ratio $\langle gf_{HFR+CPOL}/gf_{HFR} \rangle$ being found to be equal to 0.57. These effects, which are

¹The bigger the CF is, the most reliable the log gf obtained is.

Ull odd configurations



Figure 3.3: Energy Levels in U II - Original picture from Meftah et al. [6]

assumed to take into account the most important core-valence and core-core correlations, are expected to be much larger than those of intravalence correlations not explicitly considered in our multiconfiguration expansions. Furthermore, we observed that additional valence configurations have a rather negligible influence on the transition rates we computed. More exactly, as a first step, the configurations $5f^27s^27p$, $5f^26d7s7p$, $5f^26d^27p$, $5f^27s7p^2$ and $5f^26d7p^2$ were investigated. By comparing a nine-configuration *ab initio* HFR calculation (including $5f^37s^2$, $5f^36d7s$, $5f^36d^2$, $5f^47s$, $5f^46d$, $5f^26d7s^2$, $5f^26d^27s$, $5f^36d^27p$, $5f^26d^2p$) with a fourteen-configuration calculation (adding $5f^27s^27p$, $5f^26d7s7p$, $5f^26d^27p$, $5f^26d^2p^2$), the effect of the latter five configurations was appraised and found rather small. As a matter of fact, the mean difference for the strongest lines (log gf > -1) was 0.09 dex², which corresponds to a relative discrepancy of a few percent. When adding $5f^37s7d$, $5f^36d7d$, $5f^47d$, $5f^27s^27d$ and $5f^26d^27d$ to the nine-configuration expansion, the mean difference was then 0.05 dex. Finally, the inclusion of the $5f^37s8s$, $5f^36d8s$, $5f^48s$, $5f^26d^28s$, $5f^27s^28s$, $5f^37s8p$ and $5f^36d8p$ was found to affect the log gf-values by less than 0.04 dex.

²Contraction of decimal exponent: N dex = 10^N .



Figure 3.4: Cancellation factors plotted as a function of log gf-values for U II spectral lines. CF-values smaller than typically 0.05 indicate that the corresponding f-values may be affected by larger percentage errors.

Table 3.1: Strongest visible spectral lines in U II. The transitions listed are limited to those for which the log gf-values, computed in the present work, are greater than -1.0.

$\lambda_{air}{}^a$	Lower odd	$evel^b$	Upper even	$level^b$				$\log gf$		
(Å)	$E (\mathrm{cm}^{-1})$	J	$E (\mathrm{cm}^{-1})$	J	\mathbf{C}^{c}	CB^d	\mathbf{H}^{e}	\mathbf{K}^{f}	\mathbf{N}^{g}	This work ^{h}
3337.785	289.041	11/2	30240.416	11/2	-1.28			-0.897		[-0.794]
3357.930	289.041	11/2	30060.727	11/2	-1.39			-1.071		-0.703
3372.004	289.041	11/2	29936.466	11/2	-1.46			-1.170		-0.351
3406.269	914.765	9/2	30263.978	9/2	-1.42			-1.116		-0.892
3496.414	1749.123	13/2	30341.673	15/2	-1.12			-0.691	-0.821	-0.595
3546.677	1749.123	13/2	29936.466	11/2	-1.37			-1.066	-0.785	-0.549
3623.057	914.765	9/2	28507.894	11/2	-1.29			-1.002		[-0.925]
3640.945	1749.123	13/2	29206.703	11/2	-1.38			-1.121		-0.887
3670.068	914.765	9/2	28154.447	11/2	-0.72			-0.173	-0.192	-0.556
3700.571	914.765	9/2	27929.924	11/2	-1.21			-0.904		-0.909
3724.983	1749.123	13/2	28587.261	11/2	-1.45			-1.003		-0.896
3782.841	289.041	11/2	26716.697	13/2	-0.89			-0.478		-0.674
3826.507	289.041	11/2	26415.115	13/2	-1.17		-1.125	-0.904		-0.569
3859.571	289.041	11/2	26191.312	13/2	-0.62	-0.204	-0.721	-0.105	-0.067	-0.058
3865.916	2294.696	11/2	28154.447	11/2	-0.77			-0.273	-0.421	-0.800
3881.454	4585.434	13/2	30341.673	15/2	-0.80			-0.279	-0.509	-0.465
3932.021	289.041	11/2	25714.049	13/2	-0.89		-0.824	-0.528	-0.317	-0.478
3944.130	4585.434	13/2	29932.395	15/2	-1.23			-0.928		-0.959
3985.793	5259.653	15/2	30341.673	15/2	-0.71			-0.165	-0.278	-0.307
3990.420	914.765	9/2	25967.697	7/2	-1.29		-1.745	-1.116		-0.925
4004.064	1749.123	13/2	26716.697	13/2	-1.31			-1.138		-0.936
4044.412	5259.653	15/2	29978.143	13/2	-0.97			-0.554	-0.706	-0.810
4051.912	5259.653	15/2	29932.395	15/2	-0.95			-0.541		-0.692
4053.020	1749.123	13/2	26415.115	13/2	-1.51			-1.448		-0.752
4090.133	1749.123	13/2	26191.312	13/2	-0.78			-0.377	-0.184	-0.125
4116.097	0.000	9/2	24288.004	11/2	-1.19		-1.194	-1.036		-0.712
4155.409	6283.431	13/2	30341.673	15/2	-1.10			-0.759	-0.606	-0.948
4171.589	1749.123	13/2	25714.049	13/2	-0.92			-0.606	-0.474	-0.567
4172.973	6283.431	13/2	30240.416	11/2	-1.29			-1.051		[-0.917]
4174.189	5526.750	13/2	29476.743	13/2	-1.21			-0.948		-0.865
4178.995	4585.434	13/2	28507.894	11/2	-1.41			-1.261		[-0.667]
4211.658	4585.434	13/2	28322.361	11/2	-1.25			-1.040	-0.811	-0.709
4241.664	4585.434	13/2	28154.447	11/2	-0.83			-0.431	-0.103	-0.566
4282.460	4585.434	13/2	27929.924	11/2	-1.37			-1.242		-0.684
4341.686	289.041	11/2	23315.092	9/2	-1.24		-1.337	-1.161	-0.700	-0.536
4472.330	289.041	11/2	22642.478	9/2	-1.28		-1.398	-1.260		-0.863
4555.091	8394.362	15/2	30341.673	15/2	-1.34			-1.167	-0.650	-0.771
4627.075	4585.434	13/2	26191.312	13/2	-1.27			-1.178	-0.593	-0.486

^a Experimental wavelengths from Kurucz (1995) [14]

- ^b Experimental energy levels from Blaise *et al.* (1994) and Meftah *et al.* (2017) [6]
- ^c Values from Corliss (1976) [11]
- ^d Values from Chen and Borzileri (1981) [12]
- $^{\rm e}~$ Values from Henrion et~al.~(1987)~[13]
- $^{\rm f}$ Values from Kurucz (1995) [14]
- ^g Values from Nilsson *et al.* (2002) [16]
- ^h Values between square brackets correspond to uncertain line identifications in the calculations (see text)

Table 3.2:	Main LS-coupling	components	of energy	levels	involved	in the	e transitions	in U
II listed in	Table 3.1							

Energy ^{a} (cm ^{-1})	\mathbf{J}	First component $(\%)$	Second component $(\%)$	Third component $(\%)$
Even parity				
0	9/2	$77 \ 5f^37s^2 \ (^4I)^4I$	$12.6 \ 5 f^3 7 s^2 \ (^2 H)^2 H$	$3.6 \ 5f^36d2 \ (^4I)^4I$
289.041	11/2	76.8 5f ³ 6d7s (⁴ I) ⁶ L	$12.9 \ 5f^{3}6d7s \ (^{2}H)^{4}K$	$4.9 \ 5f^{3}6d7s \ (^{4}I)^{4}K$
914.765	9/2	$71.3 \ 5f^36d7s \ (^4I)^6K$	$10.5 \ 5f^{3}6d7s \ (^{2}H)^{4}I$	$10.2 \ 5f^{3}6d7s \ (^{4}I)^{4}I$
1749.123	13/2	44.5 5f ³ 6d7s (⁴ I) ⁶ L	$26.1 \ 5f^36d7s \ (^4I)^4L$	$8.3 \ 5f^{3}6d7s \ (^{2}H)^{4}K$
2294.696	11/2	$48.3 \ 5f^{3}6d7s \ (^{4}I)^{6}K$	$17.6 5f^{3}6d7s (^{4}I)^{4}K$	$7.8 \ 5f^36d7s \ (^4I)^4I$
4585.434	13/2	$28.2 \ 5f^{3}6d2 \ (^{4}I)^{6}M$	$27.3 \ 5f^{3}6d7s \ (^{4}I)^{6}L$	$14.3 \; 5f^36d7s \; (^4I)^4L$
5259.653	15/2	$67.5 \ 5f^36d7s \ (^4I)^6L$	$17.8 \ 5f^36d7s \ (^4I)^4L$	$6.4 \ 5f^{3}6d7s \ (^{2}H)^{4}K$
5526.75	13/2	$71 \ 5f^36d7s \ (^4I)^6K$	$12.3 \ 5f^{3}6d7s \ (^{4}I)^{4}K$	$5.5 \ 5f^36d7s \ (^2H)^4I$
6283.431	13/2	$38.4 \ 5f^36d2 \ (^4I)^6M$	$21.6 \ 5f^3 6d7s \ (^4I)^4L$	$16.3 \ 5f^36d7s \ (^4I)^6L$
8394.362	15/2	$60.4 \ 5f^3 6d7s \ (^4I)^6K$	$14.2 \ 5f^{3}6d2 \ (^{4}I)^{6}M$	$4.8 5f^{3}6d7s (^{4}I)^{4}K$
Odd parity				
22642.478	9/2	$10.4 \ 5 f^3 7 s7 p \ (^4 I)^6 K$	$4.8 \ 5f^2 6d27s \ (^3F)^4I$	$3.9 \; 5f^2 6d27s \; (^{3}H)^4I$
23315.092	9/2	$23.7 \ 5f^37s7p \ (^4I)^6K$	$6 5 f^4 6 d (^5 I)^6 G$	$5 5 f^3 7 s^7 p (^4 I)^4 I$
24288.004	11/2	$7.9 \ 5 f^3 7 s7 p \ (^4 I)^6 K$	$5.5 \ 5 f^3 7 s 7 p \ (^4 I)^4 K$	$3.6 5 f^4 6 d (^5 I)^6 G$
25714.049	13/2	$9.1 \ 5f^36d7p \ (^4I)^6M$	$4.5 \; 5f^2 6d27s \; (^{3}H)^4 K$	$4 5f^2 6d27s (^3H)^4L$
25967.697	7/2	$19.7 \; 5f^37s7p \; (^4I)^6I$	$5.3 \ 5f^2 6d7s^2 \ (^3F)^4H$	$3.7 \ 5 f^3 7 s7 p \ (^4 I)^4 H$
26191.312	13/2	$21.7 \ 5f^36d7p \ (^4I)^6M$	$8.9 \; 5f^2 6d27s \; (^3H)^4 K$	$8.5f^{3}6d7p (^{4}I)^{4}L$
26415.115	13/2	$8.1 \ 5f^2 6d27s \ (^3H)^6H$	$7.1 \ 5f^{3}6d7p \ (^{4}I)^{6}M$	$5.5 \ 5f^2 6d27s \ (^3H)^4K$
26716.697	13/2	$7.2 \ 5f^4 6d \ (^5F)^6H$	$5.6 \ 5f^2 6d27s \ (^{3}H)^{4}K$	$5.3 \ 5f^2 6d27s \ (^1G)^4 K$
27929.924	11/2	$5.6 \; 5f^2 6d7s^2 \; (^3H)^4H$	$5.3 5 f^3 7 s7 p (^4 I)^6 K$	$4.5 \ 5f^36d7p \ (^4I)^6L$
28154.447	11/2	$7 5 f^3 6 d7 p (^4 I)^6 L$	$6.5 \ 5 f^4 7 s \ (^3 H)^4 H$	$3.5 \; 5f^47s \; (^{3}H)^{2}H$
28322.361	11/2	$8.1 \ 5f^3 6d7p \ (^4I)^6L$	$4.7 \; 5f^2 6d27s \; ({}^3F)^6H$	$3.6 \ 5f^2 6d27s \ (^1G)^4K$
28507.894	11/2	$5 5f^4 6d ({}^5G)^6I$	$4 5 f^4 7 s (^{3}H)^4 H$	$3.7 \ 5f^2 6d7s^2 \ (^3H)^4H$
28587.261	11/2	$7.3 \ 5f^36d7p \ (^4I)^6L$	$5.3 \ 5f^2 6d27s \ (^3F)^6H$	$3.6 \; 5f^47s \; (^1H)^2H$
29206.703	11/2	$6.6 \ 5f^2 6d^3 \ (^{3}H)^6 K$	$3.1 \ 5f^2 6d^3 \ (^{3}H)^4I$	$2.6 \ 5f^2 6d27s \ (^3F)^6G$
29476.743	13/2	$12.4 \ 5f^37s7p \ (^4I)^6K$	$5.1 \ 5f^2 6d27s \ (^3H)^6I$	$2.9 \ 5 f^3 7 s7 p \ (^4 I)^4 K$
29932.395	15/2	$9.7 \ 5f^2 6d7s^2 \ (^{3}H)^4I$	$5.1 \ 5f^4 6d \ (^5F)^6H$	$5 5f^36d7p (^4I)^6M$
29936.466	11/2	$11.9 \; 5f^3 6d7p \; (^4I)^6L$	$7.6 \ 5f^2 6d27s \ (^3F)^6G$	$4.7 \ 5f^2 6d27s \ (^3H)4G$
29978.143	13/2	$13.9 \ 5f^2 6d^3 \ (^3H)^6 K$	$5.1 \ 5f^2 6d27s \ (^3H)^6I$	$3.7 \ 5f^37s7p \ (^4I)^6K$
30060.727	11/2	$5 5 f^3 6 d7 p (^4 I)^6 L$	$4.4 \ 5f^2 6d27s \ (^3H)^6G$	$2.7 \ 5f^4 6d \ (^5F)^4G$
30240.416	11/2	$3 5 f^4 7 s (^3 H)^2 H$	$2.8 \ 5f^36d7p \ (^4I)^6L$	$2.2 \ 5f^2 6d7s^2 \ (^3H)^4H$
30263.978	9/2	$11.6 \; 5f^37s7p \; (^4I)^6I$	$3.4 \ 5f^2 6d^3 \ (^3H)^6I$	$3.4 \ 5f^{3}6d7p \ (^{4}I)^{6}K$
30341.673	15/2	18.4 5f ³ 6d7p (⁴ I) ⁶ M	$12.4 \ 5f^47s \ (^1K)^2K$	$5.2 \; 5f^2 6d27s \; (^3H)^2L$

a: From Meftah *et al.* [6]

3.2 Th II

Thorium (Z = 90) was discovered on the island of Lovoy in Norway by Morten Thrane Esmark who sent a sample to his father, Prof. Jens Esmark, a distinguished mineralogist, who was unable to identify it and thus transferred the sample to the Swedish chemist Jöns Jakob Berzelius for examination in 1829 [95]. After analysis, Berzelius concluded it was a new element and named it thorium, after Thor, the Scandinavian God of thunder. The radioactivity of thorium was independently discovered in 1898 by the physicist Marie Curie and the chemist Gerhard Carl Schmidt. Between 1900 and 1903, Ernest Rutherford and Frederick Soddy demonstrated that thorium decays following an exponential decay law into a series of other elements. This led to the determination of its half-life as one of the important characteristics associated with a particles and to the establishment of the radioactivity theory [96]. Each isotope of thorium is radioactive, the most stable one being 232 Th, which has a very long half-life of 14 billion years.

The first investigation of the Th II spectrum was carried out by McNally et al. [17] in 1942. They used five sets of exposures to the thorium arc in silver, burning in a Bitter electromagnet at high fields, to identify 1091 lines of singly ionized thorium in a wavelength range from 2150 to 8140 Å. This allowed the classification of 219 levels belonging to two groups of configurations between which no combinations were found, namely $6d^27s$, $6d^3$, $6d7s^2$, $6d^27p$, 6d7s7p and 5f6d7s (with $6d^27s \ {}^4F_{3/2}$ lying lowest), on the one hand, and $5f7s^2$, 5f6d7s, 5f7s7p and 5f6d7p (with $5f7s^2 {}^2F_{5/2}$ lying lowest), on the other hand. In order to link these two groups of energy levels, McNally [18] recorded the infrared spectrum of thorium in the region 8665 to 11230 Å using IR plates exposed in a Wadsworth stigmatic grating spectrograph in 1945. The separation between the ground level ${}^{2}D_{3/2}$ (from 6d7s²) and the excited level ${}^{2}F_{5/2}$ (from 5f7s²) was found to be only 4490.29 cm^{-1} . At the same period, independent experimental studies undertaken at the Zeeman laboratory of Amsterdam led to similar conclusions and the determination of additional levels [19, 20, 21]. All these published data, together with yet unpublished energy levels, were compiled by Charles [22] in a list of 2850 classified lines of Th II from 165 odd and 191 even levels.

McNally [18] pointed out that many of the strong transitions between low-lying Th II levels appear in the IR region and, although he observed some of them in the photographic infrared, the remaining lines were outside his region of observation. The majority of these lines were observed in the emission spectrum of thorium in the 1 – 2.5 μ region recorded by Steers [23]. In this study, about 60 lines were attributed to Th II transitions but no new levels could be established. However, some values of Th II levels were revised by considering interferometric measurements from the visible and ultraviolet regions. In particular, a value of 4490.26 cm⁻¹ was suggested for $57s^2 {}^2F_{5/2}$ and the interferometric measurements were used to revise other levels on this basis. A few years later, Minski [24] discovered 28 energy levels through the first extensive parametric study of the Th II configurations in three mixed groups in intermediate coupling with configuration interaction, i.e. the low even group $(6d + 7s)^3$, the high even group $5f^27s + 5f7s7p + 5f6d7p + 5f^26d$, and the six odd configurations $5f7s^2 + 5f6d7s + 5f6d^2 + 6d7s7p + 7s^27p + 6d^27p$. Brewer [97] predicted the position of the lowest terms of $5f^27p$ at $48000 \pm 2000 \text{ cm}^{-1}$, $5f7p^2$ at 54 $000 \pm 4000 \text{ cm}^{-1}$, and $5f^3$ at $55000 \pm 5000 \text{ cm}^{-1}$. The analysis of Th II was then extended with improved observations of the spectrum between 2000 and 25000 Å by Zalubas and Corliss [25]. They classified 6500 lines as transitions between 199 odd levels and 271 even levels. The emission spectrum of thorium from 2777 to 13500 Å was remeasured from a hollow cathode discharge by means of a Fourier transform spectrometer, giving rise to wave numbers accurate to about 0.002 cm^{-1} , relative intensities accurate to about 8%, and energy levels accurate to about 0.003 cm^{-1} .

Most of the Th II data obtained in the works mentioned hereabove were listed in three compilations: those of Blaise and Wyart [1], Sansonetti and Martin [26] and Redman *et al.* [27]. In the latter, the previously published thorium line lists were combined with new precise observations of a thorium-argon hollow cathode lamp emission spectrum in the region between 3500 and 11750 Å with a high-resolution Fourier transform spectrometer to refine the energy levels in Th I, Th II, and Th III. Using these refined level values, accurate Ritz wavelengths were also calculated for 19874 thorium lines between 2500 and 55000 Å while 102 new thorium energy levels, among which 9 belonging to Th II, were found. The list of Th II energy level values reported in the NIST database [28] is entirely based on the Redman *et al.* compilation [27]. It contains 517 energy levels belonging to the 6d7s², 6d²7s, 6d³, 5f²7s, 5f7s7p, 5f6d7p, 5f²6d even-, and 5f7s², 5f6d7s, 5f6d², 6d7s7p, 6d²7p, 7s²7p, 5f²7p, 5f²

Finally, it is worth mentioning that resonant two-step laser excitation of trapped Th⁺ ions led two different groups (see [98, 99]) to the measurement of 43 previously unknown levels from 7.3 to 8.3 eV ($58875 - 66940 \text{ cm}^{-1}$), and 166 previously unknown levels from 7.8 to 9.8 eV ($62907 - 79037 \text{ cm}^{-1}$), respectively. These new experimental results are not included in the current version of the NIST database.

3.2.1 HFR+CPOL Calculations

The configurations explicitly retained in our calculations were $6d7s^2$, $6d7p^2$, $6d^3$, $5f^27s$, $5f^28s$, $5f^26d$, $5f^27d$, $5f^28d$, 5f6d7p, 5f6d8p, 5f7s7p, 5f7s8p, $6d^27s$, $6d^28s$, $6d^27d$, $6d^28d$, $7s7p^2$, 5f6d7f for the even parity, and $5f6d^2$, 5f6d7s, 5f6d8s, $5f7s^2$, $5f7p^2$, $5f7d^2$, $5f8s^2$, $5f^27p$, $5f^28p$, $5f^3$, 5f6d7d, 5f6d8d, 5f7s8s, 5f7p8p, $5f^26f$, 5f7s7d, 6d7s7p, 6d7s8p, $6d^27p$, $6d^28p$, $6d^27p$, 6d7s7p, 6d7s8p, $6d^27p$, $6d^28p$, $7s^27p$, $7s^28p$, $7p^3$ for the odd parity.

As we can see, this list of configurations includes a large amount of valence correlation outside of the Rn-like Th V ionic core, consisting of 86 electrons completely filling all subshells up to 6p, i.e. $1s^22s^22p^63s^23p^63d^{10}4s^24p^64d^{10}4f^{14}5s^25p^65d^{10}6s^26p^6$. Therefore, we estimated the core-valence interactions by considering core-polarization contributions with the dipole polarizability, α_d , equal to 10.26 a_0^3 as tabulated in [94] for the Th V ion, and the cut-off radius, r_c , equal to 1.90 a_0 , which corresponds to the HFR average value $\langle r \rangle$ for the outermost core orbital (6p) of the investigated configurations. However, as already mentioned in the U II calculations (see section 3.1), with 5f electrons deeply embedded inside the closed $6s^26p^6$ subshells, the analytical core-polarization corrections to the dipole operator, as incorporated in our model [81, 82], are no longer valid for transitions involving these electrons. Instead, in order to take polarization effects into account for the 5f-nd (n = 6,7,8) transitions, the uncorrected $\langle 5f ||r||nd \rangle$ radial integrals were reduced by 20%, in a similar way to the procedure used for U II.

In order to minimize the discrepancies between calculated energy levels and available experimental values, some radial integrals were adjusted focusing only on low-lying levels located below 33000 cm⁻¹. More precisely, the average energies (E_{av}) , the Slater electrostatic integrals (F^k, G^k) , the spin-orbit parameters (ζ_{nl}) , and the effective interaction parameters (α, β) belonging to the 6d7s², 6d³, 6d²7s even-parity configurations and to the 5f7s², 5f6d², 5f6d7s, 6d7s7p odd-parity configurations were fitted using the experimental energy levels taken from the NIST compilation [28]. The Slater configuration interaction integrals (R^k) connecting 5f6d² and 5f6d7s were also adjusted with the constraint that the ratios of their values were held fixed. For higher configurations, namely 5f²7s, 5f²6d, 5f6d7p, 5f7s7p in the even parity, and 6d²7p, 7s²7p in the odd parity, only the average energies were adjusted using the lowest level experimentally known for each of these configurations. Moreover, a scaling factor of 0.75 was applied to the *ab initio* values of all the F^k , G^k and R^k integrals not fitted in the semi-empirical process to make a rough allowance for the cumulative effect of the infinity of small perturbations not explicitly included in the physical model, as recommended by Cowan [7]. At the end of the fitting procedure, the mean deviations between calculated and experimental energy levels were found to be equal to 226 and 264 cm⁻¹ for even and odd parities, respectively. Finally, let us also note that this semi-empirical adjustment enabled us to unambiguously attribute the value of the total angular momentum, i.e. J = 1/2, to the even-parity level at 23346.8901 cm⁻¹, for which a doubt between J = 1/2 and J = 3/2 still remained in the most recent databases i.e. [27, 28].

3.2.2 Results

From our computations, we identified 91 Th II transitions with log gf > -1, involving energy levels up to 33000 cm⁻¹. These lines, appearing in the visible wavelength range from 3180 and 7526 Å, are listed in Table 3.4. In this table, our oscillator strengths are compared with the older data deduced from intensity measurements from Corliss and Bosman [9], subsequently renormalized by Corliss [100] using the experimental lifetimes, with the values listed in the database of Kurucz [14], and with the more accurate experimental results published by Nilsson *et al.* [101]. As mentioned above, it was indeed well verified that our calculated gf-values given in Table 3.4 were not subject to important cancellation effects, the cancellation factor (CF), as defined in section 2.2, being greater than 0.10 for each transition with the exception of the lines at 3863.405, 4432.963, 4844.165, 5183.989, 5415.433, and 6577.656 Å, for which the CF-values were found to be equal to 0.05, 0.08, 0.06, 0.06, 0.07, and 0.04, respectively. As a reminder, according to Cowan [7], computed line strengths may be expected to show large percent errors when the CF is smaller than about 0.05.

When one looks at Table 3.4, it can be noticed that there are large disagreements between the oscillator strengths computed in the present work and the early data published by Corliss and Bosman [9], Corliss [100] and Kurucz [14], the corresponding discrepancies being reflected by the mean ratios $\langle gf_{This\ work} / gf_{CB} \rangle = 4.97 \pm 3.16$ (57 common transitions), $\langle gf_{This\ work} / gf_C \rangle = 1.70 \pm 1.05$ (35 common transitions), and $\langle gf_{This\ work} / gf_K \rangle = 4.65 \pm 3.23$ (76 common transitions, excluding the two-order discrepancy observed for the line at 7393.438 Å), where the mean deviations represent the uncertainties. However, a much better agreement was found when comparing our results with the recent (and more accurate) experimental gf-values reported by Nilsson [101]. In this case, the mean ratio $\langle gf_{This\ work} / gf_N \rangle$ was actually found to be equal to 1.25 ± 0.46 . All these comparisons are illustrated in Figure 3.5.

It is also interesting to note that our investigations highlighted the fact that, as expected, core-valence interactions have a large influence on the final oscillator strengths, the latter being indeed systematically reduced by about 25% when including core-polarization contributions in the calculations. This is shown in Figure 3.6, where the log gf-values deduced from our HFR and HFR+CPOL models are compared.



Figure 3.5: Comparison between the log gf for the strongest Th II calculated from this work with those reported by Corliss & Boltzman [9], Corliss [100], Kurucz [14] and Nilsson [101]



Figure 3.6: Comparison between the oscillator strengths obtained for the strongest Th II lines calculated in the present work without (HFR) and with (HFR+CPOL) the core-polarization effects

Finally, it is worth mentioning that the line at 4086.52 Å does not appear in Table 3.4, although it was detected in various astrophysical spectra (see e.g. [54, 59]). This is due to the fact that, for this particular line, our calculations gave a log qf-value equal to -1.42, i.e. well below the limit (log qf > -1.0) we imposed to the results listed in the table. Moreover, we must admit that little confidence could be given to our calculated value because the corresponding line strength was found to be affected by severe destructive interference effects, which are well known to erroneously make a weak transition even weaker [7]. This was confirmed by the poor agreement (about a factor of 3) that we observed when comparing our oscillator strength (qf = 0.038) with the experimental result $(qf = 0.118 \pm 0.007)$ reported by Nilsson *et al.* [101] for this transition. It was also verified that the calculated oscillator strength was extremely sensitive to the configuration interaction, small variations in the eigenvector compositions of the levels involved in the transition (in particular for the upper odd level at 24463.790 $\rm cm^{-1}$) giving rise to rather large changes of the final gf-value, as shown in Table 3.3. This can be explained by the fact that, due to strong level mixing, the final computed line strength for this transition is the result of the superposition of six main contributions, i.e. $6d^27s \rightarrow 6d^27p$, $6d^27s$ \rightarrow 5f6d7s, 6d²7s \rightarrow 6d7s7p, 6d7s² \rightarrow 6d7s7p, 6d³ \rightarrow 5f6d², and 6d³ \rightarrow 6d²7p, which are characterized by electric dipole radial matrix elements $(7s \rightarrow 7p, 6d \rightarrow 5f, and 6d \rightarrow 7p)$ of the same order of magnitude.

Table 3.3: Influence of configuration mixing on the calculated oscillator strength corresponding to the line at 4086.52 Å

	Level	$E (\mathrm{cm}^{-1})$	1^{st} (%)	2^{nd} (%)	3^{rd} (%)	4^{th} (%)	gf	$\log gf$
Calculation A^a	Lower	0.000	$62.1 \ 6d^27s$	$26.4 6 d7 s^2$	$6.9 6d^3$	$1.7 \; 5 f^2 7 s$	0.038	-1.42
	Upper	24463.790	$76.6 \ 5f6d^2$	$9.3 \; 6d^27p$	$8.7~5\mathrm{f6d7s}$	$4.2 \ 6d7s7p$		
	_							
Calculation B ^o	Lower	0.000	$59.0 \ 6d^27s$	$29.0 \mathrm{6d7s^2}$	$7.5 6d^3$	$1.7 \ 5f^27s$	0.039	-1.41
	Upper	24463.790	$76.6 \ 5f6d^2$	$9.3 \; 6d^27p$	8.7~5f6d7s	$4.2 \ 6d7s7p$		
Colorlation C ^c	Lowen	0.000	EE 7 6127a	$21 c c d7 c^2$	0 C J 3	165427-	0.040	1 40
Calculation C	Lower	0.000	55.7 00 78	51.0 007S	8.0 00 ⁻¹	1.0 01 78	0.040	-1.40
	Upper	24463.790	76.6 5f6d ²	9.3 6d²7p	8.7 5f6d7s	4.2 6d7s7p		
Calculation D^d	Lower	0.000	$62.1 6d^27s$	$26.4.6d7s^2$	$6.9.6d^{3}$	$1.7.5f^{2}7s$	0.071	-1 15
	Uppor	24463 700	$72.056d^2$	$11.2 6d^27n$	8.5.5f6d7a	6.8 6d7a7n	0.011	1.10
	Opper	24403.190	72.0 510u	11.5 0u 7p	0.0 010075	0.8 00181p		
Calculation \mathbf{E}^{e}	Lower	0.000	$62.1 \ 6d^27s$	$26.4 6 d7 s^2$	$6.9 6d^3$	$1.7 \; 5f^27s$	0.130	-0.89
	Upper	24463 790	$64.9.5 \text{f}6 \text{d}^2$	$14.1.6d^27n$	8 3 5f6d7s	11 4 6d7s7p		
	° PPOI		01.0 010a	1.1.1 04 (p	0.0 010415	iiii oaloip		
$\mathbf{Experiment}^{f}$							0.118	-0.93

^a HFR+CPOL calculation carried out in the present work and used as reference

^b HFR+CPOL calculation with modified lower level composition, upper level mixing of calculation A unchanged

 $^{\rm c}~$ HFR+CPOL calculation with modified lower level composition, upper level mixing of calculation A unchanged

 $^{\rm d}~{
m HFR+CPOL}$ calculation with modified upper level composition, lower level mixing of calculation A unchanged

^f Experimental values from Nilsson *et al.* [101]

 $^{^{\}rm e}~$ HFR+CPOL calculation with modified upper level composition, lower level mixing of calculation A unchanged

This highlights once again the difficulty to obtain reliable transition rates in lowly ionized heavy atoms, such as Th II. Exactly as for U II as discussed in section 3.1, the overlapping between the different configurations is tremendously high due to the orbitals close binding energies (of the 5f, 6d, 7s and 6p subshells). This is illustrated in Figure 3.7. Those very high mixing effects are also highlighted in Table 3.5, where the three main LS components (taken from our calculations) are given for the energy levels involved in the transitions listed in Table 3.4.



Figure 3.7: Energy levels in Th II

Table 3.4: Strongest visible spectral lines in Th II. The transitions listed are limited to those for which the log gf-values, computed in the present work, are greater than -1.0.

$\lambda_{air}{}^a$	Lower o	dd lev	rel^b	Upper e	ven le	vel^b			log	q f	
(Å)	$E ({\rm cm}^{-1})$	Р	J	$E ({\rm cm}^{-1})$	Р	J	CB^c	\mathbf{C}^d	K^e	JJ N ^f	This work ^g
3180 193	$\frac{1521896}{1521896}$	(e)	$\frac{1}{5/2}$	$\frac{2}{32957431}$	(0)	7/2	-0.71	-0.36	-0.55	0.03	0.23
3351 228	1521.896	(e)	5/2	$31353\ 127$	(0)	3/2	-0.87	-0.49	-0.73	-0.60	-0.22
3358 602	1859 938	(e)	3/2	31625 680	(0)	$\frac{1}{2}$	-1.04	-0.66	-0.89	0.00	-0.87
3389.640	1850 038	(\mathbf{c})	$\frac{3}{2}$	$31353\ 127$	(0)	$\frac{1/2}{3/2}$	-1.36	-0.00	-1.21		-0.23
3302 035	1521 806	(\mathbf{c})	5/2	30004 267	(0)	$\frac{5}{2}$	-1.50	-0.31	0.63		-0.20
3/33 008	1850.038	(\mathbf{c})	$\frac{3}{2}$	$30072 \ 164$	(0)	5/2	0.13	-0.50	-0.03	0.54	-0.50
3456 441	0.000	(e)	3/2	28022.204	(0)	5/2	-0.89	-0.43	-0.74	-0.04	-0.55
2460.020	0.000	(e)	3/2 7/9	20923.204	(0)	$\frac{3}{2}$	0.50	0.19	0.26	0.19	-0.91
3409.920	4140.077	(e)	1/2 5/2	22957.451	(0)	1/2 5/2	-0.50	-0.16	-0.50	-0.15	-0.00
34/0.0/4	4115.509	(e)	$\frac{\partial}{2}$	52690.009 99597.960	(0)	0/2 5/0					-0.82
3497.049	0.000	(e)	3/2	28087.300	(0)	$\frac{\partial}{\partial}$	0 70		0.09		-0.52
3511.562	4490.262	(0)	5/2	32959.478	(e)	3/2	-0.78		-0.63		-0.29
3539.322	4490.262	(0)	5/2	32736.189	(e)	7/2	-1.10	-0.75	-0.95	0 5 4	-0.71
3539.587	0.000	(e)	$\frac{3}{2}$	28243.813	(0)	$\frac{5}{2}$	-1.35	-0.86	-1.20	-0.54	-0.48
3559.414	4490.262	(0)	5/2	32576.749	(e)	7/2					-0.89
3609.445	4113.359	(e)	5/2	31810.550	(0)	5/2	-0.72	-0.35	-0.57		-0.33
3613.779	4146.577	(e)	7/2	31810.550	(o)	5/2	-1.56		-1.42		-0.34
3648.421	1521.896	(e)	5/2	28923.204	(o)	5/2			-1.76		-0.73
3675.567	1521.896	(e)	5/2	28720.836	(o)	3/2	-1.22	-0.75	-1.07	-0.75	-0.52
3721.825	1859.938	(e)	3/2	28720.836	(o)	3/2	-1.16	-0.69	-1.02	-0.39	-0.49
3741.183	1521.896	(e)	5/2	28243.813	(o)	5/2	-1.00	-0.50	-0.84	-0.17	-0.25
3762.881	6168.356	(o)	7/2	32736.189	(e)	7/2	-0.84		-0.69		-0.43
3785.600	6168.356	(o)	7/2	32576.749	(e)	7/2	-1.03	-0.68	-0.88		-0.49
3839.746	6700.186	(o)	9/2	32736.189	(e)	7/2	-0.59	-0.25			-0.18
3863.405	6700.186	(o)	9/2	32576.749	(e)	7/2	-0.88	-0.53	-0.73		-0.86
3900.878	7331.485	(o)	5/2	32959.478	(e)	3/2	-0.94	-0.61	-0.79		-0.16
3929.669	0.000	(e)	3/2	25440.232	(o)	5/2	-1.61	-1.03	-1.46	-0.86	-0.88
3938.780	6244.295	(e)	1/2	31625.680	(o)	1/2			-1.43		-0.79
4019.129	0.000	(e)	3'/2	24873.984	(o)	5/2	-0.80	-0.19	-0.65	-0.23	-0.21
4036.565	1859.938	(e)	3/2	26626.479	(o)	1/2	-1.82		-1.67		-0.93
4045.627	6168.356	(o)	7'/2	30879.420	(e)	7/2			-1.83		-0.93
4059.889	7001.421	(e)	3'/2	31625.680	(o)	1/2					-0.91
4069.201	6691.387	(o)	3'/2	31259.297	(e)	5/2	-0.66	-0.27	-0.52		-0.14
4094.747	0.000	(e)	3'/2	24414.643	(o)	3'/2	-1.61	-0.99	-1.46	-0.88	-0.73
4105.330	7001.421	(e)	3'/2	31353.127	(\mathbf{o})	3'/2	-1.17		-1.02		-0.76
4105.350	8605.842	(e)	5/2	32957.431	(\mathbf{o})	7/2				-0.95	-0.98
4108.420	4490.262	(0)	5/2	28823.654	(e)	5/2	-0.98	-0.51	-0.84		-0.66
4116.714	6168.356	(0)	$\frac{7}{2}$	30452.725	(e)	9/2	-0.68	-0.25	-0.52		0.09
4148.181	7828.561	(e)	1/2	31928.714	(0)	3/2	-1.16		-1.03		-0.62
4178.059	7331.485	(0)	$\frac{-}{5/2}$	31259.297	(e)	$\frac{5}{2}$	-0.80	-0.41	-0.65		-0.48
4201.846	8018.193	(e)	3/2	31810.550	(0)	$\frac{5}{2}$	-1.29	0.11	-1.14		-0.77
4208 890	6700 186	(0)	$\frac{0}{2}$	30452 725	(e)	$\frac{0}{9}/2$	-0.89	-0.47	-0.74		-0.03
4254 453	9238 020	(0)	9/2	$32736\ 189$	(e)	$\frac{0}{2}$	0.00	0.11	0.11		-0.76
4273 357	8378 859	(0)	$\frac{0}{2}$	31773 080	(e) (e)	9/2	-1.05		-0.90		-0.48
4282 041	6168 356	(0)	$\frac{7}{2}$	29515 135	(e) (e)	$\frac{0}{2}$	-0.92	-0.48	-0.78		-0.53
4283 518	9238 020	(0)	9/2	32576749	(e) (e)	$\frac{3}{2}$	-1 34	0.10	-1 21		-0.45
4381 860	6700 186	(0)	$\frac{3}{2}$	29515 135	(C) (P)	$\frac{1}{2}$	-0.64	-0.18	-0.48		-0.35
4391 111	4490 262	(0)	5/2 5/2	25010.100 27257 148	(C) (P)	$\frac{5}{2}$	-0.96	-0.45	-0.40		-0.46
4351.111	6168 356	(0)	$\frac{5}{2}$	21201.140	(\mathbf{c})	5/2	-0.30	-0.40	1.35		-0.40
4432 062	9202 265	(0)	$\frac{1}{2}$	20025.004	(c) (d)	5/2 5/2	-1.43		-1.55		_0.04
4402.300	5202.200 8460 959	(0)	1/4 2/9	31134.210	(e)	5/2	1 40		-0.91 1.95		-0.10
4440.000	0400.303 8605 849	(e)	5/2 5/9	30012.104	(0)	5/2 7/9	-1.40 1.10		-1.20		-0.09
4400.341	0000.842	(e)	0/2 0/2	30334.207 29726 190	(0)	1/2	-1.18	0 59	-1.00		-0.00
4010.020	10072.041	(0)	9/2 7/0	32730.189	(e)	1/2	-0.80	-0.32	-0.71		-0.39
4533.304	9720.298	(0)	(/2	31773.080	(e)	9/2	-1.19		-1.04		-0.79
4534.119	10572.041	(0)	9/2	32020.857	(e)	$\frac{11}{2}$	-1.47		-1.32		-0.96
4031.701	10189.007	(0)	$\frac{11}{2}$	31773.080	(e)	9/2	-1.20		-1.1U		-0.68
4040.046	10379.123	(e)	9/2	31924.600	(0)	11/2	1 80		-1.41		-0.65
4051.555	7331.485	(o)	5/2	28823.654	(e)	5/2	-1.56		-1.45		-0.73

Table 3.4: Continued

$\lambda_{air}{}^a$	Lower o	dd lev	vel^b	Upper ev	ven le	vel^b			$\log q$	lf.	
(Å)	$E ({\rm cm}^{-1})$	Р	J	$E ({\rm cm}^{-1})$	Р	J	CB^c	\mathbf{C}^d	\mathbf{K}^{e}	\mathbf{N}^{f}	This work ^{h}
4705.760	9711.962	(e)	7/2	30956.568	(o)	9/2			-1.21		-0.59
4724.772	9720.298	(o)	7/2	30879.420	(e)	7/2			-1.63		-0.73
4740.529	6168.356	(o)	7/2	27257.148	(e)	7/2	-1.59		-1.49		-0.88
4817.833	6213.490	(e)	9/2	26963.912	(o)	7/2					-0.79
4844.165	11116.585	(o)	7/2	31754.210	(e)	5/2	-1.64		-1.53		-0.94
4863.164	6213.490	(e)	9/2	26770.492	(o)	11/2		-0.95			-0.93
4863.173	6700.186	(o)	9/2	27257.148	(e)	7/2	-1.39		-1.29		-0.55
4919.816	6168.356	(o)	7/2	26488.647	(e)	5/2	-1.53		-1.43		-0.53
5017.254	7331.485	(o)	5/2	27257.148	(e)	7/2	-1.35	-0.90	-1.28		-0.56
5028.606	10572.041	(o)	9/2	30452.725	(e)	9/2	-1.26		-1.19		-0.53
5049.796	6691.387	(o)	3/2	26488.647	(e)	5/2	-1.48	-1.00	-1.40		-0.64
5183.989	12488.288	(o)	9/2	31773.080	(e)	9/2			-1.55		-0.86
5188.717	13468.968	(o)	9/2	32736.189	(e)	7/2					-0.58
5219.964	13468.968	(o)	9/2	32620.857	(e)	11/2					-0.95
5301.404	14101.799	(o)	1/2	32959.478	(e)	3/2			-1.38		-0.60
5325.144	12485.684	(o)	7/2	31259.297	(e)	5/2			-1.35		-0.78
5415.433	14275.577	(o)	9/2	32736.189	(e)	7/2	-1.14	-0.89	-1.08		-0.93
5435.892	12488.288	(o)	9/2	30879.420	(e)	7/2			-1.45		-0.65
5437.388	12570.494	(e)	7/2	30956.568	(o)	9/2			-1.76		-0.84
5449.479	14275.577	(o)	9/2	32620.857	(e)	11/2	-1.38		-1.33		-0.87
5462.613	14275.577	(o)	9/2	32576.749	(e)	7/2	-1.53		-1.45		-0.87
5539.910	9585.404	(o)	5/2	27631.225	(e)	3/2	-1.74		-1.67		-0.72
5564.201	12485.684	(o)	7/2	30452.725	(e)	9/2		-1.12	-1.39		-0.71
5568.013	13818.338	(o)	7/2	31773.080	(e)	9/2					-0.89
5707.103	6213.490	(e)	9/2	23730.654	(o)	9/2	-2.05	-1.48	-1.98		-0.93
6015.421	15305.264	(e)	9/2	31924.600	(o)	11/2			-1.41		-0.59
6021.034	14275.577	(o)	9/2	30879.420	(e)	7/2					-0.87
6087.262	15349.880	(o)	11/2	31773.080	(e)	9/2			-1.41		-0.54
6099.083	10379.123	(e)	9/2	26770.492	(o)	11/2			-2.12		-0.88
6120.556	14545.557	(o)	5/2	30879.420	(e)	7/2			-1.51		-0.75
6577.656	15349.880	(o)	11/2	30548.665	(e)	13/2			-1.66		-0.98
7191.133	10855.324	(e)	7/2	24757.507	(o)	9/2			-1.93		-0.88
7393.438	13248.709	(e)	9/2	26770.492	(o)	11/2			-2.77		-0.76
7525.508	9400.965	(e)	5/2	22685.447	(o)	7/2			-2.03		-0.87

^a Wavelengths deduced from experimental energy levels

^b Experimental energy levels from the NIST database (Kramida *et al.* 2019 [28]). The values rounded to the first three decimal places are given. (e) and (o) stand for even and odd parity, respectively.

- ^c Values from Corliss & Bozman (1962) [9]
- $^{\rm d}~$ Values from Corliss (1979) [100] - Renormalization using the experimental lifetimes
- $^{\rm e}~$ Values from Kurucz (1995) [14]
- $^{\rm f}\,$ Values from Nilsson et~al.~(2002)~[101]
- ^g HFR+CPOL calculations (see text)

Energy (cm^{-1})	J	First component (%)	Second component $(\%)$	Third component (%)
0.0	1.5	$0.3 5 f7 s7 p (^{3}F) ^{2}D$	$44.4 \ 6d^27s \ (^3F) \ ^4F$	$26.3 \ 6d7s^2 \ (^1S) \ ^2D$
1521.9	2.5	$65.4 \ 6d^27s \ (^3F) \ ^4F$	$13.8 6d^27s (^1D) ^2D$	$7.3 6 d7 s^2 (^1S)^2 D$
1859.9	1.5	$46.9 \ 6d^27s \ (^3F) \ ^4F$	$38.3 \text{ 6d7s}^2 (^1\text{S}) ^2\text{D}$	$3.9 \text{ 6d}^3 (^2\text{D})^2\text{D}$
4113.4	2.5	$39.2 6 d7 s^2 (^1S) ^2D$	$25.2 \text{ 6d}^27\text{s} ({}^3\text{F}) {}^4\text{F}$	$19.3 6d^27s (^1D)^2D$
4146.6	$\frac{0}{3.5}$	92.1 6d ² 7s (³ F) ${}^{4}F$	$2.3.5f^27s$ (³ F) ⁴ F	$2.6d^27s$ (³ F) ² F
4490.3	2.5	$86.5.5f7s^2$ (² F) ² F	$3.7.5667s(^{3}F)^{2}F$	$3.4.5 \text{f6} \text{d}^2 (^1\text{S}) ^2\text{F}$
6168.4	$\frac{2.0}{3.5}$	82.1.56d7s (³ H) ⁴ H	13.2.5f6d7s (¹ G) ² G	$2.856d^2$ (³ F) ⁴ H
6213.5	4.5	$86.1.6d^27s$ (³ F) ⁴ F	$7.5 6d^27s (^1G) ^2G$	2.5 slot(1) H $2.3 \text{ 5f}^27\text{s}(^3\text{F}) ^4\text{F}$
6244.3	0.5	$69.3 6d^27s$ (³ P) ⁴ P	$9.6.6d^27s$ (³ P) ² P	$6.7 \text{ fd}^3 (^2\text{P}) ^2\text{P}$
6691.4	1.5	$79.756d7s(^{3}F)^{4}F$	16.5f6d7s (¹ D) ² D	$0.96d7s7p(^{3}D)^{4}F$
6700.2	1.5	45.56d7s (³ H) ⁴ H	22.45f6d7s (³ H) ² H	21.5.5f6d7s (¹ C) ² C
7001 4	$\frac{4.0}{1.5}$	$43.46d^3$ (4F) 4F	$13.4 6d7s^2$ (1S) ² D	$127.6d^3$ (² P) ² P
7331.5	$25^{1.0}$	$^{45.4}$ 61 5f6d7s (³ F) 4 F	19.45667_{S} (¹ D) ² D	12.7 od (1) 1 10 5f6d7s (³ F) ² F
7828.6	0.5	$36.6.6d^3$ (² P) ² P	$35.3.6d^{2}7s$ (³ P) ² P	$17.7 6d^{2}7s$ (3P) 4P
8018.2	1.5	$85.2 6d^27_{\rm S}$ (³ P) ⁴ P	55.5 Gu 78 (1) 1 $5 5f^27_{2} (^{3}\text{P}) 4\text{P}$	$18.6d^3$ (4F) 4F
8378.0	1.0 2.5	78.4577^2 (2F) 2F	55175(1)1 655f6d7g(3F)2F	$3.35f6d7s(^{1}C)^{2}C$
8460.4	0.0 1.5	$20.4.64^{27}$ (3D) 2D	$2716d^3$ (4F) 4F	3.5 510078 (G) G $30.6 6d^3 (^2D) ^2D$
8605.8	1.0 9.5	20.4 00 78 (1) 1 $44.7 6d^27_{\odot} (^{3}\text{F}) ^{2}\text{F}$	$57.1 \text{ Gd} (\mathbf{F}) \mathbf{F}$ 15 4 6d ² 7g (3 D) 4 D	$125.6 d7 c^2 (1S) ^2D$
0000.0	⊿.J 25	$\pm \pm .1$ ou 15 (Γ) Γ 54 1 6d ² 7 (3 D) 4D	10.4 00 75 (F) F 10.9 6d ² 7c (3F) 2F	$7 6 d7 e^2 (1 \text{g}) 2 \text{D}$
0202.1	ム.J 2 m	$45.85647_{\rm g}$ (1C) 2C	15.2 ou 15(17) r 15.8 5 f 6.47 s (30) 40	0.05f6.75(3F).4F
9202.0 0228 0	IJ.IJ ⊿ ⊑	41.85647_{\circ} (1C) 2C	$30.1.5f6d7_{2}(3\mathbf{u}).4\mathbf{u}$	$3.3 510018 (\Gamma) \Gamma$ 16 0 5f6 $47_{\rm c}$ (3F) 4F
9200.0	4.J 9 K	79.9 6d ³ (4F) 4F	$10.1 6 d^2 7_{\rm c} (^3{\rm F}) ^2{\rm F}$	$10.3 510018 (^{1}\Gamma) \Gamma$ $1.3 6d7c^{2} (^{1}C) ^{2}D$
9401.0	ム.J 2 ド	12.200 (F) F 8255f6d7g (3C) 4C	$6.1.6d^{27}n^{(3E)}4C$	5.65647_{2} (1F) 2F
9585.4	2.0 2.5	$47.1 6d^27_{\rm C}$ (¹ C) ² C	$2556d^3(^2C)^2C$	$1256d^3$ (4F) 4F
9712.0	0.0 9 5	47.1 00 78 (G) G	25.5 ou (G) G	$12.5 \text{ OU} (\Gamma) \Gamma$ 7 7 5f6 d7g (1F) 2F
9720.5	5.5 5.5	$00.3 510078 (\Gamma) \Gamma$ $00.3 510078 (\Gamma) \Gamma$	11.4 510078 (G) G 11.5 5f6 47_{2} (³ U) ² U	7.7 510078 (F) F 2.2 5f6d ² (³ E) ⁴ U
10109.1	0.0 4 5	$26.4.6d^{2}7_{2}$ (1C) 2C	11.3 510078 (11) 11 $28 0.64^3 (2C) ^2C$	3.5 5001 (F) II 16 1 6 $3^{3} (4F) 4F$
10579.1	4.0	$45.567_{\rm g}$ (³ H) ² H	20.900 (G) G 10.7 5f6d7s (³ H) ⁴ H	$15.356d^2$ (¹ D) ² H
10673.1	$\frac{4.0}{2.5}$	$20.85676 (10)^{2}$	$34.3.5667_{\rm F}$ (³ F) ⁴ F	$10.156d7_{\rm g}$ (³ F) ² F
10855 3	$\frac{2.0}{3.5}$	25.0510078 (D) D $46.4.6d^3 (4F) 4F$	$28 6 d^2 7_{\rm S} ({}^{3}{\rm F}) {}^{2}{\rm F}$	$8.7 6d^3 (^{2}F) ^{2}F$
11116 6	0.0 3 5	38.1.5f6d7s (³ C) ⁴ C	$16.4.5 \text{f} 6 47 \text{s} (^{1}\text{C})^{2}\text{C}$	$0.756d7s(^{3}F)^{4}F$
11576 4	0.0 1.5	40.9.5f6d7s (³ D) ⁴ D	31.5f6d7s (¹ D) ² D	$10.756d7s(^{3}F)^{4}F$
11725 /	0.5	$57.656d7s(^{3}D)^{4}D$	$9556d^2$ (¹ D) ² P	85667s (¹ P) ² P
1220.4	1.5	$40.7 \text{ 6d}^27 \text{s} (^1\text{D})^2\text{D}$	$10.1 6d^3 (^4P) ^4P$	$0.6d7s^2$ (1S) 2D
12220.0	$1.0 \\ 2.5$	43.7 ou rs (D) D $47.6 5\text{f}647\text{s} (^{3}\text{F}) ^{2}\text{F}$	16.75f6d7s (³ D) ⁴ D	15.45667c (¹ D) ² D
12472.2	$\frac{2.0}{3.5}$	$^{41.0}$ 510015 (T) T 36.0 5f6d ² (³ F) ⁴ H	$16.156d^2 (^{3}F)^2C$	13.25667s (³ C) ⁴ C
12400.7	5.5 4 5	$45.256d7_{\rm g}$ (³ F) ⁴ F	41.6.5f6d7s (³ C) ⁴ C	$15.2 \text{ 5f6d7s} (^{3}\text{C}) ^{2}\text{C}$
12400.5 12570.5	4.0 3.5	$34.6.6d^{27}s^{(3F)}{}^{2F}$	$30.9 6d^3 (4F) 4F$	$9 6d^3 (^2C) ^2C$
12002 4	0.0 1.5	$28.756d7_{s}$ (¹ D) ² D	$21.756d7s(^{3}D) ^{4}D$	11.35667_{2} (3P) 4P
13948 7	1.5	$525.6d^3$ (4F) 4F	$32.6 6d^{2}7s$ (¹ C) ² C	$2.65f^{2}7s$ (¹ C) ² C
13240.7	2.5	$30.6 6d^27s$ (¹ D) ² D	$16.9.6d7s^2$ (¹ S) ² D	$14.7 6d^{2}7s$ (3P) 4P
13406 4	$\frac{2.0}{6.5}$	$95.456d7s(^{3}H)^{4}H$	$4.1.56d^2$ (³ F) ⁴ H	$0.3.5f^{2}7n(^{3}H)^{4}H$
13469 0	4.5	29 5f6d7s $({}^{3}C)$ ${}^{4}C$	$31.8.56d^2 ({}^{3}F) {}^{4}I$	$18.1.56d7s(^{3}F)^{4}F$
13818 3	3.5	13.9.56d7s (³ F) ² F	19.35667_{s} (³ D) ⁴ D	$18.25 \text{ f6d7s} (^{1}\text{F}) ^{2}\text{F}$
14101 8	0.5	$29.7 5 \text{f6d}^2 (^1\text{D}) ^2\text{P}$	$27.85667s(^{3}D)^{4}D$	24.56d7s (³ P) ² P
14275.6	4.5	$47.856d^2$ (³ F) ⁴ I	$15.5 5f6d7s ({}^{3}G) {}^{4}G$	$11.356d7s(^{3}F)^{4}F$
14349 4	0.5	85 6d ³ (⁴ P) ⁴ P	$5.7 5f^2$ 6d (³ P) ⁴ P	$5.3 6d^27s$ (³ P) ² P
14484 3	5.5	$55.2 5f6d7s (^{3}H) ^{2}H$	$16.5 5 \text{f6d}^2 (^1\text{D}) ^2\text{H}$	13.1 5f6d7s (³ H) ⁴ H
14545 6	2.5	$54.5 5f6d7s (^{3}D) ^{4}D$	$10.4 5f6d7s (^{1}D) ^{2}D$	8.9 5f6d7s (³ P) ⁴ P
14791 0	$\frac{2.5}{3.5}$	41.8 5f6d7s $({}^{3}G)$ ${}^{2}G$	$24.6 5 \text{f6d}^2 (^3\text{F}) ^4\text{H}$	$10.4 5f6d7s ({}^{3}F) {}^{2}F$
15144 7	1.5	$48.5 5f6d7s (^{3}P) ^{4}P$	$13.8 5f6d7s (^{3}D) ^{4}D$	$12.5 5f6d7s (^{3}P) ^{2}P$
15236.6	1.5	$64.6 6d^3 (^4P) ^4P$	$17.8 6d^27s$ (³ P) ² P	$4.3 \text{ 5f}^2 \text{6d} (^3\text{P}) ^4\text{P}$
15242.9	$\frac{1.5}{4.5}$	$67.7 5 \text{f6d}^2 (^3\text{F}) ^4\text{H}$	$16.1 5 \text{f6d}^2 (^3\text{F}) ^2\text{G}$	$4.356d^2$ (³ F) ⁴ I
15305 3	4.5	$60.6.6d^3 (^2H)^2H$	$16.2.6d^3 ({}^{4}F) {}^{4}F$	$6.8.6d^3$ (² G) ² G
15394.9	0.5	$88.7.5f6d7s(^{3}P)^{4}P$	$3.9 6d7s7n (^{3}D) ^{4}P$	1.4.5f6d7s (³ P) ² P
15340 0	5.5	88.8.56d7s (³ C) ⁴ C	$3.9.6d^27n~({^3F})~{^4C}$	3.856d7s (¹ H) ² H
15453 0	3.5	$47.5.56d7s(^{3}D)^{4}D$	$28.6.56d7s(^{3}F)^{2}F$	$3.6.5 \text{f6d}^2 (^1\text{D}) ^2\text{F}$
15710.8	1.5	$52.256d7s(^{3}D)^{2}D$	14.85667s (³ P) ⁴ P	$14.5 5f6d^2 (^{1}D) ^{2}D$
15787 0	$\frac{1.0}{2.5}$	$84.3 6d^3 (4P) 4P$	$5.7 5f^{2}6d (^{3}P) ^{4}P$	$3.9 6d^3 (^{2}D) ^{2}D$
10101.0	4.0		58	0.0 00 (D) D

Table 3.5: Main LS-coupling components of energy levels involved in the transitions in Th II listed in Table 3.4. The energies are the experimental ones from the NIST compilation [28].

Table 3.5: Continued

Energy (cm^{-1})	J	First component $(\%)$	Second component $(\%)$	Third component $(\%)$
16033.1	2.5	$30 5 \text{f}6 \text{d}7 \text{s} (^3\text{D}) ^2\text{D}$	$31.1 \ 5f6d7s \ (^{1}F) \ ^{2}F$	$8.2 \ 5f6d^2 \ (^1D) \ ^2D$
16564.6	5.5	$83.9 5f6d^2 (^3F) ^4I$	$8.8 5 \text{f6d7s} (^{3}\text{H}) ^{2}\text{H}$	$2.1 \ 5f6d^2 \ (^1G) \ ^2I$
16818.1	3.5	$51.2 \ 6d^3 \ (^2G) \ ^2G$	$25.9 \ 6d^27s \ (^1G) \ ^2G$	$5.9 \ 6d^27s \ (^3F) \ ^2F$
16906.6	3.5	$28.1 \ 5 \mathrm{f6d^2} \ (^3\mathrm{F}) \ ^2\mathrm{G}$	$18 \ 5 f 6 d^2 \ (^3 F) \ ^4 H$	$10 \ 5 f 6 d^2 \ (^3 F) \ ^2 F$
17121.6	1.5	$29.8 5 \text{f6d7s} (^{3}\text{P}) ^{2}\text{P}$	$25.7 5f6d^2 (^1D) ^2P$	9.5f6d7s (¹ D) ² D
17272.3	4.5	54.5 5f6d7s $({}^{3}G)$ ${}^{2}G$	$10.7 5 \text{f} 6 \text{d}^2$ (¹ D) ² G	$7.856d7s(^{1}H)^{2}H$
17460.6	2.5	71 5f6d7s (³ P) ⁴ P	$12.6 5 \text{f} 6 \text{d} 7 \text{s} (^1 \text{D}) ^2 \text{D}$	$4.2 5 \text{f6d7s} (^{3}\text{D}) ^{4}\text{D}$
17723.0	4.5	47 5f6d ² (${}^{3}F$) ² G	$23.2 5 \text{f6d}^2 ({}^3\text{F}) {}^4\text{H}$	$9.5 5f6d^2 ({}^{3}P)^{2}G$
17727.2	5.5	$90.3 \text{ 6d}^3 (^2\text{H}) ^2\text{H}$	$3.8 5f^{2}6d (^{1}G)^{2}H$	$2.256d7p({}^{3}G){}^{2}H$
17771.1	5.5	$73.9 5f6d^2 ({}^{3}F) {}^{4}H$	$11.6 5f6d^2 ({}^{1}G) {}^{2}I$	$7.7 5f6d^2 ({}^{3}F) {}^{2}I$
17837.8	0.5	$28.2 5 \text{f6d7s} (^{3}\text{P}) ^{2}\text{P}$	$31.2 5 \text{f6d}^2 ({}^3\text{F}) {}^4\text{D}$	14.3 5f6d ² (³ F) ² S
17983.4	2.5	$23.8 5 \text{f6d}^2 ({}^3\text{F}) {}^2\text{F}$	$15.3 5 \text{f6d}^2 ({}^3\text{F}) {}^4\text{D}$	9.8 5f6d ² (¹ D) ² F
18118.7	1.5	$39.3 \text{ 6d}^3 (^2\text{D})^2\text{D}$	$17.7 \ 6d^3 \ (^{2}D)^{2}D$	$9.5 \ 6d^27s \ (^1D) \ ^2D$
18214.4	1.5	$49.6 5f6d^{2} ({}^{3}F) {}^{4}F$	$6.6 5f6d^2 ({}^{3}F) {}^{2}D$	$6.1 \ 6d^27p^{(3F)} \ ^4F$
18568.3	0.5	$46.2 5f6d^2 ({}^{3}F) {}^{2}S$	$24.856d^2$ (³ F) ⁴ D	$15 5f6d^2 ({}^{3}F) {}^{4}P$
18816.9	6.5	$87.5 5f6d^2 ({}^{3}F) {}^{4}I$	$45f6d^2 ({}^{1}G) {}^{2}I$	$3.7.5f6d^2$ (³ F) ² I
18973.8	3.5	$39.5 5f6d7s (^{1}F) ^{2}F$	$11.2566d^2$ (³ F) ² G	$8.956d^2$ (³ F) ⁴ D
19050.8	1.5	$37.7 5 \text{f6d}^2 ({}^3\text{F}) {}^4\text{D}$	$13.4 5 \text{f6d7s} (^{3}\text{P}) ^{2}\text{P}$	$12.3566d^2$ (³ F) ⁴ F
19248.3	2.5	$31.4 5 \text{f6d}^2 (^3\text{F}) ^4\text{F}$	12.8.56d7s (³ D) ² D	$10.75f6d^2$ (³ F) ⁴ G
19594 4	0.5	$64.5 6d^27s$ (¹ S) ² S	$10.9 \text{ 6d}^3 (^2\text{P}) ^2\text{P}$	$10.5 \text{ sf}^2\text{7s}$ (1S) ² S
19880 1	4.5	51 4 6d ³ (² G) ² G	$22.8 \text{ 6d}^3 (^2\text{H}) ^2\text{H}$	$81 6d^3 (4F) 4F$
19000.1	4.0 6.5	$64.3.56d^2$ (³ F) ⁴ H	$13.1.56d^2$ (¹ C) ² I	$10.56d^2$ (³ F) ² I
20080.7	0.0 3 5	$13.856d^2$ (³ F) ² F	$15.656d^2$ (3F) 4F	$12556d^2$ (³ F) ² C
20080.7	0.0 9.5	15.8500 (P) P $41.456d^2 (^{3}P) ^{4}C$	$17.566d^2$ (³ F) ⁴ C	12.5 5f6d^2 (³ F) ⁴ F
20120.2	2.0 2.5	41.4 5000 (1) 0 58 8 6 $d^3 (2D) 2D$	$1156d^27_{\rm P}$ (1D) 2D	$77.6d^3$ (2D) 2D
20138.7	2.0 5.5	56.600 (D) D $44.156d^2 (1C) ^{2}I$	11.5 of 78 (D) D $27.0 \text{ 5fc} \text{ d}^2 \text{ (3F)} ^2\text{I}$	7.7 od (D) D $21.4 5f \text{G}^2 (3\text{E}) 4\text{H}$
20200.0	0.0 9.5	44.1 5100 (G) 1 12.1 5f6 $d7_{\rm C}$ (1E) 2E	27.9 5100 (F) I 15.0 5f6d ² (³ D) 4C	21.4 5100 (F) 11 11 0 5f6d ² (3F) 4F
20310.9	2.0 2.5	$13.1 \ 510078 (F) F$ $20.2 \ 546 \ 42 \ (3F) \ 4C$	$10.656d^2$ (3D) 4C	11.9 5100 (F) F 16 7 5f6d2 (3F) 4F
20060.1	2.0 2.5	$29.5 5100 (^{\circ}F) G$ $45.8 5f6d2 (^{3}D) 4C$	17.75642(3E) 4C	70.56642 (3D) 2C
20909.0	3.3 4 E	$45.8 5100^{-} (^{\circ}P)^{\circ}G$	$17.7 5100^{-} (^{\circ}F)^{-}G$	$(-9) 5100^{-} (-P) - G$ 12.7 5f6 d7a (3C) 2C
20969.6	4.0	$25.5 \ 5100^{-} (^{-}D)^{-}\Pi$	$21 \text{ 51007S} (-\Pi) -\Pi$ 16 1 Effed2 (3E) 2D	$13.7 510078 (^{\circ}G) = G$ $13.2 5fc d^2 (^{3}D) 4D$
21131.8	1.0	$20.1 \ 5100/s \ (^{-}P) \ ^{-}P$ 12.7 Ffc $12 \ (^{1}D) \ ^{2}P$	$10.1 \ 5100^{-} (^{\circ}F)^{-}P$ 10.0 FfG $\frac{12}{3} (^{3}E) \ 4D$	$12.3 \text{ 5fG}^{-12}(^{\circ}\text{P}) ^{\circ}\text{D}$
21297.4	2.0	13.7 $3100^{-}(^{-}D)^{-}F$	$18.9 5100^{-} (^{\circ}F) ^{\circ}D$	$13.4 510 6^{-1} $
21082.7	3.0 F F	$42.1 \text{ 5100}^{-} (^{\circ}\text{F})^{-}\text{F}$	$10.2 \text{ 510d}^{-} (^{\circ}\text{F})^{-}\text{D}$	$(.1 \text{ DIOd}^{-} (^{\circ}\text{P})^{-}\text{F})$
22014.9	5.5	$59.9 5100 / s (^{2}H) ^{2}H$	$17.5 5100^{-} (^{-}D)^{-}H$	$4 \text{ 6d}^{-7}\text{p}(^{-1}\text{G})^{-1}\text{H}$
22028.0	7.5	96.8 5fbd ² (°F) ¹	$2.7 \text{ 516d}^2 (^{+}\text{G}) ^{-2}\text{K}$	$0.4 513 (^{-1}) ^{-1}$
22106.4	2.5	$62.6 \text{ bd}^{\circ} (^{2}\text{F}) ^{2}\text{F}$	$6.9 6d^2$ (s (°F) ² F	$6.7 \text{ bd}^{\circ} (^{2}\text{D}) ^{2}\text{D}$
22139.7	4.5	$25.0 5100^2 (^{\circ}P) ^{\circ}G$	$19 5100^{2} ({}^{4}G) {}^{2}G$	18500^{2} (°F) ² G
22355.2	0.5	$40.5 5100/s (^{+}P) ^{-}P$	$13.7 \text{ 516d/s} (^{\circ}\text{P}) ^{\circ}\text{P}$	13500^{2} (°F) ² P
22513.3	2.5	$39.9516d^2 (^{3}P)^2D$	24.1 5fbd ² (${}^{\circ}F$) $=D$	8.3 5fbd ² ($^{\circ}P$) ^{4}F
22642.1	4.5	$33.1 51607s (^{+}H) ^{-}H$	11.1 5fbd ² (1 G) 2 H	10560^2 (¹ G) ² G
22685.4	3.5	$60.2 516d^2 (^{\circ}F) ^{\circ}G$	$18.3 516d^2 (^{\circ}P) ^{\circ}G$	$5.3 516d^2$ (¹ D) ² G
22834.1	3.5	$72.6 6d^{\circ} (^{2}F) ^{2}F$	$13 6d^27s (^{9}F) ^{2}F$	$3.3 \text{ 5f}^2 \text{ 6d} (^{\circ}\text{P}) ^2\text{F}$
23012.1	1.5	$20.5 516d^2$ (³ F) 4s	$15 51607s (^{1}P) ^{2}P$	7.1 $516d^2$ (°P) *D
23187.0	6.5	$31.5 \ 516d^2 \ (^1G) \ ^2I$	$28.2 516d^2 (^{\circ}F) = H$	$22.8 516d^2 ({}^{3}F) {}^{2}I$
23346.9	0.5	$34.9 6d^27s (^{3}P) ^{2}P$	$34.9 6d^3 (^2P) ^2P$	$11.6 6d^{27}s (^{1}S) ^{2}S$
23372.6	1.5	$26.4 \ 516d^2 \ (^{9}P) \ ^{4}F$	$16.2 6 d/s/p (^{\circ}D) + F$	$14 5f6d^2 (^{3}P) ^{2}D$
23518.4	3.5	14.9 5f6d ² (1 D) 2 G	$24.8 \text{ 5f6d}^2 (^1\text{G}) ^2\text{G}$	$20 5f6d^2 (^{3}P) ^{2}G$
23697.7	3.5	$18.9 516d^2 (^{3}F) ^{4}D$	$19.4 5f6d^2 (^{3}F) ^{4}F$	11.1 $5t6d^2$ (³ P) ⁴ D
23730.7	4.5	$45.2 \ 516d^2 \ (^3F) \ ^4F$	12.95664^2 (¹ G) ² H	$11.7 5f6d7s (^{1}H) ^{2}H$
24132.0	1.5	$42.85f6d^2$ (³ F) ⁴ P	$15.6 6d7s7p (^{3}D) ^{4}F$	$13.25f6d^2$ (³ F) 4s
24309.2	5.5	$275t6d^{2}$ (¹ G) ² H	$24.1 5f6d^2$ (°F) ² H	18.2 5t6d7s (¹ H) ² H
24381.8	3.5	70.8 5f ² 7s (³ H) ⁴ H	10.9 5t6d7p (°G) ⁴ H	7.6 5t6d7p (°H) ⁴ H
24414.6	1.5	20.6 6d7s7p (°D) ⁴ F	$22.25f6d^2$ (°F) ⁴ P	11.8 5f6d ² (^{9}P) ^{4}D
24463.8	2.5	$46.3 5f6d^2$ (³ F) ⁴ P	9.8 5f6d ² (°F) ² D	7.3 5f6d7s (°D) ² D
24757.5	4.5	$46.9 5f6d^2$ (³ F) ⁴ G	$38.25f6d^2$ (°P) ⁴ G	$6.2 5t6d^2$ (°F) ² H
24874.0	2.5	8 6d7s7p (³ D) ² D	$23.9 6 d7 s7 p (^{3}D) ^{4}F$	7.9 5f6d ² (³ P) ⁴ F
24982.4	3.5	$30.6 5f6d^2 ({}^{1}G) {}^{2}G$	$20.7 \ 5f6d^2 \ (^1D) \ ^2G$	$13.7 \ 5f6d^2 \ ({}^{3}F) \ {}^{2}F$
25027.0	0.5	$52.2 5f6d^2 (^{3}P) ^{4}D$	$9.4 \ 6d^27p \ (^{3}F) \ ^{4}D$	$8.6 5f6d^2$ (³ F) ⁴ D
25188.1	1.5	$11.5 5f6d^2 (^{3}P) ^{4}D$	$25.7 5f6d^2 ({}^{3}P) {}^{4}F$	$18 5f6d^2 ({}^{3}F) {}^{4}P$
25246.3	4.5	$40 \; 5f^27s (^{3}H) \; ^{4}H$	$30.7 5f^27s$ (³ H) ² H	$5.9 \; 5f^27s \; (^1G) \; ^2G$
25266.5	0.5	$56.2 \ 5f6d^2 \ (^3F) \ ^4P$	$13.5 \ 5f6d^2 \ (^3F) \ ^2S$	$11 5 \text{f6d7s} (^{1}\text{P}) ^{2}\text{P}$

Table 3.5: Continued

Energy (cm^{-1})	J	First component $(\%)$	Second component $(\%)$	Third component $(\%)$
25381.9	1.5	$39.1 \ 6d^3 \ (^2P) \ ^2P$	$28.8 \ 6d^27s \ (^{3}P) \ ^{2}P$	$10.8 \ 6d^3 \ (^2D) \ ^2D$
25414.9	5.5	$47.5 \ 5f6d^2 \ (^3F) \ ^4G$	$24.8 \ 5f6d^2 \ (^{3}P) \ ^{4}G$	$23.8 \ 5f6d^2 \ (^1G) \ ^2H$
25440.2	2.5	$1.2 \ 6d^27p \ (^1D) \ ^2D$	$32.3 \ 5f6d^2 \ (^3F) \ ^4P$	$25.5 \ 5f6d^2 \ (^{3}P) \ ^{4}F$
25594.9	0.5	$12 5 f 6 d^2 ({}^{3}F) {}^{2}P$	$23.3 \ 6d7s7p \ (^{3}D) \ ^{4}D$	$17.1 \ 5f6d7s \ (^{1}P) \ ^{2}P$
25607.1	4.5	$0.5f^{2}6f(^{1}I)^{2}G$	$16.2 5 f 6 d^2 ({}^{3}F) {}^{4}G$	$16 5 f 6 d^2 ({}^{3}P) {}^{4}G$
26424.5	2.5	$32~5f6d^2$ (³ P) ⁴ F	$19.7 5f6d^2 ({}^{3}P) {}^{2}D$	$17.9 5 \text{f6d}^2 (^{3}\text{P}) ^{4}\text{D}$
26488.6	2.5	$30.2 5 f7 s7 p ({}^{3}F) {}^{4}G$	22.7 5f7s7p $({}^{3}F)$ ${}^{4}F$	$10.1 5 f7 s7 p({}^{1}F) {}^{2}F$
26586.3	1.5	$0.9 6d^27n (^1D) ^2P$	$19.2566d^2$ (³ F) ⁴ S	$16.1 5f6d^2 ({}^{3}F) {}^{2}D$
26626.5	0.5	$27.5 6d7s7p ({}^{3}D) {}^{4}D$	$11.6 5f6d^2 ({}^{3}F) {}^{2}P$	$9.4 6d7s7p (^{3}D) ^{2}P$
26647.8	6.5	$83.3.5 \text{f6d}^2 (^1\text{G}) ^2\text{K}$	$8.856d^2$ (¹ G) ² I	$5.3.5f6d^2$ (³ F) ² I
26762.3	1.5	$35.6.5f^27s$ (³ F) ⁴ F	$22.85f7s7n(^{3}F)^{4}F$	$21.3.56d7p ({}^{3}F) {}^{4}F$
26770.5	5.5	50.0 of 73 (1) f	$^{22.0}$ 516 2 (³ F) ⁴ G	$10.4566d^2$ (³ F) ² H
26063.0	0.0 3 5	$53.256d^2$ (³ P) ⁴ D	$21.5f6d^2$ (³ F) ⁴ D	10.4 5100 (1) 11 11 1 6d ² 7p (³ F) ⁴ D
20905.9	0.0 1.5	$33.256d^2$ (3P) 2D	213100 (T) D 20.3 5f6d ² (1D) ² D	11.1 ou (p(T)) D 18 5 5f6d ² (³ D) ⁴ E
20905.2	1.0 2.5	52.5500 (1) D 70.05f6d ² (³ D) 4E	20.3 5100 (D) D $9.8 5f6d^2 (^{3}F) 4F$	$5 1 5f6 d^2 (^{3}E) ^{2}E$
27249.0	ວ.ວ ຈະ	10.95100 (F) F 10.0557a7a (3E) 2E	3.85100 (F) F 36.95777 (3E) 4C	5.1500 (F) F 10.1 $57_{2}7_{2} (1E) 2E$
27207.1	3.3 4 F	$10.9 \ 51787p(^{-}r)$	$20.2 \text{ 51/8/p} (^{-}\text{F}) \text{ G}$	19.1 D1/S/P(F) F 11.2 Ffc 2 (1D) 2
27307.4	4.0	$19.0 \ 0100^{-} (^{-}G)^{-}H$ 1C 7 FfC 12 (3E) 2D	$17.0 \ 5100^{-} (^{\circ}P)^{-}F$ 10 $F \ F(c)^{2} (3D)^{2}D$	11.3 $\partial IOG^{-}(^{-}D)^{-}G$
27403.2	1.5	$10.7 5100^{2} (^{\circ}F)^{2}P$	$18.5 5100^{2} (^{\circ}P) ^{2}D$	$11.8 5100^{-} (^{\circ}P) ^{-}D$
27527.0	4.5	$35 5f^2/s (^{3}H) ^{2}H$	$39.6 \text{ 5f}^27\text{ s} (^{\circ}\text{H}) ^{\circ}\text{H}$	$7.4 \text{ 5fbd7p} (^{3}\text{H}) ^{2}\text{H}$
27594.0	2.5	$33.9 \text{ 5f}^2 7\text{s} (^3\text{F}) ^4\text{F}$	$19.8 \text{ 5f}^2 \text{ 7s} (^3\text{F}) ^2\text{F}$	9.3 5f/s/p (${}^{3}F$) ${}^{4}G$
27631.2	1.5	38.3 5f7s7p (°F) ⁴ F	$21.6 5f^27s (^{3}F) ^{4}F$	$9.6 6d^3 (^2D) ^2D$
27787.8	4.5	$34.9 5f6d^2 ({}^{1}G) {}^{2}G$	$25.7 5f6d^2$ (¹ G) ² H	$13.2 5f6d^2$ (¹ D) ² G
27937.1	5.5	$69.8 \ 5f^27s \ (^{3}H) \ ^{4}H$	$13.6 5f^27s (^{3}H)^{2}H$	$6.8 5f6d7p ({}^{3}G) {}^{4}H$
28011.2	1.5	$35.8 \text{ 6d}^3 (^2\text{D}) ^2\text{D}$	$25 \ 6d^3 (^2D) \ ^2D$	$12.7 5 f7 s7 p (^{3}F) ^{4}F$
28026.3	2.5	$55.6 \text{ 6d}^3 (^2\text{D}) \ ^2\text{D}$	$12.1 \text{ 6d}^3 (^2\text{F}) ^2\text{F}$	$5.1 \ 5f^2 6d \ (^1S) \ ^2D$
28243.8	2.5	24.8 6d7s7p (³ D) ${}^{4}\text{F}$	$15.6 \ 6d^27p \ (^{3}F) \ ^{4}G$	$11.4 \ 6d^27p \ (^{3}F) \ ^{2}F$
28587.4	2.5	$24.8 \ 5f6d^2 \ (^3F) \ ^2D$	$22.3 \ 5f6d^2 \ (^1G) \ ^2D$	$8 \ 6d^27p \ (^3F) \ ^4G$
28720.8	1.5	44.6 6d7s7p (^{3}D) ^{4}D	$8.4 \ 5f6d^2 \ (^{3}P) \ ^{4}D$	$8.1 \ 6d^27p \ (^{3}F) \ ^{2}D$
28823.7	2.5	24.9 5f7s7p (³ F) ${}^{4}\text{F}$	$28.4 \ 5 \text{f7s7p} \ (^3\text{F}) \ ^4\text{G}$	$10~5 f7 s7 p~(^{3}F) ~^{4}D$
28923.2	2.5	$1.9 \ 6d^27p \ (^1D) \ ^2F$	$17 \ 5f6d^2 \ (^1D) \ ^2F$	13.9 6d7s7p (³ D) ${}^{4}\text{F}$
29095.5	2.5	$44.4 \ 5f6d^2 \ (^1G) \ ^2F$	$17.4 \ 5 \text{f} 6 \text{d}^2 \ (^3 \text{F}) \ ^2 \text{F}$	$7.5 5 \text{f}6 \text{d}^2 (^3\text{F}) ^2\text{D}$
29345.9	2.5	$30.7 \ 5f^27s \ (^3F) \ ^2F$	$26.3 \ 5f^27s \ (^3F) \ ^4F$	13.3 5f6d7p (³ F) 2 F
29431.8	3.5	$30.7 \ 5f^27s \ (^3F) \ ^4F$	$21.1 \ 5f^27s \ (^1G) \ ^2G$	$12.7 5f6d7p (^{1}G) ^{2}G$
29515.1	4.5	$16.4 \; 5f^27s \; (^1G) \; ^2G$	$18.7 \ 5f^27s \ (^3F) \ ^4F$	$15.7 5f6d7p (^{1}G) ^{2}G$
29720.3	1.5	$15.5 \; 5f6d^2 \; (^1D) \; ^2D$	$10.4 \ 6d^27p \ (^1D) \ ^2D$	$10.3 5f6d^2 ({}^{3}F) {}^{2}D$
29788.5	4.5	$59.3 5f6d^2$ (³ P) ⁴ F	$15.1 \ 5 \text{f6d}^2$ (¹ D) ² G	$95f6d^2$ (³ P) ² G
29874.0	3.5	$27.3 \ 5f^27s \ (^3F) \ ^2F$	$28.5 \ 5f^27s$ (³ F) ⁴ F	$9 \; 5f^27s$ (¹ G) ² G
30101.4	3.5	$57.6 5 \text{f} 6 \text{d}^2 (^1\text{G}) ^2\text{F}$	$7.7 \ 6d7s7p \ (^{3}D) \ ^{4}F$	$6.7 \ 5f6d^2 \ (^3F) \ ^2F$
30223.1	7.5	$96~5f6d^2~(^1G)^2K$	$2.7 5 \text{f} 6 \text{d}^2$ (³ F) ⁴ I	$0.5 5 f3 (^{2}K)^{2}K$
30310.2	5.5	$20.9 5 \text{f}6\text{d}^2$ (¹ D) ² H	$38.3 5f6d^2$ (¹ G) ² H	$10.5 5f6d7s (^{3}H) ^{2}H$
30452.7	4.5	$41.2 5f6d7p (^{3}H) ^{4}I$	$13.3 5f6d7p (^{3}H) ^{2}H$	$11.7 \; 5f^27s \; ({}^3F) \; {}^4F$
30484.7	5.5	$63.9 \; 5f^27s \; (^{3}H) \; ^{2}H$	$13.1 \ 5 f^2 7 s \ (^3 H)^{4} H$	$7.3 5f6d7p (^{3}H) ^{2}H$
30548.7	6.5	$83.4 \; 5f^27s (^{3}H) \; ^{4}H$	$7.4 5f6d7p ({}^{3}G) {}^{4}H$	$5.456d7p(^{3}H)^{4}H$
30564.6	0.5	$5 \ 6d^27p \ (^{1}D)^{2}P$	$28.6 \ 5f6d^2 \ (^1D) \ ^2P$	$23.5 5f6d^2 ({}^3F) {}^2P$
30879.4	3.5	56.1 5f7s7p (${}^{3}F$) ${}^{4}F$	$13.3 5 f7 s7 p({}^{3}F) {}^{4}D$	$7 5 f7 s7 p (^{1}F)^{2}G$
30956.6	4.5	$48.456d^{2}$ (^{3}F) ^{2}H	$265f6d^{2}(1D)^{2}H$	$5.9 \ 6d^27p^{(1)}$ (1G) ² H
30972.2	2.5	$17.1 \text{ 6d7s7p} (^{1}\text{D}) ^{2}\text{D}$	$19.6 6 d7 s7 p (^{3}D) ^{4}F$	$13.7 \ 6d^27p^{(3F)} \ ^4G$
30994.3	3.5	$58.1 6 d7 s7 p (^{3}D) ^{4}F$	$5.4 \ 6d^27p^{(3}F)^{2}F$	$5.2 \ 6d^27p^{(3}F)^{4}G$
31259.3	2.5	$36.6 5f6d7p ({}^{3}F) {}^{4}G$	$12 \; 5f^{2}6d \; ({}^{3}F) \; {}^{4}G$	$11.8 5f6d7p(^{1}D)^{2}F$
31353.1	1.5	$17.8 \ 6d^27p \ (^{3}F)^{-2}D$	$16.2 6 d7 s7 p (^{3}D) ^{4}F$	$10.2 \ 6d^27p^{(3}F)^{4}F$
31625.7	0.5	$16.9 \ 7 \mathrm{s}^2 7 \mathrm{p} (^1 \mathrm{S})^{-2} \mathrm{P}$	$25.9 6 d7 s7 p (^{3}D) ^{4}D$	$11.3 \ 6d^27p^{(1S)}^{2}P$
31754.2	2.5	$37.1 5 f7 s7 p (^{1}F) ^{2}F$	$18.2 5 f7 s7 p ({}^{3}F) {}^{4}F$	$16.6 5 f7 s7 p(^{1}F)^{2}D$
31773.1	4.5	$39.9 5 f7 s7 p ({}^{3}F) {}^{4}F$	33.2 5 f7 s7 p (³ F) ⁴ G	$7.6 5 f7 s7 p ({}^{3}F) {}^{2}G$
31800.2	3.5	$32.2 5 \text{f6d}^2$ (¹ D) ² F	$14.4 5 \text{f6d}^{2} ({}^{3}\text{F}) {}^{2}\text{F}$	$8.2 5 \text{f6d}^2$ (¹ G) ² F
31810.6	2.5	$63.9 6 d7 s7 p (^{3}D) ^{4}D$	11.5 6d7s7p (³ D) ⁴ P	$5.2 \text{ 6d7s7p} (^{3}\text{D}) ^{2}\text{D}$
31924.6	5.5^{-1}	$21.9 5 \text{f6d}^2 (^3\text{F})^2\text{H}$	$23.1 5 \text{f6d}^2 ({}^3\text{F}) {}^2\text{I}$	$21.5 5 \text{f6d}^2$ (¹ D) ² H
31928.7	1.5	$23.9 5 \text{f} 6 \text{d}^2 ({}^3\text{F}) {}^2\text{D}$	$13.5 6 d7 s7 p (^{1}D) ^{2}D$	$8.5 \text{ 6d}^27 \text{p} ({}^3\text{F}) {}^2\text{D}$
325767	3.5	$26.2 5 f7 s7 p (^{1}F) ^{2}F$	$18.3 5 \text{f7s7p} (^{3}\text{F}) ^{4}\text{G}$	$9.95f7s7p(^{3}F)^{4}D$
32620.9	5.5	$69.1 \text{ 5f}^2 \text{6d} (^3\text{H}) ^4\text{K}$	$13.2 \text{ 5f}^2 \text{6d} (^1\text{G}) ^2\text{I}$	$11.2 5f^{2}6d (^{3}H) ^{2}I$
32736.2	3.5	$39.3 5 f7 s7 p ({}^{3}F) {}^{4}C$	$19.256d7n (^{3}H) ^{4}H$	$6.6.56d7n (^{3}H) ^{2}G$
32850 1	2.5	$25.5\text{ff}6\text{d}^2$ (¹ D) ² D	$9.9.566d^2$ (³ P) ² D	$8.3.5 \text{f6d}^2 (^3\text{F}) ^2\text{F}$
32957 4	$\frac{2.5}{3.5}$	$60.1 6d^27n ({}^{3}F) {}^{4}C$	$a_09.6.6d7s7n(^{3}D)^{4}F$	$5.956d^2$ (¹ D) ² F
32051.4	1.5	33.4.5f6d7n (³ F) ² D	$60^{0.0}_{-10.3} \frac{516}{516} \frac{51}{516} \frac{(10)}{20} \frac{2}{20}$	$10.5 \text{ f7s7n} (^{3}\text{F}) ^{4}\text{F}$
04000.0	1.0	our for the the	TO DO DOUTP (D) I	TO OTIBIL (T.) T

3.3 Summary

As shown in the two previous subsections, we performed extensive HFR+CPOL calculations in singly ionized uranium and thorium and have obtained very conclusive results. Indeed, in the case of U II, 38 intense spectral lines with potential astrophysical interest were identified and designated among tenth of thousands. Among those 38 transitions, there are 8 experimental comparison points and our results reproduce well this data which reinforces the predictive character of our calculations. Unfortunately, the only spectral line identified so far (to our knowledge) in astrophysical spectra is by far the most intense one in our calculations.

For Th II, 91 intense spectral lines with astrophysical interest were identified and designated among thousands (12 experimental comparison points very well reproduced). Therefore, this work provided many intense lines of Th II that will hopefully be observable in astrophysical spectra.

These two calculations also allowed us to push the methods of atomic calculations to their limits by treating lowly ionized super-heavy elements where the configuration interaction plays a very crucial role and where consequently, the mixing effects are tremendously important.

Those results have been published respectively in Gamrath *et al.* [102, 103] in 2018 and 2020.

Chapter 4

Radiative Parameter Computations in Moderately Charged Trans-Iron Ions for the Study of Hot White Dwarfs Spectra

This section is related to the study of white dwarfs spectra. Indeed, as we mentioned in chapter 1, in collaboration with the Karl Ebenard Universität of Tübingen in Germany, an extensive study of the spectra of peculiar white dwarf has been undertaken. Those white dwarfs have the particularity of containing significantly more heavy elements than expected. In order to identify those trans-iron elements, reliable atomic data is mandatory. That is why, during this thesis, we performed atomic calculations in several heavy ions, namely copper, indium, caesium and silver. We considered the third to sixth ionization states and those were chosen because of the very high temperature of the considered white dwarfs.

All those calculations have been performed using the HFR+CPOL method described in section 2.2. The calculations of each ions mentioned here above are described in details in the section in the section especially dedicated to each one of them (respectively 4.1 for the copper ions, 4.2 for the indium ions, 4.3 for the caesium ions and 4.4 for the silver ions). Exactly as we did in the previous chapter, in order to take polarization effects more realistically into account, the radial integrals were scaled down by a factor 0.80 for all the ions considered in this chapter.

4.1 Cu IV - VII

The atomic number of copper is 29. Its name comes from old English *copor* (related to the Dutch word *koper* and the German word *Kupfer*), based on the late Latin word *cuprum* that comes from the Latin word *cyprium aes*: the Cyprus metal (so called because Cyprus was the first main source of copper). The atomic structure of copper is rather similar to silver and gold, because they all have an s orbital occupied by a single electron with completely filled p and d subshells, in their fundamental configurations which allows the formation of metallic bonds. The three metals of this copper group are increasingly noble and rare, from semi-noble copper to truly noble gold, their nobility being explained by their small atomic radius and their compact atomic stacking, their higher ionization potential because of the filled d subshells, their relatively high melting point and their low reactivity or relative chemical inertia [104]. Pure copper is one of the only colored metals with gold and caesium.

4.1.1 Models Used

The main source of atomic data related to the Cu IV-VII spectra is the paper published by Sugar & Musgrove [29] in which the available experimental energy levels of the copper atom, in all stages of ionization, have been compiled with ionization energies, either experimental or theoretical, experimental Landé g-factors, and leading components of calculated eigenvectors. This compilation is still being used as the standard reference database for the copper ions of interest at the National Institute of Standards and Technology [28].

More precisely, for Cu IV, experimental values are reported for 187 levels of the $3d^8$, $3d^74s$, $3d^75s$, $3d^74d$, and $3d^64s^2$ even-parity configurations and 110 levels of the $3d^74p$ odd-parity configuration. In the case of Cu V, many $3d^7 - 3d^64p$ and $3d^64s - 3d^64p$ lines were identified by Van Kleef *et al.* [30], allowing them to classify all the levels of the $3d^7$ configuration, as well as 53 of the 63 levels of $3d^64s$ and 175 of the 180 levels of $3d^64p$. The Cu VI experimental spectrum is taken from Raassen and Van Kleef [31], who used new exposures of a sliding spark discharge to analyze the $3d^6 - 3d^54p$ and $3d^54s - 3d^54p$ transition arrays. This analysis led to the identification of all levels in the $3d^6$ configuration, except the highest ${}^{1}S_0$, as well as 208 of the 214 levels in $3d^54p$ and 13 of the 74 levels in $3d^54s$. Finally, the analysis of the Cu VII spectrum by Van Het Hof *et al.* [105] appeared too late to be included in the compilation of Sugar and Musgrove [29] . They determined all 37 levels of the $3d^5$ ground configuration and 129 of the 180 possible levels of the $3d^44p$ configuration.

The method adopted in our work to model the atomic structures and compute the radiative parameters in the Cu IV-VII ions was the HFR + CPOL (see section 2.2). For Cu IV, configuration interaction was considered among the configurations $3d^8$, $3d^74s$, $3d^75s$, $3d^74d$, $3d^75d$, $3d^64s^2$, $3d^64p^2$, $3d^64d^2$, $3d^64s5s$, and $3d^64s4d$ for the even parity, and $3d^74p$, $3d^75p$, $3d^74f$, $3d^75f$, $3d^64s4p$, $3d^64s5p$, $3d^64s4f$, and $3d^64p4d$ for the odd parity. The core-polarization parameters were the dipole polarizability of a Cu VI ionic core, as reported by Fraga *et al.* [94], i.e., $\alpha_d = 0.67$ a.u., and the cut-off radius, $r_c = 0.80$ a.u, corresponding to the HFR mean value of the outermost core orbital (3d) radius (<3d||r||3d>). Using the experimental energy levels compiled at NIST [28], some radial integrals (average energy, Slater Integrals¹, spin-orbit, and effective interaction parameters) of $3d^8$, $3d^74s$, $3d^75s$, $3d^74d$, $3d^64s^2$, and $3d^74p$ configurations were optimized by a well-established least-squares fitting procedure in which the mean deviations² were found to be equal to 206 cm⁻¹ for the even parity and 183 cm⁻¹ for the odd parity.

It is worth noting that, when performing the fit, we found that the experimental energy level at 306941.8 cm⁻¹ was incorrectly classified as J = 1 in the NIST tables, while according to our calculations, this level should be designated as J = 2. The energy levels we obtained and their good agreement with the experimental ones are to be found in Tables A1 and A2 for the even and the odd parity respectively. Those (long) tables are in appendix in order not to alter the readability of this thesis. As one can see in those tables, the experimental levels are very well reproduced by our calculations. We also give the main LS components of those levels according to our computations.

For Cu V, the configurations included in the HFR model were $3d^7$, $3d^64s$, $3d^65s$, $3d^64d$, $3d^54s^2$, $3d^54p^2$, $3d^54d^2$, and $3d^54s4d$ for the even parity, and $3d^64p$, $3d^65p$, $3d^64f$, $3d^54s4p$, $3d^54s5p$, and $3d^54s4f$ for the odd parity. In this ion the semi-empirical process was carried out to optimize the radial integrals corresponding to $3d^7$, $3d^64s$, and $3d^64p$ configurations using the experimental levels reported in the NIST database [28]. The mean deviations between calculated and experimental energy levels were 325 cm^{-1} and 259 cm^{-1} for even and odd parities, respectively. Core-polarization effects were estimated

 $^{^{1}}$ See eq. 2.31.

²The mean deviation is defined as the mean value of $|E_{exp} - E_{HFR}|$ for all the fitted energy levels.

using a dipole polarizability and a cut-off radius corresponding to a Cu VII ionic core, i.e., $\alpha_d = 0.47$ a.u. [94], and $r_c = 0.75$ a.u. (<3d||r||3d>). The comparison between the calculated energy levels and the experimental ones is shown in Tables A4 and A5 (given in appendix) for the even and odd parity respectively.

In the case of Cu VI, the configuration interaction was considered among the following configurations: 3d⁶, 3d⁵4s, 3d⁵5s, 3d⁵4d, 3d⁵5d, 3d⁴4s², 3d⁴4p², 3d⁴4d², 3d⁴4s4d, 3d⁴4s5d (even parity) and $3d^54p$, $3d^55p$, $3d^54f$, $3d^44s4p$, $3d^44s5p$, $3d^44s4f$ (odd parity). The corepolarization parameters were those corresponding to a Cu VIII ionic core, i.e., $\alpha_d = 0.40$ a.u. ([94]), and $r_c = 0.72$ a.u. (<3d||r||3d>). The radial parameters of the 3d⁶, 3d⁵4s, and $3d^{5}4p$ configurations were optimized in order to minimize the differences between the computed Hamiltonian eigenvalues and the experimental energy levels listed at NIST [28], giving rise to average deviations of 442 $\rm cm^{-1}$ (even parity) and 429 $\rm cm^{-1}$ (odd parity). The results that we obtained for those energy levels are displayed as a comparison between the calculated energy levels and the experimental ones in Tables A7 and A8 (in appendix) for respectively the even and odd parity. Finally, for Cu VII, ten even- and eight oddparity configurations were included in the HFR model in order to compute the radiative parameters, i.e., $3d^5$, $3d^44s$, $3d^45s$, $3d^44d$, $3d^45d$, $3d^34s^2$, $3d^34p^2$, $3d^34d^2$, $3d^34s5s$, $3d^34s4d$, and $3d^44p$, $3d^45p$, $3d^44f$, $3d^45f$, $3d^34s4p$, $3d^34s5p$, $3d^34s4f$, and $3d^34p4d$, respectively. An ionic core of the type Cu IX was considered to estimate the core-polarization effects with the parameters $\alpha_d = 0.34$ a.u. [94] and $r_c = 0.70$ a.u. The semi-empirical fitting procedure was carried out to adjust the radial parameters in $3d^5$ and $3d^44p$ with the experimental energy levels taken from [105], leading to average energy deviations of 78 cm⁻¹ and 365 $\rm cm^{-1}$ for even and odd parities, respectively. The comparison between the calculated energy levels and the experimental ones in Cu VII is to be found in Tables A10 and A11 (in the appendixes) for the even and odd parity, respectively.

4.1.2 Atomic Radial Parameters

The radial parameters adopted in our calculations are given in Tables 4.1, 4.2, 4.3, 4.4 for Cu IV, V, V, VII ions, respectively. As can be seen in those tables, some parameters had to be fixed (F) or linked together by their ratio (R) due to the fact that not all possible levels were experimentally known for some configurations. The fitted parameters are the mean energy, the spin-orbit and the Slater Integrals as defined in eq. 2.31.

Configuration	Parameter	HFR	Fitted	Ratio
Even Parity	1 01 01100001		110004	100010
$3d^8$	E_{av}	17190	16729	
	$F^{2}(3d, 3d)$	112092	98330	0.877
	$F^{4}(3d, 3d)$	69989	60209	0.860
	α	0	91	
	β	0	-237	
	ζ_{3d}	903	910	1.007
$3d^{7}4s$	E_{av}	147324	152124	
	$F^{2}(3d, 3d)$	118491	103197	0.871
	$F^{4}(3d, 3d)$	74277	65197	0.878
	α	0	99	
	β	0	-350	
	ζ_{3d}	978	979	1.001
	$G^2(3d,4s)$	12035	10802	0.898
$3d^75s$	E_{av}	325664	330393	
	$F^{2}(3d, 3d)$	119486	102897	0.861
	$F^{4}(3d, 3d)$	74953	65472	0.874
	α	0	100	
	eta	0	-350	
	ζ_{3d}	986	Fixed	
	$G^2(3d,4s)$	2897	2608	
$3d^{7}4d$	E_{av}	312783	320069	
	$F^{2}(3d, 3d)$	119438	103540	0.867
	$F^{4}(3d, 3d)$	74922	64201	0.857
	α	0	73	
	β	0	361	
	ζ_{3d}	985	1021	1.037
	ζ_{4d}	68	Fixed	
	$F^{2}(3d,4d)$	13224	12461	0.942
	$F^{4}(3d, 4d)$	5529	5503	0.995
	$G^{0}(3d, 4d)$	5169	3754	0.726^{R}
	$G^{2}(3d,4d)$	5040	3660	0.726^{R}
- 16 - 9	$G^{4}(3d,4d)$	3651	2651	0.726^{-n}
$3d^{0}4s^{2}$	E_{av}	334825	345297	
	$F^{2}(3d, 3d)$	124695	112225	0.900
	F ⁴ (3d,3d)	78447	70603	0.900
	α		Fixed	
	β		Fixed	
	ζ_{3d}	1056	Fixed	
Odd Parity	T	010001	004970	
3d'4p	E_{av}	218001	224378	0.974
	$F^{-}(30,30)$	74510	103882	0.874
	г -(за,за)	(4519	04989	0.872
	α		101 919	
		000	-919 1002	1.096
	ζ_{3d}	900	1200	1.020
	(54p) $F^2(3d/4n)$	1100 93861	1000 22870	1.100
	$C^1(3d 4n)$	8/25	22019 7305	0.939
	$G^{3}(3d.4n)$	7571	7132	0.942
		1 1011	1104	0.014

Table 4.1: Final radial parameters (in cm^{-1}) adopted in our HFR+CPOL calculations in Cu IV

R: Fixed ratio.

Even Parity: 187 levels (mean deviation: 206 cm^{-1}) Odd Parity: 110 levels (mean deviation: 183 cm^{-1}) 65

Configuration	Parameter	HFR	Fitted	Ratio
Even parity				
$3d^7$	E_{av}	30899	30322	
	$F^{2}(3d, 3d)$	119816	105551	0.881
	$F^{4}(3d, 3d)$	75176	65503	0.871
	α	0	109	
	β	0	-587	
	ζ_{3d}	989	1002	1.013
$3d^{6}4s$	E_{av}	234957	237924	
	$F^{2}(3d, 3d)$	125814	110315	0.877
	$F^{4}(3d, 3d)$	79209	67072	0.847
	α	0	117	
	β	0	-154	
	ζ_{3d}	1066	1154	1.082
	$G^2(3d,4s)$	12797	11794	0.922
Odd parity				
$3d^{6}4p$	E_{av}	316597	319750	
	$F^{2}(3d, 3d)$	126094	109170	0.866
	$F^{4}(3d, 3d)$	79402	66055	0.832
	α	0	114	
	β	0	213	
	ζ_{3d}	1069	1180	1.104
	ζ_{4p}	1596	1816	1.137
	$F^{2}(3d,4p)$	28011	26960	0.962
	$G^{1}(3d,4p)$	9612	9190	0.956
	$G^{3}(3d,4p)$	8916	7838	0.879

Table 4.2: Final radial parameters (in cm^{-1}) adopted in our HFR + CPOL calculations in Cu V

Even Parity: 72 levels (mean deviation: 325 cm^{-1}) Odd Parity: 175 levels (mean deviation: 259 cm^{-1})
Configuration	Parameter	HFR	Fitted	Ratio
Even Parity				
$3d^6$	E_{av}	47058	46817	
	$F^{2}(3d, 3d)$	127114	112843	0.888
	$F^{4}(3d, 3d)$	80096	69557	0.868
	α	0	103	
	β	0	-264	
	ζ_{3d}	1080	1142	1.057
$3d^{5}4s$	E_{av}	332771	334360	
	$F^{2}(3d, 3d)$	132805	116707	0.879
	$F^{4}(3d, 3d)$	83932	74133	0.883
	α	0	100	
	β	0	-250	
	ζ_{3d}	1161	Fixed	
	$G^{2}(3d,4s)$	13493	12647	0.937
Odd Parity				
$3d^54p$	E_{av}	424263	425870	
	$F^{2}(3d, 3d)$	133032	116189	0.873
	$F^{4}(3d, 3d)$	84088	72010	0.856
	α	0	127	
	β	0	-286	
	ζ_{3d}	1163	1247	1.073
	ζ_{4p}	2028	2320	1.144
	$F^{2}(3d,4p)$	31832	30768	0.967
	$G^{1}(3d,4p)$	10697	10190	0.953
	$G^{3}(3d,4p)$	10151	9203	0.907

Table 4.3: Final radial parameters (in cm^{-1}) adopted in our HFR+CPOL calculations in Cu VI

 $\begin{array}{c} F: \ Fixed \ Parameter. \\ \hline \\ Odd \ Parity: \ 208 \ levels \ (mean \ deviation: \ 429 \ cm^{-1}) \\ \hline \end{array}$

Configuration	Parameter	HFR	Fitted	Ratio
Even Parity				
$3d^5$	E_{av}	78756	78522	
	$F^{2}(3d, 3d)$	134086	119456	0.891
	$F^{4}(3d, 3d)$	84807	74397	0.877
	α	0	118	
	β	0	-512	
	ζ_{3d}	1176	1202	1.022
Odd Parity				
$3d^44p$	E_{av}	553653	554223	
	$F^{2}(3d, 3d)$	139722	123787	0.886
	$F^{4}(3d, 3d)$	88617	78219	0.883
	α	0	123	
	β	0	-380	
	ζ_{3d}	1263	1121	0.888
	ζ_{4p}	2481	2647	1.067
	$F^{2}(3d,4p)$	35417	34983	0.988
	$G^{1}(3d,4p)$	11725	11199	0.955
	$G^{3}(3d,4p)$	11316	11458	1.013

Table 4.4: Final radial parameters (in cm⁻¹) adopted in our HFR+CPOL calculations in Cu VII

Even Parity: 37 levels (mean deviation: 78 cm^{-1}) Odd Parity: 129 levels (mean deviation: 375 cm^{-1})

4.1.3 Radiative Transition Rates

The radiative transition rates obtained in the present work are listed in Tables A3, A6, A9 and A12 for the Cu IV, V, VI and VII spectral lines, respectively. It should be noted that, for Cu IV,V and VII, we are, to our knowledge, the first ones to provide data on transition probabilities and oscillator strengths. We initially the transitions for which log gf was \geq -6, which consisted in thousands of E1 transitions, and we sent them to the astrophysicists at the University of Tübingen. In this work, we decided to restrict ourselves and impose the condition log $gf \geq$ -1, corresponding to the most intense and reliable transitions (CF > 0.05).

In the case of the Cu IV, imposing the criterion $\log gf \ge -6$ gives rise to 8725 transitions. With the more restrictive criterion $\log gf \ge -1$, we obtain 1024 intense transitions. Some of these transitions have been measured and reported in the literature (see e.g. the NIST database [28] or Sugar and Musgrove [29]) but our transition probabilities and oscillator strengths are the first to be published, which potentially makes 1024 new intense lines useful for astrophysicists in the framework of our collaboration with the University of Tübingen or for other astrophysicists. Some of them have actually been used to identify new lines of Cu IV in the spectrum of RE0503-289 (see section 4.1.3.1). Those 1024 transitions are listed in Table A3, where the energies are the experimental ones given in cm⁻¹.

When it came to Cu V, the criterion $\log gf \geq -6$ led to 5456 transitions and we obtained 695 transitions with $\log gf \geq -1$, which are listed in table A6 in which the energies are the experimental ones given in cm⁻¹. Some of these transitions have been measured and reported in [30] but no comparison point exists to our knowledge in the literature when it comes to gA and $\log gf$. Once again some of those intense lines were used to identify spectral lines of Cu V in RE0503-289, as shown in section 4.1.3.1. Those data could therefore also be used to identify Cu V lines in other stellar spectra.

The case of Cu VI is particularly interesting because it is the only ion for which we found gA values in the literature. In our calculations, we once again imposed the log $gf \geq -6$ and log $gf \geq -1$ criteria and it led to respectively 3797 and 421 transitions. Those 421 most intense transitions are listed in Table A9 where the energies given are the experimental ones in cm⁻¹. Exactly as for the two previous ions, those intense lines have been used to identify lines of Cu VI in the spectrum of RE0503-289.

In their paper, Aggarwal *et al.* [106] performed a calculation using the quasi-relativistic (QR) approximation. This QR approximation is an Hartree-Fock calculation with the relativistic effects included using the Breit-Pauli approximation. To include the correlation, all one- and two-electron promotions of interest are considered in a large CI wavefunction expansion. If we compare these latter results with ours, we find an overall good agreement in particular for the strongest lines (log gf > -1), for which the mean deviation between the two sets of data was found to be about 20%, with a general tendency such that our log gf values appear systematically slightly higher than those of Aggarwal *et al.*, as shown in Figure 4.1. This could be explained by the fact that core-core correlations have been taken into account in their calculation thanks to the very large configuration interaction expansion. Nevertheless, the overall good agreement between the two calculations, especially for the strongest transitions, reinforces our results within a margin of error of about twenty percent.

Finally, for the last copper ion we treated in this work, namely Cu VII, the log $gf \ge -6$ and log $gf \ge -1$ criteria gave rise to 2253 and 284 transitions, respectively. Those 284 most intense transitions in Cu VII are given in Table A12 where, once again, the energies are the experimental ones given in cm⁻¹. Exactly as for the other copper ions, those transitions were used to identify spectral lines in RE0503-289 and could be used to identify copper lines in other stars.



Figure 4.1: Comparison between the log gf values obtained in this work and the ones of [106] for the Cu VI ion, The red line represents the equality between the gf-values obtained in this work and the ones of [106].

4.1.3.1 Application of Our New Atomic Data to the Spectral Analysis of Hot White Dwarfs

Our calculation led to the detection of many Cu IV-VII lines in the spectrum of RE0503-289 (see [77]). As shown in Figure 4.2. 54 Cu lines were identified (1 of Cu IV, 51 of



Figure 4.2: Prominent Cu lines in the observation (gray line) of RE 0503-289. Synthetic Spectra are given in red.

Cu V, and 2 of Cu VI). Detailed line-profile comparison of the Tübingen NLTE stellar atmosphere model (i.e. an effective temperature of $T_{eff} = 70~000$ K and a surface gravity³ log g = 7.5 in this case) with the UV observations⁴ from the FUSE (Far Ultraviolet Spectroscopic Explorer) and the HST (Hubble Space Telescope), led to the determination of Cu abundance of $9.3^{+3.0}_{-2.0} \times 10^{-5}$ mass fraction (132 times the solar one!).

The uncertainty is determined through the T_{eff} error propagation by the evaluation from two models at the error limits with the highest and the lowest degree of ionization, (i.e. $T_{eff} = 72\ 000$ K and log g = 7.4 and $T_{eff} = 68\ 000$ K and log g = 7.6), respectively.

The abundance error is found smaller than 0.1 dex and the final mass fraction is adopted with uncertainties of 0.2 dex.

 $^{{}^{3}}g$ is the surface gravity.

⁴The spectra are described in Rauch *et al.* [107] and Hoyer *et al.* [108].

A similar analysis has been performed in the case of the spectrum of another white dwarf: G191-B2B. The four strongest Cu V lines in the synthetic spectrum are identified as highlighted in Figure 4.3.



Figure 4.3: Prominent Cu lines in the observation (gray line) of G191-B2B. Synthetic Spectra are given in red.

They are well reproduced by a model ($T_{eff} = 60\ 000$ K, log g = 7.6) with a Cu mass fraction of $6.3^{+3.0}_{-2.0} \times 10^{-6}$ (nine times the solar one). The error estimation is performed analogously to the one of RE 0503-289 and the same uncertainty of 0.2 dex was found.

4.2 In IV - VII

Indium has an atomic number of Z = 49 and is a very rare element on Earth. It is named after its supposed indigo-like color (*indicum* in classical Latin and *indium* in medieval Latin) when put through a flame. This color is actually explained by an intense dark blue line and a weaker violet line in its atomic visible spectrum. It was discovered by Ferdinand Reich and Hieronimus Theodor Richter in 1863 [109].

4.2.1 Models Used

In this work, we obtained new sets of oscillator strengths and transition probabilities using the pseudo-relativistic Hartree-Fock (HFR + CPOL) approach combined with a semi-empirical least-squares fitting procedure of radial energy parameters. Many electron correlations were considered by means of extended multiconfiguration expansions which were included in the physical models. Those expansions were chosen in order to include low-lying configurations, for which energy levels are experimentally known, together with some higher configurations with larger configuration interactions. The core-polarization effects were modeled using a core-polarization potential (see section 2.2).

More precisely, in In IV, the configuration interaction was explicitly considered among the configurations $4d^{10}$, $4d^{9}5s$, $4d^{9}6s$, $4d^{9}7s$, $4d^{9}8s$, $4d^{9}5d$, $4d^{9}6d$, $4d^{9}7d$, $4d^{8}5s^{2}$, $4d^{8}5p^{2}$, $4d^85s5d$ in the even parity and $4d^95p$, $4d^96p$, $4d^97p$, $4d^94f$, $4d^95f$, $4d^96f$, $4d^97f$, $4d^85s5p$, $4d^85s6p$, $4d^85s5f$ in the odd one. Using the experimental data of Swapnil and Tauheed [32] and Ryabtsev and kononov [33], the radial parameters (average energies, Slater integrals, spin-orbit parameters and effective interaction parameters) of 4d¹⁰, 4d⁹5s, 4d⁹6s, 4d⁹7s, $4d^{9}8s$, $4d^{9}5d$, $4d^{9}6d$, $4d^{9}7d$, $4d^{8}5s^{2}$ in the even parity and $4d^{9}5p$, $4d^{9}6p$, $4d^{9}7p$, $4d^{9}4f$, 4d⁹5f, 4d⁸5s5p in the odd parity were optimized during the fitting procedure. The mean deviations between calculated and experimental energy levels were 68 cm⁻¹ (66 levels) in the even parity and 194 $\rm cm^{-1}$ (222 levels) in the odd parity. Concerning the latter, only 103 of 135 known levels were included in the calculation due to an energy cut-off at 395 000 cm^{-1} made because unambiguous identification was not possible for higher energy levels. α_d was chosen to be 2.02 a.u., as tabulated by Fraga *et al.* [94] for an In VI core and r_c was considered to be 1.11 a.u., which corresponds to the mean radius of the 4d orbital. The theoretical energy levels were compared to the experimental ones and the good agreement between the two sets can be seen in Tables A13 and A14 for the even and the odd parity respectively.

When it came to In V, the interacting configurations were $4d^9$, $4d^85s$, $4d^86s$, $4d^85d$, $4d^86d$, $4d^75s^2$, $4d^75p^2$, $4d^75d^2$, $4d^75s5d$ in the even parity and $4d^85p$, $4d^86p$, $4d^87p$, $4d^87p$, $4d^85f$, $4d^86f$, $4d^87f$, $4d^75s5p$, $4d^75s6p$, $4d^7$ in the odd one. In the even parity, the radial integrals corresponding to $4d^9$, $4d^85s$, $4d^86s$, $4d^85d$ and $4d^75s^2$ were adjusted to minimize the differences between the calculated Hamiltonian eigenvalues and the experimental energy levels taken from Swapnil and Tauheed [34] and Ryabtsev [35]. In this process, we found a mean deviation equal to 451 cm^{-1} (90 levels). The same procedure for $4d^85p$, $4d^86p$, $4d^87p$, $4d^84f$, $4d^85f$ and $4d^75s5p$ (158 levels) led to a mean deviation of 373 cm⁻¹ in the odd parity. We chose α_d equals to 1.62 a.u. as tabulated in [94] for an In VII core and the value of r_c was 1.07 a.u., which corresponds to the HFR mean radius of the 4d orbital. The energy levels of In V are displayed in Tables A16 and A17 (for the even and the odd parity, respectively).

In the case of In VI, the configurations included in our HFR model were $4d^8$, $4d^75s$, $4d^76s$, $4d^76d$, $4d^65s^2$, $4d^65p^2$, $4d^65d^2$, $4d^65s5d$ and $4d^75p$, 4d76p, $4d^74f$, $4d^75f$, $4d^65s5p$, $4d^65s5p$, $4d^65s5f$ for respectively the even and odd parity. The experimental data from [36] and [37] were used for the fitting procedure in order to optimize the radial

parameters for the 4d⁸, 4d⁷5s,4d⁶5s² and 4d⁷5p, 4d⁷6p, 4d⁷4f configurations. The mean deviations were found to be 88 cm⁻¹ (46 levels) in the even parity and 435 cm⁻¹ (194 levels) in the odd parity. For In IV, α_d was considered to be equal to 1.28 a.u. as tabulated by Fraga *et al.* [94] for an In VIII core and r_c taken as 1.04 a.u. which equates to the HFR mean radius of the 4d orbital. The comparison between the calculated and experimental In VI even energy levels is shown in Table A19 and the same comparison for the odd levels is in Table A20.

Finally, pertaining to In VII, we included the 4d⁷, 4d⁶5s, 4d⁶6s, 4d⁶5d, 4d⁶6d, 4d⁵5s², 4d⁵5p², 4d⁵5d² and 4d⁸5s5d configurations for the even parity and 4d⁶5p, 4d⁶6p, 4d⁶4f, 4d⁶5f, 4d⁵5s5p, 4d⁵5p6p and 4d⁵5s5f for the odd one. The radial parameters were respectively fitted for 4d⁷ and 4d⁶5p. We respectively obtained a mean deviation of 87 cm⁻¹ (17 levels) and of 202 cm⁻¹ (131 levels) from experimental data of Ryabtsev *et al.* [38]. Finally, the polarization parameters were taken as $\alpha_d = 1.01$ a.u. (from Fraga [94] for an In IX core) and $r_c = 1.02$ a.u. (HFR mean radius of the 4d orbital). Those very good agreements between experimental and calculated energy levels are shown in Tables A22 and A23 for the even and the odd parity levels of In VII.

4.2.2 Atomic Radial Parameters

The values of the *ab initio* and fitted parameters for the even parity of In IV are given in Table 4.5. As one can see, many parameters for all the configurations with known experimental levels were fitted. The values of the *ab initio* and fitted parameters for the odd parity of In IV are given in Table 4.6.

In Table 4.7, the letter means that the variation of the parameters with the same letter (a,b or c) has been linked and thus forced to undergo a proportional modification during the fitting procedure. The α and β parameters of 4d⁸6s have been given as initial values identical to those obtained for the 4d⁸5s after a first use of the fitting procedure for the latter configuration. As one can see in that table, the fitting procedure in 4d⁸6s barely changes those values.

In Table 4.8, the letter code is the same as in the previous one. The α and β parameters are fixed alongside a Rydberg serie. Thus, the α,β were fitted for 4d⁸5p and 4d⁸4f and the same values were considered for 4d⁸np and 4d⁸nf.

The values of the *ab initio* and fitted parameters for the even parity of In VI can be found in Table 4.9. In Table 4.10, the letter code is the same as in the previous tables. The α and β parameters of 4d⁷6p are considered as the same as in 4d⁷5p. In table 4.11 the letter code is the same as in the previous tables. In the case of In VII, because there is only one configuration for each parity, both parities are depicted in the same table.

Configuration	Parameter	$\mathrm{HFR}~(\mathrm{cm}^{-1})$	Fitted (cm^{-1})	Ratio
$4d^{10}$	E_{av}	2984.1	2998.0	
$4d^95s$	E_{av}	136239.9	134625.6	
	ζ_{4d}	2740.5	2842.8	1.037
	$G^{2}(4d, 5s)$	13512.6	13361.6	0.989
$4d^96s$	E_{av}	301143.3	301922.5	
	ζ_{4d}	2771.5	2855.6	1.029
	$G^{2}(4d, 6s)$	2859.5	2846.2	0.995
$4d^97s$	E_{av}	362597.5	364033.8	
	ζ_{4d}	2777.5	2869.4	1.033
	$G^{2}(4d,7s)$	1156.1	1083.8	0.937
$4d^98s$	E_{av}	392667.1	394167.1	
	ζ_{4d}	2779.6	Fixed	
	$G^{2}(4d, 8s)$	594.7	Fixed	
$4d^95d$	E_{av}	291735.9	294717.2	
	ζ_{4d}	2772.3	2834.3	1.022
	ζ_{5d}	216.6	277.0	1.278
	$F^{2}(4d, 5d)$	12313.7	12228.3	0.993
	$F^{4}(4d, 5d)$	5086.8	4947.1	0.972
	$G^{0}(4d, 5d)$	2881.4	2613.9	0.907
	$G^{2}(4d, 5d)$	3430.0	2785.0	0.811
	$G^{4}(4d, 5d)$	2760.4	2687.9	0.973
$4d^96d$	E_{av}	359682.9	361295.1	
	ζ_{4d}	2777.8	2865.9	1.031
	ζ_{6d}	96.2	118.8	1.234
	$F^{2}(4d, 6d)$	4734.7	4911.8	1.037
	$F^{4}(4d, 6d)$	1989.9	1898.4	0.954
	$G^{0}(4d, 6d)$	1126.8	907.4	0.805
	$G^{2}(4d, 6d)$	1398.3	1516.1	1.084
	$G^{4}(4d, 6d)$	1148.1	1391.2	1.212
$4d^97d$	E_{av}	391322.6	394322.6	
	ζ_{4d}	2779.8	Fixed	
	ζ_{7d}	51.8	Fixed	
	$F^{2}(4d,7d)$	2384.1	Fixed	
	$F^{4}(4d,7d)$	1025.4	Fixed	
	$G^{0}(4d,7d)$	574.3	Fixed	
	$G^{2}(4d,7d)$	725.6	Fixed	
	$G^{4}(4d,7d)$	601.0	Fixed	
$4d^85s^2$	E_{av}	300454.6	296791.9	
	$F^{2}(4d, 4d)$	83410.2	69061.7	0.827
	$F^{4}(4d, 4d)$	55223.9	42410.2	0.768
	α	0.0	-16.8	
	β	0.0	2667.6	
	ζ_{4d}	2876.5	Fixed	

Table 4.5: Radial parameters for the even parity in In IV

66 levels included - mean deviation: 68 $\rm cm^{-1}$

Configuration	Parameter	$\mathrm{HFR}~(\mathrm{cm}^{-1})$	Fitted (cm^{-1})	Ratio
$4d^95p$	E_{av}	205646.4	204851.6	
	ζ_{4d}	2753.9	2853.7	1.036
	ζ_{5p}	3529.9	4140.1	1.172
	$F^{2}(4d,5p)$	24098.2	22577.7	0.937
	$G^{1}(4d, 5p)$	8139.8	8059.9	0.990
	$G^{3}(4d,5p)$	7311.2	7694.3	1.052
$4d^96p$	E_{av}	325981.6	326545.3	
	ζ_{4d}	2773.5	2833.0	1.021
	ζ_{6p}	1244.5	1346.3	1.082
	$F^{2}(4d, 6p)$	7524.1	6969.1	0.925
	$G^{1}(4d, 6p)$	2132.2	1864.8	0.874
	$G^{3}(4d, 6p)$	2085.2	1852.1	0.888
$4d^97p$	E_{av}	374562.0	375429.4	
	ζ_{4d}	2778.1	Fixed	
	ζ_{7p}	593.6	Fixed	
	$F^{2}(4d,7p)$	3354.6	Fixed	
	$G^{1}(4d,7p)$	928.2	Fixed	
	$G^{3}(4d,7p)$	930.6	Fixed	
$4d^94f$	E_{av}	333884.8	335095.5	
	ζ_{4d}	2772.5	2799.8	1.010
	ζ_{4f}	5.7	5.7	1.000
	$F^{2}(4d, 4f)$	12411.5	12074.1	0.972
	$F^{4}(4d, 4f)$	5486.3	5979.1	1.089
	$G^{1}(4d,4f)$	8503.7	7354.2	0.865^{a}
	$G^{3}(4d, 4f)$	4886.9	4226.2	0.865^{a}
	$G^5(4d,4f)$	3341.3	2889.6	0.865^{a}
$4d^95f$	E_{av}	376284.5	377106.6	1.002
	ζ_{4d}	2774.8	Fixed	
	ζ_{5f}	4.7	Fixed	
	$F^{2}(4d, 5f)$	7149.7	Fixed	
	$F^{4}(4d, 5f)$	3614.7	Fixed	
	$G^{1}(4d,5f)$	6282.8	Fixed	
	$G^{3}(4d, 5f)$	3675.0	Fixed	
_	$G^{5}(4d, 5f)$	2528.9	Fixed	
$4d^85s5p$	E_{av}	364119.1	363264.0	
	$F^{2}(4d, 4d)$	83659.1	72948.5	0.871^{b}
	$F^{4}(4d, 4d)$	55410.8	48316.8	0.871^{b}
	α	0.0	64.6	
	β	0.0	592.8	
	ζ_{4d}	2888.6	3126.2	1.08^{c}
	ζ_{5p}	4041.1	4373.5	1.08^{c}
	$F^{2}(4d,5p)$	25645.5	26182.0	1.020
	$G^{1}(4d, 5s)$	13640.8	14018.3	1.027
	$G^{1}(4d,5p)$	8465.5	7213.6	0.851^{d}
	$G^{3}(4d,5p)$	7736.4	6592.3	0.851^{d}
	$G^{1}(5s,5p)$	51330.7	43739.7	0.851^{d}

Table 4.6: Radial parameters for the odd parity in In IV

a,b,c,d: Ratio linked during the fitting procedure.

103 levels included - mean deviation: 194 cm^{-1}

Configuration	Parameter	$\mathrm{HFR}~(\mathrm{cm}^{-1})$	Fitted (cm^{-1})	Ratio
$4d^9$	E_{av}	4962.9	5065.0	
	ζ_{4d}	2782.0	2870.5	1.031
$4d^85s$	E_{av}	180844.6	178887.0	
	$F^{2}(4d, 4d)$	84257.3	78258.7	0.928
	$F^{4}(4d, 4d)$	55857.6	54905.9	0.983
	α	0.0	49.0	
	β	0.0	-596.0	
	ζ_{4d}	2916.2	3014.8	1.034
	$G^{1}(4d, 5s)$	14296.8	14299.2	1.000
$4d^86s$	E_{av}	388421.1	395010.5	0.983
	$F^{2}(4d, 4d)$	84965.4	85965.4	1.012
	$F^{4}(4d, 4d)$	56388.7	57388.7	1.017
	α	0.0	49.2	
	β	0.0	-599.2	
	ζ_{4d}	2949.6	Fixed	
	$G^{1}(4d, 6s)$	3268.8	Fixed	
$4d^85d$	E_{av}	365891.7	368052.0	
	$F^{2}(4d, 4d)$	84939.0	75125.7	0.884^{a}
	$F^{4}(4d, 4d)$	56370.1	49857.4	0.884^{a}
	α	0.0	-36.5	
	β	0.0	1938.1	
	ζ_{4d}	2948.7	3076.1	1.042^{b}
	ζ_{5d}	326.6	340.6	1.042^{b}
	$F^{2}(4d, 5d)$	16071.9	15919.6	0.990^{c}
	$F^{4}(4d, 5d)$	7026.1	6959.6	0.990^{c}
	$G^{0}(4d, 5d)$	3892.0	3104.4	0.797^{d}
	$G^{2}(4d, 5d)$	4697.5	3746.8	0.797^{d}
	$G^{4}(4d, 5d)$	3832.3	3056.8	0.797^{d}
$4d^75s^2$	E_{av}	388424.2	384730.4	1.010
	$F^{2}(4d, 4d)$	86191.9	85051.1	0.987
	$F^{4}(4d, 4d)$	57284.0	58881.3	1.027
	α	0.0	150.3	
	β	0.0	1813.3	
	ζ_{4d}	3052.5	Fixed	

Table 4.7: Radial parameters for the even parity in In V

a,b,c,d: Ratio linked during the fitting procedure 95 levels included - mean deviation: 451 cm^{-1}

Configuration	Parameter	HFR (cm^{-1})	Fitted (cm^{-1})	Ratio
$4d^85p$	E_{av}	260182.2	259468.6	
_	$F^{2}(4d, 4d)$	84506.5	77843.3	0.920
	$F^{4}(4d, 4d)$	56044.9	55024.1	0.981
	α	0.0	41.2	
	β	0.0	-353.0	
	ζ_{4d}	2929.0	3020.0	1.030
	ζ_{5p}	4567.6	5185.4	1.135
	$F^{2}(4d,5p)$	27605.4	26629.3	0.964
	$G^{1}(4d, 5p)$	9111.4	8957.3	0.964
	$G^{3}(4d,5p)$	8422.0	8495.4	1.009
$4d^86p$	E_{av}	418587.4	418740.1	
	$F^{2}(4d, 4d)$	84995.9	76037.8	0.894
	$F^{4}(4d, 4d)$	56411.3	65434.5	1.160
	α	0.0	41.2	
	β	0.0	-353.0	
	ζ_{4d}	2951.6	3468.7	1.175
	ζ_{6p}	1721.7	1392.8	0.809
	$F^{2}(4d, 6p)$	9275.0	9861.3	1.062
	$G^{1}(4d, 6p)$	2503.4	2100.6	0.836^{a}
	$G^{3}(4d, 6p)$	2529.2	2111.9	0.836^{a}
$4d^87p$	E_{av}	485669.6	485141.6	
	$F^{2}(4d, 4d)$	85100.5	77100.5	0.905
	$F^{4}(4d, 4d)$	56485.9	56489.5	1.001
	α	0.0	41.2	
	β	0.0	-353.0	
	ζ_{4d}	2957.3	Fixed	
	ζ_{7p}	847.6	Fixed	
	$F^{2}(4d,7p)$	4267.5	Fixed	
	$G^{1}(4d,7p)$	1113.5	Fixed	
_	$G^{3}(4d,7p)$	1155.6	Fixed	
$4d^84f$	E_{av}	403399.5	403653.3	
	$F^{2}(4d, 4d)$	84561.4	77610.9	0.934^{b}
	$F^{4}(4d, 4d)$	56084.0	53436.0	0.934^{b}
	α	0.0	83.2	
	β	0.0	-1092.4	
	ζ_{4d}	2932.2	3113.5	1.061^{c}
	ζ_{4f}	22.6	24.0	1.061^{c}
	$F^{2}(4d, 4f)$	27339.6	26902.1	0.984
	$F^{4}(4d, 4f)$	14698.4	14631.3	0.995
	$G^{1}(4d, 4f)$	25856.8	26067.0	1.008^{d}
	$G^{3}(4d,4f)$	15175.8	15299.1	1.008^{d}
	$G^{5}(4d,4f)$	10456.9	10541.9	1.008^d

Table 4.8: Radial parameters for the odd parity in In V

	100	ic 4.0. commu	cu	
Configuration	Parameter	HFR (cm^{-1})	Fitted (cm^{-1})	Ratio
$4d^85f$	E_{av}	473161.3	473548.4	
	$F^{2}(4d, 4d)$	84857.1	80173.9	0.945
	$F^{4}(4d, 4d)$	56306.8	56423.1	1.002
	α	0.0	83.2	
	β	0.0	-1092.4	
	ζ_{4d}	2944.4	3220.8	$1 \ 1.091^{e}$
	ζ_{5f}	16.7	18.2	1.091^{e}
	$F^{2}(4d,5f)$	13617.8	12319.0	0.904^{f}
	$F^{4}(4d,5f)$	7751.0	7011.7	0.904^{f}
	$G^{1}(4d,5f)$	14324.3	14050.5	0.981^{g}
	$G^{3}(4d,5f)$	8688.7	8522.6	0.981^{g}
	$G^{5}(4d,5f)$	6061.7	Fixed	
$4d^86f$	E_{av}	512579.0	504639.6	

Table 4.8: continued

a,b,c,d,e,f,g: Linked parameters during the fitting procedure. 158 levels included - mean deviation: 373 cm^{-1}

Table 4.9: Radial parameters for the even parity in In VI

Configuration	Parameter	HFR (cm^{-1})	Fitted (cm^{-1})	Ratio
$4d^8$	E_{av}	16986.4	16293.8	
	$F^{2}(4d, 4d)$	85189.9	79824.0	0.937
	$F^{4}(4d, 4d)$	56556.2	55741.1	0.985
	α	0.0	45.8	
	β	0.0	-598.2	
	ζ_{4d}	2962.4	3060.2	1.033
$4d^75s$	E_{av}	237263.3	233884.7	
	$F^{2}(4d, 4d)$	87035.9	81079.2	0.931
	$F^{4}(4d, 4d)$	57917.7	57825.6	0.998
	α	0.0	47.4	
	β	0.0	-596.7	
	ζ_{4d}	3097.0	3197.5	1.031
	$G^{2}(4d,5s)$	14928.8	14805.3	0.992

47 levels included - mean deviation: 88 cm^{-1}

Configuration	1 arameter	$\Pi \Pi \Pi (C \Pi)$	Fifted (cm)	nauo
$4d^75p$	E_{av}	324553.5	323877.8	
	$F^{2}(4d, 4d)$	87251.0	80920.0	0.927
	$F^{4}(4d, 4d)$	58079.8	57202.2	0.985
	α	0.0	49.0	
	β	0.0	-481.1	
	ζ_{4d}	3109.2	3208.7	1.031
	ζ_{5p}	5618.2	6348.8	1.129
	$F^{2}(4d,5p)$	30715.7	29801.4	0.969
	$G^{1}(4d,5p)$	9918.4	9805.9	0.989
	$G^{3}(4d,5p)$	9380.9	8905.1	0.949
$4d^{7}6p$	E_{av}	522135.4	523284.2	
	$F^{2}(4d, 4d)$	87739.1	83428.5	0.950
	$F^{4}(4d, 4d)$	58446.7	42408.0	0.725
	α	0.0	49.0	
	β	0.0	-481.1	
	ζ_{4d}	3134.5	Fixed	
	ζ_{6p}	2232.5	Fixed	
	$F^{2}(4d, 6p)$	10945.7	10421.8	0.952
	$G^{1}(4d, 6p)$	2836.4	Fixed	
	$G^{3}(4d, 6p)$	2937.7	Fixed	
$4d^{7}4f$	E_{av}	466128.9	465755.9	
	$F^{2}(4d, 4d)$	86905.1	82713.4	0.951
	$F^{4}(4d, 4d)$	57818.7	51789.0	0.896
	α	0.0	-64.2	
	β	0.0	2273.2	
	ζ_{4d}	3088.5	3597.2	1.164
	ζ_{4f}	54.7	51.5	0.941
	$F^{2}(4d, 4f)$	44008.9	48334.9	1.098
	$F^4(4d,4f)$	25924.5	26185.5	1.010
	$G^1(4d,4f)$	47857.7	43367.9	0.905^{a}
	$G^{3}(4d, 4f)$	28615.0	25930.5	0.905^{a}
	$G^{5}(4d, 4f)$	19858.5	17995.5	0.905^{a}

Table 4.10: Radial parameters for the odd parity in In VI Configuration | Parameter | HFR (cm^{-1}) | Fitted (cm^{-1}) | Ratio

a: Linked parameters during the fitting procedure

185 levels included - mean deviation: 435 $\rm cm^{-1}$

Configuration	Parameter	HFR (cm^{-1})	Fitted (cm^{-1})	Ratio
Even Parity				
$4d^7$	E_{av}	25640.4	28484.5	
	$F^{2}(4d, 4d)$	73289.7	87947.6	1.200^{a}
	$F^{4}(4d, 4d)$	48835.5	58602.7	1.200^{a}
	α	0.0	39.3	
	β	0.0	-476.1	
	ζ_{4d}	3147.5	3242.7	1.029
Odd Parity				
$4d^65p$	E_{av}	384640.4	390251.0	
	$F^{2}(4d, 4d)$	74866.5	83466.0	1.114
	$F^{4}(4d, 4d)$	50001.8	59330.9	1.186
	α	0.0	44.9	
	β	0.0	-376.9	
	ζ_{4d}	3294.4	3410.8	1.035
	ζ_{5p}	6677.4	7457.0	1.117
	$F^{2}(4d,5p)$	27943.4	32758.3	1.172^{b}
	$G^{1}(4d,5p)$	8844.5	10363.8	1.172^{b}
	$G^{3}(4d,5p)$	8523.4	10285.3	1.172^{b}
	$\begin{matrix} \zeta_{5p} \\ F^{2}(4d,5p) \\ G^{1}(4d,5p) \\ G^{3}(4d,5p) \end{matrix}$	6677.4 27943.4 8844.5 8523.4	7457.0 32758.3 10363.8 10285.3	$ \begin{array}{c} 1.000 \\ 1.117 \\ 1.172^{b} \\ 1.172^{b} \\ 1.172^{b} \\ 1.172^{b} \\ \end{array} $

Table 4.11: Radial parameters for the even and odd parities in In VII

a,b: Linked parameters during the fitting procedure. Even Parity: 17 levels (mean deviation: 87 cm^{-1}) Odd Parity: 131 levels (mean deviation: 202 cm⁻¹)

4.2.3 Radiative Transition Rates

Once again, for a better readability of the manuscript, the tables showing the radiative transition rates for the indium ions will be placed in the appendices. Indeed, we initially selected the transitions for which $\log gf$ was \geq -4, which lead to (tenth of) thousands of transitions. We therefore decided to restrict ourselves and impose the condition $\log gf \geq$ -1 corresponding to the most intense and reliable transitions (CF > 0.05). The energy levels given in those tables are taken from the NIST database [28].

The Table A15 shows those most intense transitions in In IV. With the log $gf \ge -1$ condition this led to 458 intense transitions (shown in Table A15) that could be used by the astrophysicists to identify new In IV lines in stellar spectra. We also sent the astrophysicists a list with the transitions with a log $gf \ge -4$ (2710 transitions) but obviously these less intense transitions $(-4 < \log gf < -1)$ are much less likely to be observed in astrophysical spectra. However, they are used to flesh out the NLTE models built to identify new spectral lines.

When it comes to In V, once again, even though some transitions have been measured experimentally, there is no experimental comparison point in the literature for gf and gAvalues. If we apply the same criteria as for In IV on the log gf, the condition log $gf \ge -1$ gives rise to 840 transitions listed in Table A18. Once again, the energy levels mentioned in this table are taken from the NIST data base. Exactly as for In IV, we provided the astrophysicists with a list even bigger with the transitions having a log $gf \ge -4$, which represents 5895 transitions in this case.

If we look through the literature, it turns out that other HFR calculations have already been carried out in In IV. The first one by Swapnil and Tauheed [32] and the second one by Ryabtsev and Kononov [33]. In the former calculation [32], they included fewer configurations (21) than we did (22) and they did not include core-polarization effects. Regarding the calculations of [33], they included a few more configurations (29) but did not include the core polarization corrections either. In both cases, our calculation is the only one to include the core polarization corrections. If we compare the reproduction of the energy levels, with regard to the odd parity, the three calculations give quite similar results with a mean deviation around 150 cm⁻¹ (respectively 194, 177 and 140 cm⁻¹) but in the even parity, our calculation is much closer with 68 cm⁻¹ in comparison with 133 cm⁻¹ for Swapnil ad Tauheed and 97 cm⁻¹ for Ryabtsev and Kononov. Therefore, even if the mean deviation is slightly worse for odd parity, the fact that it is much better for even parity and that we added the core polarization corrections brings a real added value. Especially since the higher deviation in the odd parity comes from very high energy levels.

If we compare the gA for the most intense transitions in our calculation and in the one of Swapnil and Tauheed, we realize, as shown in Figure 4.4, that our values are systematically slightly lower than theirs. This effect is due to the addition of the core polarization corrections, which generally lower the gA as shown in many works before (e.g. [82]). The figure shows that in a [32] against our work graph, the vast majority of the data is, as expected, above the red line representing the equality between our calculations and the one of Swapnil and Tauheed.

If we make the same kind of comparison between our data and those of [33], we notice that the systematics is not as obvious as it was when we compared it to [32]. This is shown in Figure 4.5. We can even see on that figure that in fact, the values are quite close to each other. This comes from the fact that in their calculations, they have introduced configurations with incomplete 4p subshells $(4p^5)$ which is indeed considered in our calculation as core-valence interaction and which is therefore also included, but via the core polarization potential. This also explains why they have included more configurations in their model than we have. Their calculation takes into account a part of the core-valence interactions, probably the most important ones, and this is why their

results are closer to ours than the calculation of [32] without the core-valence interactions. Nevertheless, the values are slightly different because, contrary to them who only consider some interactions, we model all of them with our core polarization potential.



Figure 4.4: Comparison between the gA (in 10^9 s^{-1}) obtained in this work for In IV most intense transitions and the ones of [32]. The straight line of equality is drawn in red.



Figure 4.5: Comparison between the gA (in 10^9 s^{-1}) obtained in this work for In IV most intense transitions and the ones of [33]. The straight line of equality is drawn in purple.

The second ion we worked on is In V. For this ion, we obtained 5895 transitions with $\log gf \geq -4$ and 840 with $\log gf \geq -1$, which can be found in Table A18. The only comparison that we found in the literature for those intense transitions was with the atomic data from Swapnil and Tauheed [34]. Exactly as for In IV, they considered a bit less configurations (20) than we did (22) and they did not include core-polarization effects. The comparison between our calculations and theirs is shown in Figure 4.6. Exactly as for In IV, the gA values from our calculations with the core-polarization effects taken into account are systematically lower than theirs without it. This effect is all but surprising as it was already discussed for In IV and in section 3.2.



Figure 4.6: Comparison between the gA (in 10^9 s^{-1}) obtained in this work for In V most intense transitions and the ones of [34]. The straight line of equality is drawn in red.

The third ion treated in this section is In VI. The log $gf \ge -4$ criterion produced 2265 transitions and the selection of the most intense ones with log $gf \ge -1$ restricted this list to the 458 transitions that can be found in Table A21. There are few data concerning the transition rates of In VI in the literature. In their study, Ryabtsev *et al.* [37] produced some but there are too few comparison points between their rates and ours to draw a conclusion. The two data sets can thus be seen as complementary for astrophysicists to hope to identify lines of In VI in stellar spectra.

The fourth and last ion treated was In VII. We obtained 1072 transitions with log $gf \geq -4$ and 255 more intense ones with log $gf \geq -1$. Those transitions are listed in Table A24. There is, to our knowledge, no existing data in the literature about In VII transitions probabilities and oscillator strength. Our atomic data is therefore the first one produced in that ion. However, the method of calculation having proved itself reliable and the model being similar to that used for the other indium ions for which there were points of comparison allow us to be confident about the quality of this data.

4.2.3.1 Application of the new atomic data in Indium ions to the spectral analysis of hot white dwarfs

Using the less complete existing literature (see the previous subsection), our colleagues at the University of Tübingen already highlighted five In V lines in the spectrum of RE0503-289 as shown in Figure 4.7 while no In line could be identified in the UV observation of G191-B2B using the previously existing data.



Figure 4.7: In V lines in the spectrum of RE0503-289

This led to the determination (using the same method as the one described in section 4.1.3.1) of an In mass fraction of $3.0 \pm 0.5 \times 10^{-6}$ (56 600 times the In solar mass fraction) with an uncertainty of 0.2 dex.

This strongly fueled the motivation to undertake calculations in the Indium ions as lines of at least one of them had already been observed.

The data presented above are currently being analyzed in Tübingen and we hope that they will lead soon to the identification of many other indium lines in RE0503-289 and in G191-B2B as was the case for copper. Those new identifications could hopefully lead to a refinement of the mass fraction given here above.

4.3 Cs IV-VII

Caesium, Z = 55, was named after the Latin word *caesius* (sky blue), due to the blue color light of the two characteristic lines of its visible emission spectrum. This element was first detected in 1860 by Robert Wilhelm Bunsen and Gustav Robert Kirchhoff from the spectroscopy of Dürkheim's mineral water, made with the spectroscope they had developed in 1859 (a few months later, they discovered rubidium in the same way) [109].

4.3.1 Models Used

We started with the case of Cs IV for which we considered the configuration interaction explicitly among the following configurations: $5s^2 5p^4$, $5s^2 5p^3 6p$, $5s^2 5p^3 7p$, $5s^2 5p^3 8p$, $5s^2 5p^3 4f$, $5s^2 5p^3 5f$, $5s^2 5p^3 6f$, $5s^2 5p^2 5d 6s$, $5s^2 5p^2 5d 6d$, $5s^2 5p^2 6s^2$, $5s^2 5p^2 5d^2$, $5s^2 5p^2 6d^2$, $5s^2 5p^2 4f^2$, $5s 5p^4 6s$, $5s 5p^4 5d$, $5s 5p^4 6d$, $5s 5p^4 7d$, $5s 5p^3 5d 4f$ and $5p^6$ for the even parity and $5s\,5p^5$, $5s^2\,5p^3\,5d$, $5s^2\,5p^3\,6d$, $5s^2\,5p^3\,7d$, $5s^2\,5p^3\,6s$, $5s^2\,5p^3\,7s$, $5s^2 5p^3 8s$, $5s^2 5p^3 9s$, $5s^2 5p^3 5g$, $5s^2 5p^3 6g$, $5s^2 5p^2 5d 4f$, $5s^2 5p^2 5d 5f$, $5s^2 5p^2 5d 6f$, $5s\,5p^4\,6p, 5s\,5p^4\,4f, 5s\,5p^4\,5f, 5s\,5p^4\,6f, 5s\,5p^3\,5d^2$ and $5s\,5p^3\,6d^2$ for the odd one. The radial integrals (the average energy, Slater integrals, spin-orbit parameters and effective interaction parameters) corresponding to $5s^2 5p^4$ in the even parity and $5s 5p^5$, $5s^2 5p^3 5d$, $5s^2 5p^3 6d$, $5s^2 5p^3 7d$, $5s^2 5p^3 6s$ and $5s^2 5p^3 7s$ in the odd one were optimized during the fitting procedure using the experimental energy levels of Sansonetti [39]. That lead to a mean deviation between experimental and calculated levels of 67 cm^{-1} in the even parity (5 levels) and 409 $\rm cm^{-1}$ in the odd one (87 levels) as shown in Table A25 where the main LS coupling components (i.e. all those $\geq 5\%$) are given for the fitted levels. The core polarizability, α_d , was chosen to be 0.67 a.u. as tabulated in Fraga *et al.* ([94]) for a Cs X core and r_c was considered to be 0.83 a.u. which is to the HFR mean radius of the outermost core orbital (4d).

When it came to Cs V, the interacting configurations were $5s^2 5p^3$, $5s^2 5p^2 6p$, $5s^2 5p^2 4f$, $5s^2 5p^2 5f$, $5s^2 5p^2 6f$, $5s^2 5p 5d 6s$, $5s^2 5p 5d 6d$, $5s^2 5p 6s^2$, $5s^2 5p 5d^2$, $5s^2 5p 4f^2$, $5s 5p^3 6s$, $5s 5p^3 5d$, $5s 5p^3 6d$, $5s 5p^2 4f 5d$ and $5p^5$ in the odd parity and $5s 5p^4$, $5s^2 5p^2 5d$, $5s^2 5p^2 6d$, $5s^2 5p^2 6s$, $5s^2 5p^2 6g$, $5s^2 5p 5d 6p$, $5s^2 5p 5d 4f$, $5s^2 5p 5d 5f$, $5s^2 5p 5d 6f$, $5s 5p^3 6p$, $5s 5p^3 4f$, $5s 5p^3 6p$, $5s 5p^3 6p$, $5s 5p^3 6p$, $5s 5p^3 6p$, $5s 5p^3 6f$, $5s 5p^3 6f$, $5s 5p^3 6p$, $5s 5p^3 6p$, $5s 5p^3 6p$, $5s 5p^3 6p$, $5s 5p^3 6f$, $5s 5p^3 6f$ and $5s 5p^2 5d^2$ in the even one. In the odd parity, the radial integrals corresponding to $5s^2 5p^3$ were adjusted to minimize the differences between the calculated Hamiltonian eigenvalues and the experimental energy levels taken from [39]. In this process, we found a mean deviations of 274 cm⁻¹ (5 levels). The same procedure for $5s 5p^4$, $5s^2 5p^2 5d$ and $5s^2 5p^2 6s$ (42 levels) led to a mean deviation of 475 cm⁻¹ in the even parity. The comparison between the experimental and calculated energy levels is in Table A27. The core considered was the same as the one for Cs IV with therefore the same α_d . The r_c was considered as the HFR mean radius of the 4d orbitals: 0.83 a.u.

The third ion considered was Cs VI. The configurations included in our HFR model were $5s^2 5p^2$, $5s^2 5p 6p$, $5s^2 5p 4f$, $5s^2 5p 5f$, $5s^2 5p 6f$, $5s^2 5d 6s$, $5s^2 5d 6d$, $5s^2 6s^2$, $5s^2 5d^2$, $5s^2 4f^2$, $5s^2 5f^2$, $5s 5p^2 6s$, $5s 5p^2 6d$, 5s 5p 6s 6p, 5s 5p 6p 5d, 5s 5p 6p 6d, 5s 5p 4f 6d, $5p^4$, $5p^3 6p$, $5p^3 4f$, $5p^3 5f$ and $5p^3 6f$ in the even parity and $5s 5p^3$, $5s^2 5p 5d$, $5s^2 5p 6d$, $5s 5p^2 6d$, $5s 5p^2 6d$, $5s 5p^2 6d$, 5s 5p 5d 6d, 5s 5p

highlighted in Table A29. The core polarisability was considered equals to 0.67 a.u. (see [94]) and the r_c taken as 0.82 a.u. which is equal to the HFR mean radius of the 4d orbital.

Finally, pertaining to Cs VII, we included in our model the 5s² 5p, 5s² 6p, 5s² 7p, 5s² 4f, 5s² 5f, 5s² 6f, 5s 5p 6s, 5s 5p 7s, 5s 5p 5d, 5s 5p 6d, 5p³, 5p² 6p, 5s 5p 5g, 5s 5d 6p, 5s 5d 4f, 5s 5d 5f, 5p 6s 5d, 5p 6s 6d, 5p 5d 6d, 5p 6s² and 5p 5d² configurations in the odd parity and 5s 5p², 5s² 5d, 5s 5p 4f, 5s² 6s, 5s 5p 6p, 5s 5p 5f, 5s 5d 6s, 5s 5d 6d, 5s 6s², 5s 5d², 5s 4f², 5s 5f², 5p² 6s, 5s² 7s, 5s² 6d, 5s² 5g, 5p² 5d, 5p² 6d and 5p 6s 6p in the even one. The radial parameters were respectively fitted for 5s² 5p, 5s² 6p, 5s² 4f, 5s² 5f, 5s 5p 6s, 5s 5p 5d, 5p³ (in the odd parity) and 5s 5p², 5s² 5d, 5s 5p 4f, 5s² 6s (in the even one). We obtained respectively a mean deviation of 306 cm⁻¹ (42 levels) and 172 cm⁻¹ (30 levels) in our fit using the recent (2020) experimental data from Husain *et al.* [40] as shown in Table A31. For this final caesium ion treated in this work, the polarization parameters were taken as: $\alpha_d = 0.67$ a.u. (Fraga *et al.* [94] for a Cs X core) and $r_c = 0.82$ a.u. (mean radius of the 4d orbital from our calculations).

4.3.2 Atomic Radial Parameters

In the case of Cs IV, the fit in the even parity was limited by the small number of experimentally known levels.

In the odd parity on the other hand, the fit was much more complex due to the strong mixing effects between the configurations. The final fitted parameters for Cs IV are shown in Tables 4.12 and 4.13 respectively.

When it came to Cs V, as one can see, the mean deviation between experimental and calculated levels is quite high. In the odd parity we were once again limited by the small number of known experimental levels and therefore the small number of parameters that could be adjusted. In the even parity, the high mixing effects between the configurations created some struggle in the calculations and that explains the relatively high mean deviation.

The final fitted parameters for Cs V, Cs VI and Cs VII are shown in Tables 4.14, 4.15, 4.16, 4.17, 4.18 and 4.19 respectively.

Configuration	Parameter	HFR (cm^{-1})	Fitted (cm^{-1})	Ratio
$5s^2 5p^4$	E_{av}	27 106.0	28 994.6	
	$F^{2}(5p,5p)$	50541.5	48940.5	0.968
	ζ_{5p}	9793.1	10440.4	1.066

Table 4.12: Fitted parameters for the even parity of Cs IV

5 levels included - mean deviation: 67 cm^{-1}

Configuration	Parameter	HFR (cm^{-1})	Fitted (cm^{-1})	Ratio
$5\mathrm{s}5\mathrm{p}^5$	E_{av}	157106.0	153312.8	
	ζ_{5p}	9784.9	Fixed	
	$G^{1}(5s,5p)$	66532.5	54918.8	0.825
$5s^2 5p^3 5d$	E_{av}	176122.0	174803.3	0.992
	$F^{2}(5p,5p)$	51147.8	38545.1	0.753
	α	0.0	574.0	
	ζ_{5p}	10106.3	10663.4	1.054
	ζ_{5d}	591.3	805.8	0.734
	$F^{2}(5p, 5d)$	38220.1	36281.2	0.949
	$G^{1}(5p, 5d)$	43827.0	36368.3	0.829
	$G^{3}(5p, 5d)$	27526.0	24627.6	0.894
$5s^2 5p^3 6d$	E_{av}	277426.6	269750.8	
	$F^{2}(5p,5p)$	52122.3	44124.4	0.846
	α	0.0	-114.4	
	ζ_{5p}	10528.8	10723.0	1.018
	ζ_{6d}	184.4	246.8	0.747
	$F^{2}(5p,6d)$	10788.6	8503.1	0.788
	$G^{1}(5p, 6d)$	6966.7	6202.2	0.890
	$G^{3}(5p, 6d)$	4911.8	2879.9	0.586
$5s^2 5p^3 7d$	E_{av}	317821.9	314584.5	
	$F^{2}(5p,5p)$	52227.3	Fixed	
	ζ_{5p}	10586.0	Fixed	
	ζ_{7d}	89.0	Fixed	
	$F^{2}(5p,7d)$	4756.9	Fixed	
	$G^{1}(5p,7d)$	2740.9	Fixed	
	$G^{3}(5p,7d)$	2008.0	Fixed	
$5s^2 5p^3 6s$	E_{av}	197178.3	188404.4	
	$F^{2}(5p,5p)$	51687.8	44584.1	0.862
	α	0.0	-95.6	
	ζ_{5p}	10401.4	10723.5	1.030
	$G^{1}(5p, 6s)$	5468.4	3773.5	0.690
$5s^2 5p^3 7s$	E_{av}	281879.2	272894.4	
	$F^{2}(5p,5p)$	52137.7	45064.9	0.864
	α	0.0	-95.6	
	ζ_{5p}	10554.9	10870.9	1.029
	$G^{1}(5\mathrm{p},7\mathrm{s})$	1635.2	1518.9	0.928

Table 4.13: Fitted parameters for the odd parity of Cs IV

87 levels included - mean deviation: 409 cm^{-1}

Table 4.14: Fitted parameters	s for the odd parity of Cs V
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Configuration	Parameter	HFR (cm^{-1})	Fitted (cm^{-1})	Ratio
$5s^2 5p^3$	E_{av}	33234.4	33490.0	0.992
	$F^{2}(5s,5p)$	52316.7	51895.3	0.992
	ζ_{5p}	10631.9	11387.2	1.070

5 levels included - mean deviation: 274 cm^{-1}

Configuration	Parameter	HFR (cm^{-1})	Fitted (cm^{-1})	Ratio
$5\mathrm{s}5\mathrm{p}^4$	E_{av}	164234.4	158905.5	
	$F^{2}(5p,5p)$	52355.0	56316.5	1.075
	ζ_{5p}	10611.1	11100.8	1.046
	$G^{1}(5s,5p)$	68543.9	52750.7	0.769
$5s^2 5p^2 5d$	E_{av}	200130.9	195640.4	
	$F^{2}(5p,5p)$	52802.0	37229.6	0.705
	α	0.0	331.2	
	ζ_{5p}	10906.1	11897.8	1.090
	ζ_{5d}	725.1	509.0	0.701
	$F^{2}(5p, 5d)$	41456.6	40013.2	0.965
	$G^{1}(5p, 5d)$	48122.3	41047.3	0.853
	$G^{3}(5p, 5d)$	30427.6	29968.1	0.985
$5s^2 5p^2 6s$	E_{av}	236198.1	227079.2	
	$F^{2}(5p,5p)$	53308.0	47021.1	0.881
	ζ_{5p}	11225.0	11372.4	1.013
	$G^{1}(5p, 6s)$	6097.3	5705.9	0.935

Table 4.15: Fitted parameters for the even parity of Cs V

42 levels included - mean deviation: 475 cm^{-1}

Table 4.16: Fitted parameters for the even parity of Cs VI

Conngulation	Parameter	$\mathrm{HFR} \ (\mathrm{cm}^{-1})$	Fitted (cm^{-1})	Ratio
$5s^2 5p^2$	E_{av}	33287.9	34432.9	
	$F^{2}(5p,5p)$	53954.4	55236.4	1.023
	ζ_{5p}	11491.6	12070.5	1.050

5 levels included - mean deviation: 97 $\rm cm^{-1}$

Table 4.17: Fitted Parameters for the odd parity of Cs VI

Configuration	Parameter	HFR (cm^{-1})	Fitted (cm^{-1})	Ratio
$5\mathrm{s}5\mathrm{p}^3$	E_{av}	166287.9	161841.7	0.973
	$F^{2}(5p,5p)$	53984.8	51510.7	0.954
	α	0.0	104.6	
	ζ_{5p}	11460.6	12307.5	1.074
	$G^{1}(5s,5p)$	70428.1	59776.0	0.848
$5s^2 5p 5d$	E_{av}	218802.6	213327.8	0.974
	ζ_{5p}	11734.3	12536.3	1.068
	ζ_{5d}	854.3	1155.5	1.353
	$F^{2}(5p, 5d)$	44134.6	43073.4	0.975
	$G^{1}(5p, 5d)$	51670.0	45009.0	0.871
	$G^{3}(5p, 5d)$	32836.8	30719.1	0.935
$5s^2 5p 6s$	E_{av}	270396.1	266502.0	0.985
	ζ_{5p}	12070.8	12878.7	1.067
	$G^{1}(5p,6s)$	6635.0	6876.8	1.036

25 levels included - mean deviation: 166 cm^{-1}

.066
.066
.025
.623
.020
.092
.907
.944
.720
.088
.364
.063
.729
.826
.943
.892
.945
.100
- - - -

Table 4.18: Fitted parameters for the odd parity of Cs VII

42 levels included - mean deviation: 306 cm^{-1}

Table 4.19: Fitted parameters for the even parity of Cs VII

Configuration	Parameter	HFR (cm^{-1})	Fitted (cm^{-1})	LSF [40]	Ratio
$5s5p^2$	E_{av}	150045.0	149023.4	146889.7	
	$F^{2}(5p,5p)$	55500.2	55132.9	51993.7	0.992
	α	0.0	436.6		
	ζ_{5p}	12329.4	13283.5	13363.9	1.077
	$G^{1}(5s,5p)$	72201.2	61700.6	59525.3	0.854
$5s^2 5d$	E_{av}	219126.0	211269.8	210015.6	
	ζ_{5d}	983.6	1359.7	1283.6	1.383
5s5d4f	E_{av}	298318.2	290549.4	290 781.0	
	ζ_{5d}	360.1	277.9	352.0	0.771
	ζ_{4f}	11804.2	13875.7	12803.6	1.175
	$F^{2}(5s, 5d)$	46897.9	39457.6	43120.1	0.841
	$G^{3}(5s,5d)$	31298.4	30502.4	32055.9	0.974
	$G^{2}(5s,5d)$	29570.9	27491.3	32095.5	0.929
	$G^{4}(5s, 5d)$	22348.0	19673.0	17079.0	0.880
	$G^{1}(5d,4f)$	71157.5	51314.3	52195.7	0.721
$5s^2 6s$	E_{av}	286721.3	282484.0	279 901.7	

30 levels included - mean deviation: 172 cm⁻¹

4.3.3 Radiative Transition Rates

Exactly as for the indium ions, once the semi-empirical fit of the radial parameters performed, we calculated the transition probabilities and the oscillator strengths in the caesium ions. We calculated those with a cut-off at log $gf \ge -4$ which led to respectively 251, 163, 83 and 138 transitions in Cs IV, V, VI and VII. The log $gf \ge -1$ led to respectively 63, 73, 52 and 35 transitions listed in Tables A26 (for Cs IV), A28 (for Cs V), A30 (for Cs VI) and A32 (for Cs VII). The small number of transitions⁵ comes from the small number of known experimental levels to perform the fit. Indeed, to be able to give a precise wavelength⁶, the upper and the lower level have to be known experimentally. Therefore the real number of transitions with log $gf \ge -4$ in our calculations is 8778 but among them, a lot include at least one theoretical (i.e. calculated) level which is not known experimentally. Indeed, as highlighted in Tables 4.12, 4.14 and 4.16 in the case of Cs IV and VI only one configuration has experimentally known levels in the even parity and only one in the odd parity in the case of Cs V. Those four tables are nevertheless given in the appendices (as all the 16 transition tables of this section 4).

To our knowledge, those new radiative data are the first ones in the literature concerning gA and $\log gf$ when it comes to Cs IV, V and VI. In Cs VII, Wajid *et al.* [110] performed a MCDHF calculation. However, the points of comparison are too few (only 7 transitions) to draw a conclusion. On these 7 transitions the agreement between the two calculations is about thirty percent which is rather satisfactory. In their work, Wajid *et al.* [110] present only 19 E1 transitions. Our work therefore represents a substantial and consistent contribution of new reliable intense transitions in Cs VII.

For these four ions, what has been achieved in the framework of this thesis is therefore very innovative since it has been carried out for the first time and provides numerous reliable radiative data that were previously non-existent (to our knowledge) in the literature. We therefore hope that these new data will allow the identification of caesium spectral lines in the spectrum of RE0503-289.

⁵In comparison with Cu IV-VII or In IV-VII for example.

⁶We chose to give the Ritz wavelength for all the transitions given in this section.

4.4 Ag IV-VII

The last element we studied in this chapter is silver (Z = 47). Its symbol, Ag, comes from the Latin word *argentum* meaning shiny [111]. The exact origin of the name silver in English is quite blurred. It appears in Old English with different spelling: *seofor* or *siolfor*. Similar words are found in Old High German, Gothic and the Celtic languages. The Balto-Slavic words for silver are very similar to these Germanic ones suggesting a very old origin. This would seem logical as silver has been known by Humanity since the neolithic age. This precious malleable metal is white and shiny. Dedicated to the Moon or to the lunar goddess Artemis/Diane, it has been among the seven sacred metals since Antiquity, well known and even overvalued by medieval alchemy. It is known for the multi-millennial manufacture of jewels, coins, as well as for its increasing industrial applications in the 20th century.

The experimental data used for the semi-empirical fits found in the literature, for the ions Ag IV, V, VI and VII ions are, respectively, Ankita and Tauheed [41] in Ag IV, Kildiyarova *et al.* [42] and Van Kleef *et al.* [43] in Ag V, Joshi *et al.* [44] in Ag VI and Ryabtsev and Kononov [45] in Ag VII. The configuration models built are based on the models we made for indium (In) ions. This choice comes from the fact that, as it turns out , In VI is isoelectronic with Ag IV. The model that we have built for Ag IV has been constructed in a similar way to the one existing for In VI, and those for Ag V, VI and VII have been built by gradually removing a 4d electron to the model of the previous ion.

4.4.1 Models Used

The model for each silver ion consists of the configurations necessary to describe it (the set of these configurations is also called configuration interaction model), the dipole polarizability of the core and the cut-off radius describing the core-polarization. These parameters are introduced in the *ab initio* procedure, and the radial parts of the single-electron wave functions are then calculated following the self-consistent field procedure.

Ag IV being isoelectronic with In VI, we have taken the model describing the latter ion, but we added the configurations $4d^77s$, $4d^77d$ and $4d^77p$, in order to further improve our representation of the configuration interaction. The configurations we introduced in the model are namely: $4d^8$, $4d^75s$, $4d^75d$, $4d^65s^2$, $4d^76s$, $4d^76d$, $4d^65p^2$, $4d^77s$, $4d^77d$ and $4d^65s5d$ for the even parity and $4d^75p$, $4d^74f$, $4d^65s5p$, $4d^76p$, $4d^75f$, $4d^65s6p$, $4d^77p$ and $4d^65s5f$ for the odd one.

To describe the core-valence interactions, we considered that the last orbital of the ionic core is the 4d. We therefore took the average radius of the 4d subshell (from our HFR calculations) as the cut-off radius, which is equal to 1.2 a_0 . The polarization parameters of the core are those corresponding to an Ag VI ($4d^6$)-type ionic core (chosen to represent at best double excitations of electrons from the core to the valence electrons), which for the dipolar polarizability (from [94]) corresponds to α_d equal to 2.23 a_0^3 . The methodology explained above was the same for the following ions, and the values of r_c and α_d is modified each time to best represent the problem. The configurations of Ag IV for which there are experimentally known energy levels are $4d^8$, $4d^75s$, $4d^75d$ and $4d^76s$ for even parity, and $4d^75p$ for odd parity. The fundamental is a $4d^8$ 3F_4 state.

This led to mean deviations between the experimental and calculated energy levels of respectively 103 cm^{-1} and 159 cm^{-1} for the even and the odd parity as shown in Tables A33 and A34.

The configuration model used for Ag V is realized by removing an electron from the 4d layer of the Ag IV model. That means that the configurations introduced in the model are: $4d^7$, $4d^65s$, $4d^65d$, $4d^55s^2$, $4d^66s$, $4d^66d$, $4d^55p^2$, $4d^67s$, $4d^47d$ and $4d^55s5d$ for the

even parity and $4d^{6}5p$, $4d^{6}4f$, $4d^{5}5s5p$, $4d^{6}6p$, $4d^{6}5f$, $4d^{5}5s6p$, $4d^{6}7p$ and $4d^{5}5s5f$ for the odd one.

In the case of Ag V, the value of r_c from our calculations is 1.16 a_0 . α_d is equal to 1.69 a_0^3 ([94]) and corresponds to an Ag VII core (4 d^5). The configurations of this model whose energy levels are known experimentally are 4d⁷ and 4d⁶5s for the even parity, and 4d⁶5p for the odd parity. The fundamental of the atomic system is ${}^{4}F_{9/2}$.

Those fits led to average deviations between the experimental and calculated set of energy levels of respectively 138 cm^{-1} and 134 cm^{-1} for the even and the odd parity as shown in Tables A36 and A37.

The configurations we introduced in our model for Ag VI are: $4d^6$, $4d^55s$, $4d^55d$, $4d^45s^2$, $4d^56s$, $4d^56d$, $4d^45p^2$, $4d^57s$, $4d^37d$ and $4d^45s5d$ for the even parity and $4d^55p$, $4d^54f$, $4d^45s5p$, $4d^56p$, $4d^55f$, $4d^45s6p$, $4d^57p$ and $4d^45s5f$ for the odd one.

This time, core-polarization effects are considered using a polarizability α_d equal to 1.35 a_0^3 (Ag VIII core - 4d⁴) and a cut-off radius equal to 1.12 a_0 . The configurations of this model whose energy levels are known experimentally are 4d⁶ for the even parity, and 4d⁵5p for the odd parity. The fundamental of the atomic system is an energy level of configuration 4d⁶ 4D_4 .

The mean deviations between the experimental and calculated energy levels were found to be 198 cm^{-1} and 116 cm^{-1} for the even and the odd parity respectively, as one can see in Tables A39 and A40.

The configurations that we considered in our calculations for Ag VII are respectively $4d^5$, $4d^45s$, $4d^45d$, $4d^35s^2$, $4d^46s$, $4d^46d$, $4d^35p^2$, $4d^47s$, $4d^47d$, $4d^35s5d$ for the even parity and $4d^45p$, $4d^44f$, $4d^35s5p$, $4d^46p$, $4d^45f$, $4d^35s6p$, $4d^47p$, $4d^35s5f$ for the odd one.

Core-polarization was here taken into account by using a dipole polarizability α_d equal to 1.08 a_0^3 (Ag IX core - 4d³) and r_c equal to 1.09 a_0 . The configurations of this model whose energy levels are known experimentally are 4d⁵ for even parity, and 4d⁴5p for odd parity. The fundamental is 4d⁵ ${}^{6}S_{5/2}$.

The average deviations between the experimental and calculated energy levels resulting from our calculations were 144 cm⁻¹ and 129 cm⁻¹ for the even and the odd parity respectively, as highlighted in TablesA42 and A43.

4.4.2 Atomic Radial Parameters

The radial parameters obtained by our calculations are listed in Tables 4.20 and 4.21 for Ag IV, 4.22 for Ag V, 4.23 for Ag VI and 4.24 for Ag VII.

Configuration	Parameter	$\mathrm{HFR}~(\mathrm{cm}^{-1})$	Fit (cm^{-1})	Ratio
$4d^{8}$	E_{av}	14214.0	13526.6	
	$F^{2}(4d, 4d)$	72568.5	67253.0	0.935
	$F^{4}(4d, 4d)$	47717.9	46369.9	0.975
	α	0	348	
	β	0	0	
	ζ_{4d}	1927.3	2 001.6	1.039
$4d^{7}5s$	E_{av}	124858.5	122845.5	
	$F^{2}(4d, 4d)$	74813.2	68754.2	0.912
	$F^{4}(4d, 4d)$	49362.3	48558.9	0.982
	α	0	400	
	β	0	-4138	
	ζ_{4d}	$2\ 039.6$	21.253	1.040
	$G^{2}(4d, 5s)$	14051.3	133.459	0.946
$4d^{7}6s$	E_{av}	279447.7	280303.2	
	$F^{2}(4d, 4d)$	75658.5	70768.2	0.932
	$F^{4}(4d, 4d)$	49992.1	47935.9	0.966
	α	0	0	
	β	0	0	
$4d^{7}5d$	E_{av}	269921.8	272607.1	
	$F^{2}(4d, 4d)$	75653.5	70923.1	0.946
	$F^{4}(4d, 4d)$	49 989.4	49354.2	0.986
	α	0	0	
	β	0	0	
	ζ_{4d}	2069.9	2124.4	1.026
	ζ_{5d}	203.9	196.8	0.962
	$F^{2}(4d, 5d)$	12863.3	11236.8	0.875
	$F^{4}(4d, 5d)$	5537.7	3960.8	0.715
	$G^{0}(4d, 5d)$	3351.5	3586.6	1.076
	$G^{2}(4d, 5d)$	3872.7	4144.3	1.076
	$G^{4}(4d, 5d)$	3112.6	3330.8	1.072

Table 4.20: Radial parameters for the even configurations of Ag IV $\,$

74 levels included - mean deviation: 103 cm^{-1}

Configuration	Parameter	$\mathrm{HFR}~(\mathrm{cm}^{-1})$	Fit (cm^{-1})	Ratio
$4d^75p$	E_{av}	189157.3	187829.3	
	$F^{2}(4d, 4d)$	75113.2	68520.9	0.912
	$F^{4}(4d, 4d)$	49586.1	48204.8	0.972
	α	0	415	
	β	0	-3254	
	ζ_{4d}	2051.3	2140.5	1.043
	ζ_{5p}	306.6	346.2	1.129
	$F^{2}(4d,5p)$	24280.9	22900.3	0.943
	$G^{1}(4d,5p)$	8661.5	8180.2	0.944
	$G^{3}(4d, 5p)$	7731.3	6542.4	0.846

Table 4.21: Radial parameters for the odd parity of Ag IV $\,$

110 levels included - mean deviation: 159 cm^{-1}

Table 4.22: Radial Parameters for Ag V $\,$

Configuration	Parameter	HFR	Fit	Ratio
Even				
$4d^{7}$	E_{av}	24627.7	23504.8	
	$F^{2}(4d, 4d)$	75959.1	70981.6	0.934
	$F^{4}(4d, 4d)$	50214.7	49726.6	0.990
	α	0	386	
	β	0	-5672	
	ζ_{4d}	20836	21404	1.027
$4d^{6}5s$	E_{av}	174254.6	171195.4	0.983
	$F^{2}(4d, 4d)$	77964.4	72471.0	0.930
	$F^{4}(4d, 4d)$	51688.2	49686.9	0.866
	α	0	484	
	β	0	-4412	
	ζ_{4d}	2196.1	2310.0	1.051
Odd				
$4d^{6}5p$	E_{av}	247668.7	245697.6	
	$F^{2}(4d, 4d)$	78211.5	72095.5	0.921
	$F^{4}(4d, 4d)$	51873.5	49443.3	0.953
	α	0	48	
	β	0	-2957	
	ζ_{4d}	2207.0	2309.6	1.046
	ζ_{5p}	3919.2	44732	1.141
	$F^{2}(4d,5p)$	27492.3	25970.9	0.945
	$G^{1}(4d, 5p)$	9451.7	9142.1	0.968
	$G^{3}(4d,5p)$	8704.3	7632.6	0.876

Even Parity: 78 levels (mean deviation: 138 cm^{-1}) Odd Parity: 175 levels (mean deviation: 134 cm^{-1})

Configuration	Parameters	HFR	Fit	Ratio
Even				
$4d^{6}$	E_{av}	35313.2	33808.8	
	$F^{2}(4d, 4d)$	79035.2	74116.7	0.938
	$F^{4}(4d, 4d)$	52488.9	50919.7	0.971
	α	0	41.2	
	β	0	-438.3	
	ζ_{4d}	2242.5	2363.3	1.054
Odd				
$4d^{4}5p$	E_{av}	300000	305117.7	
	$F^{2}(4d, 4d)$	81063	74779.5	0.922
	$F^{4}(4d, 4d)$	53984.8	53334.7	0.988
	α	0	0	
	β	0	0	
	ζ_{4d}	2365.8	2470.1	1.044
	ζ_{5p}	4788.2	5348.4	1.117
	$F^{2}(4d,5p)$	30380.2	29089.3	0.957
	$G^{1}(4d, 5p)$	10124.2	9432.6	0.931
	$G^{3}(4d.5p)$	9557.5	9085.4	0.951

Table 4.23: Radial parameters for Ag VI

Even Parity: 30 levels (mean deviation: 198 cm^{-1}) Odd Parity: 110 levels (mean deviation: 116 cm^{-1})

Table 4.24:	Radial parameters for Ag VI	[

Configuration	Parameter	HFR	Fit	Ratio
Even				
$4d^5$	E_{av}	55219	52621	0.953
	$F^{2}(4d, 4d)$	81891.4	76836.8	0.938
	$F^{4}(4d, 4d)$	55166.7	54120.5	0.981
	α	0	40.9	
	β	0	-535.7	
	ζ_{4d}	2406	2474	1.028
Odd				
$4d^{4}5p$	E_{av}	375533.1	374230.7	
	$F^{2}((4d, 4d))$	83678	77934.9	0.931
	$F^{4}(4d, 4d)$	55924.1	55160.7	0.986
	α	0	46.4	
	β	0	-636.6	
	ζ_{4d}	2524.4	2630.3	1.042
	ζ_{5p}	5681.5	6303.9	1.109
	$F^{2}(4d,5p)$	33076.5	31370.5	0.948
	$G^{1}(4d, 5p)$	10756.1	10368.3	0.964
	$G^{3}(4d, 5p)$	10356	9336.2	0.901

Even Parity :34 levels (mean deviation: 144 cm^{-1}) Odd Parity : 143 levels (mean deviation: 183 cm^{-1})

4.4.3 Radiative Transition Rates

Exactly as for the previous elements, the tables containing the radiative transition rates of Ag IV, V, VI and VII are in the appendices. Once again, the calculations were performed in order to obtain all the transitions with $\log gf \geq -4$ (2989 transitions for Ag IV, 5319 for Ag V, 2168 for Ag VI and 2232 for Ag VII), but only the most intense ones with $\log gf \geq$ -1 are given in Tables A35 (615 transitions), A38 (915 transitions), A41 (362 transitions) and A44 (441 transitions) for Ag IV,V, VI and VII respectively.

One should note that for Ag V and Ag VI, even if the transitions have been measured (with their transition rates), no transition probability is available in the literature. For Ag IV, Ankita and Tauheed [41] performed a HFR calculation to obtain gA but with a more restricted model without core polarization. Figure 4.4.3 shows the comparison between our data for the most intense Ag IV lines and the ones of [41]. As expected, our values are systematically lower than theirs due to the addition of the core-polarization effects.



Figure 4.8: Comparison between the gA (in 10^9s^{-1})obtained by our HFR+CPOL calculations and the former calculation of Ankita and Tauheed [41] for the Ag IV ion. The straight line of equality is drawn in red.

For Ag VII, our theoretical gA are compared to gA obtained by Ryabtsev and Kononov [45] in figure 4.9. This figure shows the good agreement between the values. Again, as discussed for example for copper ions, in their calculations they introduced some corevalence interactions (e.g. considering configurations like $4d^35s^2$) that are actually included in our core polarization potential. It would seem that this time, given the good agreement between our data, these interactions that they explicitly consider are clearly the most important ones. However, we see a tendency for our values to be slightly lower than theirs suggesting that there are indeed core-valence interactions that have not been included in their model, making ours more complete.



Figure 4.9: Comparison between HFR intense gA (in $10^9 s^{-1}$) and experimental ones from [45] for the Ag VII ion. The straight line of equality is drawn in green

4.5 Conclusion - Applications

In the context of the collaboration with astrophysicists from the University of Tübingen, our new results were sent to them so that they could incorporate them in their NLTE models of synthetic spectra in order to identify new lines in the spectra of white dwarfs, and in particular of RE0503-289. These analyses led to the identification of Cu IV-VII lines as mentioned in Section 4.1.3.1 and were published in [77]. The other ions shown in this section are currently being analyzed by our colleagues and we hope that this will also lead to the new identifications of spectral lines in white dwarfs spectra.

The collaboration between the University of Tübingen and the University of Mons had begun before the start of this thesis and had already been performed calculations and line identifications in the spectrum of RE0503-289 in several TIE (in their third to sixth ionization stages) represented by the green boxes in the Mendeleev table shown in Figure 4.10. The elements for which we have done the full atomic calculations, and for which we presented the detailed results in the previous subsections, are represented by the red frames. The blue boxes represent elements for which the calculations are in progress and in direct collaboration between the two universities. The calculations and the semiempirical adjustments are carried out in Tübingen and the addition of the corrections of polarization of the ionic core are made by ourselves in Mons. Those elements are a work in progress and we do not have the results with the synthetic spectra yet. We do not present the detailed results for those ions (Sn IV-VII, Sb IV-VII, I IV-VII, Rb IV-VII and Y IV-VII) in this thesis since, as mentioned earlier, we have only performed a small part of the calculations.

However, we hope that these outgoing calculations, which are still in progress, are an open door to continue this collaboration between the two universities.

1 IA 1A		Periodic Table of the Elements													18 VIIIA 8A		
1 *1 H Hydrogen	2 IIA 2A							Atomic Number	Valence Charge			13 IIIA 3A	14 IVA 4A	15 VA 5A	16 VIA 6A	17 VIIA 7A	2 ° He Helium 4.003
3 +1 Lithium 6.941	4 Beryllium 9.012							Syn	nbol _{me}			5 *3 B Boron 10.811	6 +4.4 Carbon 12.011	7 Nitrogen 14.007	8 -2 Oxygen 15.999	9 -1 F Fluorine 18.996	10 ° Neon 20.180
11 *1 Na Sodium 22.990	12 *2 Mg Magnesium 24.305	3 IIIB 3B	4 IVB 4B	5 VB 5B	6 VIB 6B	7 VIIB 7B	8	9 	10	11 IB 1B	12 IIB 2B	13 *3 Aluminum 26.982	14 *4 Silicon 28.086	15 +5.+33 P Phosphorus 30.974	16 +6.2 Sulfur 32.085	17 -1 Cl Chlorine 35.453	18 0 Argon 39.948
19 *1 K Potassium 39.088	20 +2 Ca Calcium 40.078	21 *3 Scandium 44.966	22 *4 Ti Titanium 47.867	23 +5,+4,+3 V Vanadium 50,942	24 *6.+3.+2 Cr Chromium 51.996	25 +7,+4,+2 Mn Manganese 54,938	26 Fe Iron 55.845	27 +3,+2 Co Cobalt 58,933	28 +2 Nickel 58.693	29 +2.+1 Cu Copper 63.546	30 *2 Zn Zinc 65.38	31 *3 Gallium 68.723	32 *4 Ge Germanium 72.631	33 +5,+3 Ass Arsenic 74.922	34 +42 See Selenium 78.971	35 +51 Br Bromine 79.904	36 ° Kr Krypton 84.788
37 *1 Rb Rubidium 84.468	38 +2 Sr Strontium 87.62	39 +3 Y Yttrium 88.908	40 *4 Zr Zirconium 91.224	41 *5 Nobium 92,906	42 +6.+4 Mo Molybdenum 95.95	43 Tc Technetium 98.907	44 +4,+3 Ru Ruthenium 101.07	45 *3 Rhodium 102,906	46 +4,+2 Pd Palladium 108.42	47 *1 Ag Silver 107.868	48 +2 Cd Cadmium 112.414	49 *3 In Indium 114.818	50 +2,4 Sn Tin 118.711	51 *3 Sb Antimony 121.780	52 Te Tellurium 127.6	53 *51 Iodine 126.904	54 ° Xenon 131.294
55 *1 Cs Cesium 132.905	56 *2 Ba Barium 137.328	57-71	72 *4 Hf Hafnium 178.49	73 *5 Ta Tantalum 180.948	74 *6.+4 W Tungsten 183.84	75 +5,+4,+3 Re Rhenium 186,207	76 *4 Osmium 190.23	77 +4,+3 Ir Iridium 192,217	78 +4.+2 Pt Platinum 195.085	79 *3 Au Gold 196,967	80 *2.+1 Hg Mercury 200.592	81 *3.+1 TI Thallium 204.383	82 +2 Pb Lead 207.2	83 *3 Bismuth 208.960	84 +4 Po Polonium [208.982]	85 ⁻¹ At Astatine 209.987	86 ⁰ Rn Radon 222.018
87 *1 Fr Francium 223.020	88 *2 Radium 225.025	89-103	104 *4 Rf Rutherfordium	105 unk Db Dubnium	106 unk Sg Seaborgium	107 ^{unk} Bh Bohrium	108 unk HS Hassium	109 unk Mt Meitnerium	110 unk DS Darmstadtium	111 unk Rg Roentgenium	Copernicium	113 unk Uut Ununtrium unknown	114 unk FI Flerovium	115 unk Uunpentium unknown	116 unk Lv Livermorium	117 unk Uus Ununseptium unknown	118 unk Uuuo Ununoctium unknown
	Lantha Seri Actin	anide es Lantr 138 89	a anum 1905 *3	*3 59 Fium Praseo 116 *4 91	*3 60 Pr N dymium Neody 144 *5 92	* ³ 61 Prom 243 *6 93	*3 62 8 S 8 S 1.013 15 10 P	*3 63 arium 0.36 Euro 57.+4 95	U pium 964 *3 96	⁺³ 65 T Teri 725 ⁺³ 97	b b bium 1025 +3 98	*3 67 H Holi 500 *3 99	*3 68 nium .930 *3 100	*3 69 T Thu 250 *3 101	m ⁺³ 70 Yttei 934 *3 102	⁺³ 71 ⁺ L ⁺² 103	+3 tium .967 +3
	Seri	es Acti	nium Tho	rium Prota 2.038 23	ctinium Urar 0.036 238	nium Nept	unium Plute 24	Dilum Ame 1.064 243	icium Cu .061 243	rium Berk 7.070 243	elium 7.070 251	rnium Einsto 080 p2	54) 557	nium Mende	levium Nob 8.1 259	elium 2,101 [2	ncium 821

Figure 4.10: TIEs treated in collaboration with the University of Tübingen for the purpose of white dwarfs analysis - Original picture from: sciencesnote.org (©Todd Helmenstine)

Chapter 5

Radiative Decay Rates in Neutral and Singly Ionized Atoms for Stellar Nucleosynthesis Analyses

As we already mentioned in the previous chapters, abundances of heavy elements can provide crucial information about the conditions required for the formation of such elements. Those informations can be used to corroborate the theory of the nucleosynthesis described in Section 1.2. Precise radiative parameters such as transition probabilities and oscillator strengths of these heavy elements are, of course, mandatory for line identifications from which elemental abundances in stellar spectra can be determined.

This is what motivated us to undertake calculations in these elements exactly as for the two previous chapters. But, in this chapter, under the impulse of an experimental group looking for a theoretical backup to their measurements, these calculations have been combined with their experimental measurements in order to produce semi-empirical atomic data. This experimental group with whom we produced new semi-empirical data is located in the Jilin University in China. In collaboration with them, we produced data in neutral rhodium, barium, rhenium, iridium and singly ionized iridium. The astrophysical applications of each of those elements will be described in the associated sections.

In this chapter, we will therefore first describe the technique used by our collaborators for the experimental measurements. This technique is the time-resolved laser-induced fluorescence (TR-LIF) technique. We will then, as we did in the previous chapters, present our theoretical models and the results we obtained for the various ions treated in this collaboration with the University of Jilin. Those ions will be presented in a decreasing atomic number (Z) order starting with neutral and once ionized iridium¹ (Z = 77), then rhenium (Z = 75), lanthanum (Z = 57), barium (Z = 56) and finishing with rhodium (Z = 45).

The goal of this analysis was to produce a new set of semi-empirical gA- and gf-values in collaboration with the experimental group of the University of Jilin in China. Indeed, they performed some precise radiative lifetime measurements that we combined to our theoretical branching fractions (BFs) B_{ki} to get gA-values using the formula:

$$A_{ki} = \frac{B_{ki}}{\tau_k} \tag{5.1}$$

where k and i represent the upper and lower levels. The gf are obtained with:

$$gf = g_{ik}f = 1.4992 \times 10^{-16} \lambda^2 g_k A_{ki}$$
(5.2)

This technique can be seen as a normalization of HFR+CPOL gA-values using the experimental lifetimes. This method is effective when branching fractions cannot be

¹For which both neutral an singly ionized stages have been treated during this thesis.

measured for all depopulating transitions of the same upper level because the available experimental spectra do not cover the whole range of wavelengths where all lines involving the concerned level are supposed to appear. If the sum of all the intensities of all these lines is not negligible, its omission introduces a systematic error in the experimentally deduced transition probabilities. It is worth noting that the sum of the missing intensities is often estimated by experimentalists using theoretical methods, such as the HFR approach (see e.g. Sikström *et al.* [112]). Let us add that, in our work, we were mainly interested in highly excited levels for each of the elements considered. As these levels are depopulated by numerous transitions appearing in different regions of the electromagnetic spectrum, it was impossible to measure all the branching fractions because of the (partial or even total) lack of experimental spectra. The only way to obtain a reliable and consistent set of transition probabilities was therefore to combine the measured TR-LIF lifetimes with the theoretical HFR+CPOL branching fractions.

5.1 Lifetime Measurements

The lifetime, τ_i of an excited level *i* can be measured by studying the population decay of its population N_i ,

$$N_i(t) = N_i(0)e^{-t/\tau_i}.$$
(5.3)

Another way to investigate the lifetime of an excited level is by observing its fluorescent decay:

$$I(t) = -c\frac{dN_i}{dt} = I(0)e^{-t/\tau_i}$$
(5.4)

where c is a positive constant. By observing the time-resolved fluorescence signal I(t) from an excited level, its lifetime can simply be obtained by fitting an exponential to the measured decay curve.

5.1.1 TR-LIF Spectroscopy Technique

In order to investigate atomic lifetimes, a short-pulse excitation is used, shortly followed by a fast time-resolved detection of the fluorescence de-excitation.

During the excitation with the laser pulse, the population of the upper level (for a two-level system) is given by:

$$\frac{dN_2(t)}{dt} = B_{12}\rho(\nu, t).N_1(t) - [B_{21}.\rho(\nu, t) + A_{21}].N_2(t)$$
(5.5)

where B_{12} and B_{21} are the Einstein coefficients for absorption and stimulated emission and A_{21} is the spontaneous emission transition probability. $\rho(\nu, t)$ is the spectral energy density of the excitation laser and N_1 is the population of the lower level.

If $N_1(t) >> N_2(t)$, N_1 can be considered as a constant and Eq. 5.5 becomes:

$$\frac{dN_2(t)}{dt} = B_{12}\rho(\nu, t).N_1 - [B_{21}.\rho(\nu, t) + A_{21}].N_2(t)$$
(5.6)

If the lifetime of the upper level is much longer than the excitation laser pulse duration and the response of the detection system, as the example shown in Figure 5.1.1, then, after the pulse has disappeared (i.e. $\rho \approx 0$), Eq. 5.6 finally becomes

$$\frac{dN_2(t)}{dt} = -A_{21}N_2(t) \tag{5.7}$$

which can easily be integrated to an equation similar to Eq. 5.4 and the lifetime can therefore be obtained by a pure exponential fit of the measured fluorescence decay curve.



Figure 5.1: Example of a measurement with a laser pulse duration much shorter than the radiative lifetime.

If the lifetime is comparable to the laser pulse duration or to the response of the detection system, it becomes a bit more tricky. In that case, Eq. 5.6 becomes something like:

$$I(t) = C \int_{-\infty}^{t} P(t') E(t - t') dt'$$
(5.8)

where I(t) is the fluorescence intensity (as in equation 5.4), C a constant P(t) is the laser pulse shape and is proportional to $\rho(\nu, t)$. E(t) is the fluorescence decay curve for an instantaneous excitation and is equal to $e^{-t/\tau}$ if $t \ge 0$ or to 0 otherwise. This leads to

$$I(t) = C.P(t) \otimes E(t) \tag{5.9}$$

which means that the fluorescence curve of interest is the convolution between the laser pulse shape and an exponential decay with instantaneous excitation. In order to take every parameter into account, the instrumental response must be taken into account through R(t) (i.e. the experimental response function):

$$I(t) = C.[P(t) \otimes E(t)] \otimes R(t)$$
(5.10)

Since the excitation laser pulse is detected with the same detection system we can actually define

$$P_{PR}(t) = P(t) \otimes R(t) \tag{5.11}$$

and therefore equation 5.10 becomes:

$$I'(t) = C.E(t) \otimes P_{PR}(t) \tag{5.12}$$

This means that the recorded fluorescence signal can be expressed as a convolution between the recorded excitation laser pulse and a pure exponential. In practical conditions, the exciting laser pulse is recorded at the same time as the fluorescence decay curve. Therefore, by fitting this fluorescence signal to the convolution of the detected laser pulse and a pure exponential decay, the effects of the duration of the excitation laser pulse and the response time of the detector are taken into account.
5.1.2 Experimental Setup



Figure 5.2: Typical TR-LIF experimental setup used for lifetime measurements.

A typical experimental setup used for lifetime measurements is shown in Figure 5.2. In order to produce a sufficient density of atoms in metastable states in order to take precise measurements, a laser-produced plasma obtained with a laser ablation on a pure sample (a 99.8% pure tin (Sn) sample is used in the figure) is employed as an atomic source.

As shown in [113, 114], this technique is suitable, efficient and reliable for lifetime measurements. A 5 mJ 532 nm pulse, with approximately 8 ns duration, emitted by a Q-switched Nd:YAG laser working at a 10 Hz repetition rate, is focused on a thin target, fixed on a rotating platform with a rotation speed appropriate to ensure an ablation position different for each laser pulse. A dye laser with linear polarization is used for the excitation. The linewidth of this dye laser is around 0.08 cm⁻¹.

The light emitted by the excitation laser ($\approx 5-7$ ns pulse duration) is sent horizontally throughout the vacuum chamber, where it interacts with a vertical atomic beam about 10 mm above the target. The interval between the excitation and ablation pulses can be adjusted by a digital delay generator. Following that excitation, the fluorescence signal is focused into a grating monochromator by a convex silica lens in a perpendicular direction to the laser and to the atomic beam. It is afterwards detected by a photomultiplier tube (PMT). In the experiments performed at University of Jilin, the monochromator was placed by rotating it 90 degrees, so that its entrance slit was horizontal and parallel to the excitation beam in order to enhance the fluorescence collection efficiency. A spectral filter, which cuts the light with a tunable wavelength limit (e.g. 300 nm), is used between the lens and the monochromator to prevent the cascade fluorescence at about the chosen limit (in our example 320 nm). Since the levels are selectively excited by the laser, there are no cascade emissions from higher excitation levels [115].

The time-resolved fluorescence photo-current signal from the PMT is registered by a 500 MHz digital oscilloscope which is triggered by the excitation laser with a photoelectric diode. This oscilloscope is connected to a computer in which the experimental data can be stored and analyzed as shown in Figure 5.2.

The data we obtained using HFR + CPOL concerning Ir I and II (Sections 5.2.1 and 5.2.2), Re I (Section 5.3), Ba I (Section 5.5), and Rh I (Section 5.6) have been combined to the experimental data obtained using the technique described here above by our collaborators at the University of Jilin in China.

5.2 Ir I-II

Iridium (Z = 77) was discovered in 1803 by Smithson Tennant in London. Its name comes from the Latin *iris* meaning rainbow, because of its compounds which are very colorful [109, 116].

In astrophysics, the accuracy of stellar chemical abundances largely depends on the adequacy and accuracy of the atomic radiative and structure data. In the case of iridium (Z = 57), there are two stable isotopes, ¹⁹¹Ir and ¹⁹³Ir, with relative abundances of 37.3% and 62.7% on the Earth. Ir abundances in stars are of great significance not only in radioactive cosmochronology, but also in the structure and nucleosynthetic evolution of supernovae originating from the first stellar generation (see Ivarsson *et al.* [117]).

Indeed, during the last decades, high-resolution near-ultraviolet spectra from the Hubble Space Telescope were used to detect the rapid neutron-capture (r-process) elements (like osmium, iridium and platinum) in r-process enriched stars such as some metal-poor halo stars and chemically peculiar (CP) stars (see e.g. [118, 119, 120]). The abundances of these heavy elements provide valuable information about the conditions required for the formation of these elements in the supernovae, merging neutron stars, and about the atmospheric processes that lead to anomalies in spectra of CP stars, and these elements are more appropriate for the age dating of the oldest stars than the lighter elements [119, 121, 122]. Once again, as we mentioned in Section 1, the radiative parameters such as transition probabilities or oscillator strengths of atoms and ions of these heavy elements are, of course, crucial for the determination of elemental abundances.

Until now in the previous sections, we have only presented purely theoretical data. Another reliable and convenient method to obtain oscillator strengths is through the combination of measured radiative lifetimes with reliable branching fractions (BFs). I ridium (Z = 77) is a heavy element only produced in the r-process and its neutral and once ionized spectra are detected in many stars, for example the CP star χ Lupi [122], or for the MP halo star HD 160617 [119] and many others.

5.2.1 Ir I

Twelve even- and nine odd-parity configurations were explicitly included in our theoretical calculations, namely $5d^76s^2$, $5d^76p^2$, $5d^76d^2$, $5d^76s7s$, $5d^76s6d$, $5d^66s^27s$, $5d^66s^26d$, $5d^66s6p^2$, $5d^86s$, $5d^87s$, $5d^86d$ and $5d^9$ in the even parity and $5d^76s6p$, $5d^76s7p$, $5d^76s5f$, $5d^76s6f$, $5d^66s^26p$, $5d^86p$, $5d^87p$, $5d^85f$ and $5d^86f$ in the odd one. The core-polarization effects were estimated using the dipole polarizability reported by Fraga [94] for an Ir IV ionic core, i.e. $\alpha_d = 6.48 \ a_0^3$, and a cut-off radius $r_c = 1.60 \ a_0$, corresponding to the expected value of < r > for the outermost core orbital (5d), as obtained with the HFR method. Moreover, a semi-empirical fitting procedure was applied to the radial parameters related to the $5d^76s^2$, $5d^86s$, $5d^9$, $5d^76s6p$, $5d^66s^26p$ and $5d^86p$ configurations. It is important to note that the energy levels above $50000 \ \text{cm}^{-1}$ were not included in the fit because many of them were found to be strongly mixed with unknown levels which made very doubtful the correspondence between the calculated energies and the available experimental values. For this reason, our HFR+CPOL calculations of the atomic structure and radiative parameters in Ir I were limited to the energy levels situated below 50000 cm⁻¹.

The goal of this analysis was to produce a new set of semi-empirical gA- and gf-values in collaboration with the experimental group of the University of Jilin in China. Indeed, they performed some precise radiative lifetime measurements that we combined to our theoretical branching fractions (BFs).

Using the theoretical branching fractions and the experimental lifetimes, we deduced

the transition probabilities and oscillator strengths for all the lines depopulating the oddparity levels below 50000 cm⁻¹. The results obtained are reported in Table 5.1. In that table 134 Ir I spectral lines are to be found in a wavelength range going from 205 to 418 nm. As far as we know, transition probabilities were experimentally measured by Gough *et al.* [123] for only two transitions among those considered in the present work. These are found to be in good agreement (within 20%) with our values.

Upper Level ^a	Lower Level ^a	λ_{air} (nm)	BF	$gA (10^6 s^{-1})$		log gf	
$E (cm^{-1})$	$E (cm^{-1})$	/		This work	Previous ^b	This work	Previous ^c
12 (cm	L (cm			rino worn	Tierious	1 mo work	Trevious
22512 42	0	207 476	0.1	2 80 (E)		228 (F)	2.24
= () = 245(11)	2024.00	226 040	0.1	2.09 (E)		-2.36(E)	-2.34
τ (ns) = 345(11)	2034.90	330.848	0.21	0.09(D+)		-1.98 (D+)	-1.96
	6323.91	381.724	0.17	4.93 (E)		-1.97 (E)	-1.96
	7106.61	393.484	0.51	14.7 (D+)		-1.47 (D+)	-1.45
22271 12	0004.00	000.050	0.0	005 (D)	100.0	0.40 (D)	0.47
33874.43	2834.98	322.078	0.8	225 (B)	192.9	-0.46 (B)	-0.47
τ (ns) = 28.4(6)	6323.91	362.867	0.06	16.9 (E)	22.7	-1.48 (E)	-1.51
				100 (5)			
35540.34	4078.94	317.758	0.6	12.8 (D+)		-1.71 (D+)	
τ (ns) = 281(15)	7106.61	351.594	0.23	4.91 (D+)		-2.05 (D+)	
37446.13	4078.94	299.609	0.44	13.6 (D+)		-1.74 (D+)	-1.7
τ (ns) = 194(15)	5784.62	315.75	0.11	3.40 (E)		-2.29 (E)	-2.28
	6323.91	321.221	0.11	3.40 (E)		-2.28 (E)	-2.36
	9877.54	362.629	0.22	6.80 (D+)		-1.87 (D+)	-1.85
	11831.09	390.285	0.09	2.78 (E)		-2.20 (E)	-2.16
40524.73	5784.62	287.768	0.3	58.8 (D+)		-1.14 (D+)	
τ (ns) = 20.4(14)	9877.54	326.2	0.15	29.4 (E)		-1.33 (E)	
	10578.68	333.838	0.19	37.3 (E)		-1.21 (E)	
	12505.68	356.798	0.07	13.7 (E)		-1.58 (E)	
	12951.67	362.57	0.1	19.6 (E)		-1.41 (E)	
	16565.35	417.255	0.14	27.4 (E)		-1.14 (E)	
41522.22	4078.94	266.992	0.16	57.1 (E)		-1.21 (E)	
τ (ns) = 16.8(5)	5784.62	279.735	0.24	85.7 (D+)		-1.00 (D+)	
	6324.91	284.021	0.25	89.3 (D+)		-0.97 (D+)	
	7106.61	290.481	0.14	50.0 (E)		-1.20 (E)	
	9877.54	315.918	0.06	21.4 (E)		-1.49 (E)	
	10578.68	323.076	0.11	39.3 (E)		-1.21 (E)	
42267.86	4078.94	261.778	0.5	129 (D+)		-0.88 (D+)	
τ (ns) = 23.3(13)	6323.91	278.129	0.33	85.0 (D+)		-1.01 (D+)	
	9877.54	308.644	0.09	23.2 (E)		-1.48 (E)	
42279.28	2834.98	253.446	0.89	120 (C+)		-0.94 (C+)	
τ (ns) = 74.0(27)							
49176 15	0	001 500	0.00	0.0 F (E)		1 59 (5)	
431/0.15	5704.00	231.538	0.09	36.5 (E)		-1.53 (E)	
τ (ns) = 19.7(9)	5784.62	267.361	0.15	60.9(E)		-1.19 (E)	
	6323.91	271.274	0.14	56.8 (E)		-1.20 (E)	
	9877.54	300.225	0.14	56.8 (E)		-1.11 (E)	
	12218.47	322.929	0.18	73.1 (E)		-0.94 (E)	
	13087.9	332.26	0.2	81.2 (D+)		-0.87 (D+)	
43590.91	0094.00	045 001	0.07	0.00 (E)		0.04 (E)	
43329.21	2034.90	240.201	0.07	9.90 (E) 14.9 (E)		-2.04 (E)	
τ (ns) = 56.2(56)	5784.62	204.418	0.1	14.2 (E)		-1.82 (E)	
	7106.61	274	0.07	9.96 (E)		-1.95 (E)	
	9877.54	296.52	0.05	7.12 (E)		-2.02 (E)	
	13087.9	327.729	0.17	24.2 (E)		-1.41 (E)	
	13939.8	337.144	0.09	12.8 (E)		-1.66 (E)	
14506 77	4070.04	046 79	0.91	100 (D L)		1.01 (D.1)	
44596.77	4078.94	246.73	0.31	106 (D+)		-1.01 (D+)	
τ (ns) = 17.5(14)	9877.54	287.941	0.36	123 (D+)		-0.82 (D+)	
	12951.67	315.914	0.09	30.9 (E)		-1.34 (E)	
	13087.9	317.279	0.06	20.6 (E)		-1.51 (E)	
44642.67	2824.08	220 117	0.51	520 (D L)		0.24(D+)	
π (nc) $= 7.7(5)$	12218 47	208 200	0.11	114 (F)		-0.54 (D+)	
7 (IIS) = 7.7(3)	12210.47	215 456	0.11	72.7 (E)		-0.79 (E)	
	12951.07	216 217	0.07	145 (E)		-0.97 (E)	
	13087.9	310.017	0.14	145 (E)		-0.00 (E)	
44652 43	0	223 882	0.15	123 (E)		-1.03 (E)	
τ (ns) = 12.2(8)	2834 98	239.062	0.31	254 (D+)		-0.66 (D+)	
. (6323 91	260 824	0.11	90.2 (E)		-1.04 (E)	
	7106 61	266 262	0.34	$279 (D_{\perp})$		-0.53 (D+)	
	13087.9	316.719	0.07	57.4 (E)		-1.06 (E)	
				(=)			
44785.44	9877.54	286.384	0.17	95.8 (E)		-0.93 (E)	
τ (ns) = 7.1(4)	12218.47	306.971	0.27	152 (D+)		-0.67 (D+)	
	12951.67	314.041	0.1	56.3 (E)		-1.08 (E)	
	16103.32	348.549	0.14	78.9 (E)		-0.84 (E)	
	16681.2	355.716	0.15	84.5 (E)		-0.79 (E)	
				(-)		/	

Table 5.1: Branching fractions, transition probabilities, oscillator strengths for highly excited levels of Ir I and comparison with previous results

	T T 10		0.1.		
Upper Level	Lower Level	$\lambda_{air} (nm)$	BF.	$gA (10^{\circ}s^{-1})$	log gt
E (cm ⁻¹	$E (cm^{-1})$			This work	Previous(⁶ This work Previous ^c
45111.68	5784.62	254.202	0.07	31.3 (E)	-1.51 (E)
τ (ns) = 17.9(8)	7106.61	263.051	0.08	35.8 (E)	-1.43 (E)
	9877.54	283.739	0.25	112 (D+)	-0.87 (D+)
	12218.47	303.932	0.42	188 (D+)	-0.58 (D+)
	13087.9	312.18	0.07	31.3 (E)	-1.34 (E)
45185.95	7106.61	262.532	0.51	294 (D+)	-0.52 (D+)
τ (ns) = 10.4(3)	11831.09	299.719	0.07	40.4 (E)	-1.26 (E)
	12218.47	303.241	0.16	92.3 (E)	-0.89 (E)
	13087.9	311.455	0.07	40.4 (E)	-1.23 (E)
45259.14	4078.94	242.761	0.16	38.1 (E)	-1.47 (E)
τ (ns) = 16.8(5)	5784.62	253.252	0.23	54.8 (D+)	-1.28 (D+)
	9877.54	282.55	0.08	19.0 (E)	-1.64 (E)
	11831.09	299.063	0.34	80.9 (D+)	-0.96 (D+)
45570.89	4078.94	240.938	0.63	289(C)	-0.61 (C)
τ (ns) = 13.1(4)	5784.62	251.267	0.06	27.5 (E)	-1.59 (E)
	9877.54	280.081	0.15	68.7 (E)	-1.10 (E)
45895.85	0	217.817	0.23	242 (D+)	-0.76 (D+)
τ (ns) = 7.6(2)	7106.61	257.726	0.27	284 (D+)	-0.55 (D+)
	13087.9	304.715	0.28	295 (D+)	-0.39 (D+)
	13939.8	312.839	0.11	116 (E)	-0.77 (E)
46000 00	0	216 227	0.26	216 (D+)	0.65 (D+)
± 0220.32 π (ns) $-11.4(6)$	283/ 08	210.201	0.30	246 (D+)	-0.03 (D+) -0.71 (D+)
(10) = 11.4(0)	6323 01	250.422	0.20	43 Q (E)	-1 38 (E)
	13087 9	301 731	0.05	228 (D+)	-0.51 (D+)
	1000110	0011101	0.20		0.01 (D+)
46371.64	0	215.581	0.45	199 (D+)	-0.86 (D+)
τ (ns) = 22.6(8)	2834.98	229.62	0.08	35.4 (E)	-1.55 (E)
	6323.91	249.627	0.14	61.9 (E)	-1.24 (E)
	7106.61	254.604	0.2	88.5 (D+)	-1.06 (D+)
	13087.9	300.359	0.09	39.8 (E)	-1.27 (E)
47165.12	5784.62	241.587	0.06	33.6 (E)	-1.53 (E)
τ (ns) = 14.3(8)	6323.91	244.777	0.24	134 (D+)	-0.92 (D+)
	7106.61	249.56	0.11	61.5 (E)	-1.24 (E)
	12218.47	280.000	0.30	201 (D+)	-0.01 (D+)
	13087.9	295.505	0.07	39.2 (E)	-1.30 (E)
47205.57	0	211.772	0.09	28.4 (E)	-1.72 (E)
τ (ns) = 31.7(11)	2834.98	225.305	0.05	15.8 (E)	-1.92 (E)
	6323.91	244.534	0.12	37.9 (E)	-1.47 (E)
	7106.61	249.308	0.64	202 (E)	-0.73 (E)
	13939.8	300.521	0.06	18.9 (E)	-1.59 (E)
47548.69	0	210.244	0.17	62.7 (E)	-1.38 (E)
τ (ns) = 21.7(7)	2834.98	223.576	0.23	84.8 (D+)	-1.20 (D+)
	9877.54	265.376	0.07	25.8 (E)	-1.56 (E)
	12218.47	282.961	0.13	47.9 (E)	-1.24 (E)
	16103.32	317.92	0.19	70.0 (E)	-0.97 (E)
47858 47	0	208 883	0.89	2886 $(C+)$	0.28 (C+)
τ (ns) = 3.7(3)	2834.98	222.037	0.11	357 (E)	-0.58 (E)
48206.57	4078.94	226.545	0.16	116 (E)	-1.05 (E)
τ (ns) = 8.3(7)	6323.91	238.689	0.3	217 (D+)	-0.73 (D+)
	9877.54	260.821	0.15	108(E)	-0.96 (E)
	10578.68	265.681	0.16	116 (E)	-0.91 (E)
	12951.67	283.566	0.09	65.1 (E)	-1.11 (E)
	18547.04	337.063	0.05	36.1 (E)	-1.21 (E)
18110 82	10579 69	264 027	0.07	45 9 (E)	1 20 (5)
40440.83	11921 00	204.037	0.07	40.2 (E) 400 (C)	-1.32 (E)
τ (ns) = 0.2(2)	12505 69	213.07 278 107	0.02	400 (C) 64 5 (D)	-0.35 (C) 1.12 (D)
	12000.08	210.191	0.1	04.0 (D)	-1.13 (D)
48448.65	5784.62	234.317	0.09	84.7 (E)	-1.16 (E)
τ (ns) = 8.5(3)	6323.91	237.318	0.55	517 (D+)	-0.36 (D+)
. , /	7106.61	241.812	0.14	132 (E)	-0.94 (E)
	12218.47	275.931	0.1	94.1 (É)	-0.97 (E)
48629.22	0	205.572	0.06	76.2 (E)	-1.32 (E)
τ (ns) = 6.3(3)	2834.98	218.3	0.45	571 (D+)	-0.39 (D+)
	5784.62	233.33	0.24	305 (D+)	-0.60 (D+)
	7106.61	240.76	0.09	114 (E) 62 5 (E)	-1.00 (E)
	9877.54	257.976	0.05	03.3 (E)	-1.20 (E)
49779.37	4078.94	218.748	0.15	81.8 (E)	-1.23 (E)
τ (ns) = 11.0(6)	6323 91	230.05	0.1	54.5 (E)	-1.36 (E)
. () = 11.0(0)	7106.61	234.27	0.18	98.2 (E)	-1.09 (E)
	10578.68	255.021	0.12	65.5 (E)	-1.20 (E)
	13087.9	272.462	0.16	87.3 (E)	-1.01 (E)
	16565.35	300.99	0.08	43.6 (E)	-1.23 (E)
	18547.04	320.089	0.08	43.6 (E)	-1.17 (E)
40800 54	E704 C0	007 000	0.00	149 (D+)	0.06 (D+)
49823.54	0/84.02 6202.01	227.002	0.29	143 (D+) 152 (D+)	-0.90 (D+)
T(ns) = 10.2(3)	0323.91	229.810	0.31	$\frac{100}{741}$ (D+)	-0.92 (D+) 1.16 (F)
	3011.04 10060 60	∠JU.∠0J 394 079	0.10	(生.1 (凸)	-1.10 (E) 1 15 (E)
	10000.02	044.310	0.09	44.4 (Ľ)	-1.10 (10)

Table 5.1: Continued

a: From the NIST database [28]. b: From Gough *et al.* [123]. c: From Xu *et al.* [124]. The estimated uncertainties of the transition probabilities and oscillator strengths obtained in our work are also reported in Table 5.1. We used the same code letter as the one usually employed in the NIST database (see [28]). To determine them, we assigned an uncertainty to all our calculated HFR+CPOL BF-values by comparing them to those deduced from experimental measurements by Gough *et al.* [123] and Ivarsson *et al.* [117] for some transitions depopulating Ir I levels (up to 40710 cm⁻¹). This is illustrated in Figure 5.3 where the relative differences $\frac{BF_{calc}-BF_{exp}}{BF_{calc}}$ are reported against BF_{calc} . This figure clearly shows a regular pattern of increasingly deviating weak branches, the average uncertainties on calculated BF-values being found to be about 10%, for $0.8 < BF_{calc} < 1.0, 20\%$ for $0.6 < BF_{calc} < 0.8, 30\%$ for $0.4 < BF_{calc} < 0.6, 40\%$ for $0.2 < BF_{calc} < 0.4$ and 100% for $0.0 < BF_{calc} < 0.2$.



Figure 5.3: Comparison between calculated and experimental BFs in order to determine an uncertainty on the chosen value for BF

All that data represents new reliable semi-empirical atomic data that can be of use for the astrophysicists in Ir I.

5.2.2 Ir II

Ivarsson *et al.* [122] used the time-resolved laser-induced fluorescence (TR-LIF) technique to measure the radiative lifetimes for nine odd-parity levels of Ir II, and combined them with BFs determined by Fourier's transform spectroscopic measurements to obtain the oscillator strengths and transition probabilities of 23 transitions of Ir II. Based on that data, they determined the abundance of iridium in the CP star χ Lupi.

Among the 76 energy levels of Ir II included in the NIST Atomic Spectroscopy Database [28], the experimental lifetimes of a total of 10 levels in the energy range 44575.66-52510.1 cm⁻¹ have been published so far. Our experimental collaborators from the University of Jilin in China measured the radiative lifetimes of 15 highly excited levels falling between 47003 and 61475 cm⁻¹ by TR-LIF technique. Among those 15 levels, only four of them have their experimental lifetimes reported in the literature. The new radiative

lifetime data that they obtained was combined with branching fractions deduced from a HFR+CPOL calculation that we performed to determine semi-empirical transition probabilities and oscillator strengths for 124 Ir II spectral lines.

More precisely, the physical model we considered in our HFR+CPOL calculation was represented by the 5d⁷6s, 5d⁷7s, 5d⁷6d, 5d⁶6s², 5d⁶6p², 5d⁶6s7s, 5d⁶6s6d, 5d⁵6s²7s, 5d⁵6s²6d and 5d⁸ even-parity configurations, and 5d⁷6p, 5d⁷7p, 5d⁷5f, 5d⁶6s6p, 5d⁶6s7p, 5d⁶6s5f and 5d⁵6s26p odd-parity configurations. The core-polarization effects corresponding to a Ta-like ionic core were considered using the dipole polarizability of Ir V [94], i.e. $\alpha_d = 4.59$ a.u., and a cut-off radius, $r_c = 1.61$ a.u., which corresponds to the expected value of < r > for the outermost core orbital, i.e. 5d, as obtained with Cowan code.

The BFs, gA and $\log gf$ for highly excited levels of Ir II are listed in Table 5.2 with the previous available reported results in order to compare them. The lifetimes shown in that table are the experimental ones but one should note that for the 15 levels considered, the agreement between the experimental and theoretical values for the lifetimes was excellent. To be precise the ratio (between the experimental and theoretical values for the lifetimes) was found to be equal to 1.05 ± 0.14 with, as expected a clear core polarization effect lengthening the HFR radiative rates, making them therefore closer to the experimental values.

The results of BFs determined by our HFR+CPOL calculation were combined with the experimental lifetimes obtained by our colleagues of the University of Jilin to deduce the gA and log gf for all transitions with BF > 0.01 by the Eq. 5.1 and 5.2. Ivarsson *et al.* [122] measured BFs and transition probabilities for eight transitions which were also investigated in the present work, and our results are in agreement within 40%. The uncertainties affecting our gA- and gf-values were estimated by combining experimental lifetime uncertainties with those evaluated for theoretical branching fraction calculations exactly as we did for Ir I.

Once again (exactly as for Ir I), the average uncertainties on computed BF-values were systematically found to be around 10-20% for 0.8 < BF < 1.0, 20-30% for 0.6 < BF < 0.8, 30-40% for 0.4 < BF < 0.6, 40-50% for 0.2 < BF < 0.4, and 50-100 % for 0.0 < BF < 0.2. The uncertainties affected the results presented in Table 5.2 are given using the same letter convention as the one used for Ir I which is the one usually employed in the NIST database [28], i.e. B (≤ 10 %), C ($\leq 25\%$), D+ (≤ 40 %), D (≤ 50 %), and E (>50 %).

The radiative data that we presented in this section largely supplements the laconic literature of radiative data of the Ir II ion especially for high-excited states, which are of great significance in order to understand the radiative properties and could have an importance on the astronomical spectral analyses of stellar spectra.

Upper level ^a	Lower level ^a	λ^{b} (nm)	loo -	BFs			$gA(10^7 s^{-1})$		Log(gf)	
$E (am^{-1})$	Edwer level	× (IIII)	This work	Drs		This work	gA (10 S)		This work	Dravious
	E (CIII-1)		THIS WORK	F revious	C 1 d	1 HIS WORK	Frevious	$G \downarrow d$	I HIS WOLK	Frevious
Lifetime (ns)	0	010 001	0 790	Exp	0.720	107 44(01)	Exp. 170.07	100 74*	0.12 (01)	Exp.
47003.95	4787.00	212.081	0.730	0.688	0.738	197.44(C+)	64.01	189.74"	0.13(C+)	0.07
$\tau = 4.1(3)$	4/0/.92	230.803	0.181	0.20	0.181	48.05 (E) 17.10 (E)	04.91	40.07	-0.39 (E)	-0.20
	10270.04	360 584	0.004		0.004	2.88 (E)		2 76*	-0.03 (E) 1.25 (E)	
50302.01	13213.04	198 799	0.487	0.637	0.491	12.00 (E)	16.87	12.70	-1.12 (C)	-1
$\tau = 34(3)$	2262 84	208.097	0.014	0.001	0.014	0.38 (E)	10.01	0.38*	-2.60 (E)	-1
7 - 34(3)	4787.92	219 643	0.253	0.3	0.014 0.253	6.71 (D+)	7.93	6.63*	-1.31 (D+)	-1.24
	8186.89	237 373	0.019	0.0	0.019	0.50 (E)	1100	0.50*	-2.37 (E)	1.21
	11719 11	259 105	0.053		0.053	1.40 (E)		1 39*	-1.85 (E)	
	12714 66	265 968	0.035		0.035	0.43 (E)		0.42*	-2.34 (E)	
	17210.16	302 101	0.052		0.052	1.37 (E)		1 35*	-1.73 (E)	
	17477 99	304 565	0.032		0.032	1.01 (E)		1.01*	-1.85 (E)	
	19279.04	322 249	0.047		0.047	1.01(E) 1.23(E)		1.01	-1.72 (E)	
51333	10210.04	104 806	0.606	0.845	0.606	$12.57 (C \pm)$	17.87	12.22	1.15(C+)	0.00
$\pi -53(3)$	4787 02	214.778	0.000	0.845	0.000	12.37 (C+) 0.43 (E)	11.01	0.45*	-1.13(CT)	-0.99
7 = 55(5)	17210.16	214.110	0.021		0.021	$4.45 (D_{\pm})$		4.54*	1.24 (D+)	
	10270.04	232.373	0.133		0.133	2.43 (D+) 2.75 (E)		2.04	1.24 (D+) 1.40 (E)	
51371.97	3090 16	207.051	0.154		0.153	11.63 (E)		11 71*	-1.13 (E)	
$\tau = 6.6(4)$	8186 80	231 401	0.104	0.25	0.104	$21.78 (D \perp)$	18.06	21.88*	0.76 (D+)	0.82
7 =0.0(4)	8974 95	231.491	0.161	0.146	0.161	12.16 (E)	11.07	12 23*	-0.99 (E)	-1.03
	12714.66	258 606	0.201	0.469	0.291	$22.10 (D_{\pm})$	35.54	22.20	-0.66 (D+)	-0.45
	15676.25	280.063	0.069	0.405	0.069	5 25 (E)	00.04	5 97*	1.21 (E)	-0.40
	18944 91	308 295	0.003		0.003	0.95 (E)		0.95*	-1.21 (E)	
53678 68	3000 16	107 673	0.017		0.017	1.37 (E)		1.24	-1.07 (E)	
$\pi -6.3(10)$	8186 80	210 751	0.501		0.502	30.70(C)		36.13	-2.10(E)	
/ =0.0(10)	8074.05	213.101	0.001		0.002	6 32 (E)		5 73	1.32 (E)	
	0062.22	223.020	0.03		0.03	3.28 (E)		2 08	-1.52 (E) 1.61 (E)	
	11307 53	224.002	0.041		0.041	6.61 (E)		5.00	-1.01 (E) 1.26 (E)	
	11057.83	230.615	0.003		0.033	1.38 (E)		1.25	-1.20 (E) 1.03 (E)	
	12714 66	244 043	0.059		0.059	4 70 (E)		4 26	-1.38 (E)	
	17400.26	244.043	0.000		0.124	4.70 (E) 10.62 (F)		9.20	-1.55 (E)	
	18044.01	210.510	0.134		0.134	1.01 (E)		0.04	-0.91 (E)	
	20440.64	201.02	0.013		0.013	1.01(E) 1.58(E)		1 43	-1.90 (E) 1.67 (E)	
E2601 29	20440.04	196.95	0.02		0.02	101 55 (D)		1.40	-1.07 (E)	
-24(2)	2262.84	104 444	0.314		0.315	101.55 (D+) 18.24 (F)		100.05	-0.28 (D+)	
7 = 3.4(3)	4797.00	204.410	0.050		0.050	150.24 (E) 150.07 (C)		20.23	-0.99 (E)	
	4/0/.92	204.419	0.494		0.495	159.97 (C)		20.02	0.00(C)	
	17210.16	236.179	0.111		0.111	33.80 (E) 4.20 (E)		39.93	-0.52 (E) 1.22 (E)	
	22266.02	214.032	0.015		0.015	4.30 (E)		4.70	-1.52 (E) 1.61 (E)	
55952 5	22200.92	186 602	0.005		0.005	1.05 (E) 1.96 (E)		1.61	-1.01 (E)	
5 8(2)	4787.02	105.003	0.015		0.015	1.60 (E) 4.15 (E)		1.49	-2.01 (E)	
$\tau = 0.8(3)$	4787.92	195.83	0.034		0.034	4.15 (E)		3.32	-1.62 (E)	
	8180.89	209.728	0.062		0.062	(.47 (E)		5.98	-1.31 (E)	
	8974.95	213.255	0.207		0.207	24.99 (D+)		20.04	-0.77 (D+)	
	9927.84	217.08	0.026		0.026	3.19 (E) 5.47 (E)		2.00	-1.04 (E)	
	11307.53.	224.421	0.045		0.045	5.47 (E)		4.38	-1.38 (E)	
	11719.11	220.510	0.14		0.14	10.87 (E)		13.52	-0.89 (E)	
	12/14.00	231.744	0.133		0.132	15.99 (E) 11.26 (E)		12.77	-0.89 (E)	
	15070.25	248.829	0.094		0.094	11.30 (E)		9.09	-0.98 (E)	
	17499.26	260.656	0.093		0.093	11.24 (E)		9	-0.94 (E)	
	18944.91	270.867	0.095		0.095	11.43 (E)		9.15	-0.90 (E)	
F (000 00	20003.07	330.06	0.014		0.014	1.05 (E)		1.32	-1.57 (E)	
= -2.2(2)	2262.84	105 004	0.127		0.127	34.70 (E) 16.21 (E)		20.40	-0.78 (E)	
7 = 3.3(2)	4797.00	104.270	0.00		0.00	10.31 (E) 20.22 (E)		13.37	-1.08 (E)	
	9196 90	208 064	0.111		0.084	30.32 (E) 32.01 (E)		24.93	-0.11 (E)	
	11710.11	208.004	0.084		0.034	20.09 (D)		58.20	-0.33(D)	
	19714.66	224.014	0.20		0.20	17.05 (E)		14.01	-0.21 (D+)	
	17210.16	256 177	0.003		0.005	7.03 (E)		5.04	-0.37 (E)	
	17477.00	257.947	0.215		0.020	58.60 (D+)		48.15	$0.23 (D \pm)$	
	10270 04	270 52	0.018		0.018	4 01 (F)		4 02	-1.97 (E)	
56241 53	3090 16	188 142	0.039		0.010	1.36 (E)		1 75	-2.14 (E)	
$\tau = 8.5(4)$	8974 95	211 400	0.011		0.011	0.40 (E)		0.51	-2.57 (E)	
3.0(1)	9062.22	211.89	0.058		0.058	2.06 (E)		2.65	-1.86 (E)	
	11307.53	222.479	0.193		0.193	6.83 (D+)		8.75	-1.30 (D+)	
	11957.83	225.746	0.417		0.417	14.73 (C)		18.9	-0.95 (C)	
1	15676.25	246.442	0.11		0.11	3.89 (E)		4.99	-1.45 (E)	
	17413.25	257.467	0.038		0.038	1.33 (E)		1.71	-1.88 (E)	
	18676.49	266.126	0.051		0.051	1.82 (E)		2.32	-1.71 (E)	
	18944.91	268.041	0.02		0.02	0.69 (E)		0.89	-2.13 (E)	
	22467.78	296.002	0.035		0.035	1.23 (E)		1.58	-1.79 (E)	
56354.21	8186.89	207.544	0.19			10.2 (D+)			-1.18 (D+)	
$\tau = 9.3(3)$	9927.84	215.327	0.021			1.12(E)			-2.11 (E)	
	11957.83	225.173	0.049			2.63 (E)			-1.70 (E)	
	12714.66	229.079	0.57			30.66 (Ć)			-0.62 (C)	
	17499.26	257.291	0.049			2.63 (È)			-1.58 (E)	
	18676.49	265.33	0.044			2.36 (E)			-1.60 (É)	
	23727.67	306.41	0.021			1.16 (E)			-1.79 (É)	
	25563.67	324.682	0.015			0.80 (E)			-1.90 (E)	
56644.46	8186.89	206.3	0.018			1.92 (E)			-1.91 (E)	
$\tau = 4.6(4)$	8974.95	209.711	0.103			11.16 (E)			-1.13 (E)	
l `´	9062.22	210.095	0.116			12.60 (É)			-1.08 (É)	
	11307.53	220.501	0.419			45.59 (C)			-0.48 (C)	
	11957.83	223.711	0.186			20.20 (D+)			-0.82 (D+)	
	15676.25	244.018	0.058			6.33 (E)			-1.25 (E)	
	17499.26	255.382	0.019			2.10 (E)			-1.69 (E)	
	18944.91	265.176	0.021			2.33 (E)			-1.61 (É)	
	22467.78	292.511	0.033			3.56 (E)			-1.34 (E)	
56875.79	9062.22	209.079	0.728		0.728	13.23 (C+)		14.68	-1.06 (C+)	
$\tau = 5.5(3)$	18676.49	261.707	0.197		0.197	3.58 (D+)		3.98	-1.43 (D+)	
l `´	20440.64	274.379	0.06		0.06	1.09 (E)		1.2	-1.91 (E)	
59132.98	3090.16	178.435	0.022		0.022	1.85 (E)		1.74	-2.06 (E)	

Table 5.2: Branching fractions, transition probabilities, oscillator strengths for highly excited levels of Ir II, and comparison with available data in the literature

Upper level ^a	Lower level ^a	λ^{b} (nm)		BFs	0 0 11 01		$gA (10^7 s^{-1})$		Log(gf)	
$E (cm^{-1})$	E (cm-1)		This work	Previous		This work	Previous		This work	Previous
Lifetime (ns)				Exp^{c}	Cal^d		Exp. ^c	Cal. ^d		Exp. ^c
$\tau = 5.9(3)$	8186.89	196.286	0.146		0.146	12.41 (E)	F.	11.68	-1.14 (E)	
	8974.95	199.37	0.185		0.186	15.7 (D+)		14.81	-1.03 (D+)	
	9062.22	199.717	0.303		0.303	25.67 (D+)		24.2	-0.81 (D+)	
	9927.84	203.166	0.056		0.056	4.74 (E)		4.47	-1.53 (E)	
	11307.53	209.027	0.045		0.046	3.85 (E)		3.63	-1.60 (E)	
	11957.83	211.908	0.047		0.047	3.99 (E)		3.75	-1.57 (E)	
	17499.26	240.117	0.06		0.06	5.08 (E)		4.79	-1.36 (E)	
	17413.25	239.622	0.014		0.014	1.21 (E)		1.14	-1.98 (E)	
	18944.91	248.755	0.02		0.02	1.69 (E)		1.59	-1.81 (E)	
	22467.78	272.657	0.012		0.012	1.00 (E)		0.94	-1.95 (E)	
	28600.34	327.424	0.01		0.01	0.85 (E)		0.8	-1.86 (E)	
60313.63	2262.84	172.263	0.055			11.32 (E)			-1.30 (E)	
$\tau = 3.4(3)$	4787.92	180.097	0.013			2.68 (E)			-1.89 (E)	
	8186.89	191.84	0.302			62.18 (D+)			-0.46 (D+)	
	8974.95	194.785	0.125			25.74 (E)			-0.83 (E)	
	11719.11	205.719	0.244			50.24 (D+)			-0.50 (D+)	
	15676.25	223.958	0.027			5.56 (E)			-1.38 (E)	
	17499.26	233.495	0.062			12.76 (E)			-0.98 (E)	
	18944.91	241.655	0.02			4.12 (E)			-1.44 (E)	
	20294.25	249.804	0.062			12.76 (E)			-0.92 (E)	
	23727.61	273.248	0.028			5.76 (E)			-1.19 (E)	
61474.19	2262.84	168.886	0.032			5.73 (E)			-1.61 (E)	
$\tau = 3.9(3)$	3090.16	171.28	0.262			47.06 (D+)			-0.68 (D+)	
	8186.89	187.662	0.03			5.41 (E)			-1.54 (E)	
	11307.53	199.335	0.092			16.59 (E)			-1.01 (E)	
	11719.11	200.919	0.022			3.99 (E)			-1.62 (E)	
	12714.66	205.022	0.142			25.46 (E)			-0.79 (E)	
	15676.25	218.283	0.122			21.81 (E)			-0.81 (E)	
	17210.16	225.847	0.104			18.68 (E)			-0.84 (E)	
	17413.25	226.888	0.077			13.77 (E)			-0.97 (E)	
	18944.91	235.06	0.033			5.91 (E)			-1.31 (E)	
	19279.04	236.922	0.013			2.34 (E)			-1.71 (E)	
	22467.78	256.291	0.026			474(E)			-1.33 (E)	

Table 5.2: Continued

a: Energy levels from the NIST database [28].
b: λ above 200 nm given in air and inn vacuum below.
c: From Ivarsson et al. [122].
d: From Xu et al. [124].

5.3 Re I

The framework for this section is exactly the same as for the previous ones: in collaboration with the University of Jilin in China, we combined their TR-LIF experimental radiative lifetimes with our theoretical branching fractions in order to obtain reliable semiempirical transition probabilities and oscillator strengths in neutral rhenium. Exactly as for Ir I, Ir II, we did not participate to the experimental part of this work.

Rhenium (Z = 75) was discovered in 1925 in Germany and was named after the river Rhine (in latin *Rhenus*). Rhenium was actually the last stable element to be discovered. It is even one of the very last natural elements to be discovered, before francium, technetium and astatine, which are short-lived radioactive and exist only in trace amounts on Earth [125].

In this section, we will focus on the determination of radiative parameters in neutral rhenium (Re I, Z = 75) which has already been observed in peculiar stars (see e.g. Guthrie *et al.* [126]) and on which too few works have focused, resulting in a relatively incomplete set of atomic data in the literature.

The first extended experimental analysis of neutral rhenium's spectrum is the one of Klinkenberg *et al.* [127]. They classified 2764 lines between 171 and 1162 nm with transitions observed among 282 atomic energy levels. However, they only considered the configurations $5d^56s^2$ and $5d^66s$ in their least-squares fit of the energy levels and these two-configuration calculations resulted in a rather high average deviation of 371 cm⁻¹. More than 20 years later, the inclusion of the $5d^7$ configuration by Wyart [128] significantly reduced this deviation to 89 cm⁻¹.

In our calculation, we introduced the following configurations: $5d^6ns$, $5d^56sns$, $5d^7$, $5d^66d$, $5d^56s6d$, $5d^46s^26d$, $5d^56p^2$ and $5d^46s6p^2$ (n = 6–8) in the even parity and $5d^6np$, $5d^56snp$, $5d^46s26p$ and $5d^46p^3$ (n = 6–8) in the odd parity exactly as in Palmeri *et al.* [129]. We considered a $5d^4$ (Re IV) ionic core surrounded by three valence electrons. The dipole polarizability was adopted from tabulated values from Fraga *et al.* [94], i.e. 6.81 au. The cut-off radius used was the HFR mean radius of the 5d orbital in the Re I ground configuration, i.e. 1.87 a.u.

The HFR + CPOL method was then combined with a least-squares optimization fitting procedure minimizing the discrepancies between calculated and experimental energy levels published by Klinkenberg *et al.* [127] and Wyart [128]. The average mean deviations of those fits were found to be 88 and 176 cm⁻¹ for the even and odd parity respectively.

As one can see, this calculation is exactly the same as the one performed by Palmeri *et al.* [129]. This previous calculation was very accurate and no new experimental level would have justified a different analysis. However, thanks to the new radiative lifetimes measured at the University of Jilin, we were able to extract new branching fractions from that calculation that have been combined with the new radiative lifetimes to produce brand new reliable transition probabilities and oscillator strengths using the method explained in Section 5.2 and the Eq. 5.1 and 5.2. Palmeri *et al.* [129] already did something similar in their paper but with a smaller number of measured radiative lifetimes and therefore a smaller number of gA and gf given. Our values and the comparison between them and what already existed in the literature is given in Table 5.3. The uncertainty for our values is given using the NIST code [28] as in Ir I, II in the previous sections.

It is worth remembering that carrying out accurate calculations in such a complex heavy neutral atom as Re I with a large number of overlapping configurations is a very challenging task. In Re I, a strong configuration interaction is also present for the low-lying levels [129] and even more so for the high-lying ones measured in this study as highlighted in Table 5.4. The major LS components are to be found equal to 20 % or even less. This has consequences on the calculation of the line strengths of depopulating channels and

Table 5.3: New reliable BF, gA and $\log gf$ obtained for Re I

Upper level ^a		Lower level ^{a}		λ (air)	BF	$gA (10^6 s^{-1})$		log gf	
$E (cm^{-1})$	J	$E(cm^{-1})$	J	(nm)		This work	Previous ^b	This work	Previous ^b
32592	1.5	0	2.5	306.738	0.804	24.4 (C)	24.0	-1.47	-1.47
$\tau = 132(8) \text{ ns}$						()			
41557	1.5	0	2.5	240.56	0.669	84.1 (D+)	74.2	-1.12	- 1.19
$\tau = 31.6(15) \text{ ns}$		17238	0.5	441.089	0.150	18.9(E)	16.7	-1.29	-1.37
41844	3.5	11755	4.5	332.2481	0.664	68.7(D+)	-	-0.95	-
$\tau = 77.3 \text{ ns}$		15770	2.5	383.4234	0.149	15.4(E)	-	-1.47	-
42254	1.5	0	2.5	332.248	0.441	90.1 (D+)	-	-0.95	-
$\tau = 19.6(8)$		11584	2.5	325.955	0.236	48.1 (D)	-	-1.12	-
		13826	1.5	351.664	0.148	30.3(E)	-	-1.25	-
43044	2.5	14217	3.5	346.796	0.198	42.0(E)	-	-1.12	-
$\tau = 28.3(8) \text{ ns}$									
43342	1.5	14621	2.5	348.085	0.551	56.6(D+)	-	-0.98	-
$\tau = 38.9(15) \text{ ns}$		17238	0.5	382.981	0.21	21.6(D+)	-	-1.32	-
43815	3.5	0	2.5	228.1619	0.648	274(C)	-	-0.67	-
$\tau = 18.9(7) \text{ ns}$		11755	4.5	311.82	0.234	98.9(D+)	-	-0.85	-
49350	2.5	14217	3.5	336.2287	0.373	226(D)	-	-0.42	-
$\tau = 9.9(7) \text{ ns}$		14621	2.5	340.8672	0.159	96.3(E)	-	-0.77	-
		0	2.5	227.4611	0.18	109(E)	-	-1.07	-
45876	1.5	0	2.5	217.909	0.753	78.9(C)	-	-1.25	-
$\tau = 38.2(16) \text{ ns}$									
45937	3.5	0	2.5	217.6204	0.724	460(C)	-	-0.49	-
$\tau = 12.6(10) \text{ ns}$									
46112	2.5	0	2.5	216.7941	0.526	304(D+)	-	-0.67	-
$\tau = 10.4(6) \text{ ns}$		14621	2.5	317.4614	0.21	121(D+)	-	-0.74	-
46353	3.5	14217	3.5	311.086	0.411	154(D+)	-	-0.65	-
$\tau = 21.4(9)$ ns		0	2.5	215.668	0.275	103(D+)	-	-1.14	-
		15770	2.5	326.8894	0.116	43.3(E)	-	-1.16	-
46509	2.5	17331	3.5	342.6189	0.205	60.1(D+)	-	-0.97	-
$\tau = 20.5(10) \text{ ns}$		0	2.5	214.9426	0.455	133(D+)	-	-1.03	-
		15058	3.5	317.8608	0.123	35.9(E)	-	-1.26	-
46649	2.5	14217	3.5	308.2426	0.476	182(D+)	-	-0.58	-
$\tau = 15.7(9) \text{ ns}$		0	2.5	214.2974	0.326	124(D)	-	-1.06	-
46733	1.5	0	2.5	213.9124	0.611	136(C)	-	-1.03	-
$\tau = 18.0(6) \text{ ns}$		16328	1.5	328.7891	0.165	36.6(E)	-	-1.23	-
47102	2.5	14217	3.5	304.0039	0.161	59.6(E)	-	-1.08	-
$\tau = 16.2(6) \text{ ns}$		16328	1.5	324.8549	0.115	42.6(E)	-	-1.17	-
		17331	3.5	335.8032	0.122	45.4(E)	-	-1.11	-
		11584	2.5	281.4673	0.183	67.7(E)	-	-1.09	-
		15770	2.5	319.0785	0.128	47.4(E)	-	-1.14	-
47358	3.5	0	2.5	211.0891	0.493	94.9(D+)	-	-1.20	-
$\tau = 41.6(17) \text{ ns}$		15058	3.5	309.506	0.15	28.8(E)	-	-1.38	-
47971	2.5	14621	2.5	299.7684	0.387	94.8(E)	-	-0.89	-
$\tau = 24.5(25) \text{ ns}$		16328	1.5	315.9311	0.163	39.9(E)	-	-1.22	-
		15770	2.5	310.4651	0.171	42(E)		-1.22	-

: From NIST database [28] b: Palmeri *et al.* [129]

therefore on the corresponding theoretical lifetimes, hence the interest in producing semiempirical data by combining them with experimental measurements. It allowed us to deduce the semi-empirical transition probabilities gA and oscillator strengths for 47 lines from 18 upper levels in the wavelength range between 204 and 441 nm as shown in Table 5.3. One should note that only the transitions with $BF \ge 0.1$ are given in that table (the other ones being not reliable enough due to cancellation effects).

Table 5.4: LS composition and comparison between experimental and calculated level energies and Landé g-factors, for the Re I odd-parity energy levels involved in the transitions mentioned in Table 5.3

E_{expa}	E_{calc}	J	g^a_{exp}	g_{calc}	LS Composition ^{b}
32 591.63	32 817	3/2	1.762	1.781	21 B $({}^{4}D){}^{6}D^{o}$ + 18 C $({}^{5}D){}^{6}D^{o}$ + 9 C $({}^{5}D){}^{4}P^{o}$
41 557.08	40 752	3/2	1.655	1.496	$20 \text{ B} (^{4}\text{P})^{6}\text{D}^{o} + 12 \text{ B} (^{6}\text{S})6\text{P}^{o} + 8 \text{ C} (^{5}\text{D})^{6}\text{F}^{o}$
41 843.85	41 743	7/2	1.19	1.302	$18 \text{ B} (4 \text{ G})6\text{H}^{o} + 8 \text{ B} (^{6}\text{D})6\text{P}^{o} + 7 \text{ B} (^{4}\text{D})^{4}\text{F}^{o}$
42 254.19	42 499	3/2	1.578	1.489	$14 \text{ B} (^{6}\text{S})^{4}\text{P}^{o} + 11 \text{ B} (^{4}\text{P})6\text{P}^{o} + 7 \text{ C} (^{5}\text{D})^{4}\text{P}^{o}$
43 44.02	42 997	5/2	1.449	1.446	$8 \text{ B} (^{4}\text{D})^{4}\text{D}^{o} + 7 \text{ B} (^{4}\text{P})^{6}\text{D}^{o} + 7 \text{ B} (^{4}\text{D})^{4}\text{D}^{o}$
43 341.85	$43 \ 340$	3/2	0.975	1.032	$17 \text{ B} (^{4}\text{P})^{6}\text{D}^{o} + 9 \text{ B} (^{2}\text{D})^{4}\text{F}^{o} + 9 \text{ B} (4 \text{ G})^{4}\text{F}^{o}$
43 815.01	$43 \ 937$	7/2	1.348	1.388	$14 \text{ B} (^{6}\text{S})6\text{P}^{o} + 14 \text{ B} (^{4}\text{G})6\text{G}^{o} + 8 \text{ A} (^{5}\text{D})6\text{P}^{o}$
43 949.98	43 852	5/2	1.385	1.567	$19 \text{ B} (^{4}\text{P})^{6}\text{S}^{o} + 13 \text{ B} (^{4}\text{D})6\text{P}^{o} + 5 \text{ A} (^{5}\text{D})^{4}\text{P}^{o}$
45 876.34	45 974	3/2	1.384	1.555	$14 \text{ B} (^{4}\text{P})^{6}\text{D}^{o} + 9 \text{ C} (^{5}\text{D})^{6}\text{F}^{o} + 8 \text{ B} (^{4}\text{D})^{6}\text{F}^{o}$
45 937.18	$46 \ 49$	7/2	1.298	1.282	11 B $({}^{6}S)6P^{o} + 8$ B $({}^{4}G){}^{6}F^{o} + 6$ C $({}^{3}G){}^{4}G^{o}$
46 112.24	46 223	5/2	1.405	1.345	$20 \text{ B} (^{4}\text{D})^{6}\text{F}^{o} + 12 \text{ B} (^{4}\text{P})^{6}\text{D}^{o} + 11 \text{ B} (^{4}\text{G})^{6}\text{F}^{o}$
46 352.99	$46 \ 392$	7/2	1.271	1.274	$15 \text{ B} ({}^{4}\text{G}){}^{6}\text{F}^{o} + 13 \text{ B} ({}^{4}\text{D}){}^{6}\text{F}^{o} + 7 \text{ B} ({}^{4}\text{G})6\text{G}^{o}$
46 509.4	$46 \ 476$	5/2	1.371	1.528	$17 \text{ B} (^{6}\text{S})^{4}\text{P}^{o} + 8 \text{ B} (^{4}\text{P})^{6}\text{S}^{o} + 7 \text{ B} (^{6}\text{S})6\text{P}^{o}$
46 649.42	46 573	5/2	1.334	1.304	$15 \text{ B} ({}^{4}\text{G}){}^{6}\text{F}^{o} + 8 \text{ C} ({}^{5}\text{D}){}^{6}\text{F}^{o} + 7 \text{ B} ({}^{4}\text{F}){}^{6}\text{F}^{o}$
46 733.38	46 680	3/2	1.858	1.796	$18 \text{ B} (^{4}\text{D})6\text{P}^{o} + 16 \text{ B} (4 \text{ G})^{6}\text{F}^{o} + 14 \text{ B} (^{4}\text{P})6\text{P}^{o}$
47 101.61	46 984	5/2	0.893	0.864	$14 \text{ B} (^{2}\text{F})^{4}\text{G}^{o} + 13 \text{ B} (^{4}\text{G})^{4}\text{G}^{o} + 10 \text{ C} (^{3}\text{F})^{4}\text{G}^{o}$
47 358.36	$47 \ 365$	7/2	1.151	1.076	$14 \text{ B} (^{2}\text{F})^{4}\text{G}^{o} + 14 \text{ B} (^{4}\text{G})^{4}\text{G}^{o} + 8 \text{ C} (^{3}\text{F})^{4}\text{G}^{o}$
47 970.82	47 875	5/2	1.169	1.287	11 B $({}^{4}\text{G}){}^{6}\text{F}^{o}$ + 9 C $({}^{5}\text{D}){}^{6}\text{F}^{o}$ + 7 B $({}^{4}\text{P}){}^{6}\text{D}^{o}$
				a: Fr	om [127].

b: First three major components given in %. A, B, and C mean respectively the $5d^{6}6p$, $5d^{5}6s6p$ and $5d^{4}6s^{2}6p$ configurations.

5.4 La I

Lanthanum is a chemical element with an atomic number of Z = 57. Lanthanum gave its name to the family of lanthanides which are part of the rare earths. This element usually occurs together with cerium (as an oxyde) and was first found by the Swedish researcher Carl Gustaf Mosander in 1839 as an impurity in cerium nitrate. The name lanthanum comes from the Ancient Greek *lanthanein*, which means to lie hidden. Even though it is chemically classified as a rare earth element, lanthanum is actually the 28th most abundant element in the Earth's crust, almost three times as abundant as lead. But its etymology comes from the fact that pure lanthanum metal was only first isolated in 1923 [109].

Lanthanides represent a very hot topic in atomic astrophysics since the observation of gravitational waves by the LIGO-VIRGO interferometer in 2017 [130]. Indeed, the radiative parameters can be used for the calculation of the corresponding opacities in the astrophysical context of kilonovae. Those kilonovae result from the coalescence of neutron stars, such as the GW170817 event detected in 2017 [130]. They indeed have a spectrum characterized by many lines belonging to heavy elements among which the lanthanides seem to play an important role. Because of the huge amount of spectral lines in their spectra, their contribution to the observed opacities is high as highlighted by Kasen *et al.* [131]. In order to estimate these opacities, it is therefore essential to have a precise knowledge of the radiative data relating to the very numerous lines belonging to the lanthanide atoms.

Since this work is about low ionization states, we focused on neutral lanthanum, which is described by the $5d6s^2 {}^2D_{3/2}$ ground level, while the lowest excited levels belong to many different configurations such as $5d6s^2$, $5d^26s$, $5d^3$, 4f6s6p, $5d^27s$ and 5d6s7s in the even parity, and 5d6s6p, $5d^26p$, 4f5d6s, $6s^26p$ and $4f6s^2$ in the odd one (see [28]). The overlap of these configurations is responsible for the strong mixing of most energy levels, which makes both experimental and theoretical analyses very tricky.

5.4.1 HFR+CPOL Calculations

The first computational procedures that we used in order to model the atomic structure and to calculate the radiative parameters in La I were the HFR [7] and HFR+CPOL [81, 82] ones. Three different physical models were developed in our calculations. For the first model (HFR-NOPOL), only intravalence correlations were considered by explicitly including the following 37 even- and 37 odd-parity configurations, namely 5d6s², 5d²6s, 5d²7s, 5d²6d, 5d³, 5d6p², 5d6d², 5d7s², 5d6s6d, 5d6s7s, 5d6p7p, 5d6d7s, 4f²5d, 4f²6d, 4f²6s, 4f²7s, 4f5d6p, 4f5d7p, 4f6s6p, 4f6s7p, 4f6p6d, 4f6p7s, 4f6d7p, 4f7s7p, 6s²6d, 6s²7s, 6s6p², 6s6d², 6s7s², 6s6p7p, 6s6d7s, 6p²6d, 6p²7s, 6p6d7p, 6p7s7p, 6d7s², 7s6d², and 5d²6p, 5d²7p, 5d6s6p, 5d6s7p, 5d6p6d, 5d6p7s, 5d6d7p, 5d7s7p, 4f³, 4f²6p, 4f²7p, 4f5d², 4f6s², 4f6p², 4f6d², 4f7s², 4f5d6s, 4f5d7s, 4f5d6d, 4f6s6d, 4f6s7s, 4f6p7p, 4f6d7s, 6s²6p, 6s²7p, 6s6p6d, 6s6p7s, 6s6d7p, 6s7s7p, 6p³, 6p²7p, 6p6d², 6p7s², 6p6d7s, 6d²7p, 6d7s7p, 7s²7p, respectively. One should note that those multiconfiguration expansions are considerably more extensive than the ones included in a previous HFR calculation performed by the UMONS Atomic Physics and Astrophysics group which was published nearly 20 years ago [132].

In the second model (HFR+CPOL1), the same set of configurations as the one given hereabove was explicitly considered in the computations. In addition, core-polarization effects were estimated by assuming a Xe-like La IV ionic core with the dipole polarizability value reported by Fraga [94] i.e. $\alpha_d = 9.50 \ a_0^3$, and a cut-off radius equal to the HFR average value of the outermost core orbital (5p), i.e. $r_c = 1.80 \ a_0$. However, as mentioned, for example, by Hibbert *et al.* [133], the cut-off radius is not an unambiguously defined parameter. Therefore, we differently took into account the core-polarization effects in a third model (HFR+CPOL2), in which we used the same dipole polarizability as the one used in HFR+CPOL1, but with a different value of the cut-off radius, namely $r_c = 1.20 a_0$, representing the distance at which the total density of probability of the ionic core orbitals falls to 10 % of its maximum value, as suggested by Hameed [84]. This is illustrated in Figure 5.4, which shows the calculated probability density of the La IV ionic core in the ground configuration of the lanthanum atom.



Figure 5.4: Electron probability density of the La IV ionic core in the ground configuration of neutral Lanthanum (5d6s²). Dashed vertical line marks a radius of $r_c = 1.20 a_0$.

In each of these three models, the calculated eigenvalues of the Hamiltonian were optimized using the observed energy levels via a least-squares fitting procedure in which all the experimentally known levels included in the NIST compilation [28] up to 32 140 cm⁻¹ were included, most of the level values above that limit being dubious or having unknown assignments. One should note that the newly identified even-parity level at 25 558.774 cm⁻¹ (J = 3/2) from Basar *et al.* [134] was also incorporated in our fitting process. For this particular level, the leading component (52%) was found to be 5d³ ²D_{3/2}, according to our calculations. In this semi-empirical procedure, some radial energy parameters describing the 5d6s², 5d²6s, 5d²7s, 5d²6d, 5d³, 5d6s7s and 4f6s6p even-parity configurations and the 5d²6p, 5d6s6p, 4f6s², 4f5d6s and 6s²6p odd-parity configurations were adjusted, giving rise to standard deviations of 129 cm⁻¹ and 173 cm⁻¹ for even and odd parities, respectively, in all three models.

5.4.2 MCDHF Calculations

In order to assess the reliability of our pseudo-relativistic Hartree–Fock computations described above, the other theoretical method that we described in section 2.3 was used for neutral lanthanum. The version we used is the one implemented in the GRASP2K computer package [89].

In a first step, the 5d6s², 5d²6s, 5d²7s, 5d²6d, 5d³, 5d6s7s and 4f6s6p even-parity configurations and the 5d²6p, 5d²7p, 5d6s6p, 5d6s7p, 6s26p, 6s27p, 4f5d² and 4f6s² oddparity configurations were chosen as a multireference (MR) to optimize all the involved orbitals using the extended average level (EAL) option (see [89]). The valence-valence correlations were then taken into account by allowing single and double excitations from the multireference to 5d, 5f, 5g, 6s, 6p, 6d, 7s, 7p, 7d, 8s, 8p and 8d orbitals, giving rise to 20 265 CSFs. In this step, the additional 5f, 5g, 7d, 8s, 8p and 8d orbitals were first obtained by an EOL variational procedure, keeping all the other orbitals frozen, before reoptimizing all the orbitals together. Finally, the most important core-valence correlations were considered by including the 5p \rightarrow 4f, 5s \rightarrow 5d single excitations, and the 5p² \rightarrow 5d², 5s² \rightarrow 4f² and 5s5p \rightarrow 4f5d double excitations within the relativistic configuration interaction (RCI) approximation.

5.4.3 Results

5.4.3.1 Radiative Lifetimes

In Table 5.5, the calculated lifetime values that we obtained using the three different HFR models described in section 5.4.1 are compared with the available measurements in the literature² for 96 odd-parity levels in La I.

This table shows that the theoretical results are in very good agreement with the most recent and the most accurate experimental data of Den Hartog *et al.* [135],with the exception of the three levels at 17 947.13, 23 221.10 and 24 173.83 cm⁻¹ for which large discrepancies are observed. This can be explained by the uncertain representation of these levels in our theoretical models. This effect is highlighted by the rather bad agreement we found when comparing the calculated HFR Landé *g*-factors, i.e. g = 1.06, 1.08, and 0.72, with the experimental values from the NIST database [28], namely g = 1.516, 0.781, and 0.806. It is, however, interesting to notice that, for the level at 24 173.83 cm⁻¹, the lifetime computed by Karaçoban and Özdemir [136], i.e. $\tau = 6.04$ ns, is in better agreement with our values (ranging from 9.6 to 12.0 ns) than with the experimental one (35.9 ns).

²Most of them performed by time-resolved laser-induced fluorescence spectroscopy (TR-LIF).

When we looked at those results in more details (with the exception of the three levels mentioned above), we found that, by comparing our data to the experimental values of Den Hartog [135] (noted EXP[135]), the mean ratios between them are found to be:

- $< \tau (\text{HFR-NOPOL}) / \tau (\text{EXP}[135]) > = 0.77 \pm 0.18;$
- $< \tau (\text{HFR+CPOL1}) / \tau (\text{EXP}[135]) > = 0.90 \pm 0.23;$
- $< \tau (\text{HFR+CPOL2}) / \tau (\text{EXP}[135]) > = 0.94 \pm 0.22;$

where the uncertainty corresponds to the standard deviation from the average.

As expected, it is clear from those comparisons that the core-valence correlations play a non-negligible role, the calculated lifetimes increasing by about 15% when including core-polarization contributions³. It then appears that the HFR+CPOL2 model gives the best overall agreement with the experimental radiative lifetimes from [135]. This agreement is also better than the one obtained between the previously calculated theoretical lifetimes from Biémont *et al.* [137] (for 17 levels) and from Karaçoban and Özdemir [136](for 37 levels) and the experimental measurements. Indeed, in these two cases, the mean ratios $\langle \tau(\text{THEORY})/\tau(\text{EXP}[135]) \rangle$ are found to be equal to 0.98 ± 0.33 and 0.89 ± 0.47 . As one can see, the standard deviations (and therefore the scattering of results) are larger than the value that we obtained with our HFR+CPOL2 model which can therefore be considered as the most reliable one.

The agreement between our radiative lifetimes computed with the latter model and the TR-LIF experimental data of [135] is illustrated in Figure 5.5.



Figure 5.5: Comparison between the radiative lifetimes computed in La I using the HFR+CPOL2 model and the most recent laser-induced fluorescence experimental measurements from [135], where the dashed line indicates equality between them.

³Which would seem logical because the addition of the CPOL effects tends to lower the transitions probabilities.

Some other TR-LIF lifetime measurements were published before those of Den Hartog *et al.* [135]. This data [137, 138, 139, 140] is also reported in Table 5.5. The comparison between our HFR+CPOL2 calculated values and those older experimental measurements gives the mean ratios:

- $< \tau (\text{HFR+CPOL2}) / \tau (\text{EXP}[137]) > = 0.81 \pm 0.20;$
- $< \tau (\text{HFR+CPOL2}) / \tau (\text{EXP}[138]) > = 0.93 \pm 0.24;$
- $< \tau (\text{HFR+CPOL2}) / \tau (\text{EXP}[139]) > = 0.88 \pm 0.20;$
- $< \tau (\text{HFR+CPOL2}) / \tau (\text{EXP}[140]) > = 0.91 \pm 0.43.$

As one can see from those comparisons, the larger scattering observed between theoretical and experimental data is with the data of Yarlagadda *et al.* [140], which is mainly due to the fact that many of the levels considered in their analysis have quite long lifetimes $(\tau > 100 \text{ ns})$, which are more difficult to precisely determine both experimentally and theoretically⁴.

The MCDHF lifetimes calculated in the present work are not listed in Table 5.5 because, for many levels (about 50%), either the identifications are rather difficult due to unambiguously identification of the energy levels in the calculations (in particular for E > 26 000 cm⁻¹), or most of the computed radiative decay rates are strongly affected by severe cancellation effects leading to very uncertain lifetimes (in particular for $\tau > 100$ ns).

Nevertheless, for unambiguous identified levels in our MCDHF calculations, it is interesting to point out that the theoretical lifetimes are generally slightly shorter than the experimental data of Den Hartog *et al.*[135] exactly like the HFR+CPOL2 ones. If we compare the mean ratios between MCDHF and the experimental data and between MCDHF and HFR+CPOL2, we find $\langle \tau (\text{MCDHF})/\tau (\text{EXP} [22]) \rangle = 0.85 \pm 0.46$ and $\langle \tau (\text{MCDHF})/\tau (\text{HFR+CPOL2}) \rangle = 0.81 \pm 0.43$, respectively. This can be explained by the fact that core-valence interactions are taken into account more effectively by using the core-polarization corrections in the HFR method than by explicitly incorporating a limited set of core-excited configurations in the MCDHF model. That all means that our HFR+CPOL2 calculations would tend to be a better representation of the atomic structure of La I.

⁴It is due to the fact that they involve less intense transitions which are generally much more affected by the cancellation effects.

Table 5.5: Comparison of the radiative lifetimes computed in the present work using three different HFR models with the available experimental values for odd-parity levels in neutral lanthanum.

			This work ^{b} (ns)			Experiments (ns)
$E^{a} (cm^{-1})$	J	HFR+NOPOL	HFR+CPOL1	HFR+CPOL2	DH^{c}	
13,260.38	1.5	232	287	335		$256.9 \pm 12.3 \ ^{f}$
13,631,04	2.5	213	260	295		224.5 ± 13.8 ^f
14 095 69	0.5	110	1/0	170		$220.0 \pm 14.3 f$
14,000.00	15	159	109	220		$166.2 \pm 0.2 f$
14,706.92	1.0	104	190	239		$100.3 \pm 9.3^{\circ}$
14,804.08	2.5	194	230	270		237.9 ± 21.3^{-5}
$15,\!019.51$	3.5	247	305	357		313 ± 17.8 ^J
15,031.64	1.5	155	192	224	162 ± 8	$183.7 \pm 12.8 \ ^{f}$
15,196.83	2.5	106	123	132	108 ± 5	127 ± 7 f
15,219.89	0.5	355	459	585		$205.4 \pm 16.9 \ ^{f}$
15,503,64	2.5	106	132	158		131.8 ± 6.8 ^f
16,099,29	3.5	102	102	153		$156.7 \pm 14.2 f$
16,000.20	1 5	102	260	227		100.1 ± 14.2
10,280.20	1.0	211	209	00 7	059 49	271.0 ± 19.2
16,538.39	3.5	68.1	78.8	83.7	85.3 ± 4.3	112.9 ± 9.5
16,856.80	2.5	34.6	40.6	42.2	52.4 ± 2.6	68.4 ± 5.1^{-1}
17,797.29	1.5	236	287	341		130.2 ± 11.5 ^J
$17,\!910.17$	3.5	44.4	52	54.5	48.9 ± 2.4	$64.6 \pm 2.7 \ ^{f}$
17,947.13	2.5	115	138	154	51.4 ± 2.6	$68.3 \pm 3.1 \ ^{f}$
18,156.97	2.5	28.4	33.1	34.5	64 ± 3.2	$68.4 \pm 3.1 \ ^{f}$
18,172,35	1.5	10.7	12.7	13.3	15.7 ± 0.8	17.7 ± 1.4^{d}
18 603 92	3.5	27.5	31.8	23.0	37.6 ± 1.0	$54.8 \pm 3.5 f$
10,000.02	J.J 4 5	21.0	25	25.0	37.0 ± 1.5 20.4 ± 1.5	$46 \pm 26^{\circ}$
19,129.31	4.0	21.7	20	20.9	29.4 ± 1.0	40 ± 2.0
19,379.40	2.5	10.3	12.2	12.8	15.3 ± 0.8	17.2 ± 1^{-a}
						15.9 ± 1^{a}
20,018.99	1.5	11.2	13.2	13.9	14.1 ± 0.7	17 ± 0.8 ^J
20,082.98	1.5	14.2	16.4	17.1	15.1 ± 0.8	$17.5 \pm 1.6 f$
$20,\!117.38$	5.5	20.6	23.7	24.6	27.2 ± 1.4	$32 \pm 2.2 f$
20,197.34	0.5	8.4	9.9	10.5	9.8 ± 0.5	$17.2 \pm 0.8 \ ^{f}$
20.338.25	2.5	15.1	17.5	18.3	18.7 ± 0.9	20 ± 0.9 ^f
20.763.21	3.5	15.2	17.6	18.3	20.4 ± 1	25.8 ± 1.4 ^f
20,972,17	2.5	17.9	2110	22.1	25.7 ± 1.3	35 + 35 f
20,372.17	4.5	14.6	17	177	10.0 ± 1	30 ± 0.0
21,384.00	4.0	14.0	17	11.1	13.3 ± 1	20 ± 2.1
21,447.86	3.5	26	30	31.4	29.2 ± 1.5	34.1 ± 3.3 ^f
21,662.51	3.5	20.4	23.8	25	32.1 ± 1.6	39.8 ± 2.1
22,246.64	0.5	6.7	7.9	8.3	8.6 ± 0.4	$10.1 \pm 0.9 \ ^{a}$
						$9.6 \pm 0.6 f$
22,285.77	4.5	47	53.5	56.1	51.8 ± 2.6	$73.4 \pm 6.1 f$
$22,\!439.36$	1.5	6.6	7.7	8.2	8.8 ± 0.4	$10.2 \pm 0.5 \ ^{d}$
						$9.5\pm0.7{}^{f}$
22,804.25	2.5	6.6	7.7	8.1	8.9 ± 0.4	$10.7 \pm 1 \ ^{d}$
,						10.4 ± 0.3 ^f
23 221 10	3.5	109	127	134	21.1 ± 1.1	22 ± 1.4^{d}
20,221110	0.0	100		101	2 2	$27.5 \pm 2.7 f$
<u> </u>	05	12.6	16	17		$27.0 \pm 2.1^{\circ}$ 19.1 \pm 1.5 f
23,200.92	0.0	13.0	10	21	147 07	16.1 ± 1.0
25,505.20	5.5	0.9	0.1	0.0	14.7 ± 0.7	10.1 ± 1^{-1}
						16.5 ± 1.1^{f}
23,466.84	4.5	56	64.7	67.8	60.6 ± 3	67.9 ± 3.8 ^f
$23,\!528.45$	0.5	16.6	19.3	20.3	25.2 ± 1.3	27.8 ± 1.8 ^{<i>j</i>}
23,704.81	1.5	20.4	23.7	24.8	27 ± 1.4	$31.2 \pm 2.5 \ ^{f}$
$23,\!874.95$	2.5	9.2	10.8	11.2	14.7 ± 0.7	16.2 ± 1 ^d
						$14.7 \pm 1.1 \ ^{e}$
24.046.10	2.5	21.6	25.1	26.2	32.1 ± 1.6	16.1 ± 1 f
24.088.54	3.5	81.9	95.6	100		247 ± 12^{e}
,	0.0	0.000				207.5 ± 14.5 ^f
24 173 83	15	9.6	11.4	19	35.0 ± 1.8	207.0 ± 11.0 37.7 ± 1.4 f
24,110.00	3.5	17.0	20.7	21.6	14.3 ± 0.7	$15.7 \pm 0.7 d$
24,409.00	5.5	11.3	20.1	21.0	14.3 ± 0.7	10.7 ± 0.7 $14.6 \pm 1.9.6$
94 507 97	0.5	19 5	15.0	107	10.9 ± 1	14.0 ± 1.2
24,507.87	2.5	13.0	15.9	10.7	19.3 ± 1	21.9 ± 1^{-1}
						19.2 ± 1.5
						22.2 ± 1.9^{-1}
						20 ± 0.8 g
24,639.26	1.5	13.9	16.4	17.3	16 ± 0.8	$14.9 \pm 0.9 \ ^{e}$
24,762.60	1.5	11.3	13.2	13.7	10.6 ± 0.5	$12.4 \pm 1.1 \ ^{e}$
24,910.38	1.5	16.8	19.4	20.3	30.6 ± 1.5	32.4 ± 1.8 ^f
24,984.29	2.5	19.1	22.3	23.4	21.6 ± 1.1	$27.2 \pm 1.9 \ ^{f}$

	I able 5.5: Continued Level Functional (no)											
$\mathbf{D}_{\mathbf{a}}$ (-1)	Level		This work ^o (ns)		DUG	Experiments (ns)						
E^{α} (cm ⁻¹)	J	HFR+NOPOL	HFR+CPOLI	HFR+CPOL2		$a_{1,1} + a_{2,2} = f$						
25,083.36	3.5	9.5	11	11.5	19.1 ± 1	21.1 ± 0.9 ^J						
25,218.27	2.5	9.8	11.6	12.3	14.4 ± 0.7	$15.7 \pm 1.1 \ ^{a}$						
$25,\!380.27$	3.5	13.2	15.6	16.4	21.4 ± 1.1	23.2 ± 1.3 ^J						
25,453.95	0.5	6.6	7.8	8.4	9.6 ± 0.5	$19.4 \pm 0.8 \ ^{a}$						
$25,\!616.95$	0.5	15.3	17.7	18.5	17.8 ± 0.9	$17.6 \pm 1.1 \ ^{f}$						
$25,\!643.00$	1.5	18.7	21.7	22.8	13.7 ± 0.7	$16.2 \pm 0.8 \ ^{e}$						
$25,\!874.52$	5.5	46.4	53	55.4		$61.7 \pm 3.1 \ ^{f}$						
25,950.32	1.5	7.6	8.9	9.5	11.9 ± 0.6	$11.8 \pm 0.9 \ ^{e}$						
25,997.17	4.5	14.1	16.8	17.7	21.2 ± 1.1	$23.3 \pm 1.5 \ ^{d}$						
						$21.8 \pm 0.9 \ ^{f}$						
						21.6 ± 0.6 ^g						
26,338.93	2.5	15.9	18.5	19.3	16.7 ± 0.8	$16.5 \pm 1.2 \ ^{e}$						
27,022.62	2.5	13.7	16.3	16.8	19.5 ± 1	$18.9 \pm 1.4 \ ^{e}$						
						$20.9 \pm 1.3 \ ^{f}$						
27.054.96	4.5	56.5	64.3	67.1		89.7 ± 4.4 ^g						
$27,\!132.44$	3.5	13.5	15.9	16.8	16.4 ± 0.8	$16.6 \pm 1.2 \ ^{e}$						
27.225.26	1.5	9.3	10.8	11.4	15.4 ± 0.8	17.1 ± 0.9^{d}						
27,393,04	2.5	13.1	15.6	16.2	12.4 ± 0.6	14.1 ± 0.6^{d}						
21,000.01	2.0	10.1	10.0	10.2	12.1 ± 0.0	12.6 ± 0.8^{e}						
						12.0 ± 0.0 12.6 ± 0.6						
97 455 91	35	11 1	12.0	13.6	10.6 ± 1	$21.6 \pm 1.6 d$						
21,400.01	5.5	11.1	15.2	15.0	19.0 ± 1	21.0 ± 1.0 10.9 ± 1.4^{e}						
27 610 54	45	10.0	19.7	19 /	12.7 ± 0.6	19.0 ± 1.4 14.9 ± 1.1^{e}						
27,019.04	4.0	10.9	12.7	13.4	12.7 ± 0.0	14.3 ± 1.1 $17.8 \pm 0.0 d$						
21,009.57	2.0	9.0	11.1	11.7	15.7 ± 0.8	17.6 ± 0.9^{-1}						
97 749 07	0.5	10.7	10.0	10.0		15.0 ± 0.7^{-9}						
27,748.97	0.5	10.7	12.0	13.3		27 ± 2.0^{-f}						
27,968.54	1.5	8.6	9.6	10.5	6.5 ± 0.3	9.5 ± 0.9 ^J						
28,039.45	3.5	10.4	12.4	12.9	11.9 ± 0.6	$13 \pm 0.9 \ ^{a}$						
						$11.9 \pm 0.8 e$						
28,089.17	4.5	11.5	13.8	14	18.5 ± 0.9	21.8 ± 1.8 ^J						
28,506.41	2.5	6.2	7.1	7.5	8 ± 0.4	$7.9 \pm 0.3 \ ^{a}$						
						$7.9 \pm 0.4 \ ^{e}$						
$28,\!543.08$	3.5	13.1	15.2	15.9	20.1 ± 1	21.7 ± 1.2 ^d						
						$19.7 \pm 1.1 \ ^{e}$						
28,743.24	5.5	10.9	13.1	13.2	17.8 ± 0.9	$23.8 \pm 1.6 f$						
$28,\!893.51$	0.5	10.3	12.2	12.8		$20 \pm 1.7 \ ^{f}$						
28,971.84	1.5	9.9	11.5	12		$17.2 \pm 1.2 \ ^{f}$						
29,199.57	1.5	8.6	10.1	10.5		15.4 ± 0.8 e						
29,466.67	3.5	12.2	14.2	14.7		$28.3 \pm 0.9 \ ^{f}$						
29,502.18	2.5	11.6	13.4	14.2	11.2 ± 0.6	$10.4 \pm 0.9 \ ^{e}$						
29,564.70	0.5	10.1	11.8	12.6		16.9 ± 0.8 g						
29,775.58	2.5	9.3	11	11.5	13.3 ± 0.7	$12.3 \pm 1.1 \ ^{e}$						
29,894.91	3.5	10.3	12.2	12.6	15.6 ± 0.8	$14.9 \pm 0.8 \ ^{e}$						
29,936.74	1.5	8	9.4	10	13 ± 0.7	$12.5 \pm 0.8 \ ^{e}$						
29,985.46	0.5	9.9	11.7	12.3	15.7 ± 0.8							
30.417.46	1.5	9.3	10.9	11.6	13.7 ± 0.7	$13.6 \pm 0.9 \ ^{e}$						
30.650.28	4.5	13.2	15.3	15.7	21.5 ± 1.1	$20.8 \pm 1.5 \ ^{e}$						
30.788.45	2.5	9.4	10.9	11.4		14.4 ± 1.2^{f}						
30,896,84	2.5	8.8	10.4	10.9	13 ± 0.7	18.6 ± 1.7 ^f						
30 964 71	3.5	82	9.5	9.9	10.1 ± 0.5	11.9 ± 0.6 f						
31,477,22	2.5	5.9	67	7	1011 ± 010	87 ± 0.4^{g}						
31 751 48	0.7 ± 0.22 2.0 0.07 0.1 1 0.1 ± 0.1^{-1}											
32 140 55	$52,140,55,35,52,50,62,76+0,4,73+0.5^{e}$											
02,140.00	$32,140.00$ 3.0 3.0 3.0 3.0 3.0 1.0 ± 0.4 1.0 ± 0.0											
	b: As explained in 5.4.1.											
		~	From Don Horton	111 0.4.1.								
		C:	d. From Diantog	, ci ui. [130]. at al [137]								
			a. From Form of	al [138]								
			f. From Vocaladda	$u_{l}[130]$.								
			a. From Shong a	t = a [130]								
			g. From Shang e	i ui.[199].								

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5.4.3.2 Oscillator Strengths and Transitions Probabilities

In Table 5.6, we give the oscillator strengths and transition probabilities that we computed using the HFR+CPOL2 model⁵ for a set of 392 La I transitions with log gf-values > -1.

These lines appears from 317 nm (near UV) to 7843 nm (mid-infared). The experimental data recently published by Den Hartog *et al.* [135] is also reported for comparison in the table. There are 165 transitions that can be compared between this latter work and ours. It appears that for around more than a half of the lines, the discrepancies between both sets of results do not exceed 25%. Furthermore, for about three-quarter of the transitions, we can note an agreement better than a factor of two between our calculated oscillator strengths and the experimental values. This is illustrated in Figure 5.6 where the HFR+CPOL2 and experimental log gf values are compared. It also appears that the



Figure 5.6: Comparison between the gf obtained in La I with our HFR+CPOL2 model and the experimental ones from [135]. The dashed line corresponds to a perfect agreement and the dotted ones to a discrepancy of a factor of two on the gf-value.

calculated transition rates obtained in the present work can be considered as much more reliable than the theoretical data reported by Karaçoban and Özdemir [136] and Kurucz [14], these two latter data being found to deviate by more than a factor of two from the experimental oscillator strengths, as highlighted by Den Hartog *et al.* [135]. Another interesting comparison is the one that we made between the results obtained with the HFR+CPOL2 model and those deduced from our MCDHF calculation, as described in Section 5.4.2. This comparison is displayed in Figure 5.7.

⁵Chosen because of its better agreement with the experimental data for the atomic structure, as shown in the previous section.



Figure 5.7: Comparison between the gf obtained in La I with our HFR+CPOL2 model and the ones from our MCDHF calculation. The dashed line corresponds to a perfect agreement and the dotted ones to a discrepancy of a factor of two on the gf-value.

As one can see on that figure, the agreement between both theoretical sets of oscillator strengths is found to be rather good especially knowing the complexity of the La I atomic structure. As Figure 5.7 shows, the discrepancies do not exceed 30% for more than half of the transitions (within the limit log gf > -1) and are anyway not larger than a factor of two for 95% of the entire set of common lines. A comparable agreement is observed when comparing our MCDHF calculations to the experimental gf-values of Den Hartog et al. [135], as illustrated in Figure 5.8.

5.4.3.3 Conclusion

In summary, the oscillator strengths and transition probabilities computed here using the HFR+CPOL2 model are expected to be accurate for the vast majority of the La I spectral lines listed in Table 5.6 within at maximum an uncertainty of a factor of two and even better than 30% for many of them. These new atomic and radiative parameters therefore represent the most reliable set of theoretical radiative rates produced up to now in lanthanum atom and can be considered as a valuable complement to the available experimental data from Den Hartog *et al.* [135].

As mentioned before, we computed new reliable oscillator strengths and transition probabilities for 392 spectral lines of neutral lanthanum. This was firstly assessed from



Figure 5.8: Comparison between the gf in La I obtained with our MCDHF calculation and the experimental ones from [135]. The dashed line corresponds to a perfect agreement and the dotted ones to a discrepancy of a factor of two on the gf-value

our detailed comparisons between different theoretical models based on the HFR+CPOL and the MCDHF methods, and secondly between the theoretical results and the available experimental data. Among the La I lines listed in the present work, approximately 60%have gf- and gA-values determined for the first time and that can be of use to the astrophysicists especially knowing that lanthanides have a very hot topic application in astrophysics in the study of kilonovae, as mentioned in Just *et al.* [141].

Table 5.6: Calculated oscillator strengths (log gf) and transition probabilities (gA) for spectral lines in La I

	Lower level ^b		Upper level ^b		This work ^c		$Experiment^{d}$	
λ^a	$E(cm^{-1})$	J	$E(cm^{-1})$	J	log of	$\sigma A (s^{-1})$	log of	$\sigma A (s^{-1})$
217 5082		1.5	21477	25	0.74	1.21E+08	105 51	g.r (5)
201 501	1052	1.5	20141	2.0	-0.74	$1.21E \pm 0.00$	0.40	0.0017.100
321.581	1053	2.5	32141	3.5	-0.45	2.32E+08	-0.49	2.08E+08
324.7034	0	1.5	30788	2.5	-0.99	6.34E + 07		
334.223	1053	2.5	30965	3.5	-0.37	2.53E + 08	-0.14	4.32E + 08
336.2042	1053	2.5	30788	2.5	-0.89	7.32E + 07		
340.4519	1053	2.5	30417	1.5	-0.94	6.62E + 07	-1.01	5.60E + 07
342.3726	0	1.5	29200	1.5	-0.73	1.07E + 08		
346 1184	1053	2.5	29937	1.5	-0.68	$1.16E \pm 0.8$	-0.85	$7.84E \pm 07$
348.0605	1053	2.5	20776	2.5	0.96	$6.09E \pm 07$	0.00	110111-01
250 600	1055	1 5	29110	2.0	-0.30	0.03E+07		
350.098	0	1.5	28500	2.0	-0.87	1.485+07	0.14	0.000
357.4425	0	1.5	27969	1.5	-0.44	$1.90E \pm 08$	-0.14	$3.80E \pm 08$
361.3074	0	1.5	27669	2.5	-0.54	1.47E + 08	-0.73	9.42E + 07
363.6661	1053	2.5	28543	3.5	-0.77	8.52E + 07	-0.94	5.76E + 07
364 1519	1053	2.5	28506	2.5	-0.09	$4.20E \pm 08$	0.04	$5.46E \pm 08$
370 4532	1053	2.5	28030	3.5	0.81	$7.28E \pm 0.7$	0.46	$1.66E \pm 0.8$
370.4332	1055	2.5	20039	0.0	-0.81	0.16E+07	-0.40	1.0012+08
378.0495	1055	2.5	27455	3.5	-0.7	9.105+07		
385.2424	0	1.5	25950	1.5	-0.91	$5.71E \pm 07$	-1.57	1.20E + 07
387.8879	4122	4.5	29895	3.5	-0.91	5.41E + 07	-0.83	6.56E + 07
392.7551	0	1.5	25454	0.5	-0.3	2.21E + 08	-0.37	1.86E + 08
300 4164	3010	2.5	28030	3.5	0.36	$1.70E \pm 0.8$	1 10	$2.72E \pm 0.7$
401 5200	1052	2.0	25055	1 5	0.19	2.79E+00	-1.15	2.120101
401.5588	1055	2.5	25950	1.5	-0.18	2.78E+08	-0.2	2.00E+08
404.3371	2668	1.5	27393	2.5	-0.41	1.55E+08		
406.0316	4122	4.5	28743	5.5	0.34	9.03E + 08	0.22	6.72E + 08
406.4778	3495	3.5	28089	4.5	0.18	6.15E + 08	0.03	4.32E + 08
407.917	0	1.5	24508	2.5	-0.63	$9.56E \pm 07$	-0.56	$1.11E \pm 08$
408 961	3010	2.5	27455	3 5	-0.14	$2.84E \pm 08$	-0.07	$3.36E \pm 0.8$
410 497	2668	1.5	27022	2.5	0.22	1 200 100	0.2	2.47E + 0.08
410.407	2008	1.5	27023	2.5	-0.32	1.895+08	-0.2	2.4712+08
410.9481	1053	2.5	25380	3.5	-0.68	8.32E + 07	-1.11	$3.04E \pm 07$
413.5538	0	1.5	24174	1.5	-0.6	9.84E + 07		
413.7031	1053	2.5	25218	2.5	-0.54	1.08E + 08	-0.53	1.15E + 08
414.3907	3495	3.5	27620	4.5	-0.83	5.83E + 07	-0.77	6.60E + 07
416 0258	1053	2 5	25083	3 5	0.12	$5.04E \pm 08$	-0.62	$9.20E \pm 07$
416 2202	2010	2.5	27022	9.5 9.5	.0.04	4 30 - 07	.0.07	4 08E-107
417 1104	4100	4.0	21020	4.0	-0.94	5 700 - 07	-0.97	9 70E - 07
417.1124	4122	4.5	28089	4.5	-0.82	5.78E+07	-1	3.79E+07
417.231	3495	3.5	27455	3.5	-0.79	6.11E + 07	-0.84	5.52E + 07
417.7481	1053	2.5	24984	2.5	-0.69	8.03E + 07	-0.73	7.08E + 07
418.731	0	1.5	23875	2.5	0.04	$4.27E \pm 08$	-0.06	3.31E + 08
421 6542	1053	2.5	24763	1.5	-0.93	$4.47E \pm 07$	-1 47	$1.28E \pm 0.7$
427.1148	7401	1.5	30807	2.5	0.53	$1.00E \pm 08$	0.45	1.20E + 07 $1.30E \pm 08$
427.1148	1491	1.5	30897	2.5	-0.55	1.09E+08	-0.45	1.5012+08
428.0256	1053	2.5	24410	3.5	-0.53	1.09E + 08	0.1	$4.55E \pm 08$
429.3445	7680	2.5	30965	3.5	-0.79	5.80E + 07	-1.41	1.44E + 07
430.5996	7680	2.5	30897	2.5	-0.27	1.97E + 08	-0.38	1.51E + 08
431.1725	7231	0.5	30417	1.5	-0.74	6.58E + 07	-0.91	4.40E + 07
434.072	8446	1.5	31477	2.5	-0.03	3.33E + 08		
435 4793	9184	2.5	32141	3.5	0.23	$6.01E \pm 08$	0.13	$4.72E \pm 0.8$
400.4730	0044	0.5	21751	1.5	0.20	1.42E + 08	0.15	4.1211+00
440.204	9044	0.5	31/31	1.5	-0.39	1.436+08		
440.3015	7231	0.5	29937	1.5	-0.87	4.64E + 07	-0.9	$4.36E \pm 07$
442.3905	8052	3.5	30650	4.5	0.22	5.69E + 08	0.14	4.65E + 08
444.2675	3495	3.5	25997	4.5	-0.93	4.01E + 07	-0.95	3.76E + 07
444.4197	7491	1.5	29985	0.5	-0.43	1.25E + 08	-0.52	1.00E + 08
445 2149	7012	2.5	29467	3.5	0.02	$3.50E \pm 08$		
446 8065	2010	2.5	25280	2.5	0.02	4 10E 07	0.80	$4.94 E \pm 0.7$
440.8903	3010	2.5	20000	3.5	-0.92	4.105+07	-0.89	4.2415+07
447.4538	8446	1.5	30788	2.5	-0.39	1.30E + 08		
448.6053	7491	1.5	29776	2.5	-0.17	2.29E + 08	-0.4	1.31E + 08
449.1748	7680	2.5	29937	1.5	-0.44	1.20E + 08	-0.54	9.44E + 07
449,904	9920	4.5	32141	3.5	-0.01	$3.23E \pm 08$	-0.28	$1.71E \pm 08$
450 0206	7680	2.5	29895	3.5	0.15	$4.70E \pm 0.8$	0.07	$3.83E \pm 08$
450 1565	2010	2.5	25010	2.5	0.67	6 78E 07	1 01	2.04E+07
450.1505	5010	2.5	20210	2.5	-0.07	0.185+07	-1.21	$2.04E \pm 07$
454.1773	7491	1.5	29502	2.5	-0.59	$8.06E \pm 07$	-0.46	1.12E + 08
454.9498	3010	2.5	24984	2.5	-0.93	3.90E + 07	-0.46	1.11E + 08
455.0164	2668	1.5	24639	1.5	-0.4	1.27E + 08	-1.57	8.68E + 06
455.0766	7231	0.5	29200	1.5	-0.64	7.57E + 07		
456 7904	3495	3.5	25380	3.5	-0.05	$2.86E \pm 0.8$	-0.09	$2.62E \pm 0.8$
457 0022	4122	4.5	25000	4.5	0.17	4.86E+08	0.12	4.241 00
450.0040	7200	4.0	20331	4.0	0.11	1.0512-00	0.10	9 76E - 05
408.1197	080	2.5	29502	2.5	-0.2	1.955+08	-0.00	0.10E+07
458.989	9184	2.5	30965	3.5	-0.38	1.30E + 08		
459.8436	7231	0.5	28972	1.5	-0.8	5.01E + 07		
460.4237	9184	2.5	30897	2.5	-0.26	1.76E + 08	-0.46	1.08E + 08
461.5064	7231	0.5	28894	0.5	-0.49	1.02E + 08		
462 2072	3010	2.5	24639	1.5	-0.97	$3.27E \pm 07$		
464 3120	7012	2.5	28543	3.5	_0.0	$3.92E \pm 07$	-1.01	$3.05E \pm 07$
161 6995	0061	2.0 9 F	21/77	0.0 0 =	-0.9	2 04E 1 00	-1.01	0.000-01
404.0000	9901	0.0	04500	4.0	-0.03	2.34D+00	0.00	9.947 . 07
465.0322	3010	2.5	24508	2.5	-0.55	8.90E+07	-0.98	3.24E + 07
465.1874	8446	1.5	29937	1.5	-0.86	4.24E + 07	-1.15	2.16E + 07
465.3905	7491	1.5	28972	1.5	-0.42	1.16E + 08		
470.2641	4122	4.5	25380	3.5	-0.83	4.50E + 07	-0.89	3.92E + 07
470.8186	9184	2.5	30417	1.5	-0.3	$1.51E \pm 08$	-0.57	$8.12E \pm 07$
473 3896	8446	1.5	29565	0.5	-0.67	$6.21E \pm 07$		
475 0410	0020	1.5	30065	2 5	.0.99	1 71 8-1 09	.0.01	2 885.100
475.0419	9920	4.0	30303	0.0	-0.23	1.115+00	-0.01	2.0010+00
4/5.9/11	9961	3.5	30965	3.5	-0.97	3.13E+07	-0.82	4.48E+07
476.6891	0	1.5	20972	2.5	-0.46	1.02E + 08	-0.62	7.08E + 07
477.0425	7012	2.5	27969	1.5	-0.51	9.08E + 07	-0.46	1.02E + 08
479.9992	9961	3.5	30788	2.5	-0.34	1.27E + 08		
481.7112	8446	1.5	29200	1.5	-0.51	9.09E + 07		
481 7947	0184	2.0 2 K	20037	1 5	.0.86	3 98 - 107	0.61	7.001-07
402.051	9104	2.0	29931	1.0	-0.60	0.000 +07	-0.01	0.605+07
483.9514	7012	2.5	27669	2.5	0.02	2.92E+08	-0.03	2.03E+08
485.0812	1053	2.5	21663	3.5	-0.46	$9.95E \pm 07$	-0.76	4.96E + 07
485.495	9184	2.5	29776	2.5	-0.33	1.36E + 08	-0.24	1.62E + 08
487.0558	8446	1.5	28972	1.5	-0.73	5.28E + 07		
487.8848	8052	3.5	28543	3.5	-0.1	2.26E + 08	-0.17	$1.90E \pm 0.08$
488 7505	8052	35	28506	2.5	-0.14	$2.12E \pm 0.00$	-0.56	$7.68E \pm 07$
400.1000	1052	ວ.ວ ດະະ	21110	2.0	0.14	3 05 - 07	0.00	3 765 107
490.1807	1003	4.0	21448	3.5	-0.00	3.90E+U/	-0.07	5.70E+07
492.0278	9184	2.5	29502	2.5	-0.75	4.83E + 07		a a :=
494.5845	7012	2.5	27225	1.5	-0.79	4.39E + 07	-0.88	3.64E + 07
494.9765	0	1.5	20197	0.5	-0.19	1.72E + 08	-0.18	1.80E + 08
497.7952	0	1.5	20083	1.5	-0.95	2.91E + 07	-1.35	$1.20E \pm 07$
500 1785	8052	3.5	28039	3.5	-0.51	$7.93E \pm 07$	-0.19	$1.70E \pm 0.8$
504.0071	2405	0.0	20008	0.0	-0.51	1.0512-00	0.13	0.04E - 05
504.6871	3495	3.5	23303	3.5	-0.4	1.05E+08	-0.46	9.048+07
505.0564	3010	2.5	22804	2.5	-0.29	1.34E + 08	-0.3	1.30E + 08
505.6459	2668	1.5	22439	1.5	-0.43	$9.59E \pm 07$	-0.46	$9.04E \pm 07$

Table 5.6: Continued

	Lower level ^b		Upper level ^b		This work c		$Experiment^d$	
λ^a	$E (cm^{-1})$	J	$E (cm^{-1})$	J	log gf	$gA(s^{-1})$	log gf	$\frac{gA(s^{-1})}{2}$
510.6233	2668	1.5 4.5	22247 29467	0.5	-0.05	2.23E+08 4.35E+07	-0.08	2.10E + 08
514.5417	3010	2.5	22439	1.5	0.16	3.57E+08	0.12	3.28E + 08
515.2367	8052	3.5	27455	3.5	-0.77	4.23E + 07		
515.8681	0	1.5	19379	2.5	-0.57	6.72E+07	-0.58	6.60E+07
516.7783	4122 3495	4.5	23467 22804	4.5 2.5	-0.8	$3.98E \pm 07$ 5.40E \pm 08	-0.73	4.60E+07 4.92E+08
517.9119	8446	1.5	27749	0.5	-0.76	4.23E+07	0.0	4.0211 00
518.391	1053	2.5	20338	2.5	-0.91	2.97E + 07	-0.86	3.42E + 07
521.1854	4122	4.5	23303	3.5	0.48	7.43E+08	0.21	3.98E + 08
523.4274	4122 1053	4.5 2.5	23221 20019	3.5	-0.84	$3.52E \pm 07$ 2.59E \pm 08	0.14	3.38E+08 1.60E+08
527.6413	8446	1.5	27393	2.5	-0.58	6.17E+07	-0.48	7.98E+07
530.1974	9184	2.5	28039	3.5	-0.44	8.34E + 07		
530.4012	7491	1.5	26339	2.5	-0.69	4.71E + 07	-0.48	7.80E + 07
532.3555	8446 7231	1.5	27225	1.5	-0.67	$5.02E \pm 07$ 2.72E \pm 07	-0.95	2.64E + 07
535.7856	7680	2.5	26339	2.5	-0.25	1.28E+08	-0.2	1.48E + 08
536.8136	9920	4.5	28543	3.5	-0.61	5.69E + 07		
538.0005	9961	3.5	28543	3.5	-0.71	4.57E + 07	-0.65	5.20E + 07
545.5142	1053	2.5	19379	2.5	0.16	3.26E + 08	0.04	2.44E + 08
549.106	7012	2.5	25218	2.5	-0.69	4.32E+07	-0.84	$3.24E \pm 07$
550.1337	0	1.5	18172	1.5	0.07	2.55E + 08	-0.03	2.05E + 08
550.2246	9920	4.5	28089	4.5	-0.77	3.73E + 07	-0.6	5.60E + 07
551.5274	7491	1.5	25617	0.5	-0.46	7.24E + 07	-0.61	5.32E + 07
552 9882	9920	4.5 3.5	28039	3.5 3.5	-0.75	$1.17E \pm 0.08$	-0.62	5.20E+0.07
554.1249	9184	2.5	27225	1.5	-0.14	1.57E + 08	-0.25	1.22E + 08
554.4916	9719	1.5	27749	0.5	-0.43	8.03E + 07		
556.5434	7680	2.5	25643	1.5	-0.33	9.81E + 07	-0.46	7.44E + 07
558.5518	9184 7012	⊿.ə 2.5	24910	$\frac{5.5}{1.5}$	-0.49	$2.62E \pm 07$		
558.8328	3495	3.5	21384	4.5	-0.61	5.19E + 07	-0.49	6.90E + 07
563.1222	3010	2.5	20763	3.5	-0.5	6.52E + 07	-0.41	8.16E + 07
564.5449	9961	3.5	27669	2.5	-0.71	4.06E + 07	0.41	F 00F 100
565 4868	9920 7231	$^{4.0}_{0.5}$	27620	4.5 1.5	-0.44	$5.81E \pm 08$ 7 41E \pm 07	-0.96	2.33E+08 2.28E+07
565.6586	9719	1.5	27393	2.5	-0.65	4.53E+07	-0.64	4.80E + 07
565.7719	2668	1.5	20338	2.5	-0.65	4.54E + 07	-0.58	5.52E + 07
567.1428	7012	2.5	24639	1.5	-0.89	2.62E + 07		
571.4527	9961	0.5 3.5	27455	1.5 3.5	-0.55	$5.69E \pm 07$		
571.4735	7491	1.5	24984	2.5	-0.77	3.58E + 07		
573.4941	9961	3.5	27393	2.5	-0.89	2.55E + 07	-0.36	8.94E + 07
574.0652	2668	1.5	20083	1.5	-0.08	1.63E + 08	-0.33	9.52E + 07
574.4403 576.9324	3010	2.5 2.5	20338	$\frac{3.5}{2.5}$	-0.31	$9.86E \pm 07$ $1.95E \pm 08$	-0.03	$2.44E \pm 08$ $1.87E \pm 08$
577.7682	9719	1.5	27023	2.5	-0.96	2.14E+07	0100	1012100
578.8086	7491	1.5	24763	1.5	-0.32	9.78E + 07		
578.9224	3495	3.5	20763	3.5	0.19	3.07E + 08	0.1	2.48E + 08
580.8081	9920	4.5	21384 27132	4.5 3.5	-0.4	4.07E+08 7.96E+07	0.5	3.95E+08
582.1977	9961	3.5	27132	3.5	0.1	2.51E + 08	0.17	2.94E + 08
582.3818	8052	3.5	25218	2.5	-0.38	7.79E + 07	-0.4	7.86E + 07
582.5238	7012	2.5	24174	1.5	-0.48	6.48E + 07	0.6	4.09 - 07
584.8365	9184 9961	2.5 3.5	20339	2.5 4.5	-0.17	1.30E+08	-0.0	4.926+07
585.2267	7680	2.5	24763	1.5	-0.42	7.62E + 07	-0.87	2.64E + 07
585.5586	3010	2.5	20083	1.5	-0.81	2.89E + 07	-0.78	3.24E + 07
586.995	8052	3.5	25083	3.5	-0.89	2.46E+07 5.97E+07	-1.16	1.33E+07 6 18E+07
590.4296	8052	3.5	24984	2.5 2.5	-0.88	2.59E+07	-1.01	1.86E+07
593.0608	1053	2.5	17910	3.5	-0.57	5.15E + 07	-0.55	5.36E + 07
593.0681	0	1.5	16857	2.5	-0.65	4.46E + 07	-0.79	3.10E + 07
593.5285	3495	3.5	20338	2.5	-0.77	$3.13E \pm 07$	-0.73	$3.54E \pm 07$ $2.76E \pm 07$
597.5723	7680	2.5	23218 24410	3.5	-0.04	1.71E+08	-0.93	2.19E+07 2.19E+07
599.5495	13631	2.5	30306	2.5	-0.73	3.51E + 07		/
600.736	4122	4.5	20763	3.5	-0.82	2.74E + 07	-0.83	2.80E + 07
603.8500	13260	1.5 1 K	29875	1.5 2 K	-0.36	7.69E+07 9.10E-07	.0 52	5 40EJ 07
606.8711	7231	0.5	23705	1.5	-0.54	5.13E+07 5.13E+07	-0.59	4.68E+07
607.0418	15220	0.5	31689	1.5	-0.99	1.84E + 07		
607.5237	8052	3.5	24508	2.5	-0.9	2.36E+07	0.24	9 16E - 0F
610.8477	7680	2.5	24046	2.5	-0.3	$8.84E \pm 07$ $3.68E \pm 07$	-0.34	8.16E + 07
612.577	15032	1.5	31352	2.5	-0.93	2.09E + 07		
613.4384	7231	0.5	23528	0.5	-0.55	4.82E + 07	-0.59	4.60E + 07
614.2961	13631	2.5	29905	2.5	-0.13	1.29E+08		
014.5306 616.4080	15020	3.5 1.5	31288 31248	3.5 1 5	-0.62	4.07E+07 6.69E±07		
616.5693	7491	1.5	23705	1.5	-0.44	6.18E + 07	-0.41	6.80E + 07
621.821	9920	4.5	25997	4.5	-0.94	2.04E+07		
621.9456	14096	0.5	30170	1.5	-0.62	4.16E + 07		
624 9909	9184 4122	2.5 4.5	25218 20117	⊿.5 5.5	-0.81	2.53E+07 4.86E±08	0.41	$4.42E \pm 0.8$
626.6013	9920	4.5	25875	5.5	0.06	1.96E + 08	0.06	1.94E + 08
627.827	14096	0.5	30019	0.5	-0.84	2.42E + 07		
629.3556	3495	3.5	19379	2.5	-0.92	2.02E + 07	-0.78	2.76E + 07
631 75	15504	⊿.ə 3.5	31352	⊿.ə 4.5	-0.19	$5.46E \pm 07$		
632.5908	1053	2.5	16857	2.5	-0.89	2.27E + 07	-0.8	2.62E + 07
633.3798	15504	2.5	31288	3.5	-0.58	4.56E + 07		
635.6416	8446	1.5	24174	1.5	-0.45	5.93E+07		
639 4227	16243	4.5	31924 10120	4.5 4 5	-0.85 0.33	$2.32E \pm 07$ 3 56E ± 08	0.27	3.01E⊥08
640.9845	14709	1.5	30306	2.5	-0.82	2.54E+07	0.21	0.010700
641.0984	3010	2.5	18604	3.5	0.06	1.88E + 08	-0.07	1.37E + 08
642.6591	15504	2.5	31060	3.5	-0.98	1.74E + 07		
645 4502	2668	1.5 1.5	20218 18157	2.5 2.5	-0.7	3.06E+07 1.14E±08	-0.57	$4.32E \pm 0.07$
645.5984	1053	2.5	16538	3.5	-0.26	8.89E + 07	-0.34	7.36E+07
648.5531	8052	3.5	23467	4.5	-0.64	$3.67E \pm 0.7$	-0.69	$3.30E \pm 0.07$

Table 5.6: Continued

	Lower level ^b		Upper level ^b		This work ^{c}	1.	$Experiment^d$	1.
λ^a 650.6187	$\frac{E (cm^{-1})}{14804}$		$\frac{E (cm^{-1})}{30170}$	J 1.5	log gf -0.38	$\frac{\text{gA} (\text{s}^{-1})}{6.50\text{E}\pm07}$	log gf	gA (s ⁻¹)
652.3878	9184	2.5	24508	2.5	-0.84	2.32E+07		
652.9738	14709	1.5	30019	0.5	-0.28	8.42E+07		
654.0084 656.595	15020 9184	$\frac{3.5}{2.5}$	$30306 \\ 24410$	$\frac{2.5}{3.5}$	-0.24 -0.87	2.13E+07		
657.8502	0	1.5	15197	2.5	-0.61	3.72E + 07	-0.61	3.84E + 07
658.2197	16099	3.5	31288	3.5	0.09	2.01E + 08	1.02	1471-07
660.7728	9044	2.5	24174	$\frac{2.5}{1.5}$	-0.92	3.26E+07	-1.02	1.476+07
660.8239	9961	3.5	25089	4.5	-0.15	1.12E + 08		
661.6572 663.3476	3495 14804	3.5	18604 20875	3.5	-0.76	2.69E+07 5.07E+07	-0.74	2.78E + 07
664.5148	16243	4.5	31288	3.5	0.18	2.26E+08		
666.139	4122	4.5	19129	4.5	-0.74	2.79E + 07	-0.59	3.90E + 07
667.6849 670.9481	15197	2.5	30170	1.5	-0.79	2.49E+07 6.43E+07	0.23	8 72E±07
671.5948	15020	3.5	29905	2.5	-0.68	2.91E+07	-0.25	0.1211-01
674.8109	8446	1.5	23261	0.5	-0.83	2.26E + 07		
682.3775 691.6659	7012 17023	2.5	$21663 \\ 31477$	3.5	-0.78	2.41E+07 1.47E+07	-0.48	4.72E + 07
692.524	7012	2.5	21448	3.5	-0.14	1.03E+08	-0.3	6.96E+07
697.6842	9920	4.5	24249	4.5	-0.63	3.13E+07	0.1	1.051.000
702.3688	8052 9044	3.5	22286	4.5	-0.05	1.25E+08 3.45E+07	-0.1	1.07E + 08
704.5963	2668	1.5	16857	2.5	-0.42	5.38E + 07	-0.47	4.50E + 07
705.9527	17947	2.5	32108	3.5	-0.75	2.31E + 07		
707.6374	9961 15020	3.5	24089 29046	3.5	-0.71	2.56E+07 1.84E+07		
716.1216	7012	2.5	20972	2.5	-0.12	9.78E+07	-0.25	7.32E+07
716.6031	14804	2.5	28755	2.5	-0.97	1.39E + 07		<i>'</i>
723.1903 726.2753	17141	4.5	30965 30788	3.5 2.5	-0.61	3.02E+07 $6.51E\pm07$		
734.5327	8052	3.5	21663	$^{2.0}_{3.5}$	0.02	1.31E+08	-0.17	8.24E+07
737.9665	9920	4.5	23467	4.5	-0.3	6.19E + 07	-0.16	8.60E + 07
738.2683	9719 18172	1.5	23261	0.5	-0.57	3.45E+07 5.56E-07		
743.7636	17910	$^{1.0}_{3.5}$	31352	$^{1.0}_{2.5}$	-0.55	2.54E+07		
745.8144	17947	2.5	31352	2.5	-0.95	1.33E + 07		
746.3028	8052	3.5	21448	3.5	-0.7	2.46E + 07	-0.5	3.76E + 07
750.9376	16857	$\frac{2.5}{2.5}$	30170	3.5 1.5	-0.39	$4.84E \pm 07$ $1.53E \pm 07$		
756.8598	17910	3.5	31119	2.5	-0.84	1.63E + 07		
763.6844	18157	2.5	31248	1.5	-0.32	5.36E + 07		
781.2982	19129	2.5 4.5	31925	3.5	-0.40	2.07E+07		
784.2407	18604	3.5	31352	2.5	-0.37	4.50E + 07		
790.3695	18316	4.5	30965	3.5	-0.35	4.63E + 07		
796.1502	17797 19379	1.5 2.5	30354 31925	2.5	-0.9	1.41E+07 2.35E+07		
798.815	18604	3.5	31119	2.5	-0.57	2.74E+07		
800.1873	3010	2.5	15504	2.5	-0.96	1.11E + 07		
802.8791 808.4499	17567	0.5 4.5	30019	$0.5 \\ 4.5$	-0.99	1.10E+07 3.73E+07	-0.57	2 70E±07
810.192	18311	5.5	30650	4.5	-0.33	4.83E+07	-0.01	2.1011101
811.0853	17141	4.5	29467	3.5	-0.37	4.31E + 07		
816.1092	13747	4.5	25997	4.5	-0.97	1.11E+07 1.84E+07		
832.4721	3495	3.5	15504	2.5	-0.64	2.14E+07		
833.4405	17910	3.5	29905	2.5	-0.35	4.08E + 07		
834.6542 837.966	4122	4.5 4.5	16099	3.5	-0.31	4.42E+07 7 70E+07		
846.7526	20117	5.5	31924	4.5	0.13	1.29E + 08		
851.3598	9920	4.5	21663	3.5	-0.75	1.69E + 07		
852.0643 854 3427	18172	1.5	29905 30306	2.5	-0.78	1.50E+07 9.37E+06		
854.3488	9961	3.5	21663	3.5	-0.66	2.09E+07	-0.53	2.72E + 07
854.5451	3010	2.5	14709	1.5	-0.76	1.52E + 07		
855.908	19379	2.5	31060	3.5	-0.66	2.03E+07 1.95E+07		
867.212	9920	4.5	23835	3.5 3.5	-0.75	1.64E+07	-0.5	2.80E + 07
867.4419	3495	3.5	15020	3.5	-0.94	1.08E + 07		<i>,</i>
870.3136 874 8416	9961 2668	3.5	$21448 \\ 14096$	3.5	-0.74	1.65E+07 $1.07E\pm07$		
880.1268	20393	0.5	31751	1.5	-0.73	1.60E+07		
881.8966	13747	4.5	25083	3.5	-0.97	9.08E + 06		
882.167	20019	1.5 2 K	31352	2.5 2.5	-0.7	1.68E + 07 2 50E 1.07	.0.56	2 34EJ 07
895.6565	18038	1.5	29200	1.5	-0.85	1.21E+07	-0.00	2.0411707
895.776	7012	2.5	18172	1.5	-0.67	1.75E + 07	-0.67	1.80E + 07
904.693 907 9116	20197 9961	$0.5 \\ 3.5$	$31248 \\ 20972$	1.5 2.5	-0.81	1.28E+07 $3.13E\pm07$	-0.29	4 14E±07
908.9274	18777	2.5	29776	2.5 2.5	-0.81	1.30E+07	-0.23	
912.7555	20972	2.5	31925	3.5	-0.99	7.96E + 06		
915.7172 922.6652	12787	2.5	23705	1.5	-0.78	1.29E + 07 9.70E + 06		
925.0058	13238	3.5	24046	2.5	-0.59	1.96E+07	-0.57	2.10E + 07
932.8854	20972	2.5	31689	1.5	-0.68	1.60E + 07		
937.6175 948.51	13747 21384	4.5 4 5	24410 31994	3.5 4.5	-0.59	1.97E+07 8 76E+07		
954.1972	21448	4.5 3.5	31925	4.5 3.5	-0.71	1.36E+07		
957.0444	21663	3.5	32108	3.5	-0.95	7.73E + 06		
964.0855	17023	3.5 3 E	27393	2.5 3 5	-0.34	3.16E + 07 5.47E + 07	-0.18	4.74E + 07
970.9394 972.9114	20703	$^{3.5}_{2.5}$	31248	$^{3.5}_{1.5}$	-0.13	9.81E+06		
973.7092	7680	2.5	17947	2.5	-0.85	1.00E + 07	-0.97	7.50E + 06
974.1552	21663	3.5	31925	3.5	-0.48	2.21E + 07		
977.5166 980.4358	18316 21944	$^{4.5}_{3.5}$	28543 32141	3.5 3.5	-0.74	1.27E+07 1.30E+07		
985.2573	20972	2.5	31119	2.5	-0.34	3.03E + 07		
991.119	20083	1.5	30170	1.5	-0.57	1.96E + 07		
999.7999 1000 5724	17023	3.5 4.5	27023 27132	$^{2.5}_{3.5}$	-0.86	9.03E+06 5.72E+07	-0.04	$6.08E \pm 07$
1002.9997	20338	2.5	30306	2.5	-0.58	1.86E + 07	0.01	
1006.6821	18038	1.5	27969	1.5	-0.98	6.80E + 06		

	Lower level ^b		Upper level ^b		This work ^{c}		$Experiment^d$	
λ^a	$E (cm^{-1})$	J	$E (cm^{-1})$	J	log gf	$gA(s^{-1})$	log gf	$gA(s^{-1})$
1011.2194	20019	1.5	29905	2.5	-0.78	1.04E + 07		
1013.0834	18311	5.5 4 5	28179	5.5 2 5	-0.85	9.04E + 06 1.07E + 07		
1018.4625	12431	1.5	22247	0.5	-0.73	1.21E+07 1.21E+07	-0.62	$1.54E \pm 07$
1020.963	20083	1.5	29875	1.5	-0.89	8.57E + 06		
1021.989	21969	2.5	31751	1.5	-0.34	2.96E + 07		
1027.4898	18777	2.5	28506	2.5	-0.46	2.42E + 07		
1028.147	18316	4.5	28039	3.5	-0.38	2.42E + 07		
1029.4429	18038	1.5	27749	0.5	-0.99	6.14E + 06		
1031.8059	21663	3.5	31352	2.5	-0.88	7.90E+06		
1033.0277	20197	0.5 4.5	29875	1.0	-0.85	$1.12E \pm 0.07$		
1033.7188	21384	3.5	31119	2.5	-0.34	2.67E+07		
1034.9172	9719	1.5	19379	2.5	-0.77	1.07E + 07		
1035.7755	12787	2.5	22439	1.5	-0.54	1.76E + 07	-0.47	2.12E + 07
1037.143	22286	4.5	31925	3.5	-0.19	3.74E + 07		
1044.9646	20338	2.5	29905	2.5	-0.9	7.82E + 06		
1045.0906	13238	3.5	22804	2.5	-0.37	$2.59E \pm 07$	-0.38	$2.58E \pm 07$
1040.178	13/4/	4.5	23303	3.0	-0.19	3.95E+07 7 41E+06	-0.57	2.04E+07
1048.6541	21944	3.5	31477	2.5	-0.88	8.26E+06		
1051.4688	21969	2.5	31477	2.5	-0.97	6.64E + 06		
1057.1829	21663	3.5	31119	2.5	-0.92	6.62E + 06		
1063.8575	21663	3.5	31060	3.5	-0.94	6.62E + 06		
1073.9789	18311	5.5	27620	4.5	0.1	7.40E+07		
1093.5386	20763	3.5	29905	2.5	-0.82	$8.36E \pm 06$		
1093.8005	22804	4.0 25	2/400 31095	3.0 3.5	-0.62	1.29E+07 7.91E±06		
1110.6662	22247	0.5	31248	1.5	-0.85	7.92E+06		
1115.9028	16991	0.5	25950	1.5	-0.91	6.95E + 06		
1121.7452	22439	1.5	31352	2.5	-0.82	8.18E + 06		
1128.6458	21448	3.5	30306	2.5	-0.88	6.67E + 06		
1139.4294	22286	4.5	31060	3.5	-0.83	7.33E+06		
1143.972	18316	4.5	27055	4.5	-0.79	8.00E+06		
1144.0872	0184	4.5	23875	3.5	-0.85	$7.44E\pm06$		
1151.2147	9920	4.5	18604	3.5	-0.96	5.62E+06		
1151.8035	22439	1.5	31119	2.5	-0.67	1.08E + 07		
1154.5037	20083	1.5	28742	1.5	-0.95	5.79E + 06		
1159.6811	23303	3.5	31924	4.5	-0.08	4.23E + 07		
1182.0631	21448	3.5	29905	2.5	-0.71	8.50E + 06		
1183.2985	18777	2.5	27225	1.5	-0.93	5.66E+06		
1202 35	20338	2.5	28755	2.5	-0.86	5.13E+06		
1207.0127	20763	3.5	29046	3.5	-0.88	$6.14E \pm 0.06$		
1210.991	22804	2.5	31060	3.5	-0.38	1.95E + 07		
1245.3833	16735	1.5	24763	1.5	-0.83	6.67E + 06		
1251.1674	9920	4.5	17910	3.5	-0.69	8.88E + 06		
1252.1106	23303	3.5	31288	3.5	-0.61	1.07E + 07		
1279.4518	23875	2.5	31089	1.5	-0.48	1.27E+07 5.52E+06		
1300 6688	18311	5.5	25997	4.5	-0.88	4.63E+06		
1304.5776	17099	2.5	24763	1.5	-0.67	8.81E + 06		
1306.4272	12431	1.5	20083	1.5	-0.67	7.76E + 06		
1309.1039	13747	4.5	21384	4.5	-0.19	2.50E + 07		
1310.5444	22247	0.5	29875	1.5	-0.91	4.97E + 06		
1321.7602	18311	5.5 3 K	25875	5.5 2 K	-0.53	1.14E+07 4.37E±06		
1323.9928	12787	$\frac{0.0}{2.5}$	20338	$\frac{2.5}{2.5}$	-0.52	4.5712+00 8.80E+06		
1328.5602	13238	3.5	20763	3.5	-0.41	1.42E + 07		
1465.8062	24089	3.5	30909	2.5	-0.6	7.60E + 06		
1475.9447	18316	4.5	25089	4.5	-0.79	5.26E + 06		
1486.3792	25415	2.5	32141	3.5	-0.84	4.43E+06		
1517.4482	23467	4.5	30055	3.5	-0.9	3.66E+06		
1572.4612	23221	3.5 2m	29079	2.5 2 K	-0.61	7.04E+06 5.00E+06		
1624.8588	24249	$\frac{2.0}{4.5}$	2000	3.5 3.5	-0.46	1.07E+07		
1640.6878	24841	5.5	30935	4.5	-0.32	1.45E + 07		
1647.238	16735	1.5	22804	2.5	-0.97	2.57E + 06		
1666.4281	21969	2.5	27969	1.5	-0.96	2.65E + 06		
1686.7932	25997	4.5	31924	4.5	-0.63	5.34E+06		
1589.1713	25559	1.5 3 ¤	31477	2.5	-0.82	3.66E+06 3.23E+06		
1889 6931	25007	5.5 4.5	31288	3.5	-0.82	2.23E+00 $2.26E\pm06$		
2321.1898	17141	4.5	21448	3.5	-0.53	3.98E+06		
2515.1319	18311	5.5	22286	4.5	-0.39	4.83E + 06		
2531.7177	17023	3.5	20972	2.5	-0.99	1.11E + 06		
2906.0572	27620	4.5	31060	3.5	-0.95	8.68E+05		
2987.2656	18316	4.5	21663	3.5	-0.91	1.03E+06 1.01E+06		
3143.0848	28743	0.5 4 ⊑	31924	4.5 3 ¤	-0.54	1.91E+06 8 75E + 05		
4080.4865	27455	3.5	29905	2.5	-0.95	4.30E+05		
4472.6128	29905	2.5	32141	3.5	-0.93	4.71E + 05		
7842.7216	30650	4.5	31925	3.5	-0.9	1.16E + 05		

Table 5.6: Continued

 2.5
 32141
 3.5
 -0.93
 4.71E+05

 4.5
 31925
 3.5
 -0.9
 1.16E+05

 a: Air wavelength calculated using the Edlen formula.
 b: Energies from the NIST compilation.
 c: Calculated with our HFR+CPOL2 model.

 d: From [135].
 d: From [135].

5.5 Ba I

Barium (Z = 56) is a soft, silvery alkaline earth metal. The element barium was identified for the first time in 1774, but was only reduced to a metal 34 years later with the advent of electrolysis. The name barium comes from the Greek *barys*, meaning heavy.

Barium lines are present in abnormally large quantities in the spectrum of a distinct class of peculiar giant stars that were named Barium stars. The spectral data for the strong lines of s-process elements, such as Ba II at 455.4 nm, was very useful in order to determine the chemical abundances, which are very important to build and put to the test the theoretical stellar models (see e.g. [142]). The atomic radiative lifetimes, transition probabilities, and oscillator strengths are very important data especially for the study of isotopes, atomic structure calculations, and element abundance analyses. Thus, the transition probabilities and oscillator strengths of barium, which can be deduced by combining the measured radiative lifetimes with experimental or theoretical branching fractions, are of crucial importance.

Not having taken part in the experimental measurements since these were carried out by our collaborators at the University of Jilin in China, they will not be described in this manuscript as the method used is TR-LIF spectroscopy and is described in the section 5.2. We will focus in this chapter on the results that we obtained i.e. the semi-empirical gA and gf that we determined in a similar way as we did with Ir I and II (see Section 5.2).

The physical model we used was built to take into account the effects of high Rydberg states. Therefore, the CI model considered for the HFR+CPOL calculations was constituted of the following configurations: $6s^2$, 6s(n=7-25)s, 6s(n=5-25)d, 6s(n=5-25)g, , $5d^2$, 5d(n=6-8)d, 5d(n=7-8)s, $6p^2$, 6p4f and $4f^2$ for the even parity and 6s(n=6-25)p, 6s(n=4-25)f, 5d(n=6-9)p and 5d4f the odd one. In other words, we assumed that the Ba I atomic system is composed of a Ba III ionic core with 54 electrons surrounded by 2 valence electrons. The intravalence correlation was considered through the configuration interaction (CI) by explicitly including the CI expansions mentioned here above in the calculations.

The core-polarization effects were taken into account by considering the core polarizability of the Ba III ionic core as calculated by Johnson *et al.* [143]: $\alpha_d = 1.921$ a.u. The cut-off radius was chosen to be the average radius of the outermost core orbital (5p) obtained from our HFR calculations: $r_c = 10.61$ a.u. In addition, we applied a least-squares fitting procedure to the radial parts, as explained in Chapter 2.2 which was based upon the experimental energy levels obtained by Curry *et al.* [144]. The standard deviations of the fits were found to be respectively 150 and 134 cm⁻¹ for the even and odd parities.

The transition probabilities and oscillator strengths were obtained by combining the experimental lifetimes measured by our collaborators at the University of Jilin in China and the theoretical BFs we obtained using the HFR+CPOL model describe above. Those results are reported in Table 5.7. These correspond to 46 Ba I spectral lines within the wavelength range from 240 to 3765 nm. Regarding the BFs, we only give the values larger than 0.1 in the table, most of the weaker decay channels are found to be affected by large cancellation effects in our calculations ($CF \leq 0.05$). The estimated uncertainties of the transition probabilities and oscillator strengths obtained are given using the same letter coding as the one usually used in the NIST database [28]. They were evaluated following a very similar procedure as the one used for Ir I and Ir II and explained in Section 5.2.

Firstly, an uncertainty was assigned to each of our calculated BF values by comparing them to those deduced from recent experimental measurements for some transitions by Wang *et al.* [145]. That comparison allowed us to point out some regular trends as far as the discrepancies between theoretical and experimental branching fractions were concerned. More precisely, the mean deviations $\langle \frac{BF_{calc}-BF_{exp}}{BF_{calc}} \rangle$ were found to be equal to 18% for 0.8 $\langle BF_{calc} \rangle$ 1.0, 28% for 0.6 $\langle BF_{calc} \rangle$ 0.8, 34% for 0.4 $\langle BF_{calc} \rangle$ 0.6, 39% for 0.2 $\langle BF_{calc} \rangle$ 0.4, and 53% for 0.1 $\langle BF_{calc} \rangle$ 0.2, respectively. From that, we estimated the uncertainties affecting our branching fractions to be respectively of 20%, 30%, 35%, 40%, and 55% for BF = 0.8–1.0, 0.6–0.8, 0.4–0.6, 0.2–0.4, and 0.1–0.2. These uncertainties were then combined with the experimental lifetime uncertainties derived from the measurements performed at University of Jilin to obtain the final uncertainties affecting our gA- and gf-values given in Table 5.7. As a final result, due to the fact that many of the highly excited levels considered in the present work are depopulated by quite a number of weak lines, among the 46 transitions listed in Table 5.7, about half of them have an estimated decay rate accuracy that is equal or better than 50%.

These are nevertheless very satisfying results because those new radiative data in neutral barium can, as mentioned at the beginning of this section, be useful for the observation of Ba I lines in astrophysical spectra.

Table 5.7: Branching fractions, transition probabilities and oscillator strengths for highly excited levels of Ba I.

<u>b or Da i.</u>								
Upper Level		Lower Level		λ^{b}	BF	$gA(s^{-1})$	log gf	Uncertainty
$E^{a}(cm^{-1})$	J	$E^a(cm^{-1})$	J					
26,816.27	3	9596.533	3	580.568	0.133	2.02(7)	-0.99	Е
$\tau = 46(4) \text{ ns}$		11,395.35	2	648.291	0.863	1.31(8)	-0.08	\mathbf{C}
39,311.95	1	0	0	254.299	0.296	8.30(6)	-2.09	D +
$\tau = 107(5)$ ns		11,395.35	2	358.108	0.395	1.11(7)	-1.67	D +
		26,757.30	0	796.299	0.115	3.22(6)	-1.51	E
40,662.86	1	23,062.05	2	567.998	0.148	9.06(6)	-1.36	E
$\tau = 49(4) \text{ ns}$		23,479.98	1	581.813	0.476	2.91(7)	-0.83	D +
		23,918.92	2	597.065	0.122	7.47(6)	-1.4	E
40,736.81	1	23,918.92	2	594.44	0.119	3.34(6)	-1.75	E
$\tau = 107(8) \text{ ns}$		26,757.30	0	715.136	0.194	5.44(6)	-1.38	E
. ,		28,230.23	0	799.359	0.262	7.35(6)	-1.15	D
40,742.60	1	12,266.02	0	351.065	0.326	2.45(6)	-2.34	D
$\tau = 400(40) \text{ ns}$		12,636.62	1	355.695	0.211	1.58(6)	-2.52	D
41,159.83	1	30,750.67	2	960.429	0.259	1.24(6)	-1.77	D
$\tau = 628(60)$ ns		32,943.77	2	1216.796	0.154	7.36(5)	-1.79	E
41,295.93	0	30,695.62	1	943.11	0.483	9.11(5)	-1.92	D +
$\tau = 530(50) \text{ ns}$		32,805.17	1	1177.428	0.27	5.09(5)	-1.97	D
41,296.96	1	30,695.62	1	943.018	0.107	1.29(6)	-1.76	E
$\tau = 248(20) \text{ ns}$		30,750.67	2	947.941	0.312	3.77(6)	-1.29	D
		32,943.77	2	1196.82	0.182	2.20(6)	-1.33	E
41,299.33	2	30,818.12	3	953.826	0.414	3.91(6)	-1.27	D +
$\tau = 530(34) \text{ ns}$		33,526.60	3	1286.198	0.247	2.33(6)	-1.24	D
41,307.88	1	0	0	242.011	0.335	3.54(6)	-2.51	D
$\tau = 284(28) \text{ ns}$		11,395.35	2	334.212	0.104	1.10(6)	-2.74	E
		28,230.23	0	764.453	0.107	1.13(6)	-2	E
41,404.40	1	30,695.62	1	933.557	0.124	1.22(6)	-1.8	E
$\tau = 304(30) \text{ ns}$		30,750.67	2	938.381	0.357	3.52(6)	-1.33	D
· · ·		32,943.77	2	1181.622	0.189	1.87(6)	-1.41	E
41,406.53	2	30,818.12	3	944.169	0.432	5.26(6)	-1.15	D +
$\tau = 411(40) \text{ ns}$		33,526.60	3	1268.7	0.247	3.00(6)	-1.14	D
41,411.04	1	9215.501	2	310.512	0.145	1.06(6)	-2.81	E
$\tau = 410(40) \text{ ns}$		11,395.35	2	333.063	0.1	7.32(5)	-2.91	E
. ,		30,236.83	2	894.672	0.252	1.84(6)	-1.65	D
		30,750.67	2	937.797	0.2	1.46(6)	-1.71	D
41,470.96	3	34,602.77	2	1455.589	0.233	2.40(7)	-0.12	D
$\tau = 68(5) \text{ ns}$		37,394.87	2	2452.661	0.198	2.04(7)	0.26	E
		38,815.70	2	3765.083	0.127	1.31(7)	0.44	E
41,490.09	1	30,695.62	1	926.146	0.136	9.49(5)	-1.91	E
$\tau = 430(30) \text{ ns}$		30,750.67	2	930.894	0.326	2.27(6)	-1.53	D
. ,		32,943.77	2	1169.775	0.2	1.40(6)	-1.54	D
41,494.39	1	0	0	240.923	0.112	6.09(5)	-3.28	E
$\tau = 552(22) \text{ ns}$		30,236.83	2	888.048	0.395	2.15(6)	-1.6	D +
		30,750.67	2	930.521	0.103	5.60(5)	-2.14	E
41,559.45	1	26,160.29	1	649.207	0.284	3.16(6)	-1.7	D +
$\tau = 270(15) \text{ ns}$		30,750.67	2	924.92	0.254	2.82(6)	-1.44	D +
. ,		32,943.77	2	1160.357	0.133	1.48(6)	-1.53	E

5.6 Rh I

Rhodium (Z = 45) belongs to the fifth row of the periodic table. Its name derives from the Greek word *rhodon* which means pink. This name was proposed by its discoverer (William Hyde Wollaston in 1803) because of the pink-red color of some of rhodium's lead compounds, especially the hydroxide. The first metal obtained also seems to have been slightly impure, harboring significant traces of copper or iron with a red glowing effect [109].

As mentioned in Section 1.2, reliable atomic data of heavy elements such as Rhodium (Z = 45) allows for a possible test of the nucleosynthesis models in which the s-and r-processes intervene (see [146]).

In addition, there is an important need of a large numbers of precise radiative parameters of neutral, singly, and doubly ionized heavy atoms with the aim of understanding the large overabundances of heavy elements in chemically peculiar stars (see Zhang *et al.* [147]).

Rhodium is a very important element for which lines have been observed in the solar photosphere and in meteorites for high-lying excited states (Cameron *et al.* [148]). As far as we know, there is very limited radiative data available in the literature about it. This data is unfortunately very insufficient (in number and in accuracy) to meet the needs of astrophysicists.

In 1962, the experimental transition probabilities of Rh I were first determined experimentally by Corliss and Bosman [9], but their measurements were affected by very significant errors. In 1982, radiative lifetimes of 13 levels in Rh I were measured using TR-LIF spectroscopy technique by Kwiatkowski *et al.* [149]. With their new experimental measurements, they deduced new oscillator strengths and used them to redetermine the photospheric abundances of Rh I. It appeared that the result was in excellent agreement with the meteoritic value. A year later, new experiments were made using the same method by Salih, Duquette and Lawler [150] to measure the lifetimes of 22 levels in Rh I.

Afterwards (in 1985), by combining their experimental BF with the previous lifetimes mentioned here above, Duquette and Lawler [151] obtained transition probabilities for 115 transitions in Rh I. The most recent data comes from Malcheva *et al.* [152] who measured radiative lifetimes of 17 levels in Rh I and compared them to a HFR+CPOL calculation. In summary, the lifetimes of 37 levels in Rh I have been reported in literature so far.

In the framework of the collaboration with the University of Jilin, radiative lifetime measurements were carried out for 20 odd-parity levels in Rh I in the region from 31 101.75 to 50 721.44 cm⁻¹. We then combined these lifetimes with our theoretical branching fractions obtained by the HFR+CPOL method to deduce semi-empirical transition probabilities and oscillator strengths (log gf) for 63 Rh I lines as shown in Table 5.8 (only the transitions with $BF \ge 0.1$ are given in that table, the smaller ones being affected by high cancellation effects). The uncertainty affecting those values is given using the NIST coding convention [28].

We adopted the same model for the HFR+CPOL calculations than the most recent one from [152]. The configurations explicitly included in the calculations were $4d^{8}5s$, $4d^{8}6s$, $4d^{8}6d$, $4d^{9}$, $4d^{7}5s^{2}$, $4d^{7}5p^{2}$, $4d^{7}5d^{2}$, $4d^{7}5s6s$, $4d^{7}5s5d$, and $4d^{7}5s6d$ for the even parity, and $4d^{8}5p$, $4d^{8}6p$, $4d^{8}4f$, $4d^{8}5f$, $4d^{7}5s5p$, $4d^{7}5s6p$, $4d^{7}5p5d$, and $4d^{7}5p6s$ for the odd parity.

We took the core-polarization effects into account by considering a Rh III ionic core with a dipole polarizability taken from Fraga *et al.* [94]: $\alpha_d = 7.42 \ a_0^3$, and a cut-off radius, as usual, corresponding to the HFR average value, $\langle r \rangle$, of the outermost core orbital (4d in this case): $r_c = 1.50 \ a_0$.

We also adjusted some of the radial integrals characterizing the $4d^85s$, $4d^9$, $4d^75s^2$ and

4d⁸6s even configurations, and the 4d⁸5p and 4d⁷5s5p odd configurations using the fitting procedure described in Section 2.2. The experimental energy levels used to perform this fit were taken from the NIST compilation [28]. The final average energy deviations were found to be of 35 and 43 $\rm cm^{-1}$, respectively (see [152]). However, it is worth mentioning that, despite the fact that the fit had been limited to levels below 47 000 $\rm cm^{-1}$ in Malcheva et al. [152] because of high mixing effects, we were able to identify two higher levels for which lifetimes were measured by our colleagues: 48797.74 cm⁻¹ with J = 5/2and 48811.47 cm⁻¹ with J = 7/2. For these experimental levels, the values calculated with our HFR+CPOL model were found to be equal to 48523 and 48787 cm⁻¹. Their identification in the calculations were made possible by the good agreement obtained between the theoretical Landé q-factors (1.039 and 0.918) and the equivalent experimental values (1.066 and 0.928) given in the NIST tables [28].

Upper level ^a	Lower level ^{a}	$\lambda (air)^a$	BF	$gA (10^6 s^{-1})$		log gf		
$E (cm^{-1})$	$E(cm^{-1})$	(nm)		This work	$Previous^b$	This work	$Previous^{c}$	
31101.75	2598.03	350.7311	0.311	273 (D+)	270	-0.30	- 0.28	
$\tau = 9.1(9) \text{ns}$	3309.86	359.7146	0.490	431 (D+)	470	-0.08	-0.06	
	5690.97	393.4224	0.124	109 (E)	126	-0.60 (E)	-0.59	
31613.78	1529.97	332.3091	0.507	624 (D+)	630	0.01	0.01	
$\tau = 8.1(5) \text{ ns}$	5690.97	385.6513	0.490	603 (D+)	590	0.13	0.12	
36985.25	5657.97	319.1183	0.175	135 (E)	-	-1.15	-1.23	
$\tau = 7.8(9) \text{ ns}$	10313	374.8207	0.569	438 (D+)	-	-0.04	-0.11	
	11968.23	399.6149	0.101	78 (E)	-	-0.73	-0.81	
37368.62	11006.05	379.2180	0.143	23 (E)	-	-1.30 (E)	-1.25	
$\tau = 12.5(3) \text{ ns}$	11968.23	393.5833	0.739	118 (C)	-	-0.56	-0.50	
38038.12	10313.41	360.5862	0.384	120 (D+)	-	-0.63	-0.57	
$\tau = 12.8(4) \text{ ns}$	11006.05	369.8257	0.345	108 (D+)	-	-0.65	-0.60	
38668.83	11968.23	374.4170	0.431	155 (D+)	-	-0.49	- 0.45	
$\tau = 11.1$ (4) ns	13520.69	397.5313	0.312	112 (D+)	-	-0.58	-0.54	
38718.11	5657.97	302.3910	0.145	34 (D)	-	-1.33	-1.26	
$\tau = 25.5(14) \text{ns}$	11968.23	373.7272	0.668	157 (C)	-	-0.48	- 0.41	
39126.76	10313.41	346.9620	0.136	52 (E)	-	-1.03	-1.02	
$\tau = 15.6(4) \text{ ns}$	11968.23	368.1036	0.590	227 (D+)	-	-0.34	-0.33	
39231.38	2598.03	272.8945	0.106	50 (E)	-	-1.25	-1.25	
$\tau = 8.5$ (4) ns	11006.05	354.1905	0.252	118 (D+)	-	-0.65	-0.65	
	11968.23	366.6910	0.132	62 (E)	-	-0.90	- 0.90	
	14382.19	402.3139	0.106	50 (E)	-	-0.92	-0.91	
39788.09	13520.69	380.5920	0.811	383 (B)	-	-0.08	-0.09	
$\tau = 12.7(7) \text{ ns}$								
40576.95	5657.97	286.2931	0.240	189 (D+)	-	-0.63	-0.67	
$\tau = 7.6(9) \text{ ns}$	14382.19	381.6474	0.659	520 (C)	-	0.06	0.02	
40603.48	9221.22	318.5592	0.115	58 (E)	-	-1.05	-1.13	
$\tau = 8.0(7) \text{ ns}$	10313.41	330.0462	0.218	109 (D+)	-	-0.75	-0.82	
	13974.73	375.4273	0.276	138 (D+)	-	-0.54	-0.60	
45177.63	16120.72	3440.0536	0.865	753 (B)	-	0.13	0.20	
$\tau = 9.2(7) \text{ ns}$								
46511.10	5690.97	244.9030	0.527	137 (D+)	-	-0.91	-0.97	
$\tau = 38.4(20) \text{ ns}$	14787.87	295.8764	0.239	62 (D+)	-	-1.03	-1.09	
	16120.72	328.9567	0.113	29 (E)	-	-1.33	-1.38	
48797.74	5690.97	231.9109	0.174	127 (E)	-	-0.99	-	
$\tau = 8.2(3) \text{ ns}$	7791.23	243.7898	0.552	404 (D+)	-	-0.44	-	
	11968.23	271.4409	0.109	80 (E)	-	-1.05	-	
48811.47	5690.97	231.8370	0.330	78 (D+)	-	-1.20	-	
$\tau = 33.9(12) \text{ ns}$	7791.23	243.7082	0.243	57 (D+)	-	-1.29	-	
	13520.69	283.2768	0.109	26 (E)	-	-1.50	-	
	16118.69	305.7890	0.166	39 (E)	-	-1.26	-	

Table 5.8: New reliable BF, gA and $\log gf$ obtained in Rh I and comparison with previously existing values in the literature.

a: From NIST database [28]. b: From Duquette *et al.* [151] c: From Malcheva *et al.* [152]

We hope that these new reliable semi-empirical atomic data (shown in Table 5.8) are likely to be used for the analysis and interpretation of astrophysical spectra which could contain neutral rhodium lines in order to improve abundance determinations of this element in different astrophysical objects.

General Conclusion

As mentioned in our general introduction, developments in atomic physics have always played a major role in astrophysics. Conversely, the improvement of astronomical observing instruments, with more and more powerful ground-based and space telescopes, on the one hand, and the development of more and more sophisticated stellar models, on the other hand, implies that an increasing amount of accurate atomic data is required. Such demands are particularly acute for heavy atoms and ions (typically beyond the iron group) as these elements have been little studied in the past, mainly because of their complex electronic structures. However, the latter are of indisputable interest since they are more and more often identified in the spectra of many different astrophysical sources, so that a precise knowledge of the fundamental spectroscopic parameters that characterize them is urgently required for the development of many hot topics in astronomy. The investigations of atomic structures and radiative processes that we have carried out in the present thesis are part of this context insofar as they concern neutral, lowly- and moderately-ionized atoms, presenting a particular interest in different astrophysical areas such as cosmochronology, the study of hot white dwarfs, the analysis of chemically peculiar stars and the development of stellar nucleosynthesis models.

More precisely, a large amount of new data such as energy levels, wavelengths, radiative lifetimes, oscillator strengths, and transition probabilities have been determined in our work, most of them for the first time, in atomic systems as diverse as singly ionized thorium and uranium (of interest to cosmochronology), three- to six-times ionized copper, indium, caesium and silver (of interest to hot white dwarf studies), and neutral and/or singly ionized iridium, rhenium, lanthanum, barium and rhodium (of interest for the study of chemically peculiar stars). For this purpose, the most complete physical models possible have been developed on the basis of the pseudo-relativistic Hartree-Fock (HFR) theoretical method in which valence-valence electron correlations were explicitly included in multi-configuration expansions while core-valence interactions, which are extremely important in order to model the atomic structures of neutral and lowly ionized heavy elements, were considered using a core-polarization potential and a correction to the dipole operator depending on two parameters, i.e. a dipole polarizability and a cut off radius corresponding to the ionic core, giving rise to the so-called HFR+CPOL approach.

In the specific case of the lanthanum atom, another independent theoretical method was used in our calculations, namely the fully relativistic Multiconfiguration Dirac-Hartree-Fock (MCDHF) approach. It should be noted that this method is more complex to use and requires much longer computation times than the HFR+CPOL method. It also often presents convergence problems during the optimization of orbitals, especially for neutral and lowly ionized atoms. However, we have shown that the HFR+CPOL radiative rates were in good agreement with the MCDHF results for most of the spectral lines considered in neutral lanthanum, allowing to highlight the reliability of the HFR+CPOL method when a large number of radiative data must be determined for a specific heavy atomic system.

Part of our work has also involved experimental measurements of atomic parameters. In particular, we have obtained new transition probabilities for a large number of spectral lines involving highly excited states in neutral and/or singly ionized heavy atoms such as iridium, rhenium, barium and rhodium, thanks to the combination of theoretical branching fractions calculated with the HFR+CPOL method and accurate radiative lifetimes measured using time-resolved laser-induced-fluorescence (TR-LIF) spectroscopy. The latter measurements were carried out in collaboration with Chinese experimentalists who built a TR-LIF setup at the University of Jilin. This allowed us not only to estimate the accuracy of the HFR+CPOL calculations, but also to provide new semi-empirical spectroscopic parameters that are more accurate than if they had been obtained entirely using a purely theoretical model.

As already mentioned above, all the atomic physics studies carried out in the present thesis have been motivated by their potential applications in astrophysics. In particular, our work relating to the Th II and U II ions made it possible to establish, for the first time, a list of some tens of spectral lines belonging to these ions likely to be used as cosmochronometers, allowing astrophysicists to consider future studies aiming at determining the age of some stars using the 238 U/ 232 Th ratio.

Many atomic parameters obtained in our work have also been directly applied to the study of hot white dwarfs. Indeed, the new transition probabilities and oscillator strengths that we have calculated for the ions Cu IV-VII, In IV-VII, Cs IV-VII and Ag IV-VII have not only allowed the identification of lines of these ions in the spectra of the white dwarfs RE0503-289 and RE0457-281, but have also been incorporated in the NLTE models used to interpret these spectra and to deduce the chemical abundances. This work, performed in close collaboration with the Astronomy and Astrophysics Department of the University of Tübingen in Germany, has confirmed the large overabundances (of several orders of magnitude compared to solar abundances) already deduced in these white dwarfs for other elements heavier than iron, thus consolidating the hypothesis of radiative levitation. In addition, it is worth mentioning that the new semi-empirical radiative data obtained for the highly-excited states in Ir I, Ir II, Re I, La I, Ba I and Rh I are directly applicable to the detection of these elements in chemically peculiar stars and thus to the establishment of constraints on the nucleosynthesis models developed to explain the production of heavy atomic species in these celestial objects.

Finally, we would like to point out that the different works presented in this thesis have been the subject of 10 publications in peer-review scientific journals [77, 79, 102, 103, 153, 154, 155, 156, 157, 158].

Although the results reported in the present manuscript constitute a significant contribution to the knowledge of electronic structures and the spectroscopic parameters characterizing heavy atoms and ions, a very large effort must still be pursued in this field to fully meet the needs of the astrophysical community. These crucial needs for new investigations of atomic processes of astrophysical interest were recently reminded by the prestigious American Astronomical Society in its latest review of research in Astrophysics [159] in which the urgent priorities in this scientific field were presented in various White Papers. Among these, we will pinpoint two articles co-authored by about one hundred renowned astrophysicists entitled Atomic Data for Astrophysicists: Needs and Challenges [160] and State of the Profession Considerations for Laboratory Astrophysicists [161], in which the study of atomic processes in heavy atomic systems was clearly identified as one of the key priorities in order to explore the origin of trans-iron elements in the Universe. This necessity will be even more exacerbated with the launches of new space telescopes recording high-resolution astrophysical spectra, such as, for example, the James Webb Telescope in the infrared region. The recent first detection of gravitational waves from a neutron star merger has also opened the way to huge demands for new reliable atomic data in heavy elements which seem to be created in large quantities during those mergers [131]. It is therefore obvious that the atomic physicists still have a lot of work ahead of them in order to meet all the current and future requests made by astrophysicists.

As we already mentioned here above, within the framework of our study, many ions (25) of many elements (11 different elements) have been studied. To finish on a more visual note, Figure 5.9 shows in black on the Mendeleev table, all the elements for which at least one ion has been studied in the course of this thesis.

1 IA 1A	Periodic Table of the Elements															18 VIIIA 8A	
1 *1 H Hydrogen 1.006	2 IIA 2A							Atomic	Valence Charge			13 IIIA 3A	14 IVA 4A	15 VA 5A	16 VIA 6A	17 VIIA 7A	² He Helium 4.003
3 *1 Li Lithium 6.941	⁴ Be Berytlium 9.012							Syr	nbol ame			5 *3 Boron 10.811	6 *4.4 Carbon 12.011	7 *5.3 N Nitrogen 14.007	8 -2 Oxygen 15,999	9 -1 Fluorine 18.998	10 ° Neon 20.180
11 *1 Na Sodium 22 980	12 *2 Mg Magnesium 24.305	3 IIIB 3B	4 IVB	5 VB	6 VIB	7 VIIB 7P	8		c Mass	11 IB	12 IIB	13 *3 Aluminum 20.982	14 [™] Silicon	15 +5,+3,-3 P Phosphorus 30,974	16 *6.2 Sulfur 32.005	17 -1 Cl Chlorine 35453	18 ° Argon 38.946
19 *1 K Potassium 38,098	20 *2 Ca Calcium 40.078	21 *3 Scandium	22 *4 Ti Titanium 47.867	23 *5.+4.+3 V Vanadium 50.942	24 +6.+3.+2 Cr Chromium	25 +7.+4.+2 Manganese 54.838	26 +3,+2 Fe	27 +3.+2 Co Cobalt	28 +2 Ni Nickel 58,650	29 Cu Copper 63,546	30 *2 Zn Zinc 65.38	31 +3 Gallium 69.721	32 *4 Germanium 72.631	33 +5,+3 Arsenic 74,922	34 +4.2 See Selenium 78.971	35 +5.1 Br Bromine 78 904	36 ° Krypton 84.798
37 *1 Rb Rubidium 84.488	38 +2 Strontium 87.62	39 +3 Yttrium 88,906	40 *4 Zr Zirconium 91.224	41 *5 Nobium 92,905	42 *6.+4 Mo Molybdenum 95.95	43 TC Technetium 98,907	44 +4.+3 Ru Ruthenium 101.07	45 Rh Rhodium 102.906	46 +4,+2 Pd Palladium 105.42	47 Ag 580 Silver 107.868	48 *2 Cd Cadmium 112,414	49 In Indum 114,818	50 +2.4 Sn Tin 118.711	51 *3 Sb Antimony 121,780	52 *4 Te Tellurium 127.6	53 +51	54 ° Xeon 131,294
55 Cs 0esium 132,905	56 Ba Barium 137.328	57-71	72 *4 Hf Hafnium 178.49	73 *5 Ta Tantalum 180.948	74 *6.+4 W Tungsten 183.84	75 Re Rhenium 186.207	76 *4 Os osmium 190.23	77	78 +4.+2 Pt Platinum 195.085	79 +3 Au Gold 195,997	80 +2.+1 Hg Mercury 200.592	81 *3.+1 TI Thallium 204.383	82 +2 Pb Lead 2012	83 *3 Bi Bismuth 208,990	84 +4 Po Polonium [208.982]	85 ⁻¹ At Astatine 200.987	86 0 Rn Radon 222.018
87 *1 Fr Francium 223.020	88 *2 Radium 226.025	89-103	104 *4 Rf Rutherfordium	105 unk Db Dubnium [262]	106 unk Sg Seaborgium [200]	107 unk Bh Bohrium [254]	108 unk HS Hassium [200]	109 unk Mt Meitnerium [268]	110 unit DS Darmstadtium [200]	111 unk Rg Roentgenium	112 unk Cn Copernicium	113 unk Uut Ununtrium unknown	114 unk Fl Flerovium [280]	115 unk Uunpentium unknown	116 unk Lv Livermorium [200]	117 unk Ununseptium unknown	118 unk Uuo Ununoctium unknown
	Lantha Serie	nide es Lantt 138	Ce	*3 59 F fum 1.116 Praseo	Pr 60 Neod	*3 61 M mium _243 Prom	*3 62 M 5 ethium 19	*3 63 m arium 0.36 15	*3 64 Eu oplum 1.964	*3 65 1 01inium 57.25	*3 66 D blum 8.925 16	*3 67 Hol 2.500	*3 68 10 Eric 100 Eric 100 Eric	Er *3 69 T Jum 1259 100	m ^{*3} 70 Ilum 1934 17	*3 71 *b urbium 3.055 17/	+3 tium .967
	Actin Serie	ide Ass	+3 90 AC nium 7.028	h Fium 1038 91 Protac	+5 92 a tinium Ura- 238	J Nept 029	Ip unium 7.048	*7,+4 Pu Dnium 1.064 95 Ame 24	* ³ 96 Micium 3.061 24	*3 97 Fm Irium 17.070 24	* ³ 98 Bk 0 Kelium 17.070 25	cf Einst	*3 100 S F einium 254	nium 101 Mende 25	*3 102 Id elevium 8.1 29	+2 103 Lawre 9.101 2	+3 . Г incium 62]

Figure 5.9: Heavy elements for which at least one ion have been studied during this thesis - Original picture from: sciencesnote.org (©Todd Helmenstine)

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Appendix

Preliminary Remark

The experimental values of the energy levels given in the tables comparing experimental and theoretical energy levels are given with an accuracy of 0.1 cm^{-1} in order to be directly compared to the theoretical values. All the energies are given in 0.1 cm^{-1} .

All the wavelength given in the transition tables are the Ritz wavelength determined using the most accurate known value of the experimental energy levels (i.e. with a better accuracy than 0.1 cm^{-1}). The references from which these values are taken are cited at the bottom of each table.

Cu IV-VII

Cu IV

Energy levels

Table A1: Comparison between available experimental data and calculated even energy levels (in $\rm cm^{-1})$ in Cu IV

) m C	uiv			
E^a_{exp}	E^{b}_{calc}	ΔE	J	Leading components (in %) in LS coupling c
0	8	$^{-8}$	4	99 3d ^{8 3} F
1861.4	1857	4	3	99 3d ^{8 3} F
3077.6	3074	4	2	98 3d ^{8 3} F
16248	16238	10	2	$82 \ 3d^{8} \ {}^{1}D + 17 \ 3d^{8} \ {}^{3}P$
19696.6	19750	-53	2	$82 \ 3d^{8} \ {}^{3}P + 17 \ 3d^{8} \ {}^{1}D$
20096.6	20072	25	1	99 3d ^{8 3} P
20422.6	20405	18	0	99 3d ^{8 3} P
26913	26912	1	4	$99 \ 3d^{8} \ {}^{1}G$
61456.4	61456	0	0	98 3d ⁸ ¹ S
119632.4	119747	-115	5	$99.3d^{7}({}^{4}F)4s^{5}F$
120918 7	120980	-61	4	$99.3d^{7}({}^{4}F)4s^{5}F$
121929.8	121955	-25	3	$99.3d^{7}({}^{4}F)4s^{5}F$
122663.8	122666	-2	2	$99.3d^{7}({}^{4}F)4s^{5}F$
122000.0	122000	12	1	$00.3d^{7}(^{4}F)/_{6}$ ⁵ F
128343 3	128356	-13	4	$98 3 d^{7} (^{4}F) 4s ^{3}F$
130060.3	130024	36	3	$30 3 d^7 (4 F) 4 s^3 F$
131218.6	131157	62	2	$99.3d^{7}(^{4}F)_{48}$ ³ F
120605 2	120522	172	2	93.50(1)48.1
140065 7	139522	114	0	99.50(1)48.1 06.247(4D)4.5D
140005.7	139952	114	4	$90.50 (\Gamma)48 \Gamma$
140715	140603	112	1	$97.3d(P)4s^{2}P$
144065.9	143959	107	Э 4	$97.30(G)48^{-1}G$
144749	144616	133	4	$94 3d^{-}(^{-}G)4s^{-}G$
145579.9	145422	158	3	$99.30^{\circ}(-G)48^{\circ}G$
147736.6	147668	69	2	$77 \text{ 3d}^{-}(^{-}P)\text{4s}^{-}P + 18 \text{ 3d}^{-}(^{-}P)\text{4s}^{-}P$
147929.8	148006	-76	1	$71 \text{ 3d}^{-}(^{-}P)4\text{ s}^{-}P + 15 \text{ 3d}^{-}(^{-}P)4\text{ s}^{-}P + 11 \text{ 3d}^{-}(^{-}P)4\text{ s}^{-}P$
148233.8	148438	-204	0	$67 \text{ 3d}^{-}(^{2}\text{P})4\text{s}^{-}\text{P} + 33 \text{ 3d}^{-}(^{2}\text{P})4\text{s}^{-}\text{P}$
148860.7	148746	115	4	90 3d' (^{2}G) 4s $^{1}G + 5$ 3d' (^{2}H) 4s ^{3}H
148903.6	149198	-294	2	$65 \ 3d'(^2P)4s \ ^3P + 22 \ 3d'(^4P)4s \ ^3P + 7 \ 3d'(^2D)4s \ ^3D$
149667.2	149962	-295	1	$67 \ 3d' (^{2}P)4s \ ^{3}P + 21 \ 3d' (^{4}P)4s \ ^{3}P + 8 \ 3d' (^{2}D)4s \ ^{3}D$
151622.7	151769	-146	6	$100 \ 3d' (^2H)4s \ ^2H$
152231.7	152012	220	3	$77 \ 3d' (^{2}D)4s \ ^{3}D + 22 \ 3d' (^{2}D)4s \ ^{3}D$
152301.7	152407	-105	5	95 3d' (² H)4s ³ H
152400.2	152648	-248	1	$38 \ 3d' (^{2}D)4s \ ^{3}D + 35 \ 3d' (^{2}P)4s \ ^{1}P + 14 \ 3d' (^{2}P)4s \ ^{3}P$
153198.2	153260	-62	4	$92 \ 3d' (^{2}H)4s \ ^{3}H + 6 \ 3d' (^{2}G)4s \ ^{1}G$
153375.7	153186	190	2	$65 \ 3d'(^{2}D)4s \ ^{3}D + 17 \ 3d'(^{2}D)4s \ ^{3}D + 8 \ 3d'(^{2}P)4s \ ^{3}P$
155476.7	155645	-168	1	$54 \ 3d' (^{2}P)4s \ ^{1}P + 33 \ 3d' (^{2}D)4s \ ^{3}D + 7 \ 3d' (^{2}D)4s \ ^{3}D$
156458.7	156584	-125	5	96 3d' (² H)4s ¹ H
157536.1	157257	279	2	71 $3d^{7}(^{2}D)4s^{-1}D + 18 3d^{7}(^{2}D)4s^{-1}D + 5 3d^{7}(^{2}D)4s^{-3}D$
170066.5	169989	78	2	99 $3d^{7}({}^{2}F)4s {}^{3}F$
170277.7	170245	33	3	98 $3d^{7}({}^{2}F)4s^{-3}F$
170619	170661	-42	4	99 $3d^{7}({}^{2}F)4s {}^{3}F$
174831.3	174625	206	3	98 $3d^{7}(^{2}F)4s^{-1}F$
196853.5	196964	-111	1	80 $3d^{7}(^{2}D)4s^{3}D + 19 3d^{7}(^{2}D)4s^{3}D$
197138.5	197228	-90	2	78 $3d^{7}(^{2}D)4s^{3}D + 20 3d^{7}(^{2}D)4s^{3}D$
197659.5	197695	-36	3	77 $3d^{7}(^{2}D)4s^{3}D + 22 3d^{7}(^{2}D)4s^{3}D$
201771	201650	121	2	$77 \ 3d^{7}(^{2}D)4s^{1}D + 21 \ 3d^{7}(^{2}D)4s^{1}D$
287319.5	287391	-72	5	90 $3d^{7}({}^{4}F)4d {}^{5}F + 8 3d^{7}({}^{4}F)4d {}^{5}G$
287589.3	287966	-377	4	$78 \ 3d^{7}({}^{4}F)4d \ {}^{5}F + 11 \ 3d^{7}({}^{4}F)4d \ {}^{5}D + 7 \ 3d^{7}({}^{4}F)4d \ {}^{5}G$
288566.4	288677	-111	3	$70 \ 3d^{7}({}^{4}F)4d \ {}^{5}F + 14 \ 3d^{7}({}^{4}F)4d \ {}^{5}D + 6 \ 3d^{7}({}^{4}F)4d \ {}^{5}P$
288697.8	288687	11	6	94 $3d^{7}(^{4}F)4d^{5}G + 6 3d^{7}(^{4}F)4d^{5}H$
289370.2	289474	-104	2	$82 \ 3d^{7}(^{4}F)4d \ ^{5}F + 9 \ 3d^{7}(^{4}F)4d \ ^{5}D$
289529.7	289613	-83	3	$74 \ 3d^{7}(^{4}F)4d \ ^{5}P + 12 \ 3d^{7}(^{4}F)4d \ ^{5}F + 9 \ 3d^{7}(^{4}F)4d \ ^{5}D$
289572.9	289542	31	5	$66 \ 3d^{7}({}^{4}F)4d \ {}^{5}G + 20 \ 3d^{7}({}^{4}F)4d \ {}^{3}G + 7 \ 3d^{7}({}^{4}F)4d \ {}^{5}H$
289641.5	289963	-322	4	$58 \ 3d^7(^4F)4d \ ^5D + 18 \ 3d^64s^2 \ ^5D + 16 \ 3d^7(^4F)4d \ ^5G$
289688.2	289700	-12	$\overline{7}$	99 $3d^{7}(^{4}F)4d^{5}H$
289974	290076	-102	1	$93 \ 3d^7(^4F)4d^{-5}F$
290445.4	290416	29	6	$60 \ 3d^7(^4F)4d^5H + 36 \ 3d^7(^4F)4d^3H$
290552.8	290575	-22	4	$60.3d^{7}({}^{4}F)4d^{5}G + 13.3d^{7}({}^{4}F)4d^{5}F + 10.3d^{7}({}^{4}F)4d^{3}G$

Table A1: Continued

\mathbf{E}^{a}_{exp}	E_{calc}^{o}	ΔE	J	Leading components (in %) in LS coupling ^c
290773.5	290933	-160	2	$54 \ 3d' ({}^{4}F)4d \ {}^{5}P + 29 \ 3d' ({}^{4}F)4d \ {}^{5}D + 7 \ 3d' ({}^{4}F)4d \ {}^{5}F$
290885.1	291074	-189	3	$48 \ 3d' ({}^{4}F)4d \ {}^{3}G + 24 \ 3d' ({}^{4}F)4d \ {}^{5}D + 9 \ 3d' ({}^{4}F)4d \ {}^{3}P$
291147.3	291004	143	5	$70 \ 3d' ({}^{4}F)4d \ G + 20 \ 3d' ({}^{4}F)4d \ G + 6 \ 3d' ({}^{4}F)4d \ H$
291298.7	291394 201570	-95	5	$37 33^{\circ}(F)43^{\circ}G + 21 33^{\circ}(F)43^{\circ}D + 8 33^{\circ}48^{\circ}D$ 70 $33^{\circ}(4F)43^{\circ}H + 12 33^{\circ}(4F)43^{\circ}H + 5 33^{\circ}(4F)43^{\circ}G$
291501.0	291370	-270	1	19.54 (F)44 = 11 + 12.54 (F)44 = 11 + 5.54 (F)44 = 0 $55.3d^{7}(^{4}F)4d^{5}D + 27.3d^{7}(^{4}F)4d^{5}P + 13.3d^{6}4s^{2}{}^{5}D$
291730	291745	-15	2	$92 \ 3d^7 ({}^4F) 4d^5G$
291865	291764	101	6	$63 \ 3d^7 ({}^4F)4d^{3}H + 34 \ 3d^7 ({}^4F)4d^{5}H$
291953.9	292147	-193	3	$75 \ 3d^{7}({}^{4}F)4d^{3}D + 9 \ 3d^{7}({}^{4}F)4d^{5}D + 6 \ 3d^{6}4s^{2} \ {}^{5}D$
291997.1	292224	-227	2	$39 \ 3d^{7}(^{4}F)4d^{5}P + 36 \ 3d^{7}(^{4}F)4d^{5}D + 14 \ 3d^{6}4s^{2} \ ^{5}D$
292296.7	292187	110	4	$65 \ 3d^{7}(^{4}F)4d^{3}G + 16 \ 3d^{7}(^{4}F)4d^{5}G + 8 \ 3d^{7}(^{4}F)4d^{5}H$
292440	292414	26	4	79 $3d^{7}({}^{4}F)4d {}^{5}H + 16 3d^{7}({}^{4}F)4d {}^{3}G$
292639.1	292782	-143	1	71 $3d^{7}({}^{4}F)4d^{5}P + 19 3d^{7}({}^{4}F)4d^{5}D + 8 3d^{6}4s^{2} {}^{5}D$
292913.3	292946	-33	3	89 $3d'({}^{4}F)4d {}^{5}H + 6 3d'({}^{4}F)4d {}^{5}G$
293021.7	293176	-154	2	$84 3d' ({}^{4}F)4d 3D + 6 3d' ({}^{4}F)4d {}^{3}P$
293399.2	293267	132	5	$80 \ 3d' (^{+}F)4d \ ^{+}H + 14 \ 3d' (^{+}F)4d \ ^{+}H$
293313.3	293332	160	1	$68.5d^{-}(F)4d^{-}G + 0.5d^{-}(F)4d^{-}H$
294015.5	294164	-109 -117	1	$^{95}3d^{-}(F)4d^{-}D$ $^{72}3d^{6}4e^{2}{}^{5}D \pm 213d^{7}({}^{4}F)4d^{5}D$
294464 4	294316	148	4	12 3d 43 12 12 13 12 13 14 15 14 15 14 15 14 15 16 $^$
295307.8	295383	-75	3	$72 \ 3d^{6}4s^{2} \ {}^{5}D + 22 \ 3d^{7}({}^{4}F)4d \ {}^{5}D$
295910.4	295840	70	4	$80 \ 3d^7 ({}^4F)4d^{3}F + 7 \ 3d^7 ({}^2G)4d^{3}F$
296040.3	296106	-66	2	$71 \ 3d^{6}4s^{2} \ {}^{5}D + 21 \ 3d^{7}({}^{4}F)4d \ {}^{5}D$
296494.2	296559	-65	1	$73 \ 3d^{6}4s^{2} \ {}^{5}D + 20 \ 3d^{7}({}^{4}F)4d \ {}^{5}D$
296573.4	296474	99	2	81 $3d^{7}(^{4}F)4d^{3}P + 5 3d^{7}(^{4}F)4d^{3}D + 5 3d^{7}(^{4}P)4d^{3}P$
296912.3	296847	65	3	78 $3d_{-}^{7}({}^{4}F)4d_{-}^{3}F + 7 3d_{-}^{7}({}^{2}G)4d_{-}^{3}F$
297554.4	297481	73	2	78 $3d^{7}({}^{4}F)4d {}^{3}F + 8 3d^{7}({}^{2}G)4d {}^{3}F$
297931	297840	91	1	$88 \ 3d_{2}^{7}({}^{4}F)4d_{2}^{3}P + 6 \ 3d_{2}^{7}({}^{4}P)4d_{3}^{3}P$
301632	301720	-88	5	$99 \ 3d^{7} ({}^{4}F)5s^{5}F$
302682.3	302741	-59	4	$82 \ 3d' ({}^{4}F)5s \ {}^{5}F + 17 \ 3d' ({}^{4}F)5s \ {}^{5}F$
303798.4	303819	-21	3	91 3d' (4 F)5s 6 F + 7 3d' (4 F)5s 6 F
304244.9	304274	-29	4	$82 3 d^{-}(^{-}F) 5 s^{-}F + 17 3 d^{-}(^{-}F) 5 s^{-}F$
205116	205106	-1	1	90.30 (F) 5s F 08.247(4F) 5c 5F
305856	305100	14	3	90 3d (F) 5s F 01 3d ⁷ (⁴ F) 5s ³ F \pm 7 3d ⁷ (⁴ F) 5s ⁵ F
306941.8	306904	38	2	$96 \ 3d^7 ({}^4F) 5s^{3}F$
306982.5	306884	99	1	$98 \ 3d^7 (^4P) 4d^5P$
307167	307089	78	2	$97 \ 3d^{7}(^{4}P) 4d^{5}P$
307517.3	307459	58	3	$95 \ 3d^{7}(^{4}P)4d^{5}P$
309413.9	309295	119	5	$97 \ 3d^7 (^4P) 4d^5F$
309490.4	309427	63	4	91 $3d^{7}(^{4}P)4d^{5}F$
309653.1	309630	23	3	$88 \ 3d^7(^4P)4d^5F$
309864.7	309874	-9	2	$88 \ 3d^7(^4P)4d^5F$
310057.1	310095	-38	1	89 3d ⁷ (⁴ P)4d ⁵ F + 5 3d ⁷ (² P)4d ³ D
310800.2	310865	-65	3	$80 \ 3d' ({}^{2}G)4d \ {}^{3}D + 5 \ 3d' ({}^{4}P)4d \ {}^{3}F$
311010.7	311031	-20	3	$51 \ 3d' (^{2}P)4d \ ^{2}F + 23 \ 3d' (^{2}G)4d \ ^{2}F + 5 \ 3d' (^{2}P)4d \ ^{2}F$
311177 211274	311018	159	4	81 3d (^{-}P) 4d $^{-}F + 9 3d (^{-}G)$ 4d ^{-}F 44 2d $7(^{2}C)$ 4d $^{3}D + 20 2d7(^{4}P)$ 4d $^{3}F + 5 2d7(^{2}P)$ 4d ^{3}D
311274	311507	- 93	2	44.50 (G)40 D + 50.50 (T)40 T + 5.50 (T)40 D 05.3d ⁷ (² C)4d ³ I
311726.7	311911	-184	1	$37 3d^{7}({}^{4}P)4d^{3}P + 24 3d^{7}({}^{2}G)4d^{3}D + 11 3d^{7}({}^{2}P)4d^{3}P$
311742.9	311630	113	6	$67 3d^7(^2\text{G})4d^{-3}\text{I} + 24 3d^7(^2\text{G})4d^{-1}\text{I}$
311998.3	312124	-126	5	$61 \ 3d^7(^2G)4d \ ^3G + 20 \ 3d^7(^2G)4d \ ^3H + 11 \ 3d^7(^2G)4d \ ^3I$
312061.4	312033	28	2	$51 \ 3d^{7}(^{4}P)4d^{3}F + 30 \ 3d^{7}(^{2}G)4d^{3}D + 5 \ 3d^{7}(^{4}P)4d^{3}P$
312082.5	312061	22	3	56 $3d^{7}(^{2}G)4d^{1}F + 22 3d^{7}(^{4}P)4d^{3}F + 9 3d^{7}(^{2}G)4d 3D$
312415.5	312373	43	5	$37 \ 3d^{7}(^{2}G)4d^{3}I + 31 \ 3d^{7}(^{2}G)4d^{3}G + 16 \ 3d^{7}(^{2}G)4d^{1}H$
312466.7	312609	-142	4	$65 \ 3d_{7}^{7}(^{2}G)4d_{3}^{3}G + 18 \ 3d_{7}^{7}(^{4}P)4d_{5}^{5}D + 6 \ 3d_{7}^{7}(^{2}G)4d_{3}^{3}H$
312514.9	312454	61	6	$75 \ 3d^7 ({}^2G)4d {}^3H + 20 \ 3d^7 ({}^2G)4d {}^1I$
312601.5	312713	-112	2	$34 \ 3d' ({}^{4}P)4d \ {}^{5}D + 33 \ 3d' ({}^{4}P)4d \ {}^{5}P + 9 \ 3d' ({}^{2}G)4d \ 3D$
312629.9	312676	-46	4	$74 \ 3d' (^{4}P)4d \ ^{3}D + 15 \ 3d' (^{2}G)4d \ ^{3}G$
312950.8	312990	-33	3	80 30'(-P)40 ~D = $60 317(2C)41 31 + 30 317(2C)41 311 + 10 317(2C)41 111$
21225.5	313249 212454	4	0	-301 - 301 + 1 - 1001 + 1 + 00 - 301 + 1 - 1001 + 100 - 301 + 1 - 10000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 100
313294 7	313434	107	2	30.30 (G)40 1 + 23.50 (G)40 11 + 13.50 (G)40 11
313715.4	313945	-197	3	$93 3d^{7}({}^{2}\text{G})4d^{3}\text{G}$ $56 3d^{7}({}^{4}\text{P})4d^{5}\text{D} + 20 3d^{7}({}^{4}\text{P})4d^{3}\text{P} + 7 3d^{7}({}^{4}\text{P})4d^{3}\text{D}$
313871.5	$313245 \\ 313602$	-197 50 113	3 2 6	$\begin{array}{c} 50 \ 3d^{7}(^{2}{\rm G})4d^{-1}{\rm I} + 28 \ 3d^{7}(^{4}{\rm P})4d^{-1}{\rm I} + 18 \ 3d^{7}(^{4}{\rm P})4d^{-1}{\rm G} \\ 56 \ 3d^{7}(^{4}{\rm P})4d^{-5}{\rm D} + 20 \ 3d^{7}(^{4}{\rm P})4d^{-3}{\rm P} + 7 \ 3d^{7}(^{4}{\rm P})4d^{-3}{\rm D} \\ 53 \ 3d^{7}(^{2}{\rm G})4d^{-1}{\rm I} + 28 \ 3d^{7}(^{2}{\rm G})4d^{-3}{\rm I} + 18 \ 3d^{7}(^{2}{\rm G})4d^{-3}{\rm H} \end{array}$
	$313245 \\ 313602 \\ 313936$	-197 50 113 -65	3 2 6 4	$ \begin{array}{c} \text{56} \ \text{3d}^{-}(^2\text{G})\text{4d}^{-1}\text{H} = 28 \ \text{3d}^{-}(^2\text{G})\text{4d}^{-1}\text{H} = 18 \ \text{3d}^{-}(^2\text{G})\text{4d}^{-1}\text{H} \\ \text{56} \ \text{3d}^{-}(^2\text{G})\text{4d}^{-5}\text{D} + 20 \ \text{3d}^{-}(^2\text{P})\text{4d}^{-3}\text{P} + 7 \ \text{3d}^{-}(^2\text{P})\text{4d}^{-3}\text{D} \\ \text{53} \ \text{3d}^{-}(^2\text{G})\text{4d}^{-1}\text{H} = 28 \ \text{3d}^{-}(^2\text{G})\text{4d}^{-3}\text{H} + 18 \ \text{3d}^{-}(^2\text{G})\text{4d}^{-3}\text{H} \\ \text{89} \ \text{3d}^{-}(^2\text{G})\text{4d}^{-3}\text{H} + 9 \ \text{3d}^{-}(^2\text{G})\text{4d}^{-3}\text{G} \\ \end{array} $
314262.2	313245 313602 313936 314282	-197 50 113 -65 -20	3 2 6 4 5	$ \begin{array}{l} 50 \ 3d^7 (^2{\rm G}) 4d^{-1} + 28 \ 3d^7 (^2{\rm G}) 4d^{-3}{\rm G} \\ 56 \ 3d^7 (^2{\rm G}) 4d^{-5}{\rm D} + 20 \ 3d^7 (^2{\rm P}) 4d^{-3}{\rm P} + 7 \ 3d^7 (^4{\rm P}) 4d^{-3}{\rm D} \\ 53 \ 3d^7 (^2{\rm G}) 4d^{-1}{\rm I} + 28 \ 3d^7 (^2{\rm G}) 4d^{-3}{\rm I} + 18 \ 3d^7 (^2{\rm G}) 4d^{-3}{\rm H} \\ 89 \ 3d^7 (^2{\rm G}) 4d^{-3}{\rm H} + 9 \ 3d^7 (^2{\rm G}) 4d^{-3}{\rm G} \\ 59 \ 3d^7 (^2{\rm G}) 4d^{-1}{\rm H} + 36 \ 3d^7 (^2{\rm G}) 4d^{-3}{\rm H} \\ \end{array} $
$314262.2 \\ 314987.8$	313245 313602 313936 314282 315132	-197 50 113 -65 -20 -144	$ \begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \end{array} $	$ \begin{array}{l} 50 \ 3d^7(^2G) 4d \ ^3G \\ 56 \ 3d^7(^2G) 4d \ ^5D \ + \ 20 \ 3d^7(^4P) 4d \ ^3P \ + \ 7 \ 3d^7(^4P) 4d \ 3D \\ 53 \ 3d^7(^2G) 4d \ ^{1}I \ + \ 28 \ 3d^7(^2G) 4d \ ^{3}I \ + \ 18 \ 3d^7(^2G) 4d \ ^{3}H \\ 89 \ 3d^7(^2G) 4d \ ^{3}H \ + \ 9 \ 3d^7(^2G) 4d \ ^{3}H \\ 50 \ 3d^7(^2G) 4d \ ^{3}F \ + \ 14 \ 3d^7(^2G) 4d \ ^{3}H \\ 50 \ 3d^7(^2G) 4d \ ^{3}F \ + \ 14 \ 3d^7(^2G) 4d \ ^{1}G \ + \ 8 \ 3d^7(^2P) 4d \ ^{3}F \\ \end{array} $
$314262.2 \\ 314987.8 \\ 315450$	313245 313602 313936 314282 315132 314164	-197 50 113 -65 -20 -144 1286	$ \begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \end{array} $	$ \begin{array}{c} 30 \ 3d^7(^2G) 4d^{-7}H + 25 \ 3d^7(^2G) 4d^{-3}H \\ 56 \ 3d^7(^2G) 4d^{-5}D + 20 \ 3d^7(^2G) 4d^{-3}P + 7 \ 3d^7(^4P) 4d \ 3D \\ 53 \ 3d^7(^2G) 4d^{-1}H + 28 \ 3d^7(^2G) 4d^{-3}H \\ 89 \ 3d^7(^2G) 4d^{-1}H + 36 \ 3d^7(^2G) 4d^{-3}H \\ 89 \ 3d^7(^2G) 4d^{-1}H + 36 \ 3d^7(^2G) 4d^{-3}H \\ 50 \ 3d^7(^2G) 4d^{-3}F + 14 \ 3d^7(^2G) 4d^{-1}G + 8 \ 3d^7(^2P) 4d^{-3}F \\ 84 \ 3d^7(^4P) 4d^{-3}D \\ \hline \end{array} $
314262.2 314987.8 315450 315598.5	313245 313602 313936 314282 315132 314164 315602	-197 50 113 -65 -20 -144 1286 -4	$ \begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \end{array} $	$ \begin{array}{c} 35 \ 3d^7 (^2G) 4d^{-1}F \ 25 \ 3d^7 (^2P) 4d^{-3}P \ 7 \ 3d^7 (^4P) 4d \ 3D \ 53 \ 3d^7 (^2G) 4d^{-1}H \ 23 \ 3d^7 (^2G) 4d^{-3}H \ 23 \ 3d^7 (^2G) 4d^{-1}H \ 28 \ 3d^7 (^2G) 4d^{-3}H \ 28 \ 3d^7 (^2G) 4d^{-3}H \ 29 \ 3d^7 (^2G) 4d^{-1}H \ 28 \ 3d^7 (^2G) 4d^{-3}H \ 29 \ 3d^7 (^2G) 4d^{-1}H \ 28 \ 3d^7 (^2G) 4d^{-3}H \ 26 \ 3d^7 (^2G) 4d^{-1}H \ 26 \ 3d^7 (^2G) 4d^{-3}H \ 26 \ 3d^7 \ 26 \ 3d^{-1}H \ 26 \ 3d^7 \ 26 \ 3d^{-1}H \ 26 \ 3d^7 \ 26 \ 3d^{-1}H \ 26 \ 3d^{-2}H \ 26 \ 3d$
314262.2 314987.8 315450 315598.5 315846	313245 313602 313936 314282 315132 314164 315602 315136	-197 50 113 -65 -20 -144 1286 -4 710 210	3 2 6 4 5 4 3 4 2	$ \begin{array}{l} 50 \ 3d7^{(2)}_{(2)}(4)^{3}G \\ 56 \ 3d7^{(4)}_{(2)}(4)^{3}G \\ 56 \ 3d7^{(4)}_{(2)}(4)^{3}G \\ 53 \ 3d7^{(2)}_{(2)}(4)^{4}^{5}D + 20 \ 3d7^{(4)}_{(2)}(4)^{3}H + 7 \ 3d7^{(4)}_{(2)}(4)^{3}H \\ 53 \ 3d7^{(2)}_{(2)}(4)^{4}^{1}H + 28 \ 3d7^{(2)}_{(2)}(2)^{4}d^{3}G \\ 59 \ 3d7^{(2)}_{(2)}(2)^{4}d^{3}H + 9 \ 3d7^{(2)}_{(2)}(2)^{4}d^{3}G \\ 59 \ 3d7^{(2)}_{(2)}(2)^{4}d^{3}H + 36 \ 3d7^{(2)}_{(2)}(2)^{4}d^{3}H \\ 50 \ 3d7^{(2)}_{(2)}(2)^{4}d^{3}F + 14 \ 3d7^{(2)}_{(2)}(2)^{4}d^{3}H \\ 58 \ 3d7^{(2)}_{(2)}(4)^{3}D \\ 58 \ 3d7^{(2)}_{(2)}(4)^{4}G + 12 \ 3d7^{(2)}_{(2)}(4)^{4}G + 11 \ 3d7^{(2)}_{(2)}(4)^{4}F \\ 47 \ 3d7^{(2)}_{(2)}(4)^{4}D + 10 \ 48 \ 3d7^{(2)}_{(2)}(4)^{4}F \\ 47 \ 3d7^{(2)}_{(2)}(4)^{4}D \\ 47 \ 3d7$
$\begin{array}{c} 314262.2\\ 314987.8\\ 315450\\ 315598.5\\ 315846\\ 315912.2\\ 21601.7\end{array}$	313245 313602 313936 314282 315132 314164 315602 315136 315136 315663 316494	-197 50 113 -65 -20 -144 1286 -4 710 249 232	$ \begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \\ 2 \\ 3 \\ 3 \\ $	50 3d7 (2)4d 1+ 25 3d (2)4d 1+ 15 3d (2)4d 1 51 3d7 (2)4d 3G 56 3d7 (4P)4d 5D + 20 3d7 (4P)4d 3P + 7 3d7 (4P)4d 3D 53 3d7 (2G)4d 1H + 28 3d7 (2G)4d 3I + 18 3d7 (2G)4d 3H 89 3d7 (2G)4d 3H + 9 3d7 (2G)4d 3G 59 3d7 (2G)4d 1H + 36 3d7 (2G)4d 3H 50 3d7 (2G)4d 3F + 14 3d7 (2G)4d 1G + 8 3d7 (2P)4d 3F 84 3d7 (4P)4d 3D 58 3d7 (2G)4d 1G + 12 3d7 (2P)4d 1G + 11 3d7 (2G)4d 3F 47 3d7 (2G)4d 3F + 9 3d7 (2P)4d 1D + 8 3d7 (2G)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 59 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 50 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 50 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 50 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 50 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d 3F 50 3d7 (2G)4d 3F + 9 3d7 (2P)4d 3F + 7 3d7 (2H)4d
314262.2 314987.8 315450 315598.5 315846 315912.2 316191.7 316732.3	313245 313602 313936 314282 315132 314164 315602 315136 315663 316424 317512	-197 50 113 -65 -20 -144 1286 -4 710 249 -232 -780	3 2 6 4 5 4 3 4 2 3 2 4	50 3d7 (² G)4d ³ G 56 3d7 (² G)4d ³ G 56 3d7 (⁴ P)4d ⁵ D + 20 3d7 (⁴ P)4d ³ P + 7 3d7 (⁴ P)4d 3D 53 3d7 (² G)4d ¹ I + 28 3d7 (² G)4d ³ I + 18 3d7 (² G)4d ³ H 89 3d7 (² G)4d ¹ H + 36 3d7 (² G)4d ³ H 50 3d7 (² G)4d ³ F + 14 3d7 (² G)4d ³ H 50 3d7 (² G)4d ¹ G + 12 3d7 (² G)4d ¹ G + 8 3d7 (² P)4d ³ F 84 3d7 (² G)4d ¹ D + 11 3d7 (² P)4d ¹ D + 8 3d7 (² G)4d ³ F 59 3d7 (² G)4d ³ F + 9 3d7 (² P)4d ³ F + 7 3d7 (² G)4d ³ F 59 3d7 (² G)4d ³ F + 10 3d7 (² P)4d ³ F + 7 3d7 (² P)4d ³ F 59 3d7 (² G)4d ³ F + 10 3d7 (² P)4d ³ F + 9 3d7 (² P)4d ³ F 59 3d7 (² G)4d ³ F + 10 3d7 (² P)4d ³ F + 10 3d7 (² P)4d ³ F 59 3d7 (² G)4d ³ F + 25 2d7 (² P)4d ³ F + 10 3d7 (² P)4d ³ F
$\begin{array}{c} 314262.2\\ 314987.8\\ 315450\\ 315598.5\\ 315846\\ 315912.2\\ 316191.7\\ 316732.3\\ 317017\\ \end{array}$	313245 313602 313936 314282 315132 314164 315602 315136 315663 316424 317512 316886	-197 50 113 -65 -20 -144 1286 -4 710 249 -232 -780 131	$ \begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \\ 2 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 3 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ $	50 3d7 (2)4d ¹ F + 25 3d (2)4d ¹ F + 15 3d (2)4d ¹ F 51 3d7 (2)4d ⁵ D + 20 3d7 (⁴ P)4d ³ P + 7 3d7 (⁴ P)4d 3D 53 3d7 (² G)4d ¹ I + 28 3d7 (² G)4d ³ I + 18 3d7 (² G)4d ³ H 59 3d7 (² G)4d ¹ H + 36 3d7 (² G)4d ³ G 59 3d7 (² G)4d ³ F + 14 3d7 (² G)4d ³ H 50 3d7 (² G)4d ¹ G + 12 3d7 (² H)4d ¹ G + 11 3d7 (² G)4d ³ F 58 3d7 (² G)4d ¹ D + 11 3d7 (² P)4d ¹ D + 8 3d7 (² G)4d ³ F 59 3d7 (² G)4d ³ F + 9 3d7 (² P)4d ³ F + 7 3d7 (² G)4d ³ F 59 3d7 (² G)4d ³ F + 10 3d7 (² P)4d ³ F + 9 3d7 (² P)4d ³ F 59 3d7 (² G)4d ³ F + 10 3d7 (² P)4d ³ F + 9 3d7 (² P)4d ³ F 59 3d7 (² G)4d ³ F + 10 3d7 (² P)4d ³ F + 10 3d7 (² P)4d ³ F 59 3d7 (² C)4d ³ F + 10 3d7 (² P)4d ³ F + 10 3d7 (² P)4d ³ F 59 3d7 (² C)4d ³ F + 10 3d7 (² P)4d ³ F + 10 3d7 (² P)4d ³ F 59 3d7 (² C)4d ³ F + 10 3d7 (² P)4d ³ F + 5 3d7 (² P)4d ³ F 50 3d7 (² C)204d ³ F + 25 3d7 (² P)4d ³ F + 5 3d7 (² P)4d ³ F 50 3d7 (² C)204d ³ F + 25 3d7 (² C)204d ³ F + 5 3d7 (² C)204d ³ F 50 3d7 (² C)204d ³ F + 25 3d7 (² C)204d ³ F + 5 3d7 (² C)204d ³ F 50 3d7 (² C)204d ³ F + 25 3d7 (² C)204d ³ F + 5 3d7 (² C)204d ³ F 50 3d7 (² C)204d ³ F + 25 3d7 (² C)204d ³ F + 5 3d7 (² C)204d ³ F 50 3d7 (² C)204d ³ F + 25 3d7 (² C)204d ³ F + 5 3d7 (² C)204d ³ F 50 3d7 (² C)204d ³ F + 25 3d7 (² C)204d ³ F + 5 3d7 (² C)204d ³ F 50 3d7 (² C)204d ³ F + 25 3d7 (² C)204d ³ F + 5 3d7 (² C)204d ³ F 50 3d7 (² C)204d ³ F + 5 3d7 (
$\begin{array}{c} 314262.2\\ 314987.8\\ 315450\\ 315598.5\\ 315846\\ 315912.2\\ 316191.7\\ 316732.3\\ 317017\\ 317810.5 \end{array}$	313245 313602 313936 314282 315132 314164 315602 315136 315663 316424 317512 316886 317611	-197 50 113 -65 -20 -144 1286 -4 710 249 -232 -780 131 200	$ \begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \\ 2 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ $	50 3d ⁷ (² G)4d ³ G 56 3d ⁷ (² G)4d ³ G 56 3d ⁷ (² G)4d ³ G 56 3d ⁷ (² G)4d ³ L 89 3d ⁷ (² G)4d ³ L 89 3d ⁷ (² G)4d ³ L 89 3d ⁷ (² G)4d ³ L 9 3d ⁷ (² G)4d ³ L 9 3d ⁷ (² G)4d ³ L 1 4 36 3d ⁷ (² G)4d ³ L 50 3d ⁷ (² G)4d ³ F 14 3d ⁷ (² G)4d ³ G 50 3d ⁷ (² G)4d ³ F 50 3d ⁷ (² G)4d ³ F 51 3d ⁷ (² G)4d ³ F 52 3d ⁷ (² G)4d ³ F 53 3d ⁷ (² G)4d ³ F 54 3d ⁷ (² G)4d ³ F 59 3d ⁷ (² G)4d ³ F 50 3d ⁷ (² C)4d ³
$\begin{array}{c} 314262.2\\ 314987.8\\ 315450\\ 315598.5\\ 315846\\ 315912.2\\ 316191.7\\ 316732.3\\ 317017\\ 317810.5\\ 318452.4 \end{array}$	$\begin{array}{c} 313245\\ 313602\\ 313936\\ 314282\\ 315132\\ 315132\\ 315136\\ 315602\\ 315136\\ 315663\\ 316424\\ 317512\\ 316886\\ 317611\\ 318293\\ \end{array}$	-197 50 113 -65 -20 -144 1286 -4 710 249 -232 -780 131 200 159	$ \begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \\ 2 \\ 3 \\ 2 \\ 4 \\ 3 \\ 8 \\ \end{array} $	50 3d ⁷ (² G)4d ³ G 56 3d ⁷ (⁴ P)4d ⁵ D + 20 3d ⁷ (⁴ P)4d ³ P + 7 3d ⁷ (⁴ P)4d 3D 53 3d ⁷ (² G)4d ³ I + 28 3d ⁷ (² G)4d ³ I + 18 3d ⁷ (² G)4d ³ H 89 3d ⁷ (² G)4d ¹ I + 28 3d ⁷ (² G)4d ³ G 59 3d ⁷ (² G)4d ³ H + 9 3d ⁷ (² G)4d ³ G 59 3d ⁷ (² G)4d ³ F + 14 3d ⁷ (² G)4d ³ H 50 3d ⁷ (² G)4d ³ F + 14 3d ⁷ (² G)4d ¹ G + 8 3d ⁷ (² P)4d ³ F 84 3d ⁷ (² G)4d ³ D + 11 3d ⁷ (² P)4d ¹ G + 11 3d ⁷ (² G)4d ³ F 47 3d ⁷ (² G)4d ¹ D + 11 3d ⁷ (² P)4d ¹ D + 8 3d ⁷ (² C)4d ³ F 59 3d ⁷ (² G)4d ³ F + 9 3d ⁷ (² P)4d ³ F + 7 3d ⁷ (² P)4d ³ F 59 3d ⁷ (² G)4d ³ F + 10 3d ⁷ (² P)4d ³ F + 9 3d ⁷ (² P)4d ³ F 43 3d ⁷ (² C)4d ³ F + 25 3d ⁷ (² P)4d ³ F + 10 3d ⁷ (² P)4d ³ F 68 3d ⁷ (² P)4d 3D + 7 3d ⁷ (² D)4d ³ F + 5 3d ⁷ (² D)4d 3D 26 3d ⁷ (² P)4d ³ F + 22 3d ⁷ (² H)4d ³ F + 10 3d ⁷ (² P)4d ³ F 100 3d ⁷ (² P)4d ³ F
$\begin{array}{c} 314262.2\\ 314987.8\\ 315450\\ 315598.5\\ 315846\\ 315912.2\\ 316191.7\\ 316732.3\\ 317017\\ 317810.5\\ 318452.4\\ 318510\\ \end{array}$	$\begin{array}{c} 313245\\ 313602\\ 313936\\ 314282\\ 315132\\ 315132\\ 315136\\ 315602\\ 315136\\ 315663\\ 316424\\ 317512\\ 316886\\ 317611\\ 318293\\ 318355\\ \end{array}$	-197 50 113 -65 -20 -144 1286 -4 710 249 -232 -780 131 200 159 155	3 2 6 4 5 4 3 4 2 3 2 4 3 2 4 3 8 7	$ \begin{array}{l} 50\ 3d7\ (^2G)4d\ ^3F\ +\ 25\ 3d\ (^2G)4d\ ^3F\ +\ 15\ 3d\ (^2G)4d\ ^3F\ \\ 56\ 3d^7\ (^2G)4d\ ^3F\ +\ 20\ 3d^7\ (^2G)4d\ ^3F\ +\ 7\ 3d^7\ (^2G)4d\ ^3H\ \\ 53\ 3d^7\ (^2G)4d\ ^1F\ +\ 28\ 3d^7\ (^2G)4d\ ^3F\ \\ 59\ 3d^7\ (^2G)4d\ ^1F\ +\ 28\ 3d^7\ (^2G)4d\ ^3F\ \\ 59\ 3d^7\ (^2G)4d\ ^3F\ +\ 14\ 3d^7\ (^2G)4d\ ^3F\ \\ 84\ 3d^7\ (^2G)4d\ ^3F\ +\ 14\ 3d^7\ (^2G)4d\ ^1G\ +\ 13\ 3d^7\ (^2G)4d\ ^3F\ \\ 84\ 3d^7\ (^2G)4d\ ^1G\ +\ 12\ 3d^7\ (^2H)4d\ ^1G\ +\ 11\ 3d^7\ (^2G)4d\ ^3F\ \\ 47\ 3d^7\ (^2G)4d\ ^1G\ +\ 12\ 3d^7\ (^2P)4d\ ^1G\ +\ 13\ 3d^7\ (^2G)4d\ ^3F\ \\ 59\ 3d^7\ (^2G)4d\ ^1G\ +\ 13\ 3d^7\ (^2P)4d\ ^3F\ +\ 9\ 3d^7\ (^2G)4d\ ^3F\ \\ 59\ 3d^7\ (^2G)4d\ ^3F\ +\ 10\ 3d^7\ (^2P)4d\ ^3F\ +\ 10\ 3d^7\ (^2P)4d\ ^3F\ \\ \\ 59\ 3d^7\ (^2G)4d\ ^3F\ +\ 10\ 3d^7\ (^2P)4d\ ^3F\ +\ 10\ 3d^7\ (^2P)4d\ ^3F\ \\ \\ 43\ 3d^7\ (^2P)4d\ ^3F\ +\ 25\ 3d^7\ (^2P)4d\ ^3F\ +\ 10\ 3d^7\ (^2P)4d\ ^3F\ \\ \\ \\ 68\ 3d^7\ (^2P)4d\ ^3F\ +\ 25\ 3d^7\ (^2P)4d\ ^3F\ +\ 10\ 3d^7\ (^2P)4d\ ^3F\ \\ \\ \\ \ 60\ 3d^7\ (^2P)4d\ ^3F\ +\ 33\ 3d^7\ ^4d\ (^2H)4d\ ^3F\ +\ 10\ 3d^7\ (^2P)4d\ ^3F\ \ \\ \\ \ 60\ 3d^7\ (^2H)4d\ ^3F\ +\ 39\ 3d^7\ ^4d\ (^2H)\ ^4d\ ^3F\ \ \ 10\ 3d^7\ (^2P)4d\ ^3F\ \ \ 10\ 3d^7\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $
$\begin{array}{c} 314262.2\\ 314987.8\\ 315450\\ 315598.5\\ 315598.5\\ 315846\\ 315912.2\\ 316191.7\\ 316732.3\\ 317017\\ 317810.5\\ 318452.4\\ 318510\\ 318746.1 \end{array}$	$\begin{array}{c} 313245\\ 313002\\ 313936\\ 314282\\ 315132\\ 314164\\ 315602\\ 315136\\ 315663\\ 316424\\ 317512\\ 316886\\ 317611\\ 318293\\ 318355\\ 318838\\ \end{array}$	$\begin{array}{c} -197\\ 50\\ 1113\\ -65\\ -20\\ -144\\ 1286\\ -4\\ 710\\ 249\\ -232\\ -780\\ 131\\ 200\\ 159\\ 155\\ -92 \end{array}$	$ \begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \\ 2 \\ 3 \\ 2 \\ 4 \\ 3 \\ 3 \\ 8 \\ 7 \\ 5 \end{array} $	$ \begin{array}{l} 50\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +23\ 3d7^{(2)}_{(2)} 4d\ ^{3}G \\ 56\ 3d7^{(4)}_{(2)} 4d\ ^{5}D \\ +20\ 3d7^{(2)}_{(2)} 4d\ ^{3}H \\ +9\ 3d7^{(2)}_{(2)} 4d\ ^{3}H \\ +36\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +14\ 3d7^{(2)}_{(2)} 4d\ ^{1}G \\ +11\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +3\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +9\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +25\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +10\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +25\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +10\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +25\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +10\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +20\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +10\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +10\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +20\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +10\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +10\ 3d7^{(2)}_{(2)} 4d\ ^{3}F \\ +30\ 3d7^{(2)}_{(2)} 4d\ ^{3}K \\ +39\ 3d7^{(4)}_{(2)} 1K \\ 43\ 5d7^{(2)}_{(2)} 4d\ ^{3}G \\ \end{array}$
$\begin{array}{c} 314262.2\\ 314987.8\\ 315598.5\\ 315598.5\\ 315598.5\\ 315912.2\\ 316191.7\\ 316732.3\\ 317017\\ 317810.5\\ 318452.4\\ 318510\\ 318746.1\\ 319268.4 \end{array}$	313245 313602 313936 314282 315132 315132 315136 315663 315663 316424 317512 316886 317611 318293 318355 318355 318617	$\begin{array}{c} -197\\ 50\\ 113\\ -65\\ -20\\ -144\\ 1286\\ -4\\ 710\\ 249\\ -232\\ -780\\ 131\\ 200\\ 159\\ 155\\ -92\\ 651\end{array}$	$ \begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \\ 2 \\ 3 \\ 2 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 3 \\ 7 \\ 5 \\ 3 \\ 3 \\ 7 \\ 5 \\ 7 \\ 5 \\ 3 \\ 7 \\ 5 \\ 7 \\ 5 \\ 7 \\ 5 \\ 7 \\ 5 \\ 7 \\ 5 \\ 7 \\ 5 \\ 7 \\ $	$ \begin{array}{l} \begin{array}{l} 50\ 3d7^{(2)}(2) 4d\ ^{3}G \\ 56\ 3d7^{(4)}(2) 4d\ ^{5}D\ +\ 20\ 3d7^{(4)}(2) 4d\ ^{3}P\ +\ 7\ 3d7^{(4)}(4) 4d\ 3D \\ 53\ 3d7^{(2)}(2) 4d\ ^{1}I\ +\ 28\ 3d7^{(2)}(2) 4d\ ^{3}I\ +\ 18\ 3d7^{(2)}(2) 4d\ ^{3}H \\ 89\ 3d7^{(2)}(2) 4d\ ^{3}H\ +\ 9\ 3d7^{(2)}(2) 4d\ ^{3}H \\ 50\ 3d7^{(2)}(2) 4d\ ^{3}H\ +\ 36\ 3d7^{(2)}(2) 4d\ ^{3}H \\ 50\ 3d7^{(2)}(2) 4d\ ^{3}F\ +\ 14\ 3d7^{(2)}(2) 4d\ ^{3}H \\ 50\ 3d7^{(2)}(2) 4d\ ^{1}G\ +\ 12\ 3d7^{(2)}(2) 4d\ ^{3}H \\ 50\ 3d7^{(2)}(2) 4d\ ^{1}G\ +\ 12\ 3d7^{(2)}(2) 4d\ ^{1}G\ +\ 13\ 3d7^{(2)}(2) 4d\ ^{3}F \\ 58\ 3d7^{(2)}(2) 4d\ ^{1}D\ +\ 11\ 3d7^{(2)}(2) 4d\ ^{3}F\ +\ 7\ 3d7^{(2)}(2) 4d\ ^{3}F \\ 59\ 3d7^{(2)}(2) 4d\ ^{3}F\ +\ 9\ 3d7^{(2)}(2) 4d\ ^{3}F\ +\ 7\ 3d7^{(2)}(2) 4d\ ^{3}F \\ 59\ 3d7^{(2)}(2) 4d\ ^{3}F\ +\ 10\ 3d7^{(2)}(2) 4d\ ^{3}F \\ 59\ 3d7^{(2)}(2) 4d\ ^{3}F\ +\ 10\ 3d7^{(2)}(2) 4d\ ^{3}F \\ 43\ 3d7^{(2)}(2) 4d\ ^{3}F\ +\ 10\ 3d7^{(2)}(2) 4d\ ^{3}F \\ 43\ 3d7^{(2)}(2) 4d\ ^{3}F\ +\ 122\ 3d7^{(2)}(2) 4d\ ^{3}F\ +\ 10\ 3d7^{(2)}(2) 4d\ ^{3}F \\ 100\ 3d7^{(2)}(2) 4d\ ^{3}K \\ 60\ 3d7^{(2)}(2) 4d\ ^{3}K \\ 60\ 3d7^{(2)}(2) 4d\ ^{3}K \\ 60\ 3d7^{(2)}(2) 4d\ ^{3}G \\ 37\ 3d7^{(2)}(2) 4d\ ^{1}F\ +\ 28\ 3d7^{(2)}(2)\ ^{3}F\ +\ 7\ 3d7^{(2)}(2) 4d\ ^{3}F \\ 50\ 3d7^{(2)}(2) 4d\ ^{3}G \\ 37\ 3d7^{(2)}(2) 4d\ ^{1}F\ +\ 28\ 3d7^{(2)}(2)\ ^{3}F\ +\ 7\ 3d7^{(2)}(2) 4d\ ^{3}F \\ 50\ 3d7^{(2)}(2) 4d\ ^{3}G \\ 37\ 3d7^{(2)}(2) 4d\ ^{1}F\ +\ 28\ 3d7^{(2)}(2)\ ^{3}F\ +\ 7\ 3d7^{(2)}(2) 4d\ ^{3}F \\ 50\ 3d7^{(2)}(2) 4d\ ^{3}G \\ 37\ 3d7^{(2)}(2) 4d\ ^{3}F\ +\ 28\ 3d7^{(2)}(2)\ ^{3}F\ +\ 7\ 3d7^{(2)}(2) 4d\ ^{3}F\ +\ 7\ 3d$
$\begin{array}{c} 314262.2\\ 314987.8\\ 315450\\ 315598.5\\ 315598.5\\ 315912.2\\ 316191.7\\ 316732.3\\ 317017\\ 317810.5\\ 318452.4\\ 318510\\ 318746.1\\ 319268.4\\ 319586.7\\ \end{array}$	313245 313602 313936 314282 315132 315132 315662 315663 315663 316424 317512 316886 317611 318293 318355 3183838 318617 319643	$\begin{array}{c} -197\\ 50\\ 113\\ -65\\ -20\\ -144\\ 1286\\ -4\\ 710\\ 249\\ -232\\ -780\\ 131\\ 200\\ 159\\ 155\\ -92\\ 651\\ -56\end{array}$	$ \begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \\ 2 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 4 \\ 5 \\ 5 \\ 5 \\ 4 \\ 5 \\ 5 \\ 5 \\ 5 \\ 4 \\ 5 \\ 5 \\ 5 \\ 5 \\ 4 \\ 5 \\ $	$ \begin{array}{l} \begin{array}{l} 50\ \mathrm{3d}^{-}(^{2}\mathrm{G}\mathrm{)}\mathrm{d}\mathrm{d}^{-}\mathrm{G}\mathrm{G}\mathrm{d}\mathrm{d}^{-}\mathrm{G}\mathrm{G}\mathrm{d}\mathrm{d}^{-}\mathrm{H}\mathrm{d}^{-}\mathrm{g}\mathrm{S}\mathrm{d}^{-}(^{-}\mathrm{G}\mathrm{)}\mathrm{d}\mathrm{d}^{-}\mathrm{H}\mathrm{d}^{-}\mathrm{g}\mathrm{S}\mathrm{d}^{-}(^{-}\mathrm{G}\mathrm{)}\mathrm{d}\mathrm{d}^{-}\mathrm{I}\mathrm{H}\mathrm{d}^{-}\mathrm{g}\mathrm{S}\mathrm{d}^{-}(^{-}\mathrm{G}\mathrm{)}\mathrm{d}\mathrm{d}^{-}\mathrm{I}\mathrm{H}\mathrm{d}^{-}\mathrm{g}\mathrm{S}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{G}\mathrm{)}\mathrm{d}\mathrm{d}^{-}\mathrm{I}\mathrm{H}\mathrm{d}^{-}\mathrm{g}\mathrm{S}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{G}\mathrm{)}\mathrm{d}\mathrm{d}^{-}\mathrm{I}\mathrm{H}\mathrm{d}^{-}\mathrm{g}\mathrm{S}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{G}\mathrm{)}\mathrm{d}\mathrm{d}^{-}\mathrm{I}\mathrm{H}\mathrm{d}^{-}\mathrm{g}\mathrm{S}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{G}\mathrm{)}\mathrm{d}\mathrm{d}^{-}\mathrm{I}\mathrm{H}\mathrm{d}^{-}\mathrm{g}\mathrm{S}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{G}\mathrm{)}\mathrm{d}\mathrm{d}^{-}\mathrm{I}\mathrm{H}\mathrm{d}^{-}\mathrm{g}\mathrm{S}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{G}\mathrm{)}\mathrm{d}\mathrm{d}^{-}\mathrm{I}\mathrm{H}\mathrm{d}^{-}\mathrm{g}\mathrm{S}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{G}\mathrm{)}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{H}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{g}\mathrm{d}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{H}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{H}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{H}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{H}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{H}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{H}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{H}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{G}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{H}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{H}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{H}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{H}\mathrm{d}^{-}\mathrm{d}^{-}\mathrm{G}\mathrm{d}^{-}$
$\begin{array}{c} 314262.2\\ 314987.8\\ 315450\\ 315598.5\\ 315598.5\\ 315846\\ 315912.2\\ 316191.7\\ 316732.3\\ 317017\\ 317810.5\\ 318452.4\\ 318510\\ 318746.1\\ 318746.1\\ 319268.4\\ 319586.7\\ 319703.7\\ 319700.7\\ 319700.7\\ 319700.7\\ 319700.7\\ 319700.7\\ 319700.7\\ 319700.7\\ 319700.7\\ 319700.7\\ 319700.7\\ 319700.7\\ 319700.7\\ 319700.7\\ 319700.7\\ 319700.7\\ 319700.$	313245 313602 313936 314282 315132 314164 315602 315136 315663 316424 317512 316886 317611 318293 318355 318838 318617 319643 31959	$\begin{array}{c} -197\\ 50\\ 1113\\ -65\\ -20\\ -144\\ 1286\\ -4\\ 710\\ 249\\ -232\\ -780\\ 131\\ 200\\ 159\\ 155\\ -92\\ 651\\ -56\\ 108\end{array}$	3 2 6 4 5 4 3 4 2 3 2 4 3 3 8 7 5 3 4 6	$ \begin{array}{l} 50 \ 3d7^{(2)}(2) 4d^{3}F \\ 51 \ 3d7^{(2)}(2) 4d^{3}G \\ 52 \ 3d7^{(2)}(2) 4d^{3}G \\ 53 \ 3d7^{(2)}(2) 4d^{3}F \\ 51 \ 3d7^{(2)}(2) 4d^{$
314262.2 314987.8 315450 315598.5 315846 315912.2 316191.7 316732.3 317017 317810.5 318452.4 318510 318746.1 319268.4 319586.7 319703.7 319896.1	313245 313602 313936 314282 315132 314164 315602 3151663 316424 317512 3168866 317611 318355 318355 318355 318838 318617 319596 320030	-197 50 113 -65 -20 -144 1286 -4 710 249 -232 -780 131 200 155 -92 651 -56 108 -134	$ \begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \\ 2 \\ 3 \\ 2 \\ 4 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 6 \\ 4 \\ 6 \\ 4 \\ 7 \\ 5 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 6 \\ 4 \\ 6 \\ 4 \\ 7 \\ 5 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 6 \\ 4 \\ 6 \\ 4 \\ 7 \\ 5 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 6 \\ 4 \\ 6 \\ 4 \\ 7 \\ 5 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 6 \\ 4 \\ 7 \\ 7 \\ 5 \\ 7 \\ 7 \\ 5 \\ 3 \\ 8 \\ 7 \\ 7 \\ 5 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 6 \\ 4 \\ 7 \\ $	50 3d (2)4d 1 + 25 3d (2)4d 1 + 15 3d (2)4d 1 51 3d (2)4d 3G 56 3d (2)4d 1 + 28 3d (2)4d 3P + 7 3d (2)4d 3P 53 3d (2)4d 1 + 28 3d (2)4d 3P + 7 3d (2)4d 3P 53 3d (2)4d 1 + 28 3d (2)4d 3P + 7 3d (2)4d 3P 59 3d (2)4d 1 + 36 3d (2)4d 3P 59 3d (2)4d 3P + 14 3d (2)4d 3P 50 3d (2)4d 3P + 14 3d (2)4d 1G + 8 3d (2)4d 3P 58 3d (2)4d 3P + 14 3d (2)4d 1G + 11 3d (2)4d 3P 58 3d (2)4d 3P + 14 3d (2)4d 1G + 11 3d (2)4d 3P 58 3d (2)4d 3P + 13 3d (2)4d 3P + 7 3d (2)4d 3P 59 3d (2)4d 3P + 9 3d (2)4d 3P + 7 3d (2)4d 3P 59 3d (2)4d 3P + 9 3d (2)4d 3P + 7 3d (2)4d 3P 59 3d (2)4d 3P + 25 3d (2)4d 3P + 5 3d (2)4d 3P 59 3d (2)4d 3P + 25 3d (2)4d 3P + 5 3d (2)4d 3P 59 3d (2)4d 3P + 25 3d (2)4d 3P + 5 3d (2)4d 3P 58 3d (2)4d 3P + 23 3d (2)4d 3P + 5 3d (2)4d 3P 68 3d (2)4d 3P + 32 3d (2)4d 3P + 5 3d (2)4d 3P 68 3d (2)4d 3P + 32 3d (2)4d 3P + 10 3d (2)4d 3P 60 3d (2)4d 3P + 32 3d 74d (2)H 1K 94 3d (2)H 4d 3P 67 3d (2)H 4d 3P + 28 3d 74d (2) 3P + 10 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2) 3P + 10 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2) 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2) 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2) 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2) 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2) 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2) 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2)D 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2)D 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2)D 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2)D 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2)D 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2)D 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2)D 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2)D 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2)D 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2)D 3P + 11 3d (2)H 4d 95 3d (2)H 4d 3P + 20 3d 74d (2)D 3P + 11 3d (2)H 4d 3P 94 3d (2)H 4d 3P + 20 3d 74d (2)D 3P + 11 3d (2)H 4d 3P 94 3d (2)H 4d 3P + 20 3d 74d (2)D 3P + 11 3d (2)H 4d
314262.2 314987.8 315450 315598.5 315598.5 315846 315912.2 316191.7 316732.3 317017 317810.5 318452.4 318510 318746.1 318746.1 318746.1 318768.7 319268.4 319586.7 319703.7 319896.1 319992.7	313245 313602 313936 314282 314164 315132 314164 315602 315136 315663 316424 317611 318293 318355 318838 318617 319643 319596 320030 319604 319604	$\begin{array}{c} -197\\ 50\\ 113\\ -65\\ -20\\ -144\\ 1286\\ -4\\ 710\\ 249\\ -232\\ -780\\ 131\\ 200\\ 159\\ 155\\ -92\\ 651\\ -56\\ 108\\ -134\\ 389\\ 200\\ \end{array}$	3 2 6 4 5 4 3 4 2 3 2 4 3 3 8 7 5 3 4 6 4 3 7	50 3d (2)4d 1 + 25 3d (2)4d 1 + 15 3d (2)4d 1 51 3d (2)4d 3G 56 3d (2)4d 1 + 28 3d (2)4d 3P + 7 3d (2)4d 3P 53 3d (2)4d 1 + 28 3d (2)4d 3P + 7 3d (2)4d 3P 53 3d (2)4d 1 + 28 3d (2)4d 3P + 7 3d (2)4d 3P 59 3d (2)4d 1 + 28 3d (2)4d 3P 59 3d (2)4d 3F + 14 3d (2)4d 3P 50 3d (2)4d 3F + 14 3d (2)4d 1G + 8 3d (2)4d 3F 58 3d (2)4d 3F + 14 3d (2)4d 1G + 11 3d (2)4d 3F 59 3d (2)4d 1D + 11 3d (2)4d 1D + 8 3d (2)4d 3F 59 3d (2)4d 3F + 9 3d (2)4d 3F + 7 3d (2)4d 3F 59 3d (2)4d 3F + 9 3d (2)4d 3F + 7 3d (2)4d 3F 59 3d (2)4d 3F + 10 3d (2)4d 3F + 9 3d (2)4d 3F 59 3d (2)4d 3F + 10 3d (2)4d 3F + 5 3d (2)4d 3F 58 3d (2)4d 3F + 25 3d (2)4d 3F + 5 3d (2)4d 3F 58 3d (2)4d 3F + 22 3d (2)4d 3F + 5 3d (2)4d 3F 68 3d (2)4d 3F + 22 3d (2)4d 3F + 10 3d (2)4d 3F 68 3d (2)4d 3F + 22 3d (2)4d 3F + 10 3d (2)4d 3F 60 3d (2)4d 3F + 39 3d 4 (2) 1F + 10 3d (2)4d 3F 60 3d (2)4d 3F + 39 3d 4 (2) 3F + 10 3d (2)4d 3F 60 3d (2)4d 3F + 28 3d 74d (2) 3F + 10 3d (2)4d 3F 61 3d (2)4d 3G 63 7d (2)4d 3F + 20 3d 74d (2) 3F + 11 3d (2)4d 63 3d (2)4d 3F 64 3d (2)4d 3F 64 3d (2) 3F + 11 3d (2)4d 3F 65 3d (2)4d 3F 66 3d (2)4d 3F 67 3d (2)
$\begin{array}{c} 314262.2\\ 314987.8\\ 315450\\ 315598.5\\ 315598.5\\ 31558.6\\ 315912.2\\ 316191.7\\ 316732.3\\ 317017\\ 316732.3\\ 317017\\ 318710.5\\ 318452.4\\ 318510\\ 318746.1\\ 319268.4\\ 319586.7\\ 319703.7\\ 319896.1\\ 319992.7\\ 320160.1\\ 1\end{array}$	313245 313602 313936 314282 314164 315132 314164 315602 315136 315663 316424 317512 316886 317611 318293 318355 318338 318617 319643 319596 320030 319604 319962	-197 50 113 -65 -20 -144 1286 -4 710 249 -232 -780 131 200 155 -92 651 -56 108 -134 389 180 -130 -134 -136 -136 -136 -134 -136	$\begin{array}{c} 3\\ 2\\ 6\\ 4\\ 5\\ 4\\ 3\\ 4\\ 2\\ 3\\ 2\\ 4\\ 3\\ 3\\ 8\\ 7\\ 5\\ 3\\ 4\\ 6\\ 4\\ 3\\ 7\\ 6\end{array}$	50 3d7 (² G)4d ³ G 56 3d7 (² G)4d ³ G 56 3d7 (² G)4d ³ G 56 3d7 (² G)4d ¹ I + 28 3d7 (² G)4d ³ I + 18 3d7 (² G)4d ³ H 89 3d7 (² G)4d ¹ I + 28 3d7 (² G)4d ³ I + 18 3d7 (² G)4d ³ H 89 3d7 (² G)4d ³ H + 9 3d7 (² G)4d ³ G 50 3d7 (² G)4d ³ F + 14 3d7 (² G)4d ³ H 50 3d7 (² G)4d ¹ G + 12 3d7 (² H)4d ¹ G + 11 3d7 (² G)4d ³ F 84 3d7 (² G)4d ¹ D + 11 3d7 (² P)4d ¹ D + 8 3d7 (² G)4d ³ F 59 3d7 (² G)4d ¹ D + 11 3d7 (² P)4d ¹ D + 8 3d7 (² G)4d ³ F 59 3d7 (² G)4d ³ F + 9 3d7 (² P)4d ³ F + 7 3d7 (² H)4d ³ F 59 3d7 (² G)4d ³ F + 10 3d7 (² P)4d ³ F + 10 3d7 (² P)4d ³ F 68 3d7 (² P)4d ³ F + 25 3d7 (² H)4d ³ F + 9 3d7 (² D)4d ³ F 68 3d7 (² P)4d ³ F + 22 3d7 (² H)4d ³ F + 10 3d7 (² P)4d ³ F 100 3d7 (² H)4d ³ K + 39 3d7 4d (² H) ¹ K 60 3d7 (² H)4d ³ G + 19 3d7 4d (² D) ³ F + 10 3d7 (² H)4d 43 3d7 (² H)4d ³ G + 19 3d7 4d (² D) ³ F + 10 3d7 (² H)4d 43 3d7 (² H)4d ³ G + 19 3d7 4d (² D) ³ F + 11 3d7 (² P)4d 43 3d7 (² H)4d ³ G + 19 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 43 3d7 (² H)4d ³ G + 19 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 43 3d7 (² H)4d ³ G + 10 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 43 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 43 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 43 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 43 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 43 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 43 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 53 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 53 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 53 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 53 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 53 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 53 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 53 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 53 3d7 (² H)4d ³ G
314262.2 314987.8 315450 315598.5 3155846 315912.2 316191.7 316732.3 317017 317810.5 318452.4 318510 318746.1 318268.4 319586.7 319703.7 319896.1 319992.7 320141.7 320061.1	$\begin{array}{c} 313245\\ 313060\\ 313936\\ 314282\\ 315132\\ 315132\\ 315136\\ 315662\\ 315136\\ 315663\\ 315663\\ 316424\\ 317512\\ 316886\\ 317611\\ 318293\\ 318355\\ 318838\\ 318617\\ 319643\\ 319596\\ 320030\\ 319604\\ 319962\\ 320611\\ 320746\end{array}$	$\begin{array}{c} -197\\ 50\\ 113\\ -65\\ -20\\ -144\\ 1286\\ -4\\ 710\\ 249\\ -232\\ -780\\ 131\\ 200\\ 159\\ 155\\ -92\\ 651\\ -56\\ 108\\ -134\\ 389\\ 180\\ -10\\ 36\end{array}$	$\begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \\ 2 \\ 3 \\ 2 \\ 4 \\ 3 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 6 \\ 4 \\ 3 \\ 7 \\ 6 \\ 5 \\ 5 \\ 7 \\ 6 \\ 5 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 7 \\ 6 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 7 \\ 7$	50 3d7 (2)4d ³ F + 25 3d (3) ⁴⁷ F + 7 3d7 (4)4d ³ F + 7 3d7 (2)4d ³ H 53 3d7 (2)4d ³ F + 20 3d7 (4)4d ³ F + 7 3d7 (4)4d 3D 53 3d7 (2)4d ³ H + 9 3d7 (2)4d ³ I + 18 3d7 (2)4d ³ H 59 3d7 (2)4d ³ H + 9 3d7 (2)4d ³ G 50 3d7 (2)4d ³ F + 14 3d7 (2)4d ³ G 58 3d7 (2)4d ³ F + 14 3d7 (2)4d ¹ G + 11 3d7 (2)4d ³ F 58 3d7 (2)4d ¹ G + 12 3d7 (2)4d ¹ G + 11 3d7 (2)4d ³ F 59 3d7 (2)4d ¹ G + 12 3d7 (2)4d ³ F + 7 3d7 (2)4d ³ F 59 3d7 (2)4d ¹ G + 12 3d7 (2)4d ³ F + 7 3d7 (2)4d ³ F 59 3d7 (2)4d ³ F + 9 3d7 (2)4d ³ F + 7 3d7 (2)4d ³ F 59 3d7 (2)4d ³ F + 10 3d7 (2)4d ³ F + 9 3d7 (2)4d ³ F 59 3d7 (2)4d ³ F + 10 3d7 (2)4d ³ F + 10 3d7 (2)4d ³ F 59 3d7 (2)4d ³ F + 25 3d7 (2)4d ³ F + 10 3d7 (2)4d ³ F 68 3d7 (2)4d ³ F + 25 3d7 (2)4d ³ F + 10 3d7 (2)4d ³ F 100 3d7 (2)4d ³ K 60 3d7 (2)4d ³ K + 39 3d7 4d (2)H ¹ K 60 3d7 (2)4d ³ K + 39 3d7 4d (2)D ³ F + 10 3d7 (2)4d ³ F 100 3d7 (2)4d ³ G + 19 3d7 4d (2)D ³ F + 10 3d7 (2)4)4d 53 3d7 (2)4d ³ G + 20 3d7 4d (2)D ³ F + 11 3d7 (2)4d 41 3d7 (2)4d ³ G + 20 3d7 4d (2)H ¹ F + 14 3d7 (2)4d 53 3d7 (2)4d ³ H + 39 3d7 4d (2)H ³ F + 11 3d7 (2)4d 53 3d7 (2)4d ³ G + 20 3d7 4d (2)H ³ F + 11 3d7 (2)4d 53 3d7 (2)4d ³ G + 20 3d7 4d (2)H ³ F + 11 3d7 (2)4d 53 3d7 (2)4d ³ G + 20 3d7 4d (2)H ³ F + 11 3d7 (2)4d 53 3d7 (2)4d ³ G + 20 3d7 4d (2)H ³ F + 11 3d7 (2)4d 53 3d7 (2)4d ³ G + 20 3d7 4d (2)H ³ F + 11 3d7 (2)4d 53 3d7 (2)4d ³ G + 21 3d7 4d (2)H ³ F + 11 3d7 (2)4d 53 3d7 (2)4d ³ G + 21 3d7 4d (2)H ³ F + 11 3d7 (2)4d 53 3d7 (2)4d ³ G + 21 3d7 4d (2)H ³ F + 11 3d7 (2)4d 53 3d7 (2)4d ³ G + 21 3d7 4d (2)H ³ F + 11 3d7 (2)4d 53 3d7 (2)4d ³ G + 21 3d7 4d (2)H ³ F + 11 3d7 (2)4d 53 3d7 (2)4d ³ G + 21 3d7 4d (2)H ³ F + 11 3d7 (2)4d 53 3d7 (2)4d ³ G + 21 3d7 4d (2)H ³ G + 31 53 3d7 (2)4d ³ G + 21 3d7 4d (2)H ³ G + 31 53 3d7 (2)4d ³ G + 21 3d7 4d (2)H ³ G + 31 54 3d7 (2)4)4 ³ G + 21 3d7 4d (2)H ³ G + 31 54 3d7 (2)4)4 ³ G + 21 3d7 4d (2)H ³ G + 31 54 3d7 (2)4)4 ³ G
$\begin{array}{c} 314262.2\\ 314987.8\\ 315450\\ 315598.5\\ 315598.5\\ 315846\\ 315912.2\\ 316191.7\\ 316732.3\\ 317017\\ 317810.5\\ 318452.4\\ 318510\\ 318746.1\\ 319268.4\\ 319586.7\\ 319703.7\\ 319896.1\\ 319996.1\\ 319996.1\\ 319996.1\\ 319996.1\\ 320781.7\\ 320051.7\\ 320952 7 \end{array}$	313245 313936 313936 314282 315132 315132 315136 315663 315663 316424 317512 316886 317611 318293 318355 318617 319643 319596 320030 319604 319962 320611 320746 320917	$\begin{array}{c} -197\\ 50\\ 1113\\ -65\\ -20\\ -144\\ 1286\\ -4\\ 710\\ 249\\ -232\\ -780\\ 131\\ 200\\ 159\\ 155\\ -92\\ 001\\ 159\\ 155\\ -92\\ 651\\ -56\\ 108\\ -36\\ 36\\ 36\end{array}$	$\begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \\ 2 \\ 3 \\ 2 \\ 4 \\ 3 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 6 \\ 4 \\ 3 \\ 7 \\ 6 \\ 5 \\ 4 \end{array}$	
314262.2 314987.8 315450 315598.5 315846 315912.2 316191.7 316732.3 317017 317810.5 318452.4 318510 318746.1 319268.4 319586.7 319586.7 319896.1 319992.7 320141.7 3200781.7 320052.7 321064	313245 313602 313936 314282 315132 314164 315602 3151663 316424 317512 316886 317611 318355 318355 318355 318838 318617 319596 320030 319604 319604 319604 319604 3202746 320917 321082	$\begin{array}{c} -197\\ 50\\ 113\\ -65\\ -20\\ -144\\ 1286\\ -4\\ 710\\ 249\\ -232\\ -780\\ 131\\ 200\\ 159\\ 155\\ -92\\ 651\\ 155\\ -92\\ 651\\ -56\\ 108\\ -134\\ 389\\ 180\\ -10\\ 36\\ -18\end{array}$	$\begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \\ 2 \\ 3 \\ 2 \\ 4 \\ 3 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 6 \\ 4 \\ 3 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 5$	$ \begin{array}{l} \begin{array}{l} \begin{array}{l} \begin{array}{l} \begin{array}{l} \begin{array}{l} \begin{array}{l} \begin{array}{l}$
$\begin{array}{c} 314262.2\\ 314987.8\\ 315450\\ 315598.5\\ 315598.5\\ 315598.5\\ 315846\\ 315912.2\\ 316191.7\\ 316732.3\\ 317017\\ 317810.5\\ 318452.4\\ 318510\\ 318746.1\\ 319268.4\\ 319586.7\\ 319703.7\\ 319896.1\\ 319992.7\\ 320141.7\\ 32060.1\\ 320781.7\\ 320064\\ 321135.1\\ \end{array}$	313245 313602 313936 314282 315132 314164 315602 315136 315663 316424 317512 316886 317611 318293 318355 318388 31855 318838 318617 319643 319596 320030 319604 319962 320746 320746 320917 321082	$\begin{array}{c} -197\\ 50\\ 1113\\ -65\\ -20\\ -144\\ 1286\\ -4\\ 710\\ 249\\ -232\\ -780\\ 131\\ 200\\ 159\\ 155\\ -92\\ 651\\ 155\\ -92\\ 651\\ 108\\ -134\\ 389\\ 180\\ -10\\ 36\\ 36\\ -18\\ -59\end{array}$	$\begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \\ 2 \\ 3 \\ 2 \\ 4 \\ 3 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 6 \\ 4 \\ 3 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7$	$ \begin{array}{l} \begin{array}{l} 50\ 3d^7 (^2G)4d\ ^3G \\ 56\ 3d^7 (^4P)4d\ ^5D\ +\ 20\ 3d^7 (^4P)4d\ ^3P\ +\ 7\ 3d^7 (^4P)4d\ 3D \\ 53\ 3d^7 (^2G)4d\ ^1I\ +\ 28\ 3d^7 (^2G)4d\ ^3I\ +\ 18\ 3d^7 (^2G)4d\ ^3H \\ 89\ 3d^7 (^2G)4d\ ^1I\ +\ 28\ 3d^7 (^2G)4d\ ^3H \\ 89\ 3d^7 (^2G)4d\ ^3F\ +\ 14\ 3d^7 (^2G)4d\ ^1G\ +\ 8\ 3d^7 (^2P)4d\ ^3F \\ 84\ 3d^7 (^2G)4d\ ^1G\ +\ 12\ 3d^7 (^2G)4d\ ^1G\ +\ 8\ 3d^7 (^2P)4d\ ^3F \\ 47\ 3d^7 (^2G)4d\ ^1D\ +\ 11\ 3d^7 (^2P)4d\ ^1D\ +\ 8\ 3d^7 (^2G)4d\ ^3F \\ 47\ 3d^7 (^2G)4d\ ^1D\ +\ 11\ 3d^7 (^2P)4d\ ^1D\ +\ 8\ 3d^7 (^2G)4d\ ^3F \\ 47\ 3d^7 (^2G)4d\ ^3F\ +\ 9\ 3d^7 (^2P)4d\ ^3F\ +\ 7\ 3d^7 (^2G)4d\ ^3F \\ 59\ 3d^7 (^2G)4d\ ^3F\ +\ 9\ 3d^7 (^2P)4d\ ^3F\ +\ 7\ 3d^7 (^2P)4d\ ^3F \\ 59\ 3d^7 (^2G)4d\ ^3F\ +\ 10\ 3d^7 (^2P)4d\ ^3F\ +\ 5\ 3d^7 (^2P)4d\ ^3F \\ 59\ 3d^7 (^2G)4d\ ^3F\ +\ 10\ 3d^7 (^2P)4d\ ^3F\ +\ 5\ 3d^7 (^2D)4d\ ^3F \\ 59\ 3d^7 (^2P)4d\ ^3F\ +\ 12\ 3d^7 (^2P)4d\ ^3F\ +\ 5\ 3d^7 (^2P)4d\ ^3F \\ 59\ 3d^7 (^2P)4d\ ^3F\ +\ 12\ 3d^7 (^2P)4d\ ^3F\ +\ 5\ 3d^7 (^2P)4d\ ^3F \\ 50\ 3d^7 (^2P)4d\ ^3F\ +\ 12\ 3d^7 (^2P)4d\ ^3F\ +\ 10\ 3d^7 (^2P)4d\ ^3F \\ 50\ 3d^7 (^2P)4d\ ^3F\ +\ 12\ 3d^7 4d\ (^2P)\ ^3F\ +\ 10\ 3d^7 (^2P)4d\ ^3F \\ 50\ 3d^7 (^2H)4d\ ^3G\ +\ 19\ 3d^7 4d\ (^2P)\ ^3F\ +\ 10\ 3d^7 (^2H)4d \\ 40\ 53\ 3d^7 (^2H)4d\ ^3G\ +\ 19\ 3d^7 4d\ (^2D)\ ^3F\ +\ 11\ 3d^7 (^2P)4d \\ 40\ 59\ 3d^7 (^2H)4d\ ^3H\ +\ 39\ 3d^7 4d\ (^2D)\ ^3F\ +\ 11\ 3d^7 (^2P)4d \ 40\ 59\ 3d^7 (^2H)4d\ ^3H\ +\ 39\ 3d^7 4d\ (^2D)\ ^3F\ +\ 11\ 3d^7 (^2P)4d \ 59\ 3d^7 (^2H)4d\ ^3H\ +\ 39\ 3d^7 4d\ (^2D)\ ^3F\ +\ 11\ 3d^7 (^2P)4d \ 59\ 3d^7 (^2H)4d\ ^3H\ +\ 39\ 3d^7 4d\ (^2D)\ ^3G\ +\ 11\ 3d^7 (^2D)4d \ 50\ 3d^7 (^2D)4d\ ^3F\ +\ 29\ 3d^7 4d\ (^2D)\ ^3G\ +\ 11\ 3d^7 (^2D)4d\ 50\ 3d^7 (^2D)4d\ ^3F\ +\ 29\ 3d^7 4d\ (^2D)\ ^3G\ +\ 11\ 3d^7 (^2D)4d \ 50\ 3d^7 (^2D)4d\ ^3H\ +\ 29\ 3d^7 4d\ (^2D)\ ^3G\ +\ 11\ 3d^7 (^2D)4d\ 50\ 3d^7 (^2D)4d\ ^3F\ +\ 29\ 3d^7 4d\ (^2D)\ ^3G\ +\ 11\ 3d^7 (^2D)4d\ 50\ 3d^7 (^2D)4d\ ^3F\ +\ 29\ 3d^7 4d\ ^2D\ ^3G\ +\ 11\ 3d^7 (^2D)4d\ ^3F\ +\ 10\ 3d^7 (^2$
$\begin{array}{r} 314262.2\\ 314987.8\\ 315450\\ 315598.5\\ 315598.5\\ 315546\\ 315912.2\\ 316191.7\\ 316732.3\\ 317017\\ 316732.3\\ 317017\\ 317810.5\\ 318746.1\\ 318510\\ 318746.1\\ 318586.7\\ 319268.4\\ 319586.7\\ 319992.7\\ 32040.1\\ 319992.7\\ 320141.7\\ 320952.7\\ 321064\\ 321135.1\\ 321542.1 \end{array}$	$\begin{array}{r} 313245\\ 313002\\ 313936\\ 314282\\ 315132\\ 314164\\ 315602\\ 315136\\ 315663\\ 316424\\ 317512\\ 316886\\ 317611\\ 318293\\ 318355\\ 318838\\ 318617\\ 319643\\ 319596\\ 320030\\ 319604\\ 319962\\ 320611\\ 320746\\ 320917\\ 321082\\ 321194\\ 321586\end{array}$	$\begin{array}{c} -197\\ 50\\ 113\\ -65\\ -20\\ -144\\ 1286\\ -4\\ 710\\ 249\\ -780\\ 131\\ 200\\ 159\\ 155\\ -92\\ 651\\ -56\\ 108\\ -134\\ 389\\ 180\\ -10\\ 36\\ -18\\ -59\\ -44 \end{array}$	$\begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \\ 2 \\ 3 \\ 2 \\ 4 \\ 3 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 6 \\ 4 \\ 3 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 5 \\ 7 \\ 6 \\ 7 \\ 7$	50 3d7 (2)4d ³ G 56 3d7 (² G)4d ³ G 56 3d7 (⁴ P)4d ⁵ D + 20 3d7 (⁴ P)4d ³ P + 7 3d7 (⁴ P)4d 3D 53 3d7 (² G)4d ¹ I + 28 3d7 (² G)4d ³ I + 18 3d7 (² G)4d ³ H 89 3d7 (² G)4d ³ H + 9 3d7 (² G)4d ³ G 59 3d7 (² G)4d ³ F + 14 3d7 (² G)4d ³ G 58 3d7 (² G)4d ¹ G + 12 3d7 (² H)4d ¹ G + 11 3d7 (² G)4d ³ F 84 3d7 (² G)4d ¹ D + 11 3d7 (² P)4d ¹ D + 8 3d7 (² G)4d ³ F 59 3d7 (² G)4d ¹ D + 11 3d7 (² P)4d ¹ D + 8 3d7 (² G)4d ³ F 59 3d7 (² G)4d ³ F + 9 3d7 (² P)4d ³ F + 7 3d7 (² H)4d ³ F 59 3d7 (² G)4d ³ F + 10 3d7 (² P)4d ³ F + 10 3d7 (² P)4d ³ F 68 3d7 (² G)4d ³ F + 25 3d7 (² H)4d ³ F + 9 3d7 (² D)4d ³ F 68 3d7 (² P)4d ³ D + 7 3d7 (² D)4d ³ F + 10 3d7 (² P)4d ³ F 100 3d7 (² H)4d ³ K + 39 3d7 4d (² H) ¹ K 60 3d7 (² H)4d ³ G + 19 3d7 4d (² D) ³ F + 10 3d7 (² P)4d ³ G 37 3d7 (² H)4d ³ G + 19 3d7 4d (² H) ³ F + 10 3d7 (² H)4d 43 3d7 (² H)4d ³ G + 19 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 43 3d7 (² H)4d ³ G + 12 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 43 3d7 (² H)4d ³ G + 12 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 43 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 43 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 58 3d7 (² H)4d ³ G + 20 3d7 4d (² H) ³ F + 11 3d7 (² P)4d 58 3d7 (² H)4d ³ G + 21 3d7 4d (² H) ³ G 38 3d7 (² H)4d ³ G + 21 3d7 4d (² D) ³ G 38 3d7 (² H)4d ³ G + 21 3d7 4d (² D) ³ G + 11 3d7 (² H)4d ¹ H 99 3d7 (² H)4d ³ I + 20 3d ⁶ 4s ² ³ H + 15 3d7 (² H)4d ¹ H 99 3d7 (² H)4d ³ I + 14 3d7 4d (² H) ¹ I
$\begin{array}{r} 314262.2\\ 314987.8\\ 315450\\ 315598.5\\ 315598.5\\ 31558.6\\ 315912.2\\ 316191.7\\ 316732.3\\ 317017\\ 316732.3\\ 317017\\ 316732.3\\ 318746.1\\ 318510\\ 318746.1\\ 319268.4\\ 319586.7\\ 319703.7\\ 319896.1\\ 319992.7\\ 320141.7\\ 320952.7\\ 32061.1\\ 320781.7\\ 320952.7\\ 321064\\ 321135.1\\ 321542.1\\ 322051.3\\ \end{array}$	$\begin{array}{r} 313245\\ 313936\\ 313936\\ 314282\\ 315132\\ 314164\\ 315602\\ 315136\\ 315663\\ 315663\\ 315663\\ 315663\\ 315663\\ 317611\\ 318293\\ 318355\\ 31838\\ 318617\\ 319643\\ 319596\\ 320030\\ 319604\\ 319962\\ 320611\\ 320746\\ 320917\\ 321082\\ 321194\\ 321586\\ 322028\\ \end{array}$	$\begin{array}{c} -197\\ 50\\ 113\\ -65\\ -20\\ -144\\ 1286\\ -4\\ 710\\ 249\\ -232\\ -780\\ 131\\ 200\\ 155\\ -92\\ 651\\ -56\\ 108\\ -134\\ 389\\ 180\\ -10\\ 36\\ 36\\ -18\\ -59\\ -44\\ 23\\ \end{array}$	$\begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \\ 2 \\ 3 \\ 2 \\ 4 \\ 3 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 6 \\ 4 \\ 3 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 6 \\ 3 \\ \end{array}$	
$\begin{array}{r} 314262.2\\ 314987.8\\ 315450\\ 315598.5\\ 315598.5\\ 31558.6\\ 315912.2\\ 316191.7\\ 316732.3\\ 317017\\ 316732.3\\ 317017\\ 318740.1\\ 318740.1\\ 318510\\ 318746.1\\ 319268.4\\ 319586.7\\ 319703.7\\ 319896.1\\ 319992.7\\ 320141.7\\ 320952.7\\ 320041.7\\ 320952.7\\ 321064\\ 321135.1\\ 321542.1\\ 321542.1\\ 322051.3\\ 322013.4\\ \end{array}$	313245 313602 313936 314282 315132 314164 315602 315136 315663 316424 317512 316886 317611 318293 318355 318617 319643 319596 320030 319604 319962 320611 320746 32017 321194 321194 321586 322028 322358	$\begin{array}{c} -197\\ 50\\ 1113\\ -65\\ -20\\ 113\\ -65\\ -20\\ 113\\ 1286\\ -4\\ 710\\ 249\\ -232\\ -780\\ 131\\ 200\\ 159\\ 155\\ -92\\ 651\\ -56\\ 108\\ -134\\ 389\\ 180\\ -10\\ 36\\ 36\\ -18\\ -59\\ -41\\ 23\\ -41\end{array}$	$\begin{array}{c} 3 \\ 2 \\ 6 \\ 4 \\ 5 \\ 4 \\ 3 \\ 4 \\ 2 \\ 3 \\ 2 \\ 4 \\ 3 \\ 2 \\ 4 \\ 3 \\ 3 \\ 8 \\ 7 \\ 5 \\ 3 \\ 4 \\ 6 \\ 4 \\ 3 \\ 7 \\ 6 \\ 5 \\ 4 \\ 5 \\ 7 \\ 6 \\ 3 \\ 5 \end{array}$	
314262.2 314987.8 315450 315598.5 315846 315912.2 316191.2 316191.7 317810.5 318452.4 318452.4 318510 318746.1 319268.4 319586.7 319703.7 319896.1 319992.7 320141.7 3200781.7 320781.7 320052.7 321064 321135.1 32237.4 322317.4 322338.2	313245 3130245 313936 314282 315132 314164 315602 3151663 316424 317512 316886 317611 318355 318355 318355 318838 318617 319596 320030 319604 319604 320917 320746 320917 321194 321586 322028 322156	$\begin{array}{c} -197\\ 50\\ 1113\\ -65\\ -20\\ -144\\ 1286\\ -4\\ 710\\ 249\\ -232\\ -780\\ 131\\ 200\\ 159\\ 155\\ -92\\ 651\\ 155\\ -92\\ 651\\ -56\\ 108\\ -134\\ 389\\ -10\\ 36\\ -18\\ -59\\ -44\\ 23\\ -41\\ 182\end{array}$	$egin{array}{cccccccccccccccccccccccccccccccccccc$	

Table A1: Continued

			100	
E^{a}_{exp}	E_{calc}^{b}	ΔE	J	Leading components (in %) in LS coupling c
322608.1	322491	117	2	93 $3d^{7}(^{4}P)5s {}^{5}P + 6 3d^{7}5s (^{2}P) {}^{3}P$
323155.3	323377	-222	4	$27 \ 3d^{7}(^{2}D)4d^{3}G + 24 \ 3d^{7}4d \ (^{2}D)^{1}G + 16 \ 3d^{7}(^{2}P)4d$
323249	323131	118	1	$79 \ 3d^{7}(^{4}P)5s \ ^{5}P + 5 \ 3d^{7}4d \ (^{2}D) \ 3D$
323754.8	323586	169	6	$44 \ 3d^{7}(^{2}H)4d^{1}I + 32 \ 3d^{6}4s^{2} \ ^{3}H + 18 \ 3d^{7}(^{2}H)4d^{3}H$
324118.1	323759	359	6	$38 \ 3d^{7}(^{2}H)4d^{1}I + 22 \ 3d^{6}4s^{2} \ ^{3}H + 22 \ 3d^{7}(^{2}H)4d^{3}H$
324418.7	324414	5	2	75 $3d^{7}(^{4}P)5s^{3}P + 9 3d^{6}4s^{2} {}^{3}P + 6 3d^{6}4s^{2} {}^{3}P$
324619.3	324222	397	5	$44 \ 3d^{6}4s^{2} \ ^{3}H + 41 \ 3d^{7}4d \ (^{2}H) \ ^{3}H$
324731.4	324455	276	4	$45 \ 3d^{6}4s^{2} \ {}^{3}H + 42 \ 3d^{7}4d \ (^{2}H) \ {}^{3}H$
324759.9	324572	188	5	$95 \ 3d^7(^2G)5s^{-3}G$
325225.9	325037	189	4	$75 \ 3d^7(^2G)5s \ ^3G + 17 \ 3d^75s \ (^2G) \ ^1G$
326247.5	326050	198	3	$99 \ 3d^7(^2G)5s^3G$
326979.8	326764	216	4	$69 \ 3d^{7}(^{2}G)5s \ ^{1}G + 21 \ 3d^{7}5s \ (^{2}G) \ ^{3}G$
327356.7	327318	39	4	$42 \ 3d^{7}(^{2}H)4d^{3}F + 13 \ 3d^{7}4d \ (^{2}D)^{3}F + 9 \ 3d^{7}(^{2}G)4d$
328720	328760	-40	3	$39 \ 3d^{7}(^{2}H)4d^{3}F + 12 \ 3d^{7}4d \ (^{2}D)^{3}F + 11 \ 3d^{7}(^{2}G)4d$
329181.7	329441	-259	2	$34 \ 3d^7(^2H)4d \ ^3F + 12 \ 3d^74d \ (^2G) \ ^3F + 11 \ 3d^7(^2D)4d$
329341.2	329712	-371	2	$77 \ 3d^{7}(^{2}P)5s \ ^{3}P + 8 \ 3d^{7}5s \ (^{2}D) \ 3D + 5 \ 3d^{7}(^{4}P)5s$
329632.8	330121	-488	1	$51 \ 3d^{7}(^{2}P)5s \ ^{3}P + 24 \ 3d^{7}5s \ (^{2}P) \ ^{1}P + 14 \ 3d^{7}(^{2}D)5s$
331041.9	331669	-627	1	$53 \ 3d^7(^2P)5s^{-1}P + 39 \ 3d^75s(^2P)^{-3}P$
332035.9	332203	-167	4	$61 \ 3d^{7}(^{2}H)4d^{1}G + 13 \ 3d^{7}4d^{2}F)^{1}G + 11 \ 3d^{7}(^{2}G)4d$
332436.4	332584	-148	6	99 3d ⁷ (² H)5s ³ H
332854.7	332986	-131	5	$78 \ 3d^7(^2H)5s \ ^3H + 20 \ 3d^75s \ (^2H) \ ^1H$
333005.7	332799	207	3	77 $3d^{7}(^{2}D)5s^{3}D + 22 3d^{7}5s^{2}D)^{3}D$
333736.7	333127	610	2	$27 \ 3d^{7}(^{2}D)5s \ ^{3}D + 27 \ 3d^{7}5s \ (^{2}D) \ ^{1}D + 8 \ 3d^{7}(^{2}D)5s$
333868.7	333962	-93	4	95 3d ⁷ (² H)5s ³ H
334564.8	334649	-84	5	$78 \ 3d^{7}(^{2}H)5s^{-1}H + 19 \ 3d^{7}(^{2}H)5s^{-3}H$
335885.5	335708	178	2	$44 \ 3d^{7}(^{2}D)5s^{1}D + 22 \ 3d^{7}(^{2}D)5s \ 3D + 11 \ 3d^{7}(^{2}P)5s^{3}P$
338974.8	339070	-95	5	$88 \ 3d^7(^2F)4d^{-3}H + 8 \ 3d^7(^2F)4d^{-1}H$
339378.8	339547	-168	6	96 3d ⁷ (² F)4d ³ H
339392.7	339687	-294	3	86 $3d^{7}(^{2}F)4d^{3}G + 6 3d^{7}(^{2}F)4d^{1}F$
339763.8	340079	-315	4	$89 \ 3d^7 (^2F) 4d^3G$
339808.5	339916	-108	5	90 $3d^{7}(^{2}F)4d^{1}H + 8 3d^{7}(^{2}F)4d^{3}H$
340161.9	340554	-392	5	$94 \ 3d^7 (^2F)4d^3G$
347248.7	347352	-103	4	81 $3d^{7}(^{2}F)4d^{1}G + 7 3d^{7}(^{2}H)4d^{1}G$
351520.2	351425	95	3	93 $3d_{-}^{7}({}^{2}F)5s_{-}^{3}F + 6 3d_{-}^{7}({}^{2}F)5s_{-}^{1}F$
351908.8	351901	8	4	99 $3d^{7}(^{2}F)5s^{3}F$
			T	A NIGH 11 A TOOL

a: From the NIST compilation [28] b: This work c: Only the components \geq to 5% are given

Table A2: Comparison between available experimental data and calculated odd energy levels (in cm⁻¹) in Cu IV

E^{a}_{exp}	E^b_{calc}	ΔE	J	Leading components (in %) in LS coupling c
190527.7	190558	-30	5	91 $3d^{7}({}^{4}F)4p {}^{5}F + 7 3d^{7}({}^{4}F)4p {}^{5}G$
190553.6	190616	-62	4	$54 \ 3d^{7}({}^{4}F)4p \ {}^{5}F + 38 \ 3d^{7}({}^{4}F)4p \ {}^{5}D$
191761.8	191801	-39	3	$70 \ 3d' ({}^{4}F)4p \ {}^{5}F + 23 \ 3d' ({}^{4}F)4p \ {}^{5}D$
192741	192763	-22	2	$83 3d' ({}^{4}F)4p {}^{5}F + 12 3d' ({}^{4}F)4p {}^{5}D$
192752.8	192764	-11	4	51 3d'(-F)4p *D + 34 3d'(-F)4p *F + 9 3d'(-F)4p *G
193434.4	193443	-9	6	95.5d (F)4p F + 5.5d (F)4p D $90.3d^{7}(^{4}F)4p^{-5}C$
193947.8	193923	-17	3	$63 3d^{7}({}^{4}F)4p {}^{5}D + 18 3d^{7}({}^{4}F)4p {}^{5}F + 11 3d^{7}({}^{4}F)4p {}^{5}G$
194339.1	194309	30	5	$75 3d^{7}({}^{4}F)4p {}^{5}G + 16 3d^{7}({}^{4}F)4p {}^{3}G + 9 3d^{7}({}^{4}F)4p {}^{5}F$
195054.9	195010	45	4	$78 \ 3d^{7}({}^{4}F)4p \ {}^{5}G + 10 \ 3d^{7}({}^{4}F)4p \ {}^{5}F + 7 \ 3d^{7}({}^{4}F)4p \ {}^{3}G$
195085.9	195114	-28	2	$71 \ 3d^{7}({}^{4}F)4p^{5}D + 11 \ 3d^{7}({}^{4}F)4p^{5}G + 9 \ 3d^{7}({}^{4}F)4p^{5}F$
195544.1	195496	48	3	$80 \ 3d^7({}^4F)4p \ {}^5G \ + \ 10 \ 3d^7({}^4F)4p \ {}^5F$
195684.3	195732	-48	1	$84 \ 3d^{7}(^{4}F)4p^{5}D + 10 \ 3d^{7}(4P)4p^{5}D + 5 \ 3d^{7}(^{4}F)4p^{5}F$
195827	195780	47	2	$84 \ 3d_{-}^{7}({}^{4}F)4p \ {}^{5}G + 6 \ 3d_{-}^{7}({}^{4}F)4p \ {}^{5}F + 6 \ 3d_{-}^{7}({}^{4}F)4p \ {}^{5}D$
195932	195990	-58	0	$88 \ 3d^{7}({}^{4}F)4p \ {}^{5}D + 11 \ 3d^{7}(4P)4p \ {}^{5}D$
197325	197340	-15	5	81 $3d'({}^{4}F)4p {}^{3}G + 18 3d'({}^{4}F)4p {}^{5}G$
198179.2	198209	-30	4	$88 3d' ({}^{4}F)4p {}^{9}F$
199202.3	199214	-12	4	$86 3d'({}^{+}F)4p {}^{\circ}G + 10 3d'({}^{+}F)4p {}^{\circ}G$
199598.8	199633	-34	3	$84 3 d^{-}(F) 4p^{-}F + 5 3 d^{-}(F) 4p^{-}D$
200482.0	200497 200734	-14 -14	2	92 3d (F)4p G 89 3d ⁷ (⁴ F)4p ³ F \pm 5 3d ⁷ (2G)4p ³ F
201210.9	200734	-167	3	$87 3d^{7}({}^{4}F)4p^{3}D + 6 3d^{7}({}^{4}F)4p^{3}F$
202360.6	202528	-167	2	$88 3d^7({}^4\text{F})4p {}^3\text{D}$
203139.5	203306	-167	1	$90 \ 3d^7 ({}^4F)4p^{-3}D$
203868.9	203936	-67	2	$97 \ 3d^7(4P)4p \ 5S$
213360.4	213346	14	1	$57 \ 3d^7 (4P) 4p^5 D + 11 \ 3d^7 (2P) 4p^3 P + 10 \ 3d^7 (4P) 4p^3 S$
213534.5	213340	195	2	$76 \ 3d^{7}(4P)4p^{5}D + 9 \ 3d^{7}(^{4}F)4p^{5}D$
213664.9	213412	253	3	$78 \ 3d^{7}(4P)4p \ {}^{5}D + 8 \ 3d^{7}({}^{4}F)4p \ {}^{5}D + 7 \ 3d^{7}(4P)4p \ 3D$
213932.1	213784	148	0	$82 3d^{7}(4P)4p^{5}D + 11 3d^{7}({}^{4}F)4p^{5}D + 6 3d^{7}(2P)4p^{3}P$
214318.7	214025	294	4	$89 \ 3d' (4P) 4p \ ^{9}D + 6 \ 3d' (^{4}F) 4p \ ^{9}D$
214413.4	214464	-51	1	$42 \ 3d' (4P)4p \ ^{3}S + 25 \ 3d' (4P)4p \ ^{3}D + 10 \ 3d' (2P)4p \ ^{3}S$
214835.3	214638	197	5	$67 \text{ 3d}^{\circ}(2\text{G})4\text{p}^{\circ}\text{H} + 17 \text{ 3d}^{\circ}(2\text{G})4\text{p}^{\circ}\text{H} + 10 \text{ 3d}^{\circ}(2\text{G})4\text{p}^{\circ}\text{G}$
215132.8	214971	162	4	55 3d'(2G)4p F + 12 3d'(2G)4p G + 8 3d'(2G)4p H
215755.9	215555	201	6	$^{05} 3d^7 (2G)4p^{-11} + 8.5d (2G)4p^{-1}$
216428.9	216928	-499	0	$67 3d^7(2P)4p^{-3}P + 16 3d^7(2D)4p^{-3}P + 6 3d^7(2D)4p^{-3}P$
216702.9	217017	-314	2	$31 \ 3d^7(2P)4p^{-3}P + 34 \ 3d^7(4P)4p^{-5}P + 16 \ 3d^7(4P)4p^{-3}D$
217079.2	216916	163	3	$73 \ 3d^7(2G)4p^{3}F + 16 \ 3d^7(2G)4p^{3}G$
217109.3	217546	-437	1	$48 \ 3d^{7}(2P)4p^{3}P + 18 \ 3d^{7}(4P)4p^{5}P + 9 \ 3d^{7}(2D)4p^{3}P$
217444.6	217385	60	4	$46 \ 3d^{7}(2G)4p^{1}G + 25 \ 3d^{7}(2G)4p^{3}F + 16 \ 3d^{7}(2H)4p^{1}G$
217621.1	217294	327	3	$54 \ 3d^{7}(4P)4p \ {}^{5}P + 29 \ 3d^{7}(4P)4p \ {}^{3}D + 8 \ 3d^{7}(4P)4p \ {}^{5}D$
217649.6	217743	-93	2	$48 \ 3d' (4P)4p \ ^{9}P + 26 \ 3d' (4P)4p \ ^{9}D + 5 \ 3d' (2D)4p \ ^{9}D$
217999.5	217971	29	5	$79 \text{ 3d}^{\circ}(2\text{G})4\text{p}^{\circ}\text{G} + 15 \text{ 3d}^{\circ}(2\text{G})4\text{p}^{\circ}\text{H}$
218027.5	217915	113	2	$13 \text{ 3d} (2P)4p ^{\circ}D + 28 \text{ 3d} (2P)4p ^{\circ}P + 16 \text{ 3d} (4P)4p ^{\circ}D$
218137.0	217871	200	3 1	48 3d (4r) 4p 3D + 34 3d (4r) 4p r $63 3d^7 (4P) 4p ^5P + 24 3d^7 (4P) 4p ^3S$
218628	218499	129	3	$45 3d^{7}(2G)4p^{3}G + 31 3d^{7}(2G)4p^{1}F + 9 3d^{7}(2G)4p^{3}F$
218631.1	218617	14	1	$64 \ 3d^7 (4P)4p \ 3D \ + \ 18 \ 3d^7 (2P)4p^3D$
218726.2	218501	225	2	92 $3d^{7}(2G)4p^{3}F + 5 3d^{7}(^{4}F)4p^{3}F$
218814.5	218633	182	5	$63 \ 3d^7(2G)4p^{-1}H + 27 \ 3d^7(2G)4p^{-3}H + 8 \ 3d^7(2G)4p^{-3}G$
218944.8	218965	-20	4	$72 \ 3d^7(2G)4p^{\ 3}G + 11 \ 3d^7(2G)4p^{\ 1}G + 8 \ 3d^7(2G)4p^{\ 3}H$
219402.7	219383	20	3	$36 \ 3d^{7}(2G)4p^{1}F + 34 \ 3d^{7}(2G)4p^{3}G + 8 \ 3d^{7}(2G)4p^{3}F$
219867.4	220519	-652	0	$49 \ 3d^{\prime} (4P)4p \ {}^{3}P + 39 \ 3d^{\prime} (2P)4p \ {}^{1}S + 9 \ 3d^{\prime} (2P)4p \ {}^{3}P$
220315.6	220202	114	2	$66 \ 3d' (4P)4p \ ^{9}P + 11 \ 3d' (2D)4p \ ^{9}P + 6 \ 3d' (4P)4p \ ^{9}P$
220917	220971	-54	5	92 3d'(2H)4p *G + 5 3d'(2F)4p *G
221271.0	221200	111	6	$67.3d^{-}(4P)4p^{-}P^{-} + 10.3d^{-}(2P)4p^{-}D$ $60.2d^{7}(2P)4p^{-}2P + 28.2d^{7}(2P)4p^{-}1$
221650	222030	-380	3	$61 \ 3d^7(2P)4p \ 3D + 14 \ 3d^7(2D)4p \ ^3D + 6 \ 3d^7(2D)4p \ ^3D$
221738.5	221783	-45	2	$22 \ 3d^7(4P)4p \ 3D + 18 \ 3d^7(4P)4p \ ^3P + 15 \ 3d^7(2P)4p \ ^1D$
222335.9	222349	-13	1	$29 \ 3d^7(2P)4p \ 3D + 24 \ 3d^7(2D)4p \ ^3D + 20 \ 3d^7(4P)4p \ ^3P$
222397.7	222405	-7	4	$87 \ 3d^7(2H)4p^{-3}G + 6 \ 3d^7(2F)4p^{-3}G$
222527.4	222622	-95	5	93 3d ⁷ (2H)4p 3I
222602.5	222746	-144	2	29 $3d^{7}(2D)4p 3D + 24 3d^{7}(2P)4p ^{3}D + 10 3d^{7}(2P)4p ^{1}D$
222665.8	222751	-85	7	100 3d ⁷ (2H)4p 3I
223000	222545	455	3	$47 \text{ 3d}'(2D)4p \text{ 3D} + 17 \text{ 3d}'(2D)4p ^{3}\text{F} + 12 \text{ 3d}'(2D)4p ^{3}\text{D}$
223623	223580	43	3	$(9.3a^{\circ}(2H)4p^{\circ}G + 6.3a^{\circ}(2F)4p^{\circ}G$
223764.1	223734	3U _610	1	29 Su (2D)4p SD + 27 Su (2P)4p $^{\circ}$ D + 18 Su (2P)4p $^{\circ}$ P 56 Su (2D)4p 1 S + 43 Su 7 (4P)4p 3 D
223647.4	224407 224121	-610	2	$34 \ 3d^7(2P)4p \ 3D \ \pm \ 22 \ 3d^7(2D)4p \ r$
224959.1	225045	-86	6	$69 3d^7(2\text{H})4p {}^1\text{I} + 27 3d^7(2\text{H})4p {}^3\text{I}$
225386.9	225131	256	4	$77 \ 3d^7(2D)4p \ {}^3F + 20 \ 3d^7(2D)4p \ {}^3F$
225858.9	225659	200	3	48 $3d^{7}(2D)4p^{3}F + 13 3d^{7}(2P)4p^{3}D + 11 3d^{7}(2D)4p^{3}F$
226271.3	226057	214	2	51 $3d^{7}(2D)4p^{3}F + 11 3d^{7}(2D)4p^{3}D + 10 3d^{7}(2D)4p^{3}F$
226558	227127	-569	1	$39 3d^{7}(2P)4p {}^{1}P + 24 3d^{7}(2P)4p {}^{3}S + 11 3d^{7}(2D)4p {}^{3}P$
227159.6	227375	-215	1	$53 \ 3d^7 (2P)4p^{-3}S + 20 \ 3d^7 (2P)4p^{-1}P + 9 \ 3d^7 (4P)4p^{-3}S$

Table A2: Continued

E^a_{exp}	E^{b}_{calc}	ΔE	J	Leading components (in $\%$) in LS coupling ^{c}
227959.5	227765	195	2	$28 3d^7(2D)4p {}^1D + 23 3d^7(2D)4p {}^3P + 22 3d^7(2P)4p {}^1D$
227993.2	228180	-187	6	$97 \; 3d^7 (2H) 4p \; {}^{3}H$
228479.7	228640	-160	5	$93 \ 3d^7 (2H) 4p^{-3} H$
229064	229213	-149	4	$94 \ 3d^7(2H)4p^{-3}H$
229694.2	229500	194	2	$34 \ 3d^{7}(2D)4p^{3}P + 19 \ 3d^{7}(2D)4p^{1}D + 13 \ 3d^{7}(2P)4p^{3}P$
230235.9	230367	-131	4	$67 \ 3d^7(2H)4p^{-1}G + 29 \ 3d^7(2G)4p^{-1}G$
230331.1	230057	274	3	$56 \ 3d^7(2D)4p^{-1}F + 17 \ 3d^7(2G)4p^{-1}F + 13 \ 3d^7(2D)4p^{-1}F$
231216.3	231151	65	1	49 $3d^{7}(2D)4p^{3}P + 14 3d^{7}(2P)4p^{1}P + 11 3d^{7}(2P)4p^{3}P$
231825.2	231633	192	0	$65 \ 3d^7(2D)4p \ ^3P + 17 \ 3d^7(2P)4p \ ^3P + 12 \ 3d^7(2D)4p \ ^3P$
232441.8	232271	171	1	$72 \ 3d^7(2D)4p \ ^1P + 12 \ 3d^7(2D)4p \ ^1P + 5 \ 3d^7(2P)4p \ ^3S$
233298.6	233428	-129	5	$94 \; 3d^7 (2H) 4p^{-1} H$
241854.9	241819	36	2	$57 \ 3d^7(2F)4p^{-1}D + 32 \ 3d^7(2F)4p^{-3}F + 5 \ 3d^7(2F)4p^{-3}D$
242529.8	242488	42	3	$74 \ 3d^{7}(2F)4p^{3}G + 15 \ 3d^{7}(2F)4p^{3}F + 7 \ 3d^{7}(2H)4p^{3}G$
243028.9	243071	-42	4	$60 \ 3d^{7}(2F)4p^{3}G + 21 \ 3d^{7}(2F)4p^{3}F + 11 \ 3d^{7}(2F)4p^{1}G$
243725.3	243724	1	3	49 $3d^{7}(2F)4p 3D + 34 3d^{7}(2F)4p {}^{3}F + 7 3d^{7}(2F)4p {}^{3}G$
244071.6	244091	-19	2	$62 \ 3d^{7}(2F)4p^{3}F + 28 \ 3d^{7}(2F)4p^{1}D + 5 \ 3d^{7}(2F)4p^{3}D$
244417.1	244379	38	3	$46 \ 3d^{7}(2F)4p^{3}F + 38 \ 3d^{7}(2F)4p^{3}D + 8 \ 3d^{7}(2F)4p^{3}G$
244671.4	244680	-9	5	93 $3d^{7}(2F)4p^{3}G + 6 3d^{7}(2H)4p^{3}G$
244753.1	244733	20	4	$40 \ 3d^{7}(2F)4p^{3}F + 31 \ 3d^{7}(2F)4p^{3}G + 24 \ 3d^{7}(2F)4p^{1}G$
244812.8	244714	99	2	$80 \ 3d^7(2F)4p \ 3D + 10 \ 3d^7(2F)4p^{-1}D$
244943	244768	175	1	$90 \ 3d^7(2F)4p \ 3D + 5 \ 3d^7(2D)4p \ ^3D$
245204.3	245250	-46	4	$63 \ 3d^7(2F)4p^{-1}G + 33 \ 3d^7(2F)4p^{-3}F$
250622.8	250488	135	3	$95 \ 3d^7(2F)4p^{-1}F$
266196.5	266194	3	2	$77 \ 3d^7(2D)4p^{-3}P + 20 \ 3d^7(2D)4p^{-3}P$
266460.9	266482	-21	1	$78 \ 3d^7(2D)4p^{-3}P + 18 \ 3d^7(2D)4p^{-3}P$
266775	266786	-11	0	$81 \ 3d^7(2D)4p \ ^3P + 17 \ 3d^7(2D)4p \ ^3P$
268006	268109	-103	2	$76 \ 3d^7(2D)4p \ {}^3F + 18 \ 3d^7(2D)4p \ {}^3F$
268956.3	269006	-50	3	$74 \ 3d^7(2D)4p \ {}^3F + 19 \ 3d^7(2D)4p \ {}^3F$
270239.5	270255	-16	4	$75 \ 3d^7(2D)4p \ {}^3F + 21 \ 3d^7(2D)4p \ {}^3F$
272352.4	272380	-28	1	$79 \ 3d^7(2D)4p^{-1}P + 12 \ 3d^7(2D)4p^{-1}P$
272943.7	272785	159	3	$74 \ 3d^{7}(2D)4p^{-1}F + 20 \ 3d^{7}(2D)4p^{-1}F$
275672.9	275697	-24	1	$71 \ 3d^7(2D)4p \ 3D + 21 \ 3d^7(2D)4p \ ^3D$
275970.3	276048	-78	2	$61 \ 3d^{7}(2D)4p \ 3D + 18 \ 3d^{7}(2D)4p \ ^{3}D + 13 \ 3d^{7}(2D)4p \ ^{1}D$
276545.9	276677	-131	2	$58 \ 3d^7(2D)4p \ ^1D + 20 \ 3d^7(2D)4p \ ^1D + 12 \ 3d^7(2D)4p \ ^3D$
277108.7	277111	$^{-2}$	3	$70 \ 3d^7(2D)4p \ 3D + 24 \ 3d^7(2D)4p \ ^3D$
			a: Fi	com the NIST compilation [28]
				b. This work

a: From the NIST compilation [28]
b: This work
c: Only the components ≥ to 5% are given

Transitions

abic 110.	Company	ca oboinat	01 001	ung ung un	a ura	1101010	II probac	1110105	
	Wavelength	Lower Level	J_{low}	Upper Level	J_{up}	log gf	gA	CF	1
	405.68	19697	2	266197	2	-0.62	9.65E + 09	-0.573	1
	406.339	20097	1	266197	2	-0.92	4.92E + 09	0.698	1
	406.453	26913	4	272944	3	-0.23	2.39E + 10	-0.63	1
	443 249	16248	2	241855	2	-0.87	$4.59E \pm 0.9$	0.371	1
	442 692	0	-	211000	-	0.86	4.64E+00	0.515	
	443.082	10607	4	220307	4	-0.80	4.04E+09	0.515	1
	444.213	19097	4	244813	2	-0.85	5.05E+09	-0.03	
	444.748	20097	1	244943	1	-0.9	4.29E + 09	-0.707	
	444.997	19697	2	244417	3	-0.57	9.01E + 09	-0.696	
	445.006	20097	1	244813	2	-0.49	1.09E + 10	-0.688	1
	445.394	20423	0	244943	1	-0.8	5.27E + 09	-0.654	1
	446.371	19697	2	243725	3	-0.49	1.08E + 10	-0.61	1
	447 008	26913	4	250623	3	-0.03	$3.09E \pm 10$	0.849	
	448.43	20010	-1	223000	3	0.87	$4.48E \pm 00$	0.174	
	450.006	1961		223000	3	-0.31	$4.40D \pm 0.00$	0.174	1
	450.020	1801	3	224071	2	-0.48	1.09E+10	0.599	
	451.162	0	4	221650	3	-0.16	2.26E + 10	0.793	1
	452.503	3078	2	224071	2	-0.87	4.43E + 09	-0.738	
	452.659	0	4	220917	5	0.07	3.84E + 10	0.846	1
	453.131	3078	2	223764	1	-0.4	1.28E + 10	0.782	1
	453.421	3078	2	223623	3	-0.14	2.38E + 10	0.77	1
	453 44	1861	3	222398	Ă	0.01	$3.28E \pm 10$	0.839	1
	454.8	1861	3	222030	-1	0.52	0.20E + 10 0.70E ± 0.0	0.863	
	459.102	26012	3	245204	4	-0.52	3.13 ± 0.00	-0.805	
	458.103	26913	4	245204	4	-0.88	4.17E+09	0.21	
	458.426	0	4	218138	3	-1	$3.16E \pm 09$	-0.116	1
	458.717	0	4	218000	5	-0.65	7.09E + 09	0.551	1
	459.514	0	4	217621	3	-0.9	3.94E + 09	0.237	1
	459.887	0	4	217445	4	-0.59	8.08E + 09	0.724	1
	461.326	1861	3	218628	3	-0.73	5.87E + 09	0.767	1
	462.548	16248	2	232442	ĩ	-0.45	1.11E + 10	0.553	1
	462 524	10240	4	202442	4	0.07	2 22 1 00	0.000	1
	403.334	2079	4	210704	4	-0.97	3.33E+09	-0.708	
	463.717	3078	2	218726	2	-0.27	1.65E + 10	0.751	
	463.929	3078	2	218628	3	-0.92	3.71E + 09	0.325	
	464.646	1861	3	217079	3	-0.25	1.75E + 10	0.601	
	464.829	0	4	215133	4	-0.19	2.00E + 10	0.652	1
	467.108	16248	2	230331	3	-0.44	1.10E + 10	0.693	1
	468 502	16248	2	229694	2	-0.96	3 35E±09	0.158	1
	400.002	10240	2	223034	1	-0.30	2.33 ± 0.00	0.100	
	470.040	19097	2	232442	1	-0.97	3.21E+09	-0.330	
	472.341	16248	2	227960	2	-0.22	1.80E + 10	0.731	
	472.769	19697	2	231216	1	-0.89	$3.88E \pm 09$	-0.334	1
	474.167	61456	0	272352	1	-0.28	1.57E + 10	0.786	1
	475.489	16248	2	226558	1	-0.55	8.28E + 09	-0.506	1
	476.196	19697	2	229694	2	-0.39	1.19E + 10	-0.53	1
	482.014	10607	2	227160	1	0.64	$6.58E \pm 0.0$	0.413	
	402.014	13037	2	227100	1	-0.04	0.000-00	-0.415	
	482.945	20097	1	227160	1	-1	2.84E+09	0.406	1
	484.53	26913	4	233299	5	-0.01	2.81E + 10	-0.734	
	491.598	26913	4	230331	3	-0.58	7.27E + 09	-0.279	1
	491.829	26913	4	230236	4	0.4	6.98E + 10	-0.817	1
	492.236	16248	2	219403	3	-0.57	7.42E + 09	-0.431	1
	494.12	16248	2	218628	3	-0.67	$5.89E \pm 0.09$	-0.406	1
	496 991	0	4	201211	3	-0.13	$1.99E \pm 10$	0.552	1
	408 755	1861	3	201211	2	0.31	1.30E + 10	0.500	1
	400.945	2079	3	202301	1	-0.51	7.71E + 00	0.303	
	499.845	3078	4	203140	1	-0.54	7.71E+09	0.481	
	504.594	0	4	198179	4	-0.05	2.32E + 10	0.466	
	504.862	20097	1	218171	1	-1	2.58E + 09	-0.517	1
	505.721	1861	3	199599	3	-0.2	1.66E + 10	0.426	1
	505.964	3078	2	200720	2	-0.3	1.30E + 10	0.442	1
	506.778	0	4	197325	5	-0.92	3.14E + 09	0.434	1
	513.566	19697	2	214413	1	-0.96	$2.76E \pm 0.09$	-0.225	1
	521 101	26013	4	218815	5	0.94	$2.70E \pm 0.0$	0.762	
	547 205	20310	Ū.	203140	1	0.04	2.75 ± 100 2.34 ± 100	0.102	
	547.295	20423	1	203140	1	-0.98	2.34E+09	-0.44	
	548.655	20097	1	202361	2	-0.64	5.04E+09	-0.443	
	550.921	19697	2	201211	3	-0.48	7.29E+09	-0.429	1
	774.129	198179	4	327357	4	-0.92	1.33E+09	-0.129	1
	837.661	203869	2	323249	1	-1	9.43E + 08	-0.324	1
	841.324	190554	4	309414	5	-0.74	1.72E + 09	-0.261	1
	842.182	203869	2	322608	2	-0.61	$2.33E \pm 0.09$	0.487	1
	844.101	203869	2	322338	3	-0.36	$4.05E \pm 0.09$	-0.547	1
	844 154	220917	5	339379	6	-0.49	$3.03E \pm 0.09$	0.232	1
	849.411	101762	3	300400	4	0.01	$1.15E \pm 0.00$	0.28	1
	952 924	217445	4	224565	5	-0.31	$2.15E \pm 0.0$	0.200	
	053.024	217440	4	334303	3	-0.03	2.15E+09	-0.399	1
	854.607	230236	4	347249	4	-0.25	5.17E + 09	0.472	
	856.622	192753	4	309490	4	-0.98	$9.49E \pm 08$	-0.27	1
	857.184	192753	4	309414	5	-0.82	1.39E + 09	0.16	1
	857.801	222398	4	338975	5	-0.53	2.67E + 09	0.247	1
	865.646	194132	3	309653	3	-0.92	1.08E + 09	-0.251	1
	866.867	194132	3	309490	4	-0.77	$1.50E \pm 0.09$	0.172	1
	871 241	195086	2	309865	2	-0.93	$1.03E \pm 0.09$	-0.27	1
	071.241 070.0F	105000	2	200652	2	0.92	1.0000 000	0.199	1
	012.00	195080	4	309033	3	-0.85	1.28E+09	0.188	
	875.807	195684	1	309865	2	-0.94	1.00E + 09	0.208	
	877.577	233299	5	347249	4	-0.78	1.44E + 09	0.441	
	878.913	201211	3	314988	4	-0.87	1.17E + 09	-0.44	
	880.657	202361	2	315912	3	-0.99	8.75E + 08	-0.381	
	883.225	218815	5	332036	4	-0.79	$1.39E \pm 0.9$	0.491	
	883 369	216420	õ	320633	1	-0.00	$8.76E \pm 0.08$	0.522	
	000.002	210429	0	049000 200241	1	-0.99	0.47E + 00	0.044	
	001.191	210/03	4	329341	4	-0.95	9.475+08	0.219	
	887.934	198179	4	310800	3	-0.82	1.27E + 09	0.495	
	889.022	191762	3	304245	4	-0.94	9.75E + 08	-0.507	
	891.012	217109	1	329341	2	-0.69	1.70E + 09	0.528	
	891.076	215133	4	327357	4	-0.45	3.00E + 09	-0.391	1
	891.527	222398	4	334565	5	-0.54	$2.44E \pm 0.9$	0.638	1
	801 820	100554	1	302682	1	_0.40	2 73E 00	0.246	
	001.002	101700	4	302082	4	-0.49	2.1315+09	0.240	
	892.565	191762	3	303798	3	-0.57	2.26E+09	0.235	
	893.985	192741	2	304600	2	-0.68	1.77E + 09	0.275	
	894.335	224071	2	335886	2	-0.68	1.75E + 09	-0.502	
	895.403	193434	1	305116	1	-0.72	1.57E + 09	0.401	1
	895.73	217079	3	328720	3	-0.57	2.23E + 09	-0.29	1
	896.705	220917	5	332436	6	0.17	1.23E + 10	-0.698	1
	896.925	192753	4	304245	4	-0.76	1.44E + 09	-0.557	1
				-			1.2.2		1

Table A3: Computed oscillator strengths and transition probabilities in Cu IV.

Table A3: Continued

BBS 222600 9 333000 1 -0.88 108E-108 0.03E SBS.130 221672 6 333600 4 0.043 3138+00 0.0752 SBS.811 216028 2 322541 3 0.043 3138+00 0.0753 SBS.811 222603 2 333777 2 0.771 1.46E+100 0.643 S99.913 190434 4 313820 0.181 1.325+10 0.769 S99.143 190741 4 313273 3 0.181 1.325+10 0.663 S90.145 190741 4 332682 4 0.028 1.38E+00 0.633 S90.244 221602 6 332485 4 0.038 8.44E+40 0.433 S90.542 21733 4 322682 4 0.028 8.44E+40 0.434 S90.542 21733 4 322680 4 0.048 8.44E+40 0.434 S90.542 22	Wavelength	Lower Level	JLow	Upper level	JUP	log gf	gA	CF 0.271
898.369 222327 5 333860 4 0.09 1.27E-10 0.752 898.362 214734 6 320895 1 0.757 1.48E-100 0.634 899.561 139334 1 320895 0 0.77 1.48E-100 0.649 899.561 103734 2 333777 2 0.76 1.48E-100 0.649 900.553 192741 2 333787 2 0.76 1.40E+00 0.639 901.447 191762 3 332492 4 0.42 3.418E+00 0.639 902.448 221694 6 3318470 0.665 1.18E+00 0.643 905.33 222490 5 332526 4 0.066 7.04E+00 0.645 907.65 224935 5 332526 4 0.067 7.64E+00 0.645 909.044 22483 3 333860 4 0.067 0.64E+08 0.672 905.63 2	897.782 898.023	227993 221650	6 3	339379 333006	ь З	-0.94 -0.88	$9.60E \pm 08$ $1.08E \pm 09$	-0.371 0.325
sss.pl:1 2182412 2 2182415 2 41324 1 3124415 2 41324 4132	898.139	222527	5	333869	4	0.19	1.27E + 10	-0.752
888.01 21734 4 322080 4 -0.70 1.468-00 0.049 889.61 19343 1 30400 2 -0.75 1.468-00 0.049 889.61 19343 2 33377 2 -0.75 1.468-00 0.648 900.455 191762 3 332332 -0.638 1077 1.068-00 0.638 901.447 191762 3 332342 -0.638 1.187+09 0.0439 901.447 21754 4 322428 2 -0.07 7.068-0 0.071 905.33 22348 5 333807 5 -0.06 6.351-00 -0.619 905.43 224523 5 332526 4 -0.62 1.228+00 -0.619 907.66 224523 3 335864 -0.071 1.448+00 -0.62 909.74 21413 3 324260 -0.71 1.448+00 -0.619 909.74 214141 3 <td< td=""><td>898.362 898.851</td><td>218028 221602</td><td>2</td><td>329341 332855</td><td>2 5</td><td>-0.43 0.25</td><td>3.13E+09 1 48E+10</td><td>0.524</td></td<>	898.362 898.851	218028 221602	2	329341 332855	2 5	-0.43 0.25	3.13E+09 1 48E+10	0.524
889.611 122403 1 304000 2 -0.7 1.66E+09 0.049 900.265 10054 4 301632 5 -0.07 7.03E+09 0.635 901.357 101541 130742 330282 4 -0.28 1.36E+09 0.633 901.454 121692 332248 3 -0.03 7.04E+09 -0.701 905.015 224830 5 333255 5 -0.06 5.44E+09 -0.031 905.015 224830 5 3332562 4 -0.021 7.04E+09 -0.011 905.015 224533 3 335469 4 -0.09 5.5E+09 -0.013 905.421 224530 3 335469 4 -0.04 5.5E+09 -0.619 909.474 124535 5 324640 1 -0.428 1.22E+09 -0.68 909.474 124535 5 324469 1 -0.46 2.90E+09 -0.67 909.474	898.91	215734	4	326980	4	-0.75	1.46E + 09	0.659
900.055 100054 100054 1 2000 1 2000 1 2000 2000 2000 2000 20	899.561 800.813	193434	1	304600 333737	2	-0.7	1.66E + 09 1.40E + 09	0.649 0.185
900.285 19054 4 301632 5 -0.07 7.038+09 0.685 900.384 191742 303286 6 -0.38 1.168+09 0.734 904.588 218028 332986 6 -0.38 1.168+09 0.744 904.588 218028 332986 6 -0.38 1.168+09 0.744 904.588 218028 332986 6 -0.38 1.168+09 0.744 905.614 228480 5 3342982 2 -0.05 9.268+08 -0.193 905.614 228480 5 334292 2 -0.06 8.348+08 -0.437 905.614 218028 4 332928 4 -0.08 8.348+08 -0.437 905.614 218028 4 -0.09 8.348+08 -0.449 905.614 218028 4 -0.09 8.348+08 -0.449 905.874 214835 5 335262 4 -0.06 8.398+09 -0.619 907.665 2234323 3 33360 3 -0.02 1.048+09 -0.619 909.047 213030 3 33300 3 -0.02 1.028+09 -0.619 909.047 213030 3 33300 4 -0.02 1.028+09 -0.619 909.047 213030 3 33300 5 -0.02 1.028+09 -0.681 909.044 22300 3 33300 5 -0.02 1.028+09 -0.681 909.044 22300 3 33300 5 -0.02 1.028+09 -0.681 909.047 1.92733 4 332249 4 -0.14 5.928+09 -0.681 901.091 214835 5 33249 1 -0.03 1.028+09 -0.33 910.091 22466 7 333246 1 -0.35 1.788+0 -0.276 911.665 214155 2 351529 3 -0.05 1.028+09 -0.328 911.665 214155 2 351529 3 -0.05 1.028+09 -0.328 911.665 214155 2 351529 3 -0.05 1.028+09 -0.327 912.2481 224071 3 33737 3 -0.05 1.028+09 -0.327 912.2481 224079 6 -334665 5 -0.28 1.348+00 .2 911.865 215133 4 324269 5 -0.11 7.668+00 .2 912.2481 224079 6 334665 5 -0.28 1.548+10 -0.847 912.2481 224073 1 -0.05 1.548+00 .2 912.3481 224073 1 -0.071 8.468+00 .2 912.483 3 32757 4 -0.11 7.668+00 .227 912.3481 224809 6 334266 5 -0.28 1.548+10 -0.377 912.491 215054 1 -0.052 1.208+00 -0.377 912.492 115054 3 302160 1 -1 -7.892 1.909+0.043 913.541 21455 3 -0.3377 4 -0.41 8.208+00 -0.247 913.544 224809 1 -0.377 4 -0.52 1.208+00 -0.377 912.493 124845 3 302680 2 -0.37 3.388+09 0.576 913.544 21490 5 -33757 4 -0.41 8.408+09 -0.449 915.591 218438 3 302757 4 -0.41 8.408+09 -0.449 915.591 218438 3 302757 4 -0.41 8.408+09 -0.449 915.591 218453 3 322668 2 -0.37 3.388+09 -0.449 915.591 218454 3 322668 2 -0.37 3.388+09 -0.449 915.591 218454 3 322668 2 -0.37 3.388+09 -0.449 915.595 21464 3 32469 0 -0.44 3.388+09 -0.449 915.595 214453 3 322668 4 -0.77 3.388+09 -0.449 915.595 214453 3 322689	900.055	190528	5	301632	5	0.18	1.25E+10	0.769
900.547 101702 2 300292 3 4.028 4.468+00 0.633 904.264 211002 6 332436 6 -0.35 1.064+00 0.744 904.366 215734 326244 3 0.037 6.982+00 -0.343 905.342 218726 2 32982 2 0.04 2.04440 -0.343 905.342 218726 2 32982 2 0.04 2.04440 -0.343 905.342 218726 2 32982 4 0.08 5.9240 -0.616 907.065 223023 3 33266 4 0.08 5.5240 -0.618 909.674 214435 5 324760 5 -0.414 5.922+00 0.681 909.674 214435 5 3324760 5 -0.41 5.922+00 0.611 909.674 214457 5 3324760 5 -0.01 7.824+00 -0.721 909.674 21	900.265	190554	4	301632	5	-0.07	7.03E+09	0.685
994.538 218028 3 32948 6 .0.85 1.16E+09 0.744 994.538 218028 2 0.058 02584 8 .0.93 025848 0 .0.93 025848 0 .0.93 025848 0 .0.93 025848 0 .0.93 025848 0 .0.93 025848 0 .0.93 025848 0 .0.95 025848 0 .0.9	900.435 901.547	192741 191762	2	303798 302682	3 4	-0.41	4.36E+09	0.635 0.639
994.538 21862 3 32918 3 32918 2 - 0.06 9.269-46 - 0.133 995.533 222389 4 332255 5 - 0.06 9.269-468 - 0.343 995.533 223898 4 332255 5 - 0.06 9.392-469 - 0.513 995.542 218726 2 32918 2 - 0.06 9.392-469 - 0.513 995.542 218726 3 325226 4 - 0.06 9.392-469 - 0.513 995.542 218726 3 325226 4 - 0.075 1.442-469 - 0.373 995.542 223003 3 33586 2 - 0.75 1.442-469 - 0.373 996.542 223003 3 33586 2 - 0.75 1.442-469 - 0.373 996.542 223003 3 33586 2 - 0.75 1.442-469 - 0.373 996.947 224413 1 3324419 2 - 0.97 8.662-469 - 0.572 996.947 224413 1 3324419 2 - 0.97 8.662-469 - 0.572 996.947 224413 1 3324419 2 - 0.97 8.662-469 - 0.572 996.947 224413 1 3324419 2 - 0.97 8.662-469 - 0.572 996.947 224413 1 3324419 2 - 0.97 8.662-469 - 0.572 996.947 224413 1 3324419 - 0.04 1.5322-469 - 0.618 996.947 224451 2 - 0.512 3 32236 4 - 0.04 1 5.522-469 - 0.618 996.947 224451 2 - 0.512 3 32236 4 - 0.04 1 5.522-469 - 0.521 910.013 224766 7 332246 5 - 0.01 7.5862-40 - 0.75 9 911.86 214432 3 303778 3 - 0.23 7.782-40 - 0.521 911.86 214432 3 303778 3 - 0.23 7.782-40 - 0.521 911.86 214453 2 304660 5 - 0.01 7.862-40 - 0.521 912.261 22465 4 334466 5 - 0.01 7.862-40 - 0.521 912.361 22465 4 3342466 5 - 0.01 7.862-40 - 0.521 912.361 22465 4 3342466 5 - 0.01 7.862-40 - 0.521 913.812 216568 1 30526 3 37557 4 - 0.82 1.542-40 - 0.531 915.501 215658 3 325208 2 - 0.37 3.362+40 - 0.531 915.551 21553 3 - 322208 2 - 0.37 3.362+40 - 0.531 915.551 21553 3 - 322208 2 - 0.37 - 3322+40 - 0.542 915.551 21554 3 - 326208 2 - 0.37 - 3322+40 - 0.542 915.551 21554 3 - 326208 2 - 0.37 - 3322+40 - 0.542 915.551 21554 3 - 326208 2 - 0.37 - 3322+40 - 0.542 915.551 21554 3 - 326208 2 - 0.37 - 3322+40 - 0.542 915.551 21554 3 - 326208 2 - 0.37 - 3322+40 - 0.542 915.551 21554 3 - 326208 2 - 0.37 - 3322+40 - 0.542 915.551 21554 3 - 32628 2 - 0.37 - 3322+40 - 0.542 915.541 - 0.542 32656 - 0.07 - 1.452+40 - 0.542 922.957 3 - 0.543 32660 2 - 0.37 - 3322+40 - 0.544 924.55 22452 4 - 0.53 - 3276 - 0.53 - 3276 - 0.542 924.551 - 22453 4 - 326284 4 - 0.54 - 3282+60 - 0.542 924.551 - 22455 4 - 33526	902.244	221602	6	332436	6	-0.85	1.16E + 09	-0.744
905.318 2243480 5 3388775 5 0.096 3.0451+08 0.0435 905.342 218726 2 3329182 2 0.06 7.0451+09 0.0377 905.342 218435 3 332526 4 0.06 7.0451+09 0.0377 905.372 218435 3 332526 4 0.06 7.0451+09 0.0387 909.341 225559 3 335586 2 0.075 1.4451+09 0.0387 909.044 223000 3 333066 3 0.012 0.3251+09 0.0418 909.044 223000 3 333066 1 0.012 0.0251+09 0.0418 909.0471 2124413 1 324419 2 0.077 8.0651+09 0.0387 909.0471 2124413 1 324419 2 0.077 8.0651+09 0.0387 909.0471 212455 4 332545 1 0.044 1.5325+09 0.0418 910.013 213360 1 3323249 1 0.03 1.7525+10 0.0461 910.013 213360 1 3323249 1 0.03 1.7525+10 0.0461 910.013 213360 1 3323249 1 0.03 1.7525+10 0.0461 911.045 214135 2 33578 3 0.03 1.7525+10 0.0461 911.855 241855 2 3351520 3 -0.539 2.0755+09 0.0522 912.2431 224039 6 334466 5 0.28 1.545+10 0.0842 911.845 241855 2 3351520 3 -0.539 2.0755+09 0.0522 912.2431 224039 6 334466 5 0.28 1.545+10 0.0842 912.2432 215133 4 324767 5 -0.017 7.565+09 0.0522 912.2431 224039 6 334466 5 0.28 1.545+10 0.037 912.2431 224039 6 334466 5 0.28 1.545+10 0.037 912.2431 224039 1 332249 1 0.077 8 405+00 0.222 912.2431 224039 1 332249 1 0.078 2 0.0775+09 0.0522 912.2431 224039 1 332249 1 0.078 2 0.0775+09 0.0522 912.2431 224030 3 3315120 3 0.0718 4 0.022 1.005+00 0.227 913.455 218000 5 327375 4 0.0522 1.005+00 0.227 914.435 218000 5 327375 4 0.022 1.0457+00 0.0421 915.443 24309 1 322069 2 0.077 1.445+09 0.0743 914.435 218000 5 327375 4 0.0522 1.0078+09 0.032 915.641 1.0554 3 330460 2 0.020 2 7.5345+09 0.0434 914.555 218050 5 3 322608 2 0.039 3.335+09 0.743 916.643 213054 3 332608 2 0.039 3.335+09 0.743 916.643 135540 0.0427 5.34569 0.0452 917.644 135526 4 0.037 1.445+00 0.074 918.443 243029 4 351500 3 0.048 1.2525+09 0.0434 919.555 1190535 4 330268 4 0.02 7.5385+09 0.0434 919.555 1190535 4 330268 4 0.02 7.5385+09 0.0434 919.555 1190535 4 330268 4 0.02 7.5385+09 0.0434 920.665 214403 3 326268 4 0.03 7.3455+09 0.0434 920.6	904.538 904.866	218628 215734	3 4	329182 326248	2	-0.95	9.25E+08 7 69E+09	-0.193 -0.701
905.33 222398 4 332255 5 -0.06 7.048+09 -0.013 905.342 218726 2 3208 4 -0.09 5.55±+09 -0.13 909.542 216133 4 322264 4 -0.29 5.55±+09 -0.13 909.542 216133 4 325264 4 -0.28 1.228±+09 -0.18 909.542 216133 4 325264 4 -0.28 1.248±+09 -0.23 909.044 224000 3 333066 3 -0.21 6.228±+09 -0.18 909.044 214433 1 324419 2 -0.97 8.665±40 -0.273 909.044 214433 1 324419 2 -0.97 8.665±40 -0.273 909.744 214433 1 324419 2 -0.97 8.665±40 -0.273 909.74 214433 1 324419 2 -0.97 8.665±40 -0.273 909.74 214433 2 3320850 4 -0.64 2.85±+09 -0.84 910.013 21360 1 332349 1 -0.91 0.25±+09 -0.38 910.091 222666 7 332246 1 -0.91 0.25±+09 -0.38 910.91 222666 7 332246 1 -0.91 0.25±+09 -0.38 911.85 24453 2 352524 3 -0.23 4.74±+09 -0.42 911.85 24453 2 353578 2 -0.23 4.74±+09 -0.42 911.85 24453 2 353578 2 -0.23 4.74±+09 -0.42 911.85 24459 6 334565 5 -0.01 7.86±+09 -0.32 912.361 224459 6 334565 5 -0.01 7.86±+09 -0.32 912.361 224459 6 334565 5 -0.01 7.86±+09 -0.32 912.341 224459 1 -0.58 2.06±+69 -0.37 912.441 224459 1 -0.58 2.06±+69 -0.37 912.441 224459 1 -0.58 2.06±+69 -0.37 915.551 213564 3 30575 4 -0.75 1.45±+0 -0.81 913.852 214500 5 327557 4 -0.75 1.45±+0 -0.81 913.852 214500 5 327557 4 -0.75 1.45±+0 -0.81 915.551 195684 3 30560 2 -0.02 7.53±+09 -0.54 915.551 195684 3 30560 2 -0.02 7.53±+09 -0.74 915.651 195684 3 32668 2 -0.37 3.38±+69 -0.41 915.551 195654 3 32668 2 -0.37 3.38±+69 -0.54 915.551 213566 3 322568 2 -0.37 3.38±+69 -0.54 915.551 213566 3 322568 2 -0.37 3.38±+69 -0.54 915.551 213566 3 322668 2 -0.37 3.38±+69 -0.52 915.551 213566 3 322668 2 -0.37 3.38±+69 -0.52 915.551 213566 3 322668 2 -0.37 3.38±+69 -0.52 915.551 924533 4 30562 4 -0.37 3.38±+69 -0.52 915.551 924533 4 30562 4 -0.37 3.38±+69 -0.54 936.541 92575 4 332668 2 -0.52 1.44±+10 -0.54 936.541 92575 4 332668 2 -0.75 1.45±+09 -0.54 936.541 92575 4 332668 4 -0.52 1.44±+69 -0.64 936.541 92575 4 332668 4 -0.52 1.44±+69 -0.64 936.541 92575 4 332668 4 -0.52 1.44±+69 -0.54 936.641 92575 3 331042 4 -0.75 1.45±+09 -0.54 936.641 925769 2 332444 3 3.25256 4 -0.78 3.38±+09 -0.56 937.644 926763 2	905.018	228480	5	338975	5	-0.96	8.94E + 08	-0.345
905 S74 214835 5 325226 4 0.06 9.30E+09 -0.619 907.055 228623 3 333869 4 -0.82 1.22E+09 -0.818 908.871 228829 3 335869 4 -0.82 1.22E+09 0.63 909.674 228030 3 333009 3 -0.175 1.44E+09 0.203 909.674 1292733 4 302682 4 -0.44 2.80E+09 -0.618 909.913 217079 3 3232460 5 -0.44 2.80E+09 -0.23 911.1857 221523 3 -0.57 1.47E+09 -0.23 911.1859 224071 2 333737 2 -0.57 8.83E+08 0.64 911.865 241855 2 331520 3 -0.57 1.43E+09 0.621 913.127 191327 2337476 5 -0.017 8.40E+09 0.627 913.127 1915361	905.33	222398 218726	4	332855	5	-0.06	7.04E+09 2.04E+09	-0.613 0.377
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	911.865	241855	2	351520	3	-0.59	2.07E+09	0.822
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	912.183 912.361	215133 224959	4 6	324760 334565	5 5	-0.01 0.28	7.86E+09 1.54E+10	-0.821 -0.837
913.812 195086 2 304060 2 -0.4 $3.20E+09$ 0.676 914.435 218000 5 337357 4 -0.82 1.20E+09 0.576 914.72 213322 0 337347 4 -0.82 1.20E+09 0.576 915.051 10532 2 305116 1 -0.13 5.22E+00 -0.814 915.501 218138 3 327357 4 -0.18 $\times 00E+08$ -0.574 916.812 213535 2 3327357 4 -0.1 $\times 00E+08$ -0.574 916.812 213535 2 322608 2 -0.39 $\times 3.28E+09$ -0.743 916.812 213535 2 322608 2 -0.39 $\times 3.28E+09$ -0.743 916.963 195544 3 304600 2 -0.02 $7.58E+09$ -0.743 917.512 242530 3 351520 3 -0.437 $\times 3.29E+09$ -0.759 917.512 242530 3 3351520 3 -0.437 $\times 3.39E+09$ -0.749 917.512 242530 4 331099 4 -0.26 $\times 4.38E+09$ -0.749 918.443 243029 4 331099 4 -0.26 $\times 4.38E+09$ -0.848 918.449 192753 4 301632 5 -0.66 $\times 1.68E+09$ -0.818 918.449 192753 4 301632 5 -0.66 $\times 1.68E+09$ -0.819 919.8571 195085 4 303798 3 -0.11 9.96E+09 -0.818 919.8571 195085 4 303798 3 -0.13 $\times 3.34E+00$ -0.682 9920.189 213665 3 322508 4 -0.37 $\times 3.34E+00$ -0.682 9921.733 243029 4 $\times 351520$ 4 -0.441 $2.82E+00$ -0.275 912.174 222603 2 331042 1 -0.68 $\times 1.68E+09$ -0.813 9921.735 243029 4 $\times 351520$ 4 -0.441 $2.82E+00$ -0.275 922.92 218628 3 326980 4 -0.58 2.04E+09 -0.28 922.93 194339 5 302682 4 -0.16 $\times 3.4760$ 0 -0.169 922.173 243029 4 $\times 351260$ 4 -0.58 2.04E+09 -0.275 922.174 222603 2 331042 1 -0.68 $\times 1.04E+09$ -0.276 922.173 243029 4 $\times 352526$ 4 -0.16 $\times 3.48E+09$ -0.666 922.92 218628 3 326980 4 -0.27 4.15E+09 -0.752 924.511 218815 5 3333737 2 0.25 4 $\times 4E+09$ -0.654 924.511 218815 5 33326480 4 -0.378 $\times 2.04E+09$ -0.28 924.511 218815 5 3326980 4 -0.378 $\times 2.124E+10$ -0.845 924.67 217079 3 325226 4 -0.16 $5.43E+09$ -0.666 925.626 218945 3 326248 3 -0.41 $1.38E+09$ -0.666 925.626 218945 3 326248 3 -0.41 $1.58E+09$ -0.646 925.666 218000 5 324760 5 -0.77 $4.15E+09$ -0.771 935.51 24745 4 3262806 4 -0.37 $4.38E+09$ -0.666 933.2217445 4 326980 4 -0.37 $4.38E+09$ -0.666 933.2217445 4 3326980 4 -0.37 $4.38E+09$ -0.666 933.221745 2 333642 2 -0.37 $4.38E+09$ -0.666 933.22467 2 29403 3 326248 3 -0.41 $3.38E+09$ -0.672 935	912.949	217445	4	326980	4	-0.58	2.09E + 09	0.229
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	913.127 913.812	195086 195684	2	304600 305116	2	-0.4 -0.75	3.20E+09 1.43E+09	0.621 0.576
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	914.435	218000	5	327357	4	-0.82	1.20E+09	-0.34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	914.772	213932	0	323249	1	-0.97	8.46E+08	-0.527
915.591 218138 3 327357 4 -1 8.00E+08 0.105 915.885 195592 0 305116 1 -1 7.59E+08 0.523 916.963 195544 3 304600 2 -0.02 7.53E+09 0.822 917.512 242530 3 351520 3 -0.43 2.92E+09 0.796 917.91 213665 3 322608 2 -0.37 3.39E+09 0.459 918.443 243029 4 351909 4 -0.26 4.35E+09 0.845 918.443 243029 4 351909 4 -0.26 4.35E+09 0.845 918.543 243029 4 301632 5 -0.68 1.65E+09 0.845 919.555 195055 4 303798 3 0.1 9.95E+09 0.845 919.557 195086 2 303798 3 -0.88 1.04E+09 0.833 919.557 195086 2 303798 3 -0.88 1.04E+09 0.845 920.06 216071 6 324760 5 0.27 1.45E+10 0.828 921.235 194132 3 302682 4 -0.81 1.22E+09 -0.169 921.733 243029 4 351520 3 -0.481 1.22E+09 -0.169 922.174 222603 2 331042 1 -0.62 1.91E+09 -0.503 922.92 9 194339 5 302682 4 -0.81 1.22E+09 -0.275 924.51 218615 5 326280 4 -0.16 2.37E+09 -0.28 924.93 194339 5 302682 4 -0.16 2.37E+09 -0.28 924.93 194339 5 302682 4 -0.16 2.37E+09 -0.792 924.51 218815 5 326980 4 -0.12 1.03E+10 -0.782 924.67 217079 3 325266 4 -0.16 5.43E+09 -0.662 924.67 217079 3 3252266 4 -0.16 5.43E+09 -0.666 925.626 218945 4 326980 4 -0.12 1.03E+10 -0.762 924.67 221709 2 335866 2 -0.38 3.21E+09 -0.664 925.759 21739 2 329633 1 -0.31 3.30E+09 -0.621 924.67 221709 2 335826 2 -0.18 4.92E+09 -0.648 924.67 221709 2 335826 4 -0.16 5.43E+09 -0.661 925.626 218945 4 326980 4 -0.12 1.03E+00 -0.722 926.561 227060 2 335826 2 -0.13 8.30E+09 .0.525 926.833 221739 2 329633 1 -0.31 3.80E+09 .0.525 926.833 221739 2 329633 1 -0.31 3.80E+09 .0.525 926.833 221739 2 329633 1 -0.38 3.21E+09 .0.525 926.833 221749 4 325266 4 -0.19 4.97E+09 .0.727 925.51 221760 3 33377 2 -0.20 4.38E+09 .0.583 939.266 221943 4 326986 4 -0.19 4.97E+09 .0.721 928.581 221650 3 329431 2 -0.16 1.0E+09 .0.721 928.581 221650 3 329431 2 -0.16 1.0E+09 .0.513 929.251 244671 5 351009 4 -0.53 2.32E+09 .0.543 939.266 219403 3 326248 3 -0.18 4.97E+09 .0.543 939.3661 217765 2 325426 4 -0.19 4.97E+09 .0.53 936.618 244753 4 35109 4 -0.53 2.23E+09 .0.543 937.614 193042 3 360424 5 -0.03 3.06E+09 .0.543 933.661 217603 2 325426	915.351	213360	1	322608	2	-0.18	1.44E+09	-0.614
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	915.591	218138	3	327357	4	-1	8.00E+08	0.105
916.963 195544 3 304600 2 -0.02 7.33E+09 -0.822 917.512 242530 3 315120 3 -0.43 2.92E+09 -0.796 918.144 195656 3 322608 2 -0.37 3.39E+09 -0.459 918.144 195656 4 1 304600 2 -0.9 9.90E+08 -0.267 918.143 243029 4 351909 4 -0.26 4.35E+09 -0.151 918.449 192753 4 301632 5 -0.68 1.65E+09 -0.151 919.857 195056 2 303798 3 -0.88 10.4 -9.582 99.0.833 919.857 195056 2 303798 3 -0.88 10.4 -9.95 -0.832 920.169 213665 3 322338 3 -0.37 3.34E+09 -0.682 921.73 243029 4 351520 3 -0.44 2.82E+09 -0.759 922.174 222603 2 331042 1 -0.62 1.91E+09 -0.682 922.173 243029 4 351520 3 -0.44 2.82E+09 -0.753 922.174 222603 2 331042 1 -0.65 2.04E+09 -0.285 922.993 194339 5 302682 4 -0.81 1.22E+09 -0.784 924.55 243725 3 35109 4 -0.16 5.37E+09 -0.784 924.55 243725 3 35109 4 -0.16 5.37E+09 -0.784 924.67 217079 3 325226 4 -0.16 1.31E+09 -0.644 925.759 21.411 218815 5 336080 4 -0.27 4.15E+09 -0.644 925.626 218945 4 326080 4 -0.27 4.15E+09 -0.644 925.675 2143419 4 322333 1 -0.31 3.80E+09 -0.644 925.675 2143445 4 325262 4 -0.38 3.21E+09 -0.784 926.661 227660 2 335886 2 -0.38 3.21E+09 -0.664 925.661 227600 2 335886 2 -0.38 3.21E+09 -0.784 926.675 217445 4 325226 4 -0.19 4.37E+09 -0.752 926.631 227960 2 332682 4 -0.27 4.15E+09 -0.752 926.631 221650 3 329341 2 -0.16 6.10E+09 -0.752 926.632 218945 4 325264 4 -0.19 4.37E+09 -0.754 926.831 221650 3 329341 2 -0.16 6.10E+09 -0.754 926.641 193948 6 301632 5 -0.77 4.13E+10 -0.843 929.2 218628 3 326248 3 -0.77 4.13E+00 -0.843 939.044 218726 2 326248 3 -0.77 4.13E+00 -0.845 930.044 218726 2 326248 3 -0.78 4.28E+09 -0.255 931.943 217621 3 32409 4 -0.53 2.36E+09 -0.561 931.934 218945 4 326705 5 -0.49 -0.781 -0.845 933.661 214000 5 32526 4 -0.33 -0.68 -0.9849 93.501 -0.6845 933.661 2147650 2 332419 2 -0.39 -0.685 933.528 197325 5 304648 3 -0.77 $-1.3EE+09$ -0.528 933.612 21671 3 332419 2 -0.39 -0.6849 -0.528 933.612 216721 3 332419 2 -0.39 -0.6845 933.	915.885 916.812	213535	2	305116 322608	2	-1	7.89E+08 3.23E+09	-0.523 -0.743
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	916.963	195544	3	304600	2	-0.02	7.53E + 09	-0.822
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	917.512 917 91	242530 213665	3	351520 322608	3	-0.43 -0.37	2.92E+09 3.39E+09	-0.796 -0.459
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	918.144	195684	1	304600	2	-0.9	9.90E + 08	-0.267
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	918.443	243029 192753	4	351909 301632	4	-0.26	4.35E+09 1.65E+09	-0.848
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	919.595	195055	4	303798	3	0.1	9.95E+09	-0.833
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	919.857	195086	2	303798	3	-0.88	1.04E + 09	-0.169
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	920.08	213665	3	322338	3	-0.37	3.34E+09	-0.682
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	921.235	194132	3	302682	4	-0.81	1.22E+09	-0.149
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	921.733 922.174	243029 222603	4 2	351520 331042	3	-0.44 -0.62	2.82E+09 1.91E+09	-0.275 -0.503
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	922.92	218628	3	326980	4	-0.58	2.04E + 09	-0.28
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	922.993 924 355	194339 243725	5	302682 351909	4	0.2	1.24E+10 5 37E+09	-0.845 -0.792
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	924.511	218815	5	326980	4	0.12	1.03E+10	-0.784
$\begin{array}{c} 325.759 & 214319 & 4 & 322338 & 3 & 0.05 & 8.66E+09 & -0.762 \\ 926.561 & 227960 & 2 & 335886 & 2 & -0.38 & 3.21E+09 & 0.525 \\ 926.833 & 221739 & 2 & 329633 & 1 & -0.31 & 3.80E+09 & 0.511 \\ 926.975 & 225859 & 3 & 333737 & 2 & -0.25 & 4.38E+09 & -0.759 \\ 927.805 & 217445 & 4 & 325226 & 4 & -0.19 & 4.97E+09 & 0.72 \\ 928.581 & 221650 & 3 & 22941 & 2 & -0.1 & 6.10E+09 & -0.751 \\ 928.641 & 193948 & 6 & 301632 & 5 & 0.27 & 4.11E+09 & 0.809 \\ 929.2 & 218628 & 3 & 326248 & 3 & -0.27 & 4.11E+09 & 0.809 \\ 929.206 & 225387 & 4 & 333006 & 3 & 0.08 & 9.37E+09 & -0.482 \\ 930.048 & 218726 & 2 & 326248 & 3 & -0.16 & 5.30E+09 & -0.482 \\ 930.048 & 218726 & 2 & 326248 & 3 & -0.16 & 5.30E+09 & -0.487 \\ 930.304 & 244417 & 3 & 351909 & 4 & -0.78 & 1.28E+09 & -0.256 \\ 931.943 & 217445 & 4 & 326248 & 3 & -0.56 & 2.00E+09 & -0.751 \\ 932.159 & 223764 & 1 & 331042 & 1 & -0.73 & 1.45E+09 & -0.591 \\ 932.51 & 244671 & 5 & 351909 & 4 & 0.16 & 1.11E+10 & -0.848 \\ 932.606 & 218000 & 5 & 325226 & 4 & -0.52 & 2.30E+09 & -0.666 \\ 933.221 & 244753 & 4 & 351520 & 3 & -0.28 & 3.98E+09 & 0.561 \\ 934.83 & 224071 & 2 & 331042 & 1 & -0.6 & 1.95E+09 & 0.561 \\ 934.83 & 224071 & 2 & 331042 & 1 & -0.6 & 1.95E+09 & 0.449 \\ 935.28 & 197325 & 5 & 304245 & 4 & 0.19 & 1.18E+10 & -0.848 \\ 935.937 & 219403 & 3 & 326248 & 3 & -0.4 & 3.02E+09 & 0.345 \\ 936.613 & 247753 & 4 & 351520 & 3 & -0.28 & 3.98E+09 & 0.664 \\ 336.613 & 24765 & 2 & 324419 & 2 & -0.52 & 2.30E+09 & 0.645 \\ 936.613 & 217650 & 2 & 324419 & 2 & -0.52 & 2.31E+09 & 0.528 \\ 936.618 & 244753 & 4 & 351520 & 3 & -0.48 & 302E+09 & -0.764 \\ 936.601 & 217650 & 2 & 324419 & 2 & -0.39 & 3.02E+09 & -0.764 \\ 936.613 & 244753 & 4 & 351520 & 3 & -0.42 & 2.91E+09 & -0.528 \\ 937.164 & 199202 & 4 & 305856 & 3 & 0.1 & 9.56E+09 & 0.845 \\ 938.8105 & 218628 & 3 & 325226 & 4 & -0.73 & 1.41E+09 & -0.236 \\ 938.8105 & 218628 & 3 & 325526 & 4 & -0.73 & 1.41E+09 & -0.236 \\ 938.939.37 & 200483 & 3 & 306942 & 2 & -0.3 & 3.06E+09 & -0.435 \\ 9393.499 & 20017 & 5 & 327357 & 4 & 0.34 & 1.06E+109 & -0.435 \\ 9393.499 & 20017 & 5 $	924.67 925.626	217079 218945	3	325226	4	-0.16	5.43E+09 4.15E+09	-0.666
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	925.759	214319	4	322338	3	0.05	8.69E+09	-0.762
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	926.561	227960	2	335886	2	-0.38	3.21E+09	0.525
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	926.975	225859	3	333737	2	-0.25	4.38E+09	-0.599
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	927.805	217445	4	325226	4	-0.19	4.97E+09	0.72
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	928.581 928.641	221650 193948	3 6	329341 301632	25	-0.1 0.27	6.10E + 09 1.43E + 10	-0.751
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	929.2	218628	3	326248	3	-0.27	4.11E + 09	0.809
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	929.206 929.566	225387 219403	4	$333006 \\ 326980$	3 4	$0.08 \\ -0.32$	9.37E+09 3.67E+09	-0.808 -0.452
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	930.048	218726	2	326248	3	-0.16	5.30E + 09	-0.847
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	930.304 931.834	244417 217445	3	351909 324760	4	-0.79 -0.78	1.26E+09 1.28E+09	-0.215 -0.256
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	931.943	218945	4	326248	3	-0.56	2.09E+09	-0.771
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	932.159	223764	1	331042	1	-0.73	1.45E+09	0.591
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	932.606	218000	5	325226	4	-0.53	2.26E+09	-0.666
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	933.221	244753	4	351909	4	-0.52	2.30E+09	0.345
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	933.68 934.741	244417 221739	3 2	351520 328720	3	-0.28 -0.49	3.98E+09 2.45E+09	$0.561 \\ 0.498$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	934.83	224071	2	331042	1	-0.6	1.95E + 09	0.449
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	935.28 935 937	197325 219403	5	304245 326248	4	0.19	1.18E+10 3.02E+09	-0.868 -0.764
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	936.351	217621	3	324419	2	-0.52	2.31E + 09	0.694
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	936.601 936.618	217650 244753	2	324419 351520	2	-0.99	7.71E + 08 6.27E + 09	0.325 0.845
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	936.677	218000	5	324760	5	0.04	8.30E+09	0.702
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	937.142	244813	2	351520	3	-0.42	2.91E+09	-0.528
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	937.614	245204 199202	4 4	305856	4 3	-0.39	9.56E+09	-0.863
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	938.105	218628	3	325226	4	-0.73	1.41E+09	-0.236
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$938.561 \\ 939.327$	$216703 \\ 200483$	2 3	$323249 \\ 306942$	1 2	-0.71 -0.03	1.46E+09 7.06E+09	-0.493 -0.845
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	939.499	220917	5	327357	4	0.34	1.64E + 10	-0.675
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	940.536 940 901	222398 218138	4	$328720 \\ 324419$	3 2	0.21	1.21E+10 3.06E+09	-0.648
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	940.901	218945	4	325226	4	-0.5	2.38E + 09	0.224
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	941.113	199599	3	305856	3	-0.18	4.94E+09 3.81E⊥00	0.547 0.597
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	941.697	229694	2	335886	2	-0.3	1.27E+09	0.283
<u>942.012</u> 1901/9 4 004240 4 0.03 8.10E+09 0.737	942.639	228480	5	334565	5	-1	7.52E+08	-0.13
1 1/1	942.812	198179	4	<u> </u>	4	0.03	0.10E+09	0.137

Table A3: Continued

Wavelength	Lower Level	JLow	Upper level	JUP	log gf	gA	CF
945.895	223000	3	328720	3	-0.89	9.68E + 08 5.07E + 00	0.277 0.577
946.653	216703	2	322338	3	-0.99	7.53E+08	0.306
946.975	217650	2	323249	1	-0.83	1.10E + 09	-0.247
947.34	223623	3	329182	2	0	7.46E+09	-0.555
947.379	230331 223764	3	335886 329182	2	-0.31	$3.66E \pm 09$ 4 46E \pm 09	-0.424
951.149	200720	2	305856	3	-0.8	1.16E + 0.09	0.755
951.374	224071	2	329182	2	-0.82	1.12E + 09	0.356
951.661	217445	4	322524	5	-0.98	7.74E + 08	-0.12
951.962	227960	2	333006	3	-0.89	$9.45E \pm 08$ 2.85E ± 09	0.441
953.639	227993	6	332855	$\frac{2}{5}$	-0.87	9.80E + 08	-0.695
954.156	229064	4	333869	4	0.04	8.02E + 09	0.666
954.616	190554	4	295308	3	-0.91	8.98E+08	0.133
954.954	217621	3	322338	3	-0.76	1.26E + 09	0.198
955.602	199599	3	304245	4	-0.62	1.74E+09	-0.491 0.759
955.611	201211	3	305856	3	-0.66	1.61E + 09	0.63
956.195	202361	2	306942	2	-0.79	1.18E + 09	0.726
956.909	198179	4	302682	4	-0.79	1.19E + 09 1.19E + 10	0.332
957.458	227995	1	322608	2	-0.73	1.12E+10 1.35E+09	0.005 0.526
958.084	228480	5	332855	5	0.08	8.76E + 09	0.658
958.252	223000	3	327357	4	-0.46	2.53E + 09	-0.23
958.507	230236	4	334565	5	-0.09	5.84E + 09	-0.711
958.97	243029	3	296040	2	-0.88	$9.60E \pm 08$ 1.53E \pm 09	-0.525
959.687	218138	3	322338	3	-0.59	1.86E + 0.00	0.51
960.586	220316	2	324419	2	-0.3	3.64E + 09	0.558
962.628	227160	1	331042	1	-0.82	1.09E + 09	-0.47
963.37	203140	1	306942	2	-0.41	2.78E+09 1.41E+10	-0.743
965.025	190528	5	294152	4	-0.8	1.14E+09	0.226
966.227	202361	2	305856	3	-0.32	3.39E + 09	-0.584
966.709	232442	1	335886	2	-0.7	1.43E + 09	-0.304
967.066	230331	3	333737	2	-0.37	3.03E+09	-0.345
968.072	229694 203869	2	307167	2	-0.00	$1.36E \pm 09$ $1.16E \pm 10$	-0.567
968.982	220917	5	324118	6	-0.47	2.38E + 09	0.281
969.489	221272	1	324419	2	-0.95	8.04E + 08	0.327
969.804	203869	2	306983	1	0.03	7.54E+09	-0.717
970.169	226558	1	329633 304245	1	-0.79	1.15E+09 4.22E+09	0.352
970.707	221602	6	324619	5	-0.97	7.52E + 0.08	0.132
972.185	225859	3	328720	3	-0.84	1.03E + 09	-0.26
972.405	220917	5	323755	6	-0.65	1.58E + 09	-0.241
974.48	230236	4	332855	5	-0.68	1.47E+09 9.16E+08	-0.612 0.237
975.416	231216	4	333737	2	-0.54	1.99E+09	-0.503
975.652	244753	4	347249	4	-0.52	2.14E + 09	0.395
977.281	218628	3	320953	4	-0.74	1.28E + 09	-0.258
978.267	222398	4	324619	5	-0.27	3.76E + 09 1.28E + 00	0.356
978.65	222327	1	329341	2	-0.98	7.38E+08	-0.343
979.966	245204	4	347249	4	-0.04	6.31E + 09	-0.521
980.683	225387	4	327357	4	-0.59	1.78E + 09	-0.448
982.089	217445	4	319268	3	-0.84	9.96E + 08 1.24E + 10	-0.144
983.238	230230	3	332036	4	-0.33	3.24E+09	-0.400
984.737	219403	3	320953	4	-0.5	2.20E + 09	-0.352
985.499	201211	3	302682	4	-0.89	8.78E+08	-0.471
986.201	192753	4	294152	4	-0.4	2.74E+09	0.34
987.496	232442	5	334565	5	0.1	$3.29E \pm 09$ $8.66E \pm 09$	0.611
987.743	218028	$\tilde{2}$	319268	3	-0.97	7.23E + 08	-0.088
988.383	194132	3	295308	3	-0.57	1.86E + 09	0.332
989.038	223623	3 7	324731	4	-0.32	3.29E + 09	0.434
990.546	195086	2	296040	2	-0.92	$9.43E \pm 08$ $8.19E \pm 08$	-0.334 0.337
992.266	215133	4	315912	3	-0.7	1.36E + 09	0.16
995.365	215133	4	315599	4	-0.32	3.24E + 09	0.194
996.453	195684 216703	1	296040 317017	2	-0.8	1.07E+09 4.67E+09	0.458 0.342
997.786	195086	2	295308	3	-0.76	1.17E + 09	0.45
998.739	222398	4	322524	5	-1	6.75E + 08	0.581
999.804	194132	3	294152	4	-0.88	8.87E+08	0.414
1000.008	190554 222527	4 5	290553 322524	4	-0.86	9.20E + 08 1 04E + 10	0.044
1000.595	221602	6	321542	6	0.46	1.94E + 10	-0.76
1000.657	213360	1	313295	2	-0.73	1.24E + 09	-0.183
1000.824	190528	5	290445	6	-0.75	1.18E+09	0.111
1001.356	215734 215133	4	315599	4	-0.38	2.81E+09 3.32E+09	-0.504
1002.104	222527	5	322317	5	0.01	6.86E + 09	-0.507
1002.175	218028	2	317811	3	-0.55	1.86E + 09	0.175
1002.404	213535	2	313295	2	-0.92	7.92E+08	-0.185
1003.169	220917 224959	э 6	324619	ь 5	-0.93	$0.98E \pm 09$ 7.79E \pm 08	-0.288 -0.247
1003.476	222398	4	322051	3	-0.92	7.98E + 08	-0.598
1003.716	213665	3	313295	2	-0.71	1.29E + 09	0.378
1004.459	233299	5	332855	5	-0.84	9.62E+08	0.182
1005.405	213535	2	321004 312957	о З	-0.27	1.08E+09	-0.540
1006.366	217650	2	317017	3	-0.69	1.34E + 09	0.229
1007.131	213665	3	312957	3	-0.26	3.61E + 09	-0.387
1008.053	192753	4	291954	3	-0.91	8.11E+08	0.182
1008.481	∠∠4959 191762	о З	524118 290885	о З	0.25	1.10E + 10 1.49E + 00	-0.735 0.109
1008.941	190528	5	289642	4	-0.36	2.85E + 09	-0.226
1008.954	217079	3	316192	2	-0.36	2.89E + 09	0.442
1009.418	213535	2	312602	2	-0.96	7.25E + 08	-0.2
1009.64	190528 190554	э 4	289573 289573	о 5	-0.51 0.16	2.00E+09 9.52E+09	0.132 -0.386
1009.982	191762	3	290774	2	-0.17	4.44E + 09	0.309
1010.208	218028	2	317017	3	0.03	6.98E + 09	-0.461

Table A3: Continued

Wavelength 1010.213	Lower Level 192741	J_{Low}	Upper level 291730	J_{Up}	log gf -0.66	gA 1.44E+09	CF 0.179
1010.314	220917	5	319896	4	-0.55	1.83E+09	0.658
1010.343	218945	4	317811	3	-0.94	7.42E+08	-0.305
$1011.808 \\ 1011.841$	$217079 \\ 192741$	$\frac{3}{2}$	$315912 \\ 291571$	3 1	-0.09 -0.34	5.27E+09 3.01E+09	-0.315 -0.417
1012.056	192753	4	291562	5	-0.54	1.89E+09	0.232
1012.19	191762	3	290553	4	0.08	7.42E+09 7.79E+09	-0.284
1012.788 1012.832	$233299 \\ 198179$	5 4	$332036 \\ 296912$	4	$0.11 \\ -0.99$	8.36E+09 6.59E+08	-0.641 0.136
1013.517	222398	4	321064	5	-0.14	4.74E+09	-0.525
1013.807 1014.349	197325	4 5	295910	3 4	-0.89 -0.54	8.38E+08 1.86E+09	$0.344 \\ -0.445$
1014.634	192741 221602	2	291299 320142	$\frac{3}{7}$	-0.16	4.49E+09 6.77E+08	-0.244
1014.937	215734	4	314262	5	-0.72	1.25E+09	-0.262
1015.03 1015.545	$217079 \\ 222666$	$^{3}_{7}$	$315599 \\ 321135$	$\frac{4}{7}$	-0.8 0.53	1.03E+09 2.19E+10	$0.316 \\ -0.758$
1016.074	214835	5	313253	5	-0.28	3.42E+09	-0.219
1016.608	213360	1	311727	1	-0.83	9.60E + 08	-0.249
1016.852 1017.178	$221650 \\ 214319$	3 4	$319993 \\ 312630$	$\frac{3}{4}$	-0.29 -0.1	3.25E+09 5.20E+09	-0.565 -0.578
1017.215	194132	3	292440	4	-0.43	2.39E + 09 0.47E + 00	0.457
1017.852	221650	3	319896	4	-0.84	9.47E+09 9.28E+08	0.063
$1018.453 \\ 1018.64$	$214413 \\ 190528$	1 5	$312602 \\ 288698$	2 6	$0.02 \\ 0.64$	6.70E+09 2.80E+10	-0.634 -0.7
1018.808	217445	4	315599	4	-0.23	3.83E+09	-0.148
1018.91	215734	2 4	290885 313872	3 4	0.23	1.10E+10	-0.5
1018.99	193434 215133	1 4	291571 313257	1	-0.52 -0.86	1.97E+09 9.01E+08	-0.556 -0.37
1019.346	221602	6	319704	6	-0.79	1.04E+09	0.824
1020.07 1020.275	$192741 \\ 190554$	$\frac{2}{4}$	$290774 \\ 288566$	2 3	-0.21 0.32	3.95E+09 1.33E+10	$0.424 \\ 0.821$
1020.871	199599	3	297554	2	-0.9	8.13E+08	0.181
1020.901	222666	7	320601	6	-0.26	3.48E+09 3.48E+09	-0.584
$1021.61 \\ 1021.662$	$218028 \\ 191762$	2 3	$315912 \\ 289642$	3 4	-0.74 -0.22	1.15E+09 3.83E+09	-0.308 0.3
1021.819	194132	3	291997	2	-0.91	7.81E+08	-0.046
1022.191 1022.193	220917 217621	5 3	318746 315450	5 3	0.53 -0.86	2.18E+10 8.59E+08	-0.779 0.172
1022.209	195086 194132	2	292913 291954	3	-0.66	1.41E+09 1.25E+09	$0.308 \\ 0.342$
1022.551	214835	5	312630	4	-0.91	7.85E+08	0.604
1022.831 1023.215	$191762 \\ 198179$	3 4	$289530 \\ 295910$	$\frac{3}{4}$	-0.09 0.33	5.19E+09 1.35E+10	$0.402 \\ -0.512$
1023.437	199202	4	296912	3	-0.72	1.22E+09	-0.287
1023.083	216071	6	313715	6	-0.68	1.34E+09	0.183
1024.261 1024.397	$214835 \\ 221650$	5 3	$312467 \\ 319268$	4 3	-0.22 -0.75	3.83E+09 1.12E+09	-0.742 -0.338
1024.502	191762	3	289370	2	0.15	9.03E+09	0.811
1024.798	214835 224959	6	322524	5	-0.25	2.27E+09 2.27E+09	-0.535
1024.971 1025.187	218628 217445	3 4	316192 314988	2 4	-0.32 0.19	3.06E+09 9.87E+09	-0.357 -0.665
1025.244	241855	2	339393	3	0.04	6.99E+09	-0.718
1025.399	194339 215734	5 4	291865 313257	3	-0.39	2.58E+09 2.93E+09	-0.635
1025.437 1025.658	215734 222398	4	313253 319896	$\frac{5}{4}$	0.49 0.1	1.96E+10 7 97E+09	-0.582 -0.629
1025.695	220316	2	317811	3	-0.97	6.79E+08	-0.156
1026.004 1026.457	218726 218028	$\frac{2}{2}$	316192 315450	23	-0.43	6.64E+09 2.29E+09	-0.684 0.468
1026.797	222603 195055	2	319993	3	-0.16	4.30E+09 1.49E+09	-0.502
1020.001	195544	3	292913	3	-0.72	1.20E+09	0.175
1027.045 1027.134	$217621 \\ 224959$	3 6	$314988 \\ 322317$	$\frac{4}{5}$	-0.76 -0.92	1.11E+09 7.60E+08	-0.278 0.198
1027.391	215133	4	312467	4	0.11	8.17E+09	0.697
1027.607	199599	3	296912	4 3	0.21	1.02E+09 1.02E+10	-0.478
1027.609 1027.618	214413 218138	1 3	311727 315450	1 3	-0.29 -0.3	3.23E+09 3.09E+09	$0.537 \\ -0.48$
1027.787	225859	3	323155	4	0.19	9.86E+09	-0.353
1027.916	218628 215133	3 4	312416	3 5	-0.37	1.22E+09	-0.448
1028.447	242530 192741	3	$339764 \\ 289974$	4	-0.77 -0.16	1.07E+09 4 42E+09	0.13
1028.568	194339	5	291562	5	-0.84	9.23E+08	0.093
1028.616 1028.923	218628 222398	$\frac{3}{4}$	$315846 \\ 319587$	2 4	-0.76 0.2	1.08E+09 1.01E+10	-0.111 -0.71
1028.955	218726	2	315912	3	-0.64	1.44E + 09	-0.563
1029.198	214835	5	311998	5	0.26	1.16E+10	0.649
1029.516 1029.656	$243029 \\ 218726$	$\frac{4}{2}$	$340162 \\ 315846$	$\frac{5}{2}$	-0.44 -0.61	2.30E+09 1.53E+09	$0.183 \\ 0.572$
1030.011	195827	2	292913	3	0.53	2.11E+10	-0.814
1030.165 1030.274	200483 190528	3 5	297554 287589	$\frac{2}{4}$	-0.75 0.14	1.13E+09 8.70E+09	-0.381 0.807
1030.549 1031.005	190554 223000	4	287589 319993	$\frac{4}{3}$	$0.48 \\ -0.68$	1.90E+10 1.30E+09	-0.602 -0.159
1031.052	218000	5	314988	4	0.02	6.64E+09	-0.729
1031.241 1031.274	218628 218945	$\frac{3}{4}$	$315599 \\ 315912$	$\frac{4}{3}$	-0.63 -0.14	1.48E+09 4.50E+09	-0.209 -0.547
1031.408 1031.872	195684 195086	1	292639 291997	$\frac{1}{2}$	-0.15	4.44E+09 4.77E+09	-0.683
1031.902	221602	6	318510	7	0.93	5.35E+10	-0.9
1031.911 1032.033	214835 223000	5 3	$311743 \\ 319896$	$\frac{6}{4}$	$0.84 \\ 0.17$	4.37E+10 9.40E+09	-0.841 -0.586
1032.035 1032.112	195544 192753	3 4	292440 289642	4	0.61	2.54E+10 1.71E+10	-0.88 -0.656
			156	-	5.10		0.000

Table A3: Continued

$\begin{array}{l c c c c c c c c c c c c c c c c c c c$	Wavelength	Lower Level	JLow	Upper level	JUp	log gf	gA	CF
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1032.304 1032.333	222398 195086	4	319268 291954	3	-0.64 -0.96	1.40E+09 6.82E+08	-0.483 0.557
1002.315 2425.00 3 339393 3 0.15 8.972+09 0.684+0 1003.416 200750 2 297554 2 0.13 0.588+0 0.481 1003.2463 200750 2 297554 2 0.13 0.588+0 0.490 1003.247 217445 4 3414263 0.4055 1.1082+10 0.519 1003.145 190753 4 20075 5 0.588 2.3772+10 0.577 1003.124 190554 5 2.3782+00 0.517 1.3384+00 0.438 1003.2563 194132 3 290885 3 0.22 1.118+10 0.70 1003.4564 194322 3 290885 3 0.23 1.44845+00 0.438 1033.456 194323 2 290897 1 0.423 2.7564+09 0.614 1034.462 2929377 1 0.23 1.4072+00 0.438 0.33 1.4072+00 0.438	1032.359	215133	4	311998	5	0.25	1.13E+10	-0.559
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1032.387	242530	3	339393	3	0.15	8.97E+09	-0.668
1032.463 200730 2 29753 5 0.013 9.582+00 -0.619 1032.47 21745 4 28732 5 0.024 1.002+04 -0.619 1033.14 190758 5 287320 5 0.58 2.3772+10 -0.519 1033.145 190558 5 21569 4 -0.519 1.334-00 0.517 1033.425 190554 4 237320 5 0.518 1.112+10 0.532 1033.451 190554 4 297320 5 0.51 1.112+10 0.782 1033.452 190554 4 299359 4 0.037 2.3782+00 0.438 1033.461 19524 299359 4 0.33 4.384-00 0.778 1034.461 223330 4 312696 4 0.3784+00 0.789 1034.411 223430 4 0.357 3.0278+00 0.789 0.789 1034.4141 2234344 3.131	1032.412 1032.522	214413 218138	3	311274 314988	2	-0.83 -0.54	$9.28E \pm 08$ $1.81E \pm 09$	-0.448 0.313
$\begin{array}{llllllllllllllllllllllllllllllllllll$	1032.691	200720	2	297554	2	0.19	9.58E + 09	-0.681
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1032.843	192753	4	289573	5	0.21	1.00E+10 1.71E+00	-0.519
1033.14 217079 3 313872 4 -0.67 1.34E+09 0.167 1033.229 214815 5 315590 4 0.37 2.71E+10 0.728 1033.229 214815 5 315590 4 0.37 2.71E+10 0.517 1033.542 190554 4 287320 5 -0.18 4.11E+09 0.182 1033.564 195544 3 292297 4 -0.14 4.48E+06 0.348 1033.563 195592 213929 4 -0.32 3.758+09 -0.614 1034.62 233920 21228 3 -0.22 3.758+09 -0.631 1034.62 218954 4 315599 4 -0.53 3.854+09 -0.637 1034.72 124953 290774 2 0.077 7.85E+09 0.637 1034.62 218403 3 31395 4 0.15 8.73E+09 0.637 1034.112 13668 20.077 </td <td>1032.87</td> <td>191762</td> <td>3</td> <td>288566</td> <td>3</td> <td>0.15</td> <td>8.85E+09</td> <td>-0.343</td>	1032.87	191762	3	288566	3	0.15	8.85E+09	-0.343
1033.145 10028 5 287320 5 0.58 2.375+10 0.728 1033.240 124813 5 3.13594 4 280530 3 0.22 1.055+10 -0.437 1033.452 130554 4 287320 5 -0.18 4.118+10 0.79 1033.564 135544 3 220985 3 0.23 1.118+10 0.79 1033.564 135544 3233764 4 4.0.07 7.555+69 -0.411 1034.06 139920 4 333764 4 -0.02 3.755+69 -0.411 1034.161 213360 1 310457 1 -0.32 3.755+69 -0.411 1034.221 213361 2 312418 5 0.33 1.405+10 -0.411 1034.62 218435 4 312418 5 0.35 8.784+69 0.657 1034.722 128436 2 313057 1 -0.15 8.784+69 0.371	1033.14	217079	3	313872	4	-0.67	1.34E + 09	0.167
103.276 243029 4 139869 5 0.28 1.21E+10 0.833 1033.364 192753 4 28530 3 0.22 1.05E+10 0.415 1033.422 190554 4 287320 5 -0.18 4.11E+69 0.183 1033.667 230328 3 2302980 4 -0.37 2.88E+69 -0.77 1034.67 230328 3 230297 1 -0.32 3.78E+69 -0.414 1034.62 221834 1 112446 1 -0.33 1.40E+10 -0.476 1034.421 222603 1 -0.32 3.78E+69 -0.614 1034.431 1165682 2177 2 0.02 3.87E+69 -0.614 1034.441 1165682 2177 2 0.02 5.88E+69 -0.78 1034.919 2260623 3 313295 2 0.02 5.88E+69 -0.64 1035.391 230007 2 3.387E+69<	1033.145	190528 218815	5	287320 315599	5 4	0.58	2.37E+10 2.71E+09	-0.728 -0.517
1033.304 192753 4 289530 3 0.22 1.058+10 0.457 1033.463 104132 3 290887 3 0.21 1.11E+10 0.73 1033.663 104132 3 290887 3 0.22 1.11E+10 0.73 1033.661 104162 4 0.007 7.35E+09 0.441 1034.045 1999202 4 290510 4 0.023 3.75E+09 0.641 1034.163 199202 2 319268 1 -0.23 3.75E+09 0.641 1034.401 2218945 4 0.155 7.35E+09 0.481 1034.724 190666 2 201730 2 -0.25 3.48E+09 0.657 1035.842 104132 2 1035 4 0.156 7.35E+09 -0.38 1035.842 10433 3 31957 4 0.16 4.556 0.557 1035.842 10433 3 31957 <td< td=""><td>1033.276</td><td>243029</td><td>4</td><td>339809</td><td>5</td><td>0.29</td><td>1.21E+10</td><td>-0.833</td></td<>	1033.276	243029	4	339809	5	0.29	1.21E+10	-0.833
1033.242 100.53 4 287.820 5 -1.18 1.11E+109 0.182 1033.264 12032.64 320280 4 -0.37 2.08E+09 -0.797 1033.667 20030 4 320280 4 -0.37 2.08E+09 -0.614 1034.04 195032 4 205710 4 -0.38 2.70E+09 -0.614 1034.05 195032 1 1222731 1 -0.38 1.40E+10 -0.476 1034.432 222003 2 312085 4 -0.38 1.40E+10 -0.476 1034.422 218945 4 315599 4 -0.15 3.87E+09 -0.671 1034.724 1105086 2 207710 2 -0.077 7.28E+09 -0.389 1035.285 216703 2 313295 2 -0.69 1.27E+09 0.571 1035.44 1934341 280974 1 -0.16 3.32E+09 0.533 1036.627 213535 313295 2 -0.77 3.67E+10 -0.829	1033.304	192753	4	289530	3	0.22	1.05E + 10	-0.457
1033.65 1057.65 230236 4 220277 4 -0.14 4.488+09 0.348 1033.67 230236 4 330764 4 0.07 7.355+09 -0.71 1034.04 199022 4 292637 1 -0.23 3.755+09 -0.411 1034.05 199022 2 215734 4 12146 5 -0.35 1.067+00 -0.416 1034.401 2226932 2 310268 3 -0.23 3.645+09 -0.468 1034.724 196086 2 21730 2 -0.25 3.485+09 0.657 1034.725 216703 2 31225 2 -0.64 1.765+10 -0.802 1035.841 193134 228074 1 -0.16 3.574+09 -0.64 1035.223 213303 2 310571 1 -0.83 7.725+09 -0.64 1036.027 213330 2 310567 2 -0.03 6.887+09 -0.63 1036.027 213330 2 30065 2 -0	1033.422 1033.563	190554	4	287320 290885	5	-0.18	4.11E+09 1.11E+10	0.182 0.79
1033.657 230226 4 326980 4 -0.37 2.68E+09 -0.441 1034.763 243029 4 25510 4 -0.35 2.70E+09 -0.641 1034.161 123300 1 31007 1 -0.184 -0.165 -0.458 1034.461 1222603 2 31268 3 -0.23 3.46E+09 -0.468 1034.422 21845 4 315599 4 -0.55 8.78E+09 -0.368 1034.422 21845 4 315599 4 -0.45 8.78E+09 -0.367 1034.525 216703 2 217374 2 -0.25 3.48E+09 -0.687 1035.285 216703 2 313295 2 -0.66 1.77E+10 -0.802 1035.439 124043 3 315912 1 -0.118 4.32E+09 0.411 1036.167 124043 3 315912 1 -0.123 3.78E+09 0.331 1035.452 216071 3 312957 1 -0.123 3.78E+09	1033.564	195544	3	292297	4	-0.14	4.48E+09	0.348
103.7.63 243029 4 333640 4 0.00 7.38E+09 -0.813 1034.161 213360 1 310057 1 -0.18 4.15E+09 0.781 1034.322 215734 4 312416 5 0.33 3.64E+09 0.781 1034.422 218945 4 315599 4 0.15 S.73E+09 0.781 1034.523 218945 4 315599 4 0.15 S.73E+09 0.781 1034.524 218945 4 315599 4 0.45 1.77E+109 0.604 1034.525 216703 2 317347 2 -0.72 5.48E+09 0.637 1034.525 216703 2 317347 2 -0.64 2.36E+09 0.641 1035.252 216703 3 31942 3 -0.16 4.32E+09 -0.557 1036.167 219403 3 319912 3 -0.676 0.557 1036.167	1033.657	230236	4	326980	4	-0.37	2.68E+09	-0.797
1034.161 19322 0 292339 1 -0.22 3.76E+09 -0.813 1034.161 213360 1 312416 5 0.35 1.40E+10 -0.476 1034.452 213454 4 315599 4 0.15 8.73E+60 0.739 1034.755 194132 290774 2 0.07 7.26E+10 0.387 1034.841 197711 2 29370 2 0.02 5.98E+09 0.387 1035.285 216703 2 313295 2 0.66 1.27E+10 0.302 1035.384 1934913 313912 1 -0.16 4.38E+08 -0.577 1035.617 194055 4 291562 5 0.77 3.67E+09 0.343 1036.875 214031 3 315121 1 -0.23 3.78E+09 0.343 1036.875 214071 6 312515 6 0.38 6.68E+09 -0.377 1036.875 214071 6 312416 5 1.61 9.028E+09 -0.437	1033.753	243029 199202	4	339764 295910	4	-0.36	7.35E+09 2.70E+09	-0.441
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1034.05	195932	0	292639	1	-0.22	3.75E + 09	-0.813
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1034.161	213360	1	310057	1	-0.18	4.15E+09	0.799
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1034.323	222603	4 2	319268	3	-0.23	3.64E+09	-0.478
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1034.622	218945	4	315599	4	0.15	8.73E + 09	0.708
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1034.724	195086	2	291730	2	-0.25	3.48E+09	0.657
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1034.884	194132 192741	2	289370	2	-0.02	5.98E+09	-0.398
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1034.919	250623	3	347249	4	0.45	1.76E + 10	-0.802
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1035.285	216703	2	313295	2	-0.69	1.27E+09 8.17E+09	$0.204 \\ 0.597$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1035.844	193434	1	289974	1	-0.16	4.35E+09	-0.553
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1036.027	213535	2	310057	1	-0.85	8.74E + 08	-0.737
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1036.167 1036.197	219403 195055	3	315912 291562	3	-0.43 0.77	2.30E+09 3.67E+10	0.411
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1036.223	213360	1	309865	2	0.03	6.68E + 09	-0.64
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1036.432	195086	2	291571	1	-0.22	3.78E+09	0.393
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1036.875	216071 219403	6	312515 315846	6 2	0.38	$1.49E \pm 10$ $6.77E \pm 09$	-0.82 -0.647
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1037.025	200483	3	296912	3	-0.62	1.50E + 09	-0.587
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1037.125	194132	3	290553	4	0.16	9.00E+09	-0.515
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1037.945	216028	5 6	312416	4 5	-0.76	6.17E+08	0.217
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1038.096	213535	2	309865	2	0.05	7.01E + 09	0.798
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1038.284	195684	1	291997	2	$0 \\ 0.72$	6.25E+09	-0.827
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1038.806	215734	4	311998	4 5	-0.72	8.43E+08	-0.150
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1038.919	216703	2	312957	3	-0.09	4.99E + 09	-0.52
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1039.334	217079 195086	3	313295 201200	2	-0.87	8.37E+08 7 50E+09	-0.515 -0.596
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1039.503	213665	3	309865	2	-0.85	8.75E + 08	-0.695
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1039.546	219403	3	315599	4	-0.16	4.27E + 09	-0.572
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1039.584	200720 195544	2	296912 291730	3	-0.65	1.39E+09 7 10E+08	-0.262 0.246
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1039.741	217079	3	313257	3	-0.01	6.08E + 09	0.741
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1039.76	224959	6	321135	7	-0.88	8.19E+08	0.606
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1039.824 1040.154	228480	2 5	324619	2 5	-0.57	7.61E+09	-0.553 0.397
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1040.312	213932	0	310057	1	-0.2	3.87E + 09	-0.654
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1040.313	227993	6	324118 309653	6	-0.23	3.59E+09 1.46E+10	0.23 0.715
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1040.515	194339	5	290445	6	0.85	4.36E+10	-0.899
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1040.665	195055	4	291147	5	-0.73	1.14E + 09	0.153
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1040.886 1041.187	221739 215133	2	317811 311177	3	-0.78	1.19E+10 1.02E+09	0.863
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1041.249	243725	3	339764	4	-0.03	5.77E + 09	0.429
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1041.795	213665	3	309653	3	0.08	7.39E + 09	0.798
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1042.254	216071	6	311998	5	-0.23	3.63E+09	-0.709
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1042.513	224071	2	319993	3	-0.56	1.69E + 09	0.178
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1042.72 1042.768	195827 216703	2	291730 312602	2	-0.32	2.92E+09 1 30E+09	-0.294
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1042.993	215133	4	311011	3	-0.59	1.60E + 0.09	0.56
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1043.36	222666	7	318510	7	-0.86	8.33E+08	0.877
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1043.512 1043.564	213665	4 3	290885	3 4	-0.53	1.81E+09 2.37E+10	-0.799
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1043.675	220917	5	316732	4	0.14	8.59E + 09	0.786
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1043.747	217445 222666	4 7	313253 318459	5 8	0.02	6.38E+09 6.12E±10	-0.828
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1044.059	226271	2	322051	3	0.25	1.10E+10	0.779
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1044.26	227993	6	323755	6	0.03	6.48E+09	-0.536
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1044.336 1044.491	$195544 \\ 193948$	3 6	291299 289688	3 7	-0.02 0.95	5.40E+10	-0.414 -0.898
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1045.182	225387	4	321064	5	-0.93	7.30E + 08	0.748
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1045.242	216071	6	311743	6	-0.29	3.16E + 09	0.843
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1045.288 1045.288	213133 229064	4 4	324731	3 4	0.38	1.49E + 10 7.68E+09	-0.853 0.549
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1045.532	217650	2	313295	2	-0.24	3.48E + 09	0.403
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1045.605 1046.340	228480 202361	5	324118	6 1	-0.3	3.01E+09 5.86E→ 00	0.295
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1046.499	216071	6	311628	$\frac{1}{7}$	0.94	5.37E+10	-0.896
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1046.514	229064	4	324619	5	-0.56	1.67E + 09	0.632
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1046.565	217079 217079	3	312630 312602	4 2	-0.82 -0.75	9.23E+08 1.08E+09	0.247 0.462
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1047.021	194132	3	289642	4	-0.51	1.90E + 09	-0.171
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1047.143	195055	4	290553	4	0.21	9.81E+09	-0.457
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1047.206 1047.225	217109 244671	1 5	312602 340162	2 5	-0.86 0.33	8.38E+08 1.32E+10	-0.159
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1047.431	195827	2	291299	3	-0.51	1.88E + 09	-0.224
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1047.655 1047.694	214413 218815	1	309865	2 5	-0.66	1.33E+09	-0.263
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1048.077	222398	4	317811	3	-0.1	4.83E+09	0.626
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1048.121	244753	4	340162	5	0.3	1.22E+10	-0.696
157	1048.275 1048.355	225387 217079	4 3	320782 312467	5 4	0.79 -0.14	3.72E+10 4.44E+09	-0.886 -0.396
1+11			-	157			1	

Table A3: Continued

Wavelength 1048.442	Lower Level 216703	J_{Low}	Upper level 312083	J_{Up}	log gf -0.49	gA 1.95E+09	CF 0.706
1048.581	221650	3	317017	3	-0.53	1.79E+09	-0.185
1048.804	244417	3	339764	4	0.22	1.35E+10 1.35E+10	-0.83
$1048.925 \\ 1049.086$	$217621 \\ 244072$	3 2	$312957 \\ 339393$	3 3	-0.39 0.08	2.52E+09 7.24E+09	$0.245 \\ -0.523$
1049.126	218945	4	314262	5	0.42	1.61E+10	0.839
1049.239 1049.292	194339	2 5	289642	4	-0.48	2.03E+09	-0.569
1049.555 1049.735	$221739 \\ 199202$	$^{2}_{4}$	$317017 \\ 294464$	3 4	-0.98 -0.97	6.39E + 08 6.46E + 08	$0.107 \\ 0.148$
1049.827	218000	5	313253	5	-0.9	7.63E + 08	-0.154
1049.94 1050.047	194339	3 5	289573	4 5	$0.24 \\ 0.36$	1.04E+10 1.38E+10	-0.852 -0.607
1050.444 1050 582	224071 217445	2	319268 312630	3 4	-0.24	3.45E+09 1.13E+09	0.4 0.486
1050.612	224959	6	320142	7	0.94	5.17E + 10	-0.902
1050.733 1051.144	$214319 \\ 220316$	$\frac{4}{2}$	$309490 \\ 315450$	$\frac{4}{3}$	-0.06 0.32	5.25E+09 1.23E+10	$0.809 \\ -0.648$
1051.259 1051.578	218171 214319	$\frac{1}{4}$	313295 309414	2	-0.11 0.76	4.76E+09 3.51E+10	-0.575 -0.853
1051.593	225859	3	320953	4	0.47	1.79E+10	-0.867
1051.72 1051.897	$221650 \\ 215734$	$\frac{3}{4}$	$316732 \\ 310800$	$\frac{4}{3}$	$0.51 \\ -0.5$	1.96E+10 1.91E+09	-0.853 0.675
1052.018 1052.387	244753 217445	4	339809 312467	5	-0.08	5.01E + 09 2.47E + 09	0.259 0.311
1052.513	244753	4	339764	4	-0.3	3.02E+09	-0.243
$1052.534 \\ 1052.535$	$217621 \\ 195544$	3 3	$312630 \\ 290553$	4 4	$0.37 \\ -0.42$	1.43E+10 2.27E+09	-0.805 -0.129
1052.829	217079	3	312061	2	-0.08	5.07E+09	0.715
1052.945 1052.954	217445	5 4	312416	$\frac{4}{5}$	-0.82 0.15	9.13E+08 8.56E+09	$0.562 \\ 0.77$
$1053.102 \\ 1053.444$	245204 218945	4	340162 313872	$\frac{5}{4}$	0.23	1.02E+10 1 42E+09	-0.858 -0.142
1053.731	218815	5	313715	6	0.87	4.41E+10	-0.914
$1054.345 \\ 1054.639$	217621 218138	3 3	$312467 \\ 312957$	$\frac{4}{3}$	-0.27 -0.84	3.24E+09 8.78E+08	-0.704 0.129
1054.947 1055.409	203140	1	297931 288698	1	-0.26	3.30E + 09 1.86E + 10	-0.794
1055.884	244671	5	339379	6	0.45	4.22E+10	-0.851
1055.972 1056.119	$201211 \\ 119632$	3 5	$295910 \\ 214319$	4 4	$0.23 \\ -0.87$	1.02E+10 8.00E+08	-0.802 0.43
1056.173	220917	5	315599	4	-0.97	6.37E+08	-0.297
1056.758	218628	4 3	313257	3	0.08 0.04	6.59E+09 6.59E+09	-0.514
1057.036 1057.369	$245204 \\ 221272$	4	$339809 \\ 315846$	$\frac{5}{2}$	$0.55 \\ -0.65$	2.14E+10 1.31E+09	-0.782 -0.461
1057.405	216703	2	311274	2	-0.88	7.82E+08	0.288
1057.455 1057.622	202361	4 2	287320 296912	5 3	$0.04 \\ 0.11$	6.57E+09 7.66E+09	-0.311 -0.8
1057.753 1057.856	197325 218726	5	291865 313257	6 3	0.85	4.24E+10 4.68E+09	-0.9 -0.668
1058	195055	4	289573	5	-0.57	1.62E+09	-0.078
1058.029 1058.098	218000 225387	$\frac{5}{4}$	$312515 \\ 319896$	6 4	0.7	2.95E+10 3.93E+09	-0.868 -0.654
1058.287	218138	3	312630	4	0.02	6.28E + 09 7.67E + 09	-0.506
1058.605	218138	3	312602	2	-0.73	1.11E+09	-0.495
1058.953 1059.143	$217650 \\ 218000$	2 5	$312083 \\ 312416$	3 5	-0.82 0.22	8.94E+08 9.95E+09	-0.239 0.611
1059.155 1050.150	203140	1	297554	2	-0.09	4.80E + 09 1.02E + 00	-0.797
1059.786	194339	5	288698	6	-0.7	1.02E+09 1.18E+09	-0.073
1060.118 1060.308	$218138 \\ 218945$	3 4	$312467 \\ 313257$	4 3	-0.87 -0.96	8.00E+08 6.49E+08	-0.179 0.18
1060.319	199202	4	293514	3	-0.85	8.35E+08	0.656
1060.358	216703	$\frac{4}{2}$	311011	3	-0.19	3.79E+09 3.79E+09	-0.697
1060.407 1060.561	244671 195684	5 1	$338975 \\ 289974$	5 1	-0.67 -0.95	1.28E+09 6.72E+08	$0.765 \\ 0.166$
1060.622	195086	2	289370	2	-0.93	7.06E+08	0.066
1060.858	198179	4	292440	5 4	-0.76	1.04E+09 7.87E+08	0.606 0.444
1061.159 1061.327	197325 244753	5 4	$291562 \\ 338975$	5 5	-0.94 0.44	6.84E+08 1.64E+10	-0.126 -0.832
1061.427	202361	2	296573	2	-0.12	4.43E+09	-0.685
1061.606	199202	4	293399	$\frac{4}{5}$	-0.13	4.39E+09 3.71E+10	-0.907
1061.63 1061.868	217079 221739	3 2	$311274 \\ 315912$	2 3	-0.03 -0.36	5.54E+09 2.54E+09	-0.707 -0.576
1062.502	198179	4	292297	4	-0.11	4.62E+09	0.691
1062.792 1063.029	227960 220917	2 5	314988	3 4	-0.49 -0.41	1.92E+09 2.33E+09	0.471
1063.208 1063.355	218028 195932	2	312083 289974	3 1	-0.84 -0.8	8.63E+08 9.43E+08	-0.292 -0.364
1063.409	225859	3	319896	4	-0.99	6.03E+08	-0.043
1063.446 1063.637	218028 223000	2 3	312061 317017	2 3	-0.74 -0.12	1.08E+09 4.49E+09	-0.472 0.633
1063.843	218000 200483	5 3	311998 294464	$\frac{5}{4}$	0.28	1.14E+10 2.95E+10	-0.484
1064.413	221650	3	315599	4	-0.91	7.22E+08	-0.39
1064.796 1065.068	199599 218171	3 1	$293514 \\ 312061$	3 2	-0.27 -0.72	3.18E+09 1.12E+09	0.586 -0.557
1065.481	219403	3	313257	3	-0.38	2.46E+09	0.234
1065.845	218028 197325	3 5	$\frac{512467}{291147}$	4 5	-0.68	1.23E+09 1.44E+10	-0.152 -0.88
1066.386 1066.433	$198179 \\ 245204$	4 4	$291954 \\ 338975$	3 5	$0.05 \\ -0.58$	6.59E+09 1.56E+09	-0.736 0.568
1066.742	218000	5	311743	6	-0.6	1.48E+09	-0.147
1066.997 1067.105	217079 221739	3 2	310800 315450	3 3	-0.9 -0.45	1.38E+08 2.04E+09	-0.241 -0.204
$1067.231 \\ 1067.396$	218815 195684	5 1	$312515 \\ 289370$	$^{6}_{2}$	-0.69 -0.57	1.20E+09 1.58E+09	-0.059 -0.194
1067.406	218945	4	312630	4	-0.57	1.56E+09	0.334
1068.098 1068.763	217650 217445	4	311274 311011	2 3	-0.94 -0.48	0.00E+08 1.94E+09	-0.264 -0.429
			158				

Table A3: Continued

$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Wavelength 1068.88	Lower Level 217621	J _{Low}	Upper level 311177	J_{Up}_4	log gf 0.13	gA 7.97E+09	CF 0.625
$\begin{array}{l c c c c c c c c c c c c c c c c c c c$	1068.937	224959	6	318510	7	-0.95	6.53E+08	-0.014
$\begin{array}{l c c c c c c c c c c c c c c c c c c c$	1069.268	218945 222398	4	312467 315912	$\frac{4}{3}$	-0.8	9.14E+09	0.184
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$1069.495 \\ 1069.742$	$213665 \\ 195086$	3	$307167 \\ 288566$	2 3	-0.97 -0.5	6.24E+08 1.84E+09	-0.355 -0.136
$\begin{array}{c} 10001010101010101010101010101010101010$	1069.976	229064	4	322524	5	0.12	7.60E+09	-0.518
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1070.012 1070.039	194132 218628	3	287589 312083	4 3	-0.25 -0.38	3.28E+09 2.43E+09	-0.179 -0.305
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1070.317 1070.401	218631 199599	1	312061	2	0.02	6.13E+09 7.01E+09	-0.634
$\begin{array}{c} 107, 1.19, 21769, 2 & 31.011, 3 & -0.17, 3.93, -0.0, 0.51, \\ 1071, 137, 22165, 3 & 314988, 4 & -0.39, 2.34, -0.9, 0.65, \\ 1072, 347, 22904, 4 & 322317, 5 & 0.38, 1.29, -109, 0.363, \\ 1072, 347, 22904, 4 & 322317, 5 & 0.38, 1.29, -109, 0.481, 1.29, -109, 0.41, 1.29, -109, 0.41, 1.29, -109, 0.41, 1.29, -109, 0.41, 1.29, -109, 0.41, 1.29, -109, 0.41, 1.29, -109, 0.41, 1.29, -109, 0.41, 1.29, -109, 0.41, 1.29, -109, 0.41, 1.29, -109, 0.41, 1.29, -109, 0.41, 1.29, -109, 0.41, 1.29, -109, 0.41, 1.29, -109, 0.41, 1.48, -100, 0.441, 1.48, -100, 0.441, 1.48, -100, 0.41, 1.48, -100, 0.41, 1.48, -100, 0.41, 1.48, -100, 0.471, 1.21, -104, 1.21, -104, 1.21, -104, 1.21, -104, 1.21, -104, 1.21, -104, 1.21, -104, 1.21, -104, 1.21, -104, 1.21, -104, 1.21, -104, 1.21, -104, 1.21, -104, 1.21, -104, 1.21, -104, 0.41, 1.21, -104, 1.2$	1070.988	193948	6	287320	5	-0.16	4.06E+09	-0.799
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1071.11 1071.132	217650 225387	2 4	$311011 \\ 318746$	3 5	-0.17 -0.77	3.93E+09 1.01E+09	$0.51 \\ -0.74$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1071.173 1071.377	217445 221650	4	310800 314988	3 4	-0.42	2.22E+09 2.34E+09	-0.222
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1071.865	200720	2	294015	1	-0.16	4.05E+09	-0.881
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$1072.347 \\ 1072.384$	$229064 \\ 194339$	4 5	$322317 \\ 287589$	5 4	$0.35 \\ -0.91$	1.29E+10 7.28E+08	-0.881 -0.113
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1072.528 1073.148	199202 218815	4	292440 311998	4	-0.5	1.84E+09 7.06E+08	-0.33 0.065
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1073.22	218000	5	311177	4	-0.85	8.10E+08	-0.642
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1073.53 1073.631	$217650 \\ 227993$	$\frac{2}{6}$	$310800 \\ 321135$	$\frac{3}{7}$	-0.98 0.72	6.07E+08 3.01E+10	$0.415 \\ -0.916$
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1073.679 1073.879	218945 197325	4	312083 290445	3	-0.79	9.42E + 08 2.22E + 09	0.312
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1073.889	198179	4	291299	3	-0.95	6.50E + 08	-0.272
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$1074.178 \\ 1074.548$	$199202 \\ 228480$	4 5	$292297 \\ 321542$	$\frac{4}{6}$	$0.06 \\ 0.62$	6.64E+09 2.38E+10	-0.447 -0.908
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1074.706 1074.813	151623	6	244671 311177	5	-0.81	9.00E + 08 1.48E + 10	0.439 0.807
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1074.912	200483	3	293514	3	0.41	6.78E+09	-0.639
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$1075.263 \\ 1075.463$	$218726 \\ 218028$	$\frac{2}{2}$	$311727 \\ 311011$	1 3	-0.43 -0.14	2.19E+09 4.16E+09	-0.671 0.535
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1075.495	194339	5	287320	5	-0.79	9.32E+08	-0.105
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1075.638	198179	$\frac{2}{4}$	291147	5	-0.7	1.10E+09 1.81E+10	-0.751
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$1076.202 \\ 1076.738$	$230236 \\ 218138$	4 3	$323155 \\ 311011$	4 3	-0.77 -0.33	9.84E+08 2.70E+09	-0.565 0.735
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1077.108	199599	3	292440	4	-0.89	7.43E+08	-0.113
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1077.662	200720	2	293514	4 3	0.48 0.23	9.72E+09	-0.625
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1078.211 1078.773	120919 199599	4	$213665 \\ 292297$	3 4	-0.96 0.34	6.28E + 08 1.26E + 10	$0.441 \\ -0.659$
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1078.984	219403	3	312083	3	-0.03	5.34E+09	-0.646
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1079.377 1079.414	218628 218631	3	311274 311274	2	-0.53 -0.25	1.72E+09 3.26E+09	-0.727 -0.453
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1079.821 1080.097	227993 228480	6 5	320601 321064	6 5	$0.51 \\ 0.43$	1.84E+10 1.53E+10	-0.799 -0.752
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1080.279	223623	3	316192	2	-0.83	8.60E+08	0.179
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1080.509	218628 218726	3 2	311177 311274	$\frac{4}{2}$	-0.74 -0.68	1.04E+09 1.21E+09	-0.55 -0.697
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1081.928 1082.454	223764 218628	1	$316192 \\ 311011$	2 3	-0.71 -0.68	1.11E+09 1.21E+09	0.361 -0.254
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1082.754	229694	2	322051	3	-0.38	2.40E+09	-0.389
$\begin{array}{llllllllllllllllllllllllllllllllllll$	1082.777 1083.563	230236	3 4	322524	3 5	-0.89 -0.06	4.98E+09	0.125
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1083.589 1084.678	220316 200720	2	312602 292913	2 3	-0.22 -0.51	3.44E+09 1 77E+09	-0.589 0.778
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1085.99	223764	1	315846	2	-0.94	6.45E + 08	0.276
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1085.994 1086.564	230236 227960	$\frac{4}{2}$	322317 319993	5 3	-0.93 -0.26	6.65E+08 3.06E+09	$0.123 \\ 0.47$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$1089.142 \\ 1089.196$	230236 201211	4	322051 293022	3	-0.83 -0.43	8.31E+08 2 10E+09	$0.632 \\ 0.271$
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1090.272	230331	3	322051	3	-0.17	3.80E+09	-0.611
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1091.052 1091.608	202361 219403	2 3	$294015 \\ 311011$	1 3	-0.54 -0.75	1.63E+09 9.88E+08	$0.403 \\ -0.21$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$1093.896 \\ 1093.959$	228480 220316	5	319896 311727	4	-0.09 -0.7	4.51E+09 1 12E+09	-0.675 0.584
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1094.122	219403	3	310800	3	-0.9	7.06E+08	0.463
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1094.167 1094.746	198179 225387	$\frac{4}{4}$	$289573 \\ 316732$	$\frac{5}{4}$	-0.3 -0.92	2.77E+09 6.89E+08	-0.289 -0.223
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1094.824 1095.042	242530 233299	3 5	$333869 \\ 324619$	4 5	-0.61 -0.43	1.37E+09 2.03E+09	-0.879 -0.655
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1096.995	225859	3	317017	3	-0.83	8.28E+08	0.141
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1097.611 1099.404	228480 220316	$\frac{5}{2}$	$319587 \\ 311274$	$\frac{4}{2}$	-0.74	1.01E+09	-0.771 -0.456
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1099.457 1099.763	199599 229064	3 4	290553 319993	$\frac{4}{3}$	-0.77 -0.78	9.40E + 08 9.14E + 08	-0.215 -0.786
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1100.403	203140	1	294015	1	-0.19	3.53E+09	-0.582
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1100.981 1101.085	230236 233299	$\frac{4}{5}$	321064 324118	5 6	-0.68 0.33	1.15E+09 1.15E+10	-0.561 -0.838
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1101.147 1101.893	216703 227993	2	307517 318746	3 5	-0.49 0.38	1.76E+09 1.31E+10	-0.509 -0.889
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1102.013	201211	3	291954	3	0.28	1.04E + 10	-0.733
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1102.205 1102.332	152302 230236	$\frac{5}{4}$	$243029 \\ 320953$	$\frac{4}{4}$	-0.94 -1	6.32E+08 5.41E+08	$0.45 \\ 0.33$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1103.009 1103.49	202361 230331	2	293022 320953	2 4	-0.04	5.06E+09 5.28E+09	-0.469 -0.239
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1104.767	227993	6	318510	7	-0.87	7.36E+08	-0.536
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1105.507 1105.521	233299 221272	$\frac{5}{1}$	$323755 \\ 311727$	6 1	0.32 - 0.74	1.13E+10 1.01E+09	-0.824 -0.356
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1106.88 1107.438	$221739 \\ 229694$	$\frac{2}{2}$	$312083 \\ 319993$	3 3	-0.86 -0.86	7.43E+08 7.45E+08	$0.31 \\ -0.151$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1107.67	216703	2	306983	1	-0.75	9.69E+08	0.548
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1107.832 1107.863	228480 213535	$\frac{5}{2}$	$318746 \\ 303798$	5 3	-0.88 -0.81	$^{7.17E+08}_{8.45E+08}$	-0.298 -0.856
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1107.91	220917 229064	5 4	311177 319268	4	-0.75 -0.65	9.55E+08 1.20E+09	-0.632 0.585
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1110.028	201211	3	291299	3	-0.79	8.71E+08	-0.296
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1112.394 1112.567	$217621 \\ 203140$	$\frac{3}{1}$	$307517 \\ 293022$	$\frac{3}{2}$	-0.05 -0.95	4.82E+09 6.08E+08	-0.759 -0.24
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1112.747 1112.883	217650 233299	2	307517 323155	3 4	-0.59 -0.97	1.39E+09 5.78E+08	-0.28 -0.702
1114.122 230230 4 319993 3 -0.1 4.25E+09 0.787 150	1113.266	243029	4	332855	5	-0.81	8.41E+08	-0.756
1.1.7	1114.122	230236	4	319993 150	3	-0.1	4.25E+09	0.787

Table A3: Continued

Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA 8.53E⊥08	CF 0.377
1115.148	201211 202361	2	290885	3	-0.8	5.64E+08	-0.195
1116.746	217621	3	307167	2	-0.5	1.70E + 09	0.524
1116.981	221650 218138	3	311177 307517	4	-0.9	$6.62E \pm 08$ 2.61E \pm 09	0.276
1119.408	217650	2	306983	1	-0.66	1.17E+09	0.375
1119.425	153198	4	242530	3	-0.89	6.80E+08	0.5
1119.971 1120.757	226558	5	315846 322524	2 5	-0.96	1.05E+10	-0.682
1122.87	227960	2	317017	3	-0.77	8.96E + 08	0.184
1123.185	230236	4	319268	3	0.14	7.19E+09	-0.809
1123.358	233299	3 5	322317	2 5	-0.6	1.33E+09 9.24E+09	$0.725 \\ 0.761$
1123.376	213665	3	302682	4	-0.71	1.05E + 09	-0.846
1123.642	218171	1	307167	2	-0.5	1.69E + 09	-0.53
1124.388 1125.977	218171	3 1	306983	3 1	-0.87	5.23E+08	-0.440 0.478
1133.228	233299	5	321542	6	-0.72	9.93E + 08	-0.14
1137.831	227960	2	315846	2	-0.79	8.20E+08	-0.386
1139.401	233299 244671	5	332436	6	-0.55	1.31E+09 1.46E+09	-0.215
1141.884	230236	4	317811	3	-0.82	7.64E + 08	-0.631
1143.126	230331	3	317811	3	-0.79	8.35E+08	-0.313
1145.301 1145.701	214319 244753	4	332036	4	-0.92	6.17E+08	0.48
1151.654	245204	4	332036	4	-0.51	1.56E + 09	-0.542
1154.043	242530	3	329182	2	-0.91	6.18E+08	-0.4
1159.775	225859 243029	3 4	312083	3	-0.86	$5.93E \pm 08$	-0.396
1169.387	230331	3	315846	2	-0.76	8.31E + 08	0.309
1190.104	230236	4	314262	5	-0.11	3.61E+09	0.781
1204.567	230236	4 5	313253	5 4	-0.81	$7.13E \pm 08$ $7.58E \pm 08$	0.398
1215.068	233299	5	315599	4	-0.53	1.33E+09	-0.581
1216.847	230236	4	312416	5	-0.69	9.12E+08	-0.507
1223.221	230331 148861	3 4	312083 230331	3 3	-0.82 -0.56	0.79E+08 1.20E+09	0.306 -0.574
1228.304	250623	3	332036	4	-0.42	1.68E+09	-0.502
1228.876	148861	4	230236	4	-0.19	2.85E+09	0.613
1237.768	148904 197139	2	229694 277109	2	-0.76	7.49E+08 9.36E+08	-0.316 0.642
1258.666	197660	3	277109	3	0.2	6.59E + 09	-0.703
1258.97	243725	3	323155	4	-0.98	4.44E + 08	0.353
1259.049	152400 197139	1	231825 276546	2	-0.88	5.43E+08 6.41E+08	0.46
1263.954	196854	1	275970	2	-0.61	1.03E+09	0.762
1264.928	148904	2	227960	2	-0.7	8.13E+08	0.538
1268.524	197139 196854	2	275970 275673	2	-0.1 -0.23	3.26E+09 2.46E+09	-0.636 -0.745
1271.808	147930	1	226558	1	-1	4.18E + 08	-0.246
1273.327	197139	2	275673	1	-0.85	5.81E + 08	-0.448
1274.493	213535 139695	2	291997 218138	2	-0.92	4.95E+08 2.35E+09	-0.425 -0.749
1276.963	197660	3	275970	2	-0.92	4.91E + 08	-0.401
1277.857	148904	2	227160	1	-0.65	9.09E+08	0.403
1280.328	140066	2	218171 218138	1	-0.44 -0.85	1.46E+09 5.77E+08	-0.607 0.245
1282.803	139695	3	217650	2	-0.75	7.29E + 08	-0.277
1283.272	139695	3	217621	3	-0.43	1.51E + 09	-0.258
1283.517	218000 153376	5	295910 231216	4	-0.99	4.14E+08 $1.63E\pm09$	0.523 0.536
1289.401	140066	2	217621	3	-0.06	3.45E+09	0.757
1290.947	152232	3	229694	2	-0.32	1.93E+09	0.711
1291.061	140715 121930	1	218171 199202	4	-0.77	6.73E+08 5.09E+08	-0.356
1296.872	213665	3	290774	2	-0.76	6.97E + 08	-0.51
1298.066	153198	4	230236	4	-0.87	5.30E+08	-0.74
1298.573	139695 148861	3	216703 225859	2	-0.74 -0.98	7.36E+08 4 16E+08	-0.548
1299.805	140715	1	217650	2	-0.3	1.99E+09	0.646
1300.546	149667	1	226558	1	-0.84	5.74E + 08	-0.328
1301.407	156459	5	233299 197325	5 5	-0.49	1.14E+10 1.26E+09	-0.76
1309.406	151623	6	227993	6	0.51	1.26E + 10	-0.758
1309.783	155477	1	231825	0	-0.89	4.97E+08	-0.662
1310.298	153376 152302	2 5	229694 228480	25	-0.91	4.83E+08 1.07E+10	-0.258 -0.759
1315.999	140715	1	216703	2	-0.49	1.27E + 09	0.774
1318.117	153198	4	229064	4	0.35	8.62E+09	-0.808
1319.171 1319.409	197139 174831	2	272944 250623	3 3	-0.87 0.26	5.15E+08 7.04E+09	-0.825 -0.798
1320.313	155477	1	231216	1	-0.5	1.21E + 0.09	0.736
1320.519	152232	3	227960	2	-0.6	9.68E+08	-0.499
1321.152	152302 214319	5	227993 289642	6 4	-0.61	9.50E+08 4 74E+08	0.734
1328.348	153198	4	228480	5	-0.72	7.28E + 08	0.739
1329.593	214319	4	289530	3	-0.61	9.44E+08	-0.631
1335.012	220917 157536	э 2	293910 232442	4 1	-0.75	0.02E+08 2.93E+09	0.501 0.842
1335.533	170067	2	244943	1	-0.12	2.82E + 09	0.832
1337.125	218726	2	293514	3	-1	3.73E+08	-0.555
1337.624	201771 152400	2	270546 227160	2	-0.96	4.25E+09 4.06E+08	-0.798 0.262
1340.062	139695	3	214319	4	0.35	8.22E + 09	0.858
1340.747	170619	4	245204	4	-0.12	2.84E+09	-0.814
1341.65 1342.019	170278 222398	3 4	244813 296912	2 3	-0.02 -0.84	3.34E+09 5.36E+08	$0.741 \\ 0.438$
1342.725	170278	3	244753	4	0.12	4.92E + 09	0.838
1344.025	149667	1	224071	2	-0.69	7.42E+08	0.239
1344.979 1345.616	119632	2 5	244417 193948	3 6	-0.33 0.56	1.71E+09 1.32E+10	0.825 0.893
1347.391	155477	ĩ	229694	$\tilde{2}$	-0.83	5.35E + 08	-0.654
1347.722	201771	2	275970	2	-0.79	6.04E+08	0.435
1347.785 1348.81	$144749 \\170278$	4 3	218945 244417	4 3	0.07	4.28E+09 3.68E+09	-0.464 -0.568
1348.907	170619	4	244753	4	-0.26	2.03E+09	-0.336
			160				

Table A3: Continued

Wavelength	Lower Level	JLow	Upper level	JUp	log gf	gA	CF
1349.593 1350.156	$148904 \\ 144749$	2 4	223000 218815	3 5	-0.57	9.69E+08 1.81E+09	-0.385
1350.395	170619	4	244671	5	0.45	1.02E + 10	0.852
1351.258 1351.907	170067 130605	2	244072 213665	2	-0.04	3.34E+09 3.00E+09	-0.844
1352.565	144066	5	218000	5	0.34	7.99E+09	-0.749
1352.605	223623	3	297554	2	-0.98	3.83E+08	0.421
1352.935 1353.565	147737 144749	2	221650 218628	3	-0.18	2.41E+09 3.86E+08	-0.856 0.151
1353.709	152400	1	226271	2	-0.45	1.29E+09	0.335
1354.294	139695	3	213535	2	-0.8	5.77E+08	0.807
1354.595	145580 170619	3	219403 244417	3	-0.11	2.83E+09 1.20E+09	0.837 0.231
1355.309	153376	2	227160	1	-0.99	3.80E + 08	-0.574
1355.432	156459	5	230236	4	0.22	5.99E+09	0.815
1356.882	140715 170067	2	214413 243725	1	-0.6 -0.56	9.20E + 08 9.95E + 08	0.65
1358.71	140066	2	213665	3	-0.11	2.80E + 09	0.49
1359.897	147737	2	221272	1	-0.72	6.93E+08	-0.436
1361.122	140066 170278	2	213535 243725	2	-0.12	2.70E+09 4.23E+08	0.837 0.077
1362.019	120919	4	194339	5	0.43	9.69E + 09	0.895
1362.793	144066	5	217445	4	-0.42	1.37E+09	0.374
1363.05	145580	3 2	218945 213360	4	-0.26	$1.96E \pm 09$ $1.21E \pm 09$	0.863 0.793
1365.178	144749	4	218000	5	-0.35	1.62E + 09	0.853
1365.801	140715	1	213932	0	-0.63	8.33E+08	0.838
1365.865	120919 153376	4 2	194132 226558	3	-0.38	1.48E+09 4.78E+08	$0.214 \\ 0.328$
1366.94	121930	3	195086	2	-0.47	1.21E + 09	0.262
1366.957	152232	3	225387	4	0.38	8.64E+09	0.889
1367.123	145580	3	218726 195055	2	0.11	$4.59E \pm 09$ $8.16E \pm 09$	0.879 0.894
1367.607	119632	5	192753	4	-0.32	1.71E + 09	0.212
1367.871	170619	4	243725	3	0.12	4.65E+09	0.803
1308.901 1369.154	143380 148234	3 0	218028 221272	3 1	-0.73	5.00E+09 6.63E+08	-0.853 0.393
1369.478	122664	2	195684	1	-0.5	1.13E + 0.09	0.43
1371.078	149667	1	222603	2	-0.67	7.65E+08	-0.287
1372.352	122004 128343	2 4	201211	3	$0.25 \\ 0.12$	4.70E+09	$0.894 \\ 0.627$
1373.259	140715	1	213535	2	-0.63	8.23E + 08	0.328
1373.721	157536	2	230331	3	0.18	5.30E+09	0.846
1373.774 1374.548	170278	3	243029	4	-0.02	3.18E+0.09	0.86
1374.638	148904	2	221650	3	-0.01	3.46E + 09	0.587
1375.599	144749	4	217445	4	-0.15	2.49E+09	-0.85
1375.758 1376.322	123140 152302	5	224959	6	-0.24	4.44E+09 2.04E+09	0.893
1376.55	140715	1	213360	1	-0.6	8.81E + 08	0.375
1377.79	197660	3	270240	4	0.37	8.31E+09	0.858
1378.464	123140	1	195684	1	-0.08	1.47E+09	-0.76
1379.63	153376	2	225859	3	0.21	5.70E + 09	0.87
1379.638	155477	1	227960	2	-0.61	8.48E+08	-0.483
1380.009	122664	2	195086	2	-0.02	3.16E+09	-0.87
1381.027	170619	4	243029	4	0	3.50E + 09	0.851
1381.486	147930	1	220316	2	-0.87	4.67E+08	0.177
1383.12	130060	4 3	202361	2	-0.02	3.36E+09	0.838 0.671
1384.043	170278	3	242530	3	-0.17	2.34E + 09	0.812
1384.992	121930 157536	3	194132	3	0.13	4.68E+09 1.15E+09	-0.872 0.524
1385.840 1387.515	137550 149667	1	223034 221739	2	-0.48	2.85E+09	-0.324
1388.785	144066	5	216071	6	0.55	1.21E + 10	0.906
1390.094	147930	1	219867	0	-0.9	4.47E + 08 2 59E + 09	-0.447 0.851
1392.003	152232	3	224071	2	-0.13	3.64E+08	-0.789
1392.097	120919	4	192753	4	0.26	6.23E + 09	-0.88
1392.412	197139 170067	2	268956 241855	3	0.17	$5.08E \pm 09$ 9.83E \pm 08	0.767 -0.478
1395.033	155477	1	227160	1	-0.83	5.04E + 08	0.488
1395.276	152400	1	224071	2	-0.57	9.08E+08	-0.246
1395.323 1396.562	$144066 \\ 149667$	5 1	215734 221272	4 1	-0.89 -0.59	4.38E+08 8.66E+08	-0.407 0.672
1397.093	170278	3	241855	2	-0.55	9.54E + 08	-0.826
1400.325 1401.260	148904	2	220316	2	-0.95	3.77E+08	-0.218
1401.209 1402.587	192400 197660	3	268956	3	-0.33	1.59E+09 8.58E+08	0.833
1403.4	128343	4	199599	3	-0.33	1.58E + 09	-0.869
1405.033	201771	2	272944	3	0.24	5.82E+09	0.83
1405.432	130060	3	201211	∠ 3	-0.39	1.38E+09	-0.709
1405.639	131219	2	202361	2	-0.54	9.90E + 08	-0.832
1406.84 1407.125	155477 144066	1	226558 215133	$\frac{1}{4}$	-0.57 0.23	9.07E + 08 5 72E + 09	-0.411 0.876
1407.596	151623	6	222666	÷ 7	0.23	1.38E+10	0.919
1408.75	144749	4	215734	4	-0.5	1.06E + 09	0.584
1410.016	119632	5	190554	4	0.24	5.76E + 09	-0.875
1411.084	197139	2	268006	2	-0.64	7.61E + 08	0.795
1411.57	120919	4	191762	3	0.11	4.35E+09	-0.874
1412.206 1412.537	121930 155477	3	192741 226271	2	-0.06 -0.11	2.91E+09 2.56E+09	-0.874 -0.878
1413.016	122664	2	193434	1	-0.36	1.45E+09	-0.879
1413.04	144066	5	214835	5	-0.17	2.25E + 09	0.855
1413.062 1414.401	152232 147930	3	223000 218631	3 1	0.17	4.86E + 09 8 75E + 08	-0.858
1414.529	153376	2	224071	2	-0.28	1.77E+0.09	-0.664
1415.234	130060	3	200720	2	-0.52	1.01E+09	-0.871
$1416.804 \\ 1417.595$	201771 148861	2 4	272352 219403	1 3	-0.13 -0.09	2.45E+09 2.68E+09	0.822 0.736
1419.767	147737	2	218171	1	-0.89	4.25E + 08	-0.413
1419.954	153198	4	223623	3	0.21	5.33E+09	0.899
1419.983	157536	2	227960	2	-0.28	1.72E+09	-0.649
			101				

Table A3: Continued

Wavelength	Lower Level	JLow	Upper level	JUn	log gf	gA	CF
1420.434	147737	2	218138	3	-0.24	1.90E + 09	0.491
1420.509	148234	0	218631	1	-0.52	9.87E + 08	0.505
1420.781	144749	4	215133	4	-0.69	$6.69E \pm 08$	0.189
1421	174831	3	245204	4	0.2	$5.31E \pm 0.09$	0.9
1422.584	123140	1	193434	1	-0.44	$1.20E \pm 0.09$	-0.483
1423.98	152302	5	222527	5	-0.75	$5.92E \pm 0.08$	0.712
1424 455	152400	ĩ	222603	2	-0.56	$9.12E \pm 0.08$	0.355
1425 435	145580	3	215734	4	0.23	$5.62E \pm 0.09$	0.761
1426.58	147930	1	218028	2	-0.5	$1.02E \pm 0.09$	-0.374
1426.615	152302	5	220020	4	0.33	$7.01E \pm 0.00$	0.873
1420.015	132302	4	222396	-14 5	0.33	6.52E+09	0.873
1420.012	149793	4	214035	4	0.3	1.70E + 0.0	0.034
1420.000	199664	4	100741	4	-0.20	$1.79E \pm 0.0$	0.113
1420.998	122004	2	192741	2	-0.41	1.27E+09	-0.310
1426.949	174031	3	244615	4	-0.08	0.00E+00	0.870
1429.002	151623	6	221602	6	-0.6	8.12E+08	0.857
1429.515	148861	4	218815	5	0.37	7.64E+09	0.908
1430.169	174831	3	244753	4	-0.34	1.51E+09	-0.566
1430.175	196854	1	266775	0	-0.56	8.87E + 08	0.891
1430.349	147737	2	217650	2	-0.53	9.71E + 08	-0.722
1430.932	147737	2	217621	3	-0.31	1.59E + 09	-0.594
1431.928	128343	4	198179	4	0.35	7.32E + 09	-0.866
1432.008	121930	3	191762	3	-0.32	1.56E + 09	-0.26
1433.336	148861	4	218628	3	-0.28	1.71E + 09	0.585
1434.313	147930	1	217650	2	-0.56	8.85E + 08	-0.464
1436.062	120919	4	190554	4	-0.25	1.83E + 09	-0.259
1436.629	196854	1	266461	1	-0.82	4.92E + 08	-0.532
1437.755	145580	3	215133	4	-0.91	3.96E + 08	0.313
1438.052	130060	3	199599	3	0.11	4.15E + 09	-0.652
1438.82	131219	2	200720	2	-0.02	3.07E + 09	-0.696
1440 542	152232	3	221650	3	-0.68	$6.88E \pm 08$	-0.342
1442 204	152400	1	221739	2	-0.62	$7.73E \pm 0.8$	-0.27
1442 394	153198	4	2221103	5	0.43	$8.67E \pm 0.09$	0.86
1442.535	107130	2	266461	1	0.18	$2.10E \pm 0.00$	0.886
1442.000	152302	5	200401	6	-0.13	$2.10D \pm 0.00$ 8.58E ± 0.0	0.833
1443.004	152302	6	221002	5	0.43	8.58E+09	0.833
1445.12	101020	0	220917	0	0.44	6.76E+09	0.899
1443.751	131219	2	200483	3	0.23	5.44E + 09	0.88
1444.246	174831	3	244072	2	-0.42	1.24E + 09	-0.792
1444.377	148904	2	218138	3	-0.42	1.20E + 09	0.506
1444.527	153376	2	222603	2	-0.28	1.70E + 09	-0.555
1446.299	130060	3	199202	4	0.34	7.01E + 09	0.897
1446.366	148861	4	218000	5	-0.49	1.04E + 09	0.475
1446.678	148904	2	218028	2	-0.23	1.87E + 09	-0.604
1448.058	197139	2	266197	2	-0.83	4.67E + 08	-0.462
1449.66	128343	4	197325	5	0.4	7.98E + 09	0.897
1454.057	147930	1	216703	2	-0.47	1.07E + 09	0.633
1454.859	157536	2	226271	2	-0.81	4.88E + 08	0.37
1458.068	148861	4	217445	4	-0.08	2.61E + 09	-0.528
1459.066	197660	3	266197	2	0.08	3.72E + 09	0.887
1459.845	156459	5	224959	6	0.46	9.07E + 09	0.923
1459.873	147930	1	216429	0	-0.96	3.44E + 08	-0.869
1462.615	155477	1	223847	0	-0.91	3.93E + 08	0.766
1466.153	148904	2	217109	1	-0.48	1.03E + 09	-0.645
1466.327	174831	3	243029	4	-0.49	$1.02E \pm 0.09$	0.78
1468.776	152232	3	220316	2	-0.92	$3.72E \pm 0.08$	-0.602
1474 941	148904	2	216703	2	-0.91	$3.82E \pm 0.8$	-0.168
1482 753	149667	1	217109	1	-0.79	$4.94E \pm 0.8$	-0.42
1492 012	174831	3	241855	2	-0.16	2.10E+0.09	0 769
1405 367	1/8861	4	215734	4	0.78	4.08E±08	0.105
1407 865	140667	1	216/20	0	0.82	4.50E + 00 $4.50E \pm 08$	0.563
1497.809	147737	2	210423	1	0.52	4.00 ± 0.00	0.637
1499.112	147757	2	214413	1	-0.52	2.92E+08	0.037
1502.98	149961	4	224071	4	-0.89	3.82E+08	0.73
1508.951	146601	4	210100	4	-0.85	4.09E+08	0.297
1515.248	128343	4	194339	5	-0.53	8.49E+08	0.431
1515.735	148861	4	214835	5	-0.66	6.28E + 08	0.183
1535.087	156459	5	221602	6	-0.29	1.45E + 09	0.329
1538.589	130060	3	195055	4	-0.92	3.39E + 08	0.38
1551.08	152232	3	216703	2	-0.8	4.48E + 08	-0.811
1557.574	157536	2	221739	2	-0.94	3.18E + 08	0.36
1558.273	139695	3	203869	2	-0.14	2.01E + 09	0.926
1567.32	140066	2	203869	2	-0.39	1.13E + 09	-0.792
1583.433	140715	1	203869	2	-0.69	5.45E + 08	0.566
1600.356	156459	5	218945	4	-0.89	3.34E + 08	-0.617
1616.381	157536	2	219403	3	-0.81	3.98E + 08	0.613
1636.878	157536	2	218628	3	-0.98	2.61E + 08	0.63
1639.723	156459	5	217445	4	-0.38	1.03E + 09	0.737
1867.187	170067	2	223623	3	-0.98	2.02E + 08	-0.681
1884.748	139695	3	192753	4	-0.99	1.94E + 08	-0.864
1918.649	170278	3	222398	4	-0.89	2.34E + 08	-0.753
1988.151	170619	4	220917	5	-0.81	2.61E + 08	-0.83

Energy Levels

) -				
E^a_{exp}	E^{b}_{aala}	ΔE	J	Leading components (in $\%$) in LS coupling ^{c}
0	136	-136	4.5	$00.3d^{7.4}F$
1015 0	130	-130	4.0	99 50 F
1615.9	1715	-99	3.5	100 3d - F
2759.3	2840	-81	2.5	99 3d′ ⁴ F
3528.1	3596	-68	1.5	$99 \ 3d^7 \ ^4F$
20826.8	20622	205	2.5	99.3d ⁷ ⁴ P
21065.0	20052	114	1.5	01 3d7 4P \pm 8 3d7 2P
21005.3	20352	114	1.0	3150 1 ± 050 1
21935.1	21818	117	0.5	96 3d - P
22575.3	22345	230	4.5	$96 \ 3d'_{-2}G$
24099.8	23858	242	3.5	$99 \ 3d^7 \ ^2G$
27015.9	27397	-381	1.5	$76.3d^{7}{}^{2}P + 13.3d^{7}{}^{2}D + 8.3d^{7}{}^{4}P$
28366.6	28054	-587	0.5	06 3d7 2P
20300.0	20504	-367	0.0	100.017.21
30401.7	30561	-159	5.5	100 3d' ² H
30966	30512	454	2.5	$77 \ 3d' \ ^2D + 22 \ 3d' \ ^2D$
31823.4	31946	-123	4.5	97 3d ^{7 2} H
33292.4	32954	338	1.5	$67.3d^{7/2}D + 16.3d^{7/2}D + 16.3d^{7/2}P$
40400	40277	112	2.5	$00.247.2_{\rm F}$
49490	49377	113	2.0	99 50 F
50071.9	50070	2	3.5	99 3d' - F
76838.2	76962	-124	1.5	$80 \ 3d' \ ^2D + 19 \ 3d' \ ^2D$
77668	77725	-57	2.5	$77 \ 3d^7 \ ^2D + 22 \ 3d^7 \ ^2D$
187779.4	187825	-46	4.5	$99.3d^{6}(5D)4s^{6}D$
100020 7	188007	74	25	00.246(5D)4c.6D
100502.7	100000	-74	3.5	99 5d (5D)48 D
189586.9	189682	-95	2.5	99 3d°(5D)4s°D
190100.3	190210	-110	1.5	$99 \ 3d^{0}(5D)4s^{0}D$
190400.3	190520	-120	0.5	$99 \ 3d^{6}(5D)4s^{6}D$
199441.3	199411	30	3.5	$99.3d^{6}(5D)4s^{4}D$
200648.2	200665	17	25	$00.24^{6}(5D)/a^{4}D$
200048.2	200005	-17	2.0	99.50(5D)48
201412.8	201459	-46	1.5	$99 \ 3d^{\circ}(5D)4s^{-1}D$
201849.7	201913	-63	0.5	$99 \ 3d^{0}(5D)4s^{-4}D$
219203.4	219228	-25	2.5	$60 \ 3d^{6}(3P)4s^{4}P + 39 \ 3d^{6}(3P)4s^{4}P$
220207.8	220486	-278	6.5	$99.3d^{6}(3H)4s^{4}H$
220622.8	220820	107	5 5	$062d^{6}(2H)4a^{4}H$
220022.8	220820	-197	0.0	90.50(511)48 11 04.016(011)4.411 + 0.016(017)4.477 + 0.016(017)4.477
220938.1	221022	-84	4.5	$84 \ 3d^{\circ}(3H)4s^{-}H + 6 \ 3d^{\circ}(3F)4s^{-}F + 6 \ 3d^{\circ}(3G)4s^{-}G$
221271.9	221321	-49	3.5	$89 \ 3d^{0}(3H)4s^{-4}H$
221664.1	221818	-154	1.5	$56 \ 3d^{6}(3P)4s^{4}P + 35 \ 3d^{6}(3P)4s^{4}P$
222401.3	222321	80	4.5	$64 3d^{6}(3F)4s^{4}F + 19 3d^{6}(3F)4s^{4}F + 12 3d^{6}(3H)4s^{4}H$
222101.0	222021	76	25	60.246(2E)4c.4E + 10.246(2E)4c.4E + 7.246(2E)4c.4E
222885.1	222810	70	3.5	$59.54(3F)4s$ F $\mp 19.54(3F)4s$ F $\mp 7.54(5H)4s$ H
223214.2	223136	78	2.5	$76 \ 3d^{\circ}(3F)4s^{+}F + 19 \ 3d^{\circ}(3F)4s^{+}F$
223375.5	223571	-196	0.5	$60 \ 3d^{0}(3P)4s^{4}P + 37 \ 3d^{0}(3P)4s^{4}P$
223476.5	223428	49	1.5	$80 \ 3d^{6}(3F)4s^{4}F + 19 \ 3d^{6}(3F)4s^{4}F$
226310.8	226324	-13	5.5	$67.3d^{6}(3G)4s^{4}G + 30.3d^{6}(3H)4s^{2}H$
220010.0	220021	1.41	1 5	$(62)^{10} = (21)$
220000.0	227030	-141	1.5	50.50(3F)48F + 55.50(3F)48F + 5.50(3F)48F
227542.6	227577	-34	4.5	$66 3d^{\circ}(3G)4s^{-1}G + 25 3d^{\circ}(3H)4s^{-1}H + 5 3d^{\circ}(3F)4s^{-1}F$
227800.5	228027	-227	5.5	$68 \ 3d^{6}(3H)4s^{-2}H + 29 \ 3d^{6}(3G)4s^{-4}G$
228020.3	227952	68	3.5	$76 \ 3d^{6}(3G)4s^{4}G + 10 \ 3d^{6}(3F)4s^{2}F + 5 \ 3d^{6}(3F)4s^{4}F$
228047.5	228150	-103	4.5	$68.3d^{6}(3H)4s^{2}H + 24.3d^{6}(3G)4s^{4}G + 5.3d^{6}(3G)4s^{2}G$
22001110	220100	120	0.5	00 00
228105.5	221913	132	2.5	$65.50(3G)48$ G $\pm 10.50(3F)48$ F
229587.5	229420	168	3.5	$60 \ 3d^{\circ}(3F)4s^{2}F + 17 \ 3d^{\circ}(3F)4s^{2}F + 15 \ 3d^{\circ}(3G)4s^{4}G$
229773.6	229975	-201	0.5	58 3d ⁶ (3P)4s ² P + 36 3d ⁶ (3P)4s ² P
230531.7	230526	6	2.5	$70 \ 3d^{6}(3F)4s^{2}F + 17 \ 3d^{6}(3F)4s^{2}F + 13 \ 3d^{6}(3G)4s^{4}G$
234036.4	234037	-1	4.5	$94.3d^{6}(3G)4s^{2}G$
225052.5	225044	0	25	$022d^{6}(2C)4a^{2}C + 52d^{6}(2E)4a^{2}E$
200002.0	2005550	407	0.0	35.50(30)48 + 5.50(31)48 + 5.50(31)48
236039.8	235553	487	1.5	98 3d [*] (3D)4s ⁻ D
236058.9	235609	450	2.5	$98 \ 3d^{0}(3D)4s^{4}D$
236108.8	235599	510	0.5	$98 \ 3d^{6}(3D)4s^{4}D$
236331.2	235900	431	3.5	$99 \ 3d^{6}(3D)4s^{4}D$
238233 6	238377	-143	6.5	$00.3d^6(11)/e^2$
238235.0	200011	-145	0.0	35 50 (11)45 1
238305.2	238426	-121	5.5	98 3d (11)4s 1
239540.9	238438	1103	4.5	$63 \ 3d^{\circ}(1G)4s^{-2}G + 32 \ 3d^{\circ}(1G)4s^{-2}G$
239614.5	238499	1116	3.5	$63 \ 3d^{6}(1G)4s^{2}G + 32 \ 3d^{6}(1G)4s^{2}G$
243140.4	242661	479	2.5	97 3d ⁶ (3D)4s ² D
246476 5	247554	-1078	2.5	$75 3d^{6}(1D)4s^{2}D + 21 3d^{6}(1D)4s^{2}D$
246624.2	241004	1007	1 5	74.246(1D)/42D + 20.246(1D)/42D
240024.3	24/031	-1007	G.1	14 Ju (1D)48 D + 20 Ju (1D)48 D
256272.5	256475	-203	3.5	96 3d (1F)4s "F
256272.9	256496	-223	2.5	96 3d ^o (1F)4s ² F
265691.5	265657	35	1.5	$80 \ 3d^{6}(3F)4s^{4}F + 19 \ 3d^{6}(3F)4s^{4}F$
265752.4	265730	22	4.5	77 $3d^{6}(3F)4s^{4}F + 22 3d^{6}(3F)4s^{4}F$
265996	265991	 K	2.5	$78 3d^{6}(3F)/c 4F \pm 10 3d^{6}(2F)/c 4F$
200000	203001	ں ب	2.0	76.916(3F) 4.4F + 90.916(3F) 4.4F
265975	265980	-5	3.5	$70 \ 3d^{\circ}(3F)4s^{\circ}F + 20 \ 3d^{\circ}(3F)4s^{\circ}F$
272755.1	272606	149	3.5	76 3d°(3F)4s ${}^{2}F + 21$ 3d°(3F)4s ${}^{2}F$
272800.8	272670	131	2.5	79 $3d^{6}(3F)4s^{2}F + 20 3d^{6}(3F)4s^{2}F$
278281.8	278581	-299	4.5	$65 \ 3d^{6}(1G)4s^{2}G + 34 \ 3d^{6}(1G)4s^{2}G$
278201.0	278641	_261	3 5	$64 3d^{6}(1C)/a^{2}C + 33 3d^{6}(1C)/a^{2}C$
210300	210041	-201	5.5	04 04 (10)48 G T 33 34 (10)48 G

Table A4: Comparison between available experimental data and calculated even energy levels (in $\rm cm^{-1})$ in Cu V

a: Experimental energies from [30] b: This work c: Only the components ≥ to 5% are given

Table A5: Comparison between available experimental data and calculated odd energy levels (in cm⁻¹) in Cu V

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E^a_{exp}	E_{calc}^{o}	ΔE	J	Leading components (in $\%$) in LS coupling ^{c}
266226 7	266263	-36	4.5	$97.3d^{6}(5D)4p^{6}D$
200220.1	200203	-30	4.0	
266560	266652	-92	3.5	94 3d ^o (5D)4p ^o D
267068.8	267218	-149	2.5	96 3d ⁶ (5D)4p ⁶ D
267488 7	267680	_101	15	08 3d ⁶ (5D)/n ⁶ D
201400.1	207080	-131	1.0	38 54 (5D)4p D
267759	267975	-216	0.5	$99 \ 3d^{\circ}(5D)4p^{\circ}D$
274003.9	273786	218	5.5	$99 \ 3d^{6}(5D)4p^{6}F$
274064 5	272805	170	4.5	$(2.246(5D)/a^{-6}E + 5.246(5D)/a^{-4}E$
274004.5	213895	170	4.0	$32.30(3D)4p$ r $\pm 3.30(3D)4p$ r
274073.2	273952	121	3.5	$89 \ 3d^{\circ}(5D)4p^{\circ}F$
274146.2	274061	85	2.5	$92 \ 3d^{6}(5D)4p^{6}F$
074100 5	074107	60	1 5	04.916(FD) 4.6E
274188.5	2/412/	02	1.5	94 5d (5D)4p F
274209.7	274160	50	0.5	$95 \ 3d^{\circ}(5D)4p^{\circ}F$
276368	276236	132	3.5	$77 3d^{6}(5D)4p ^{6}P \pm 15 3d^{6}(5D)4p ^{4}D$
210000	270200	102	0.0	$70 \circ 10(5) 10^{-1} + 10 \circ 10(5) 10^{-1} = 10$
278294.6	278210	85	2.5	$79 3d^{\circ}(5D)4p^{\circ}P + 16 3d^{\circ}(5D)4p^{\circ}D$
278663.1	278601	62	3.5	$77 \ 3d^{6}(5D)4p^{-4}D + 18 \ 3d^{6}(5D)4p^{-6}P$
279421-1	279246	175	4.5	92 $3d^{6}(5D)4p$ $^{4}F + 6 3d^{6}(5D)4p$ ^{6}F
0704000	210210	10	2.0	r = 0.16(r p) + 4p + 10.0.16(r p) + 6p
279496.8	279479	18	2.5	$75 3d^{\circ}(5D)4p^{-2}D + 19 3d^{\circ}(5D)4p^{-2}P$
279589.5	279530	60	1.5	$84 \ 3d^{6}(5D)4p^{6}P + 13 \ 3d^{6}(5D)4p^{4}D$
280065 7	280080	-14	15	$78 3d^{6}(5D)4p 4D + 14 3d^{6}(5D)4p 6P$
280003.7	280080	-14	1.0	$(35)^{4}$
280373.3	280427	-54	0.5	91 3d ^o (5D)4p [*] D
280928.7	280810	119	3.5	$93 \ 3d^{6}(5D)4p^{4}F + 5 \ 3d^{6}(5D)4p^{6}F$
281042 4	201052	00	25	05.246(5D)4p.4F
201942.4	201002	90	2.0	35 50 (5D)4p F
282621.5	282550	72	1.5	$96 \ 3d^{\circ}(5D)4p^{-4}F$
284520.9	284782	-261	2.5	$96.3d^{6}(5D)4p^{4}P$
201020.0	005041	201	1 5	$65.04(62)10^{-1}$
285546.4	285841	-295	1.5	97.3d (5D)4p P
286068.7	286393	-324	0.5	97 3d ^o (5D)4p ⁴ P
300401.2	300616	-215	5.5	$65 3d^{6}(3H)4p {}^{4}G + 22 3d^{6}(3F)4p {}^{4}G + 8 3d^{6}(3G)4p {}^{4}G$
200827 1	200700	210	4 5	20.246(211)4 - 40 + 22.26(217)4 - 40 + 10.216(201)4 - 40
300837.1	300768	69	4.5	$30 3u^{\circ}(3H)4p - G + 25 3d^{\circ}(3F)4p - G + 10 3d^{\circ}(3G)4p + G$
301080.5	301048	33	2.5	$24 \ 3d^{6}(3P)4p \ ^{4}P + 22 \ 3d^{6}(3P)4p \ 4P + 10 \ 3d^{6}(3P)4p \ ^{4}D$
301255 4	301141	114	2 5	$27 3d^{6}(3E)4p 4G \pm 21 3d^{6}(3E)4p 4G \pm 11 2d^{6}(2G)4 = 4G$
001200.4	001141	114	5.5	2100 (01)4p = 41 + 02 236 (01)4p = 41 = 0 (00)4p = 6
301286.4	301317	-31	5.5	$50 \ 3d^{\circ}(3H)4p^{-1}H + 32 \ 3d^{\circ}(3H)4p^{-1}H + 11 \ 3d^{\circ}(3G)4p^{-4}H$
301336.1	301490	-154	6.5	49 $3d^{6}(3H)4p^{4}I + 34 3d^{6}(3H)4p^{4}H + 10 3d^{6}(3H)4p^{2}I$
201205.0	201500	101	4 5	25 216(211)4 41 + 20 216(211)4 411 + 10 216(211)4 40
301385.0	301509	-123	4.0	$35 3d^{-}(3H)4p^{-}I + 29 3d^{-}(3H)4p^{-}H + 18 3d^{-}(3H)4p^{-}G$
301533.4	301520	13	2.5	$43 \ 3d^{\circ}(3F)4p \ {}^{4}G + 34 \ 3d^{\circ}(3H)4p \ {}^{4}G + 7 \ 3d^{\circ}(3G)4p \ {}^{4}G$
301586 7	301667	-80	3.5	$26 3d^{6}(3H)4p ^{4}H + 20 3d^{6}(3H)4p ^{4}G + 17 3d^{6}(3H)4p ^{2}G$
001000110	001001	100	0.0	44 + 36(6R) + 4R + 40 + 36(6R) + 4R
302961.2	303061	-100	0.5	$44 \ 3d^{\circ}(3P)4p^{-}P + 42 \ 3d^{\circ}(3P)4p^{-}P$
302980.4	302984	-4	4.5	$43 \ 3d^{6}(3H)4p^{4}I + 16 \ 3d^{6}(3H)4p^{2}G + 13 \ 3d^{6}(3H)4p^{4}H$
303200 3	303251	-42	35	$20.3d^{6}(3H)4p^{4}H \pm 17.3d^{6}(3F)4p^{4}F$
303203.3	303231	-42	0.0	$20.50(51)$ 4p $11 \pm 17.50(51)$ 4p 1
303241.7	303153	89	2.5	$28 \text{ 3d}^{\circ}(3P)4p \ ^{\circ}D + 19 \text{ 3d}^{\circ}(3P)4p \ ^{\circ}P + 19 \text{ 3d}^{\circ}(3P)4p \ ^{\circ}D$
303456.4	303417	39	7.5	$99 \ 3d^{6}(3H)4p^{4}I$
202470 1	202505	26	25	47246(2E)454E = 16246(2E)454E = 8246(2E)454E
303479.1	303303	-20	2.0	47.50(3F)4p F $+ 10.50(3F)4p$ F $+ 0.50(3E)4p$ F
303679.5	303754	-75	1.5	$60 \ 3d^{\circ}(3F)4p \ {}^{4}F + 20 \ 3d^{\circ}(3F)4p \ {}^{4}F + 11 \ 3d^{\circ}(3D)4p \ {}^{4}F$
303734.1	303801	-67	1.5	$23 \ 3d^{6}(3P)4p^{4}S + 21 \ 3d^{6}(3P)4p^{4}D + 7 \ 3d^{6}(3P)4p^{2}D$
202021 7	204054	100		42.216(211)4 $411 + 40.216(211)4$ $41 + 7.216(20)4$ 411
303931.7	304054	-122	5.5	$43 3d^{\circ}(3H)4p H + 42 3d^{\circ}(3H)4p I + 7 3d^{\circ}(3G)4p H$
304062.3	304286	-224	6.5	$53 \ 3d^{0}(3H)4p^{4}H + 34 \ 3d^{0}(3H)4p^{4}I + 7 \ 3d^{0}(3G)4p^{4}H$
304092.2	304129	-37	4.5	44 $3d^{6}(3F)4p^{4}F + 17 3d^{6}(3F)4p^{4}F + 10 3d^{6}(3H)4p^{4}G$
204100	204174	05	2.0	$4C_{21}b(2D) 4 + 4D + 07_{21}b(2D) 4 + 4D + 7_{21}b(2D) 4 + 4U$
304199	304174	25	3.5	$46 \ 3d^{\circ}(3P)4p^{-1}D + 27 \ 3d^{\circ}(3P)4p^{-1}D + 7 \ 3d^{\circ}(3H)4p^{-1}H$
304456.1	304732	-276	4.5	$38 \ 3d^{6}(3H)4p^{-2}G + 21 \ 3d^{6}(3H)4p^{-4}H + 12 \ 3d^{6}(3G)4p^{-2}G$
304655	304739	-84	3.5	$20.3d^{6}(3H)4p^{2}G \pm 19.3d^{6}(3E)4p^{4}E \pm 10.3d^{6}(3H)4p^{4}G$
004000	004105	04	0.0	20001(01)4p = 0 + 15001(01)4p = 1 + 10001(01)4p = 0
305453.3	305657	-204	3.5	$41 \ 3d^{\circ}(3F)4p^{-1}D + 13 \ 3d^{\circ}(3H)4p^{-2}G + 9 \ 3d^{\circ}(3F)4p^{-1}D$
305844.4	306031	-187	1.5	$16 \ 3d^{6}(3P)4p^{4}P + 16 \ 3d^{6}(3P)4p^{4}P + 14 \ 3d^{6}(3P)4p^{2}D$
305882 7	305838	45	65	70 $3d^{6}(3H)4p^{2}I \pm 16 3d^{6}(3H)4p^{4}I$
303002.1	303838	40	0.5	$(31)^{4}p + (31)^{4}p + (31)$
306115.6	306249	-133	2.5	$49 \ 3d^{\circ}(3F)4p \ ^{4}D + 10 \ 3d^{\circ}(3F)4p \ ^{4}D + 10 \ 3d^{\circ}(3D)4p \ ^{4}D$
306678.1	306886	-208	1.5	$55 \ 3d^{6}(3F)4p^{4}D + 11 \ 3d^{6}(3D)4p^{4}D + 11 \ 3d^{6}(3F)4p^{4}D$
206802.2	206715	177	55	$74246(2H)4p^{2}I + 5246(2F)4p^{4}C + 5246(2H)4p^{4}I$
300892.2	300715	177	5.5	$(4 \text{ of } (3\pi)^4\text{p} + 3 \text{ of } (3\pi)^4\text{p} + 3 \text{ of } (3\pi)^4\text{p} + 1$
306905.8	307159	-253	2.5	$37 \ 3d^{0}(3P)4p^{4}D + 18 \ 3d^{0}(3P)4p^{4}D + 8 \ 3d^{0}(3F)4p^{4}D$
306989-1	307210	-221	0.5	$63.3d^{6}(3F)4p^{4}D + 14.3d^{6}(3D)4p^{4}D + 11.3d^{6}(3F)4p^{4}D$
207120.0	207400	0.07	1 5	(0, 0) = 0
307138.8	307406	-267	1.5	$24 3d^{\circ}(3P)4p^{\circ}D + 14 3d^{\circ}(3P)4p^{\circ}D + 10 3d^{\circ}(3P)4p^{\circ}D$
307824.5	307669	156	4.5	$28 \ 3d^{\circ}(3F)4p \ {}^{4}G + 16 \ 3d^{\circ}(3H)4p \ {}^{4}G + 13 \ 3d^{\circ}(3F)4p \ {}^{2}G$
307909.5	307805	105	2.5	$24 \ 3d^{6}(3F)4p^{2}F + 14 \ 3d^{6}(3G)4p^{4}G + 14 \ 3d^{6}(3H)4p^{4}G$
207000 7	207071	20	2 5	24246(2E)4 = 4C + 17246(2E)4 = 4C + 11246(2E)4 = 2E
307990.7	307971	20	3.5	$24 3d^{\circ}(3F)4p^{\circ}G + 17 3d^{\circ}(3H)4p^{\circ}G + 11 3d^{\circ}(3F)4p^{\circ}F$
308064.9	308024	41	5.5	$47 \ 3d^{6}(3F)4p^{4}G + 14 \ 3d^{6}(3F)4p^{4}G + 13 \ 3d^{6}(3H)4p^{2}I$
308817.8	308845	-27	4.5	$53 \ 3d^{6}(3G)4p^{4}F + 23 \ 3d^{6}(3G)4p^{4}G + 7 \ 3d^{6}(3D)4p^{4}F$
200000 1	200400			21 216(20) 4 211 + 25 216(20) 4 40 + 12 216(21) 4 411
309269.1	309498	-229	5.5	$31 3d^{\circ}(3G)4p^{\circ}H + 25 3d^{\circ}(3G)4p^{\circ}G + 13 3d^{\circ}(3H)4p^{\circ}H$
309294.1	309129	165	3.5	$22 \ 3d^{\circ}(3F)4p^{-2}F + 14 \ 3d^{\circ}(3H)4p^{-4}G + 12 \ 3d^{\circ}(3F)4p^{-2}F$
309569.9	309249	321	2.5	$33 \ 3d^{6}(3H)4p^{4}G + 16 \ 3d^{6}(3F)4p^{4}G + 10 \ 3d^{6}(3F)4p^{4}G$
200702.0	200001	100	0.5	$20 2d^{6}(2D) 4p^{2}D + 0r^{2}d^{6}(2D) 4p^{2}D + 10 2d^{6}(2D) 4p^{2}C$
309702.9	209831	-128	0.5	$20 \text{ su} (3r)4p r + 20 \text{ su} (3r)4p P + 18 \text{ su}^2(3P)4p ^2\text{ su}$
309772	309710	62	4.5	$26 \ 3d^{\circ}(3F)4p^{-2}G + 22 \ 3d^{\circ}(3G)4p^{-2}H + 13 \ 3d^{\circ}(3F)4p^{-4}G$
309801.3	309738	63	3.5	40 $3d^{6}(3G)4p^{4}F + 36 3d^{6}(3G)4p^{4}G + 5 3d^{6}(3F)4p^{4}F$
210450.4	210022	400	1.0	49.246(2P) 4 = 2P + 20.246(2P) 4 = 2P + 5.26(2P) 4 = 4P
310450.4	310932	-482	1.5	$42 \ 3a^{\circ}(3P)4p^{-}P + 30 \ 3d^{\circ}(3P)4p^{-}P + 5 \ 3d^{\circ}(3G)4p^{-}F$
310483.1	310472	11	5.5	$45 \ 3d^{6}(3G)4p \ {}^{4}G + 17 \ 3d^{6}(3H)4p \ {}^{2}H + 14 \ 3d^{6}(3H)4p \ {}^{4}G$
310753.8	310708	46	2.5	$32.3d^{6}(3G)4p^{4}F + 31.3d^{6}(3G)4p^{4}C + 8.3d^{6}(2F)4p^{2}F$
01000.0	0100	-10	2.0	2 or $(3 $ $3 $ $2 $ $7 $ $7 $ $3 $ $3 $ $3 $ $3 $ $3 $ 3
310874.9	310872	3	4.5	21 $3d^{\circ}(3F)4p = G + 13 3d^{\circ}(3H)4p = H + 5 3d^{\circ}(3F)4p = G$
311220.3	310952	268	3.5	$55 \ 3d^{6}(3F)4p^{2}G + 13 \ 3d^{6}(3F)4p^{2}G + 8 \ 3d^{6}(3F)4p^{4}G$
211020.0	211007	_ 50 _ 6 4	1 -	20.246(2C)4p.4C + 16.246(2T)4-2TT + 10.246(2T)4-4C
311232.9	311297	-04	4.0	33 34 (3G)4p G + 10 34 (3H)4p H + 10 3G (3H)4p G
311582.4	311651	-69	3.5	$39 \ 3d^{\circ}(3G)4p \ {}^{4}G + 24 \ 3d^{\circ}(3G)4p \ {}^{4}F + 9 \ 3d^{\circ}(3D)4p \ {}^{4}F$
311706.3	311627	79	1.5	$57 \ 3d^{6}(3G)4p \ {}^{4}F + 17 \ 3d^{6}(3D)4p \ {}^{4}F + 6 \ 3d^{6}(3P)4p \ {}^{2}D$
211027.0	911705	70	0.5	27.246(2C)4p.4C + 20.246(2C)4-4p + 11.246(2p)4-4p
311837.8	311765	73	2.5	$37.3 a^{(3G)}4p^{-G} + 29.3 a^{(3G)}4p^{-F} + 11.3 a^{(3D)}4p^{-F}$
311888.8	311877	12	6.5	82 3d ^o (3G)4p ⁴ H + 13 3d ^o (3H)4p ⁴ H
311082	312200	-227	0.5	49 3d ⁶ (3P)4p ${}^{2}S + 22$ 3d ⁶ (3P)4p ${}^{2}S \pm 0$ 3d ⁶ (3P)4p ${}^{2}D$
011002	012209	- 441	0.0	-35 or (31) $+p$ $5 + 22$ or (31) $+p$ $5 + 3$ or (31) $+p$ F
312073.1	312087	-14	3.5	$64 \ 3d^{\circ}(3G)4p \ H + 14 \ 3d^{\circ}(3H)4p \ H + 7 \ 3d^{\circ}(3F)4p \ G$
312105.5	312128	-23	5.5	$66 \ 3d^{6}(3G)4p^{4}H + 14 \ 3d^{6}(3H)4p^{2}H + 7 \ 3d^{6}(3H)4p^{4}H$
310100	310100	16	4 5	$65 3d^{6}(3C)/p 4H \pm 10 3d^{6}(2H)/p 4H \pm 9 3d^{6}(2H)/a 2H$
312138	312122	10	4.0	10 30 (30) 4p 11 + 10 30 (31) 4p H + 8 30 (31) 4p H
314237.9	314264	-26	2.5	$59 \ 3d^{\circ}(3F)4p^{2}D + 10 \ 3d^{\circ}(3P)4p^{2}D + 8 \ 3d^{\circ}(3F)4p^{2}D$
314988	315060	-72	1.5	$61 \ 3d^{6}(3F)4p^{2}D + 16 \ 3d^{6}(3P)4p^{2}D + 6 \ 3d^{6}(3P)4p^{2}D$
910104	210405	0.00	2.0	20.246(20)4-2E+0.0216(2D)4-2E+10.026(2D)4-2E
316134	316427	-293	2.5	$33 3 a^{(3G)4p} F + 22 3 a^{(3D)4p} F + 10 3 a^{(1D)4p} F$
316149.4	316217	-68	5.5	51 3d ^o (3H)4p ² H + 37 3d ^o (3G)4p ² H
316642.6	316833	-190	3 5	$45.3d^{6}(3G)4p^{2}F + 21.3d^{6}(3D)4p^{2}F + 9.3d^{6}(3F)4p^{2}F$
0170011	017040	150	0.0	$10.04 (00)_{\text{TP}} = 1.21.04 (0D)_{\text{TP}} = 7.9.04 (0T)_{\text{TP}} $
317201.1	317043	158	4.5	$32 3a^{\circ}(3G)4p^{-}H + 31 3d^{\circ}(3H)4p^{-}H + 6 3d^{\circ}(3G)4p^{-}G$
317240.4	317272	-32	6.5	96 3d ⁶ (1I)4p ² K
318022.1	318600	224	25	$84.3d^{6}(3D)4p^{4}P$
0100010	010112	101	2.0	(1, 2, 1)
319304.2	319143	101	3.5	$\sigma_{1} \sigma_{2} \sigma_{3} \sigma_{1} \sigma_{2} \sigma_{2} \sigma_{1} \sigma_{2} \sigma_{2} \sigma_{2} \sigma_{1} \sigma_{2} \sigma_{2$

1	6	5
_1	. U	J

E^{a}_{exp}	E^{b}_{calc}	ΔE	J	Leading components (in %) in LS coupling c
319404.1	319180	224	1.5	$67 \ 3d^{6}(3D)4p \ ^{4}P + 11 \ 3d^{6}(3D)4p \ ^{2}P + 8 \ 3d^{6}(3D)4p \ ^{4}D$
319407.6	319379	29	7.5	99 $3d^{6}(1I)4p^{2}K$
319418.8	318815	604	4.5	$42 \ 3d^{6}(1G)4p^{2}H + 19 \ 3d^{6}(1G)4p^{2}H + 13 \ 3d^{6}(3G)4p^{2}H$
319689	319707	-18	4.5	$64 \ 3d^{6}(3G)4p^{2}G + 16 \ 3d^{6}(3H)4p^{2}G + 10 \ 3d^{6}(3H)4p^{2}H$
319951.5	319765	187	5.5	$42 \ 3d^{\circ}(11)4p^{-2}H + 32 \ 3d^{\circ}(1G)4p^{-2}H + 9 \ 3d^{\circ}(1G)4p^{-2}H$
320216.4	320024	192	0.5	$43 \ 3d^{\circ}(3D)4p^{-1}P + 24 \ 3d^{\circ}(3D)4p^{-1}D + 17 \ 3d^{\circ}(3D)4p^{-2}P$ $47 \ 3d^{\circ}(3D)4- \frac{4}{7}P + 10 \ 3d^{\circ}(3D)4- \frac{4}{7}P + 16 \ 3d^{\circ}(3D)4- \frac{2}{7}P$
320935.3	320671	204	0.5	$47.3d^{-}(3D)4p^{-}P + 19.3d^{-}(3D)4p^{-}D + 16.3d^{-}(3D)4p^{-}P$
321074	320733	225	2.5	$40 \ 3d^{6}(3D)4p^{-4}F + 20 \ 3d^{6}(3C)4p^{-4}F + 13 \ 3d^{6}(3D)4p^{-4}D$
321304.3	320082	451	3.5	49 50 $^{(3D)4p}$ 17 $^{+}$ 20 50 $^{(3C)4p}$ 17 $^{+}$ 13 50 $^{(3D)4p}$ 16 16 $^{16)4p}$ 2 16 $^{16)4p}$ 16 16 16 $^{16)4p}$ 16
321443 1	321034	409	1.5	$30 3d^{6}(3D)4p^{2}P + 18 3d^{6}(3D)4p 4P + 18 3d^{6}(3D)4p^{4}D$
321795.8	321587	209	3.5	$26 \ 3d^{6}(3D)4p^{4}D + 16 \ 3d^{6}(1G)4p^{2}G + 11 \ 3d^{6}(3H)4p^{2}G$
322192.1	321878	314	2.5	$64 \ 3d^{6}(3D)4p \ ^{4}D + 16 \ 3d^{6}(3D)4p \ ^{4}F + 7 \ 3d^{6}(3F)4p \ ^{4}D$
322375.9	321553	823	4.5	$49 \ 3d^{6}(1G)4p^{2}G + 22 \ 3d^{6}(1G)4p^{2}G + 8 \ 3d^{6}(1G)4p^{2}H$
322464.1	321921	543	3.5	$55 \ 3d^{6}(3D)4p \ {}^{4}F + 12 \ 3d^{6}(3G)4p \ {}^{4}F + 11 \ 3d^{6}(1G)4p \ {}^{2}F$
322470	322037	433	1.5	46 $3d^{6}(3D)4p^{4}D + 30 3d^{6}(3D)4p^{2}P + 7 3d^{6}(1S)4p^{2}P$
322569	322293	276	0.5	$35 \ 3d^{6}(3D)4p^{4}D + 30 \ 3d^{6}(3D)4p^{2}P + 12 \ 3d^{6}(1S)4p^{2}P$
322744.4	322544	200	3.5	$45 \ 3d^{\circ}(3D)4p \ ^{4}D + 13 \ 3d^{\circ}(1G)4p \ ^{2}F + 7 \ 3d^{\circ}(3F)4p \ ^{4}D$
322875.8	322434	442	4.5	$77 \ 3d^{\circ}(3D)4p^{4}F + 14 \ 3d^{\circ}(3G)4p^{4}F$
323222.4	322958	264	2.5	$34 \ 3d^{\circ}(1G)4p^{-}F^{+} + 16 \ 3d^{\circ}(3G)4p^{-}F^{+} + 16 \ 3d^{\circ}(1G)4p^{-}F^{-}$
323616.8	322762	-145	0.0 4.5	29 3d (1G)4p H + 28 3d (11)4p H + 20 3d (1G)4p H 70 3d ⁶ (11)4p ² H + 10 3d ⁶ (3C)4p ² H + 9 3d ⁶ (1G)4p ² H
323010.8	323702	- 226	4.5	$^{0.5d}(11)_{4p}^{-11} + ^{10.5d}(33)_{4p}^{-11} + ^{9.5d}(13)_{4p}^{-11}$
324668.3	324824	-156	5.5	$87 3d^{6}(1I)4p^{-2}I + 9 3d^{6}(1I)4p^{-2}H$
324908.8	324866	43	1.5	$70 \ 3d^{6}(3D)4p^{2}D + 8 \ 3d^{6}(1D)4p^{2}P + 6 \ 3d^{6}(1F)4p^{2}D$
325518.5	325443	76	2.5	$84 \ 3d^{6}(3D)4p^{-2}D$
325923.4	325688	235	1.5	$32 \ 3d^{6}(1S)4p^{2}P + 20 \ 3d^{6}(1D)4p^{2}P + 12 \ 3d^{6}(3D)4p^{2}D$
326477.1	326236	241	3.5	$64 \ 3d^{6}(3D)4p^{2}F + 11 \ 3d^{6}(1D)4p^{2}F + 7 \ 3d^{6}(3G)4p^{2}F$
327268	327269	-1	2.5	$57 \ 3d^{6}(3D)4p^{2}F + 14 \ 3d^{6}(1D)4p^{2}F + 7 \ 3d^{6}(1G)4p^{2}F$
327379.7	326541	839	0.5	$40 \ 3d^{6}(1S)4p^{2}P + 25 \ 3d^{6}(3D)4p^{2}P + 12 \ 3d^{6}(1S)4p^{2}P$
329339.6	329710	-370	2.5	$25 \ 3d^{\circ}(1D)4p^{-2}D + 24 \ 3d^{\circ}(1D)4p^{-2}F + 11 \ 3d^{\circ}(1F)4p^{-2}D$
329960.8	330412	-451	1.5	$50 \ 3d^{\circ}(1D)4p^{-}D + 12 \ 3d^{\circ}(1F)4p^{-}D + 10 \ 3d^{\circ}(1D)4p^{-}D$
330705.1 221252.6	331371	-606	2.5	$30 \ 30^{\circ} (1D) 4p \ D + 23 \ 30^{\circ} (1D) 4p \ F + 18 \ 30^{\circ} (1F) 4p \ D$ $58 \ 24^{6} (1D) 4p \ ^{2}P + 22 \ 24^{6} (1D) 4p \ ^{2}P + 0 \ 24^{6} (1S) 4p \ ^{2}P$
331333.0	3321011	-237 -673	3.5	56 3d (1D)4p T + 22 3d (1D)4p T + 9 3d (13)4p T $54 3d^{6}(1D)4p ^{2}F + 14 3d^{6}(1D)4p ^{2}F + 9 3d^{6}(3G)4p ^{2}F$
332946.3	332577	369	1.5	$32 \ 3d^{6}(1D)4p^{2}P + 17 \ 3d^{6}(1S)4p^{2}P + 14 \ 3d^{6}(1D)4p^{2}D$
335935.2	336160	-225	3.5	$87 \ 3d^{6}(1F)4p^{2}G$
338015.8	338917	-901	2.5	$48 \ 3d^{6}(1F)4p^{2}D + 20 \ 3d^{6}(1D)4p^{2}D + 6 \ 3d^{6}(1D)4p^{2}D$
338059.3	338289	-230	4.5	$92 \ 3d^6(1F)4p^2G$
339377.8	339843	-465	1.5	$28 \ 3d_{0}^{6}(3F)4p_{4}^{4}D + 22 \ 3d_{0}^{6}(3P)4p_{4}^{4}D + 22 \ 3d_{0}^{6}(1F)4p_{4}^{2}D$
339845.5	339817	29	0.5	$38 3d^{0}(3P)4p^{4}D + 35 3d^{0}(3F)4p^{4}D + 17 3d^{0}(3P)4p^{4}D$
340482.7	340952	-469	1.5	$53 3d^{\circ}(1F)4p^{-}D + 13 3d^{\circ}(3P)4p^{-}D + 10 3d^{\circ}(3F)4p^{-}D$
340722.8	340840	-78	2.5	$59.3d^{(3F)4p} D + 28.3d^{(3F)4p} D + 13.3d^{(3F)4p} D$ $52.3d^{6}(3F)4p^{4}D + 22.3d^{6}(3P)4p^{4}D + 11.3d^{6}(3F)4p^{4}D$
343301.1	343466	-165	2.5	$80 \ 3d^{6}(1F)4p^{-2}F + 5 \ 3d^{6}(1F)4p^{-2}D + 5 \ 3d^{6}(1G)4p^{-2}F$
343337.2	343465	-128	3.5	$81 \ 3d^6(1F)4p^2F + 5 \ 3d^6(1G)4p^2F$
347219	346993	226	2.5	76 $3d^{6}(3F)4p^{4}G + 17 3d^{6}(3F)4p^{4}G$
347793.1	347578	215	3.5	$75 \ 3d^{6}(3F)4p^{4}G + 17 \ 3d^{6}(3F)4p^{4}G$
348323.7	348098	226	4.5	71 $3d^{6}(3F)4p \ {}^{4}G + 17 \ 3d^{6}(3F)4p \ {}^{4}G$
349167.6	348848	320	5.5	77 $3d_{0}^{6}(3F)4p_{4}^{4}G + 20 3d_{0}^{6}(3F)4p_{4}^{4}G$
349300.5	349038	263	1.5	$72 \ 3d^{6}(3P)4p^{4}S + 25 \ 3d^{6}(3P)4p^{4}S$
351430.8	351331	100	1.5	$49 \ 3d^{\circ}(3F)4p^{-2}D + 22 \ 3d^{\circ}(3P)4p^{-2}D + 9 \ 3d^{\circ}(3P)4p^{-2}D$
351671.9	351981	-309	0.5	$46 \ 3d^{\circ}(3P)4p^{-}P + 39 \ 3d^{\circ}(3P)4p^{-}P + 7 \ 3d^{\circ}(3P)4p^{-}S$
352419.2	352501	- 398	2.5	$47 \text{ 3d } (3F)4p \ r + 40 \text{ 3d } (3F)4p \ r$ $45 \text{ 3d}^6(3F)4p \ ^2D + 21 \text{ 3d}^6(3P)4p \ ^2D + 11 \text{ 3d}^6(3P)4p \ ^2D$
352582.3	352325	257	4.5	$63 \ 3d^{6}(3F)4p^{2}G + 16 \ 3d^{6}(3F)4p^{2}G$
353485.7	353743	-257	2.5	$24 \ 3d^{6}(3P)4p^{4}P + 20 \ 3d^{6}(3P)4p^{4}P + 12 \ 3d^{6}(3P)4p^{4}D$
353590	353445	145	0.5	$45 \ 3d^{6}(3F)4p^{4}D + 22 \ 3d^{6}(3P)4p^{4}D + 15 \ 3d^{6}(3P)4p^{4}D$
353645.9	353464	182	3.5	$65 \ 3d^{6}(3F)4p^{2}G + 15 \ 3d^{6}(3F)4p^{2}G + 8 \ 3d^{6}(3F)4p^{4}F$
354039.3	353996	43	1.5	29 $3d^{6}(3F)4p^{4}D + 19 3d^{6}(3P)4p^{4}D + 13 3d^{6}(3P)4p^{4}D$
354548	354714	-166	2.5	$24 \ 3d^{6}(3F)4p \ {}^{4}F + 22 \ 3d^{6}(3P)4p \ {}^{4}P + 19 \ 3d^{6}(3P)4p \ 4P$
354796.7	354750	47	1.5	$51 \ 3d^{0}(3F)4p^{4}F + 17 \ 3d^{0}(3F)4p^{4}F + 9 \ 3d^{0}(3F)4p^{4}D$
354905.2	354857	48	3.5	$39 3d^{\circ}(3F)4p^{-1}F + 15 3d^{\circ}(3F)4p^{-1}F + 15 3d^{\circ}(3P)4p^{-1}D$
355606	355610	-4	2.5	$34 3d^{-}(3F)4p^{-}F + 20 3d^{-}(3F)4p^{-}D + 14 3d^{-}(3F)4p^{-}D$
356372 1	356428	-56	4.5	04 04 04 04 04 14 17 14 17 14 17
356661.9	356858	-196	1.5	$26 3d^6(3\text{F})4p^2\text{D} + 21 3d^6(3\text{F})4p^2\text{D} + 17 3d^6(3\text{F})4p^2\text{D}$
357881	358177	-296	0.5	$52 \ 3d^6(3P)4p^2P + 36 \ 3d^6(3P)4p^2P$
357948.3	358385	-437	2.5	$33 \ 3d^{6}(3P)4p^{2}D + 26 \ 3d^{6}(3P)4p^{2}D + 24 \ 3d^{6}(3F)4p^{2}D$
358724.8	359025	-300	3.5	$51 \ 3d^{6}(3F)4p^{2}F + 22 \ 3d^{6}(3F)4p^{2}F + 14 \ 3d^{6}(1G)4p^{2}F$
359141.2	359648	-507	1.5	42 $3d_{e}^{6}(3P)4p_{2}^{2}P + 30 3d_{e}^{6}(3P)4p_{2}^{2}P + 8 3d_{e}^{6}(3P)4p_{2}^{2}D$
359491.9	359658	-166	2.5	$66 \ 3d^{\circ}(3F)4p^{-2}F + 25 \ 3d^{\circ}(3F)4p^{-2}F$
360058.2	360296	-238	4.5	$57 3d^{\circ}(1G)4p^{-2}H + 34 3d^{\circ}(1G)4p^{-2}H$ 26 246(1G)4 - 2G + 25 246(1G)4 - 2F + 10 246(1G)4 - 2F
362142.8	362340	-308	5.5 5.5	$20.50 (1G)4p^{-2}F + 12.50^{\circ}(1G)4p^{-2}F$ 61.3d ⁶ (1G)4p ² H + 36.3d ⁶ (1G)4p ² H
363396.8	363765	-368	2.5	$54 \ 3d^6(1G)4p^{-2}F + 26 \ 3d^6(1G)4p^{-2}F + 8 \ 3d^6(1F)4p^{-2}F$
364606.6	364872	-265	4.5	$63 \ 3d^6(1G)4p^{-2}G + 27 \ 3d^6(1G)4p^{-2}G$
365071.1	365357	-286	3.5	$40 \ 3d^{6}(1G)4p^{2}G + 17 \ 3d^{6}(1G)4p^{2}G + 16 \ 3d^{6}(1G)4p^{2}F$
386004.2	385757	247	1.5	78 $3d^{6}(1D)4p^{2}D + 17 3d^{6}(1D)4p^{2}D$

Table A5: Continued

Transitions

010 110	· Comput	cu oscina	001 50	ionguns a	nu ura	113101	m probai	JIIIUICS	
ſ	Wavelength	Lower Level	J_{low}	Upper Level	J_{up}	log gf	gA	CF	1
	297.059	50072	3.5	386705	$2.\hat{5}$	-0.57	2.03E+10	-0.58	1
	297.164	49490	2.5	386004	1.5	-0.7	$1.49E \pm 10$	-0.626	
	298 022	20827	2.5	356372	3.5	-1	$7.48E \pm 0.09$	-0.284	
	200.022	20021	2.5	264607	4 5	-1	1.40 ± 10	0.482	
	299.218	30402	5.5	364607	4.5	-0.41	2.92E + 10	0.483	
	300.077	31823	4.5	365071	3.5	-0.57	2.01E + 10	0.408	1
	300.824	21066	1.5	353486	2.5	-0.99	7.59E+09	0.312	
	302.737	31823	4.5	362143	3.5	-0.87	9.78E + 09	0.308	
	304.438	20827	2.5	349301	1.5	-0.54	2.09E+10	-0.755	
	304.66	21066	1.5	349301	1.5	-0.77	1.21E + 10	0.638	
	305.469	21935	0.5	349301	1.5	-0.99	$7.34E \pm 0.09$	-0.723	
	307 245	30402	5.5	355875	4.5	-1	7.10E + 0.9	-0.59	
	310 385	30402	5.5	352582	1.5	0.26	3 80E+10	0.383	
	210.333	21922	4.5	252646	9.5	-0.20	2.60 ± 10	-0.383	
	210.75	00007	4.5	240000	0.0	-0.28	$3.03E \pm 10$	-0.403	
	312.507	20827	2.5	340820	3.5	-0.28	3.57E + 10	-0.804	
	312.835	21066	1.5	340723	2.5	-0.76	1.20E + 10	-0.507	
	314.392	76838	1.5	394912	0.5	-0.68	1.42E + 10	0.79	
	315.875	77668	2.5	394249	1.5	-0.39	2.70E + 10	0.77	
	316.876	49490	2.5	365071	3.5	-0.92	8.01E + 09	-0.287	
	317.93	50072	3.5	364607	4.5	-0.45	2.33E + 10	-0.848	
	318.566	49490	2.5	363397	2.5	-0.66	$1.46E \pm 10$	-0.244	
	319.844	49490	2.5	362143	3.5	-0.8	$1.05E \pm 10$	-0.462	
	320 132	30966	2.5	343337	3.5	-0.82	9 99E+09	-0.291	
	220.132	22202	1.5	242201	0.0	-0.82	6.40E+00	0.265	
	322.372	40400	1.5	250402	2.5	-1	$0.49E \pm 0.09$	-0.205	1
	322.379	49490	2.5	339492	2.5	-0.64	1.40E + 10	0.419	
	322.616	1616	3.5	311582	3.5	-0.58	1.68E + 10	0.426	
	323.451	76838	1.5	386004	1.5	-0.53	1.90E + 10	0.674	
	323.542	2759	2.5	311838	2.5	-0.57	1.73E + 10	0.498	
	323.586	77668	2.5	386705	2.5	-0.39	2.57E + 10	0.6	
	323.772	22575	4.5	331435	3.5	-0.99	6.54E + 09	0.078	
	323.816	0	4.5	308818	4.5	-0.21	3.92E + 10	0.521	
	323.989	50072	3.5	358725	3.5	-0.27	3.46E + 10	0.586	1
	324 19	2759	2.5	311220	3.5	_0.91	$7.75E \pm 0.0$	0.809	1
	324.15	1616	3.5	300801	3.5	0.30	$2.58E \pm 10$	0.464	
	224.40	2500	1.5	211706	1.5	-0.33	2.00 ± 10 2.00 ± 10	0.404	
	324.400	3020	1.5	311700	1.5	-0.43	2.36E+10	0.842	
	324.511	1010	3.5	309772	4.5	-0.88	8.40E+09	0.567	
	324.607	0	4.5	308065	5.5	-0.21	3.93E + 10	-0.865	
	324.681	2759	2.5	310754	2.5	-0.76	1.11E + 10	0.339	1
	324.806	50072	3.5	357948	2.5	-0.7	1.27E + 10	0.185	
	324.86	0	4.5	307825	4.5	-0.4	2.51E+10	-0.873	
	325.037	30402	5.5	338059	4.5	-0.22	3.80E + 10	-0.74	
	325.494	3528	1.5	310754	2.5	-0.53	1.85E + 10	-0.784	1
	325.519	1616	3.5	308818	4.5	-0.42	$2.40E \pm 10$	-0.871	
	325 531	33292	1.5	340483	1.5	-0.7	$1.27E \pm 10$	-0.36	
	325.68	30966	2.5	338016	2.5	0.71	1.27E + 10 $1.23E \pm 10$	0.164	
	225.00	2750	2.5	200801	2.5	-0.71	1.25 ± 10 1.84 ± 10	-0.104	
	325.088	2759	2.5	309801	3.0	-0.53	1.84E+10	-0.583	
	325.847	0	4.5	306892	5.5	-0.86	8.66E+09	-0.85	1
	325.934	2759	2.5	309570	2.5	-0.78	1.03E+10	0.538	
	326.227	2759	2.5	309294	3.5	-0.93	7.32E + 09	0.427	
	326.398	1616	3.5	307991	3.5	-0.63	1.48E + 10	-0.716	
	326.575	1616	3.5	307825	4.5	-0.53	1.85E + 10	-0.413	
	326.872	27016	1.5	332946	1.5	-0.73	1.16E + 10	-0.236	1
	327.382	0	4.5	305453	3.5	-0.74	1.14E + 10	-0.338	1
	327.62	2759	2.5	307991	3.5	-0.59	$1.59E \pm 10$	-0.432	
	328 408	1616	3.5	306116	2.5	-0.25	3.50E + 10	-0.796	
	220.400	2529	1.5	207010	2.5	0.58	1.69E 10	0.629	
	328.000	0	1.5	204100	2.5	-0.38	$1.02E \pm 10$ $2.44E \pm 10$	-0.038	
	326.132	21002	4.5	304199	0.0	-0.4	2.4415 ± 10	0.031	
	328.820	31823	4.5	335935	3.5	-0.33	2.87E + 10	-0.507	
	329.035	2759	2.5	306678	1.5	-0.42	2.33E+10	-0.81	
	329.054	22575	4.5	326477	3.5	-0.09	5.04E + 10	-0.542	
	329.219	27016	1.5	330765	2.5	-0.88	8.18E + 09	-0.22	
	329.532	3528	1.5	306989	0.5	-0.68	1.29E + 10	-0.842	
	329.805	0	4.5	303209	3.5	-0.37	2.64E + 10	0.533	
	329.85	24100	3.5	327268	2.5	-0.08	5.06E + 10	-0.613	1
	330.047	28367	0.5	331354	0.5	-0.66	1.33E + 10	-0.844	1
	330.604	1616	3.5	304092	4.5	-0.7	1.21E + 10	0.584	
	330,745	50072	3.5	352419	2.5	-0.12	4.68E + 10	0.749	1
	330 771	27016	1.5	329340	2.5	-0.61	$1.49E \pm 10$	-0.499	
	331 101	49490	2.5	351431	1.5	-0.20	$3.11E \pm 10$	0.78	1
	331 216	20827	2.5	322744	3.5	-0.8	974E±00	-0.398	1
	331 94	20021	2.0	304655	3 5	0.05	6 75 - 00	0.491	1
	331.24	2109	0.5	220061	1.5	0.50	1.561 10	0.441	1
	221 000	20307	0.0	200100	1.0	-0.09	1.50E+10 9.94E+00	-0.081	1
	331.823	20827	2.5	322192	2.5	-0.87	0.24E+09	-0.576	
	332.406	0	4.5	300837	4.5	-0.77	1.02E + 10	0.558	
	332.813	30966	2.5	331435	3.5	-0.74	1.10E + 10	0.265	1
	332.888	0	4.5	300401	5.5	0.02	6.29E + 10	0.627	
	332.915	21066	1.5	321443	1.5	-0.95	6.73E + 09	-0.626	
	333.146	22575	4.5	322744	3.5	-0.46	2.10E + 10	0.464	1
	333.479	21066	1.5	320935	0.5	-0.79	9.64E + 09	-0.692	
	333.555	22575	4.5	322376	4.5	-0.07	5.06E + 10	-0.627	1
	333,557	30966	2 5	330765	2.5	-0.69	1.22E + 10	0.35	1
	333 580	1616	3.5	301386	45	-0.03	7 80E-L00	0.478	1
	222 710	1010	1 1	222046	1 5	0.09	1 505 109	0.904	1
	333.718	33292	1.0	332940	1.0	-0.08	1.095+10	0.364	
	333.734	1010	3.5	301255	3.5	-0.84	8.57E+09	0.383	
	333.871	24100	3.5	323617	4.5	-0.59	1.56E+10	0.213	1
	333.929	1616	3.5	301081	2.5	-0.8	9.50E + 09	-0.656	1
	334.201	1616	3.5	300837	4.5	-0.5	1.88E + 10	0.337	1
	334.311	24100	3.5	323222	2.5	-0.29	3.05E + 10	-0.327	1
	334.607	22575	4.5	321433	3.5	-0.99	6.11E + 09	-0.166	1
	334.641	2759	2.5	301587	3.5	-0.95	6.65E + 09	-0.33	1
	334.922	20827	2.5	319404	1.5	-0.76	$1.03E \pm 10$	-0.566	1
	335 013	2750	2.5	301255	2.5	_0.91	9.21E.L00	0.226	1
	335 469	2103	2.0 2.5	218000	0.0 0 K	_0.91	2 04E-10	-0.65	1
	000.402 225 565	20021	2.0	201522	2.0	-0.31	2.34D+10 1.01E - 10	-0.00	
	333.305	3528	1.0	301333	2.5	-0.77	1.01E+10	0.291	
	335.691	27016	1.5	324909	1.5	-0.78	9.808+09	-0.298	1
	335.731	21066	1.5	318923	2.5	-0.56	1.64E + 10	0.658	
	335.913	24100	3.5	321796	3.5	-0.57	1.58E+10	0.221	1
Į	336.07	28367	0.5	325923	1.5	-0.95	6.64E+09	0.565	J

Table A6: Computed oscillator strengths and transition probabilities in Cu V.

Table A6: Continued

Wavelength	Lower Level	JLow	Upper level	J _{Up}	log gf	gA	CF
336.165 336.169	33292 21935	1.5	330765 319404	2.5 1.5	-0.87	8.04E+09 1 39E+10	0.215 0.64
336.274	22575	4.5	319952	5.5	-0.18	3.93E+10	0.527
336.323	24100	3.5	321433	3.5	-0.16	4.10E + 10	-0.661
337.008 338.617	22575 24100	4.5	319304	3.5	-0.83	$8.66E \pm 09$ $3.18E \pm 10$	0.173 0.754
338.748	24100	3.5	319304	3.5	-0.20	1.60E+10	-0.21
339.032	30966	2.5	325923	1.5	-0.24	3.32E + 10	0.587
339.414	22575	4.5	317201	4.5	-0.36	2.52E+10	-0.368
339.498	30402	2.5 5.5	325519 324668	2.5 5.5	-0.49	1.87E+10 1.18E+10	-0.361 -0.467
339.88	30402	5.5	324624	6.5	-0.12	4.40E + 10	-0.896
340.035	33292	1.5	327380	0.5	-0.37	2.46E + 10	0.652
340.058	22575	4.5	316643	3.5	-0.18	3.85E+10 $6.27E\pm00$	-0.311
340.355	49490	2.5	343301	2.5 2.5	-0.59	1.49E+10	-0.536
340.63	22575	4.5	316149	5.5	-0.55	1.63E + 10	-0.353
340.988	50072	3.5	343337	3.5	-0.5	1.83E+10 5.01E+10	-0.501
341.478	31823	4.5	324668	5.5	-0.23	3.36E+10 3.36E+10	-0.666
342.426	24100	3.5	316134	2.5	-0.49	1.85E + 10	-0.249
342.496	30402	5.5	322376	4.5	-0.94	6.54E + 09	-0.2
342.708	31823	4.5 4.5	323517	$^{4.0}_{5.5}$	-0.86	1.10E+11 7.77E+09	-0.8 0.373
343.055	30966	2.5	322464	3.5	-0.87	7.60E + 09	0.705
343.736	31823	4.5	322744	3.5	-0.9	7.10E+09	-0.556
344.172 344.86	31823	4.5 4.5	322376 321796	4.5 3.5	-0.95	$6.26E \pm 09$ 2 23E \pm 10	$0.215 \\ 0.445$
344.911	33292	1.5	323222	2.5	-1	5.65E+09	0.106
345.364	30402	5.5	319952	5.5	0	5.56E + 10	-0.524
345.387	22575	4.5	312106	5.5 4.5	-0.83	8.29E+09 5.90E+10	-0.59
346	30402	5.5	319419	4.5	-0.84	7.96E+09	0.317
347.256	27016	1.5	314988	1.5	-0.87	7.45E + 09	0.377
347.333	22575	4.5	310483	5.5	-0.98	5.83E + 09 2.27E + 10	0.217
347.943	77668	4.5 2.5	365071	3.5 3.5	-0.37	$2.37E \pm 10$ $2.17E \pm 10$	0.309 0.615
348.163	27016	1.5	314238	2.5	-0.48	1.80E + 10	0.363
348.193	22575	4.5	309772	4.5	-0.36	2.39E+10	-0.496
348.286 348.892	24100 28367	3.5 0.5	311220 314988	$\frac{3.5}{1.5}$	-0.6	1.39E+10 8 46E+09	-0.351 0.369
348.969	76838	1.5	363397	2.5	-0.32	2.61E + 10	0.527
349.959	30402	5.5	316149	5.5	-0.29	2.78E + 10	-0.195
350.046	30966	2.5	316643	3.5	-0.36	2.39E+10 1.20E+10	-0.372
350.571	22575	4.5	307825	4.5	-0.85	7.68E+09	-0.463
350.816	21066	1.5	306116	2.5	-0.89	6.96E + 09	-0.202
350.919	27016	1.5	311982	0.5	-0.74	9.78E+09	-0.289
351.525	20827 77668	2.5	362143	3.5 3.5	-0.81	$2.85E \pm 10$	-0.193 -0.557
352.815	27016	1.5	310450	1.5	-0.79	8.72E + 09	-0.253
353.018	30966	2.5	314238	2.5	-0.42	2.03E+10	0.521
353.555 353.748	33292 27016	1.5 1.5	316134 309703	2.5 0.5	-0.46 -0.87	1.87E+10 7 24E+09	-0.4 0.211
353.79	76838	1.5	359492	2.5	-0.61	1.32E + 10	0.358
354.76	22575	4.5	304456	4.5	-0.6	1.34E + 10	-0.213
354.983	30402 77668	5.5 2.5	312106 359141	5.5 1.5	-0.77	9.00E+09 1 17E+10	-0.263
355.413	50072	3.5	331435	3.5	-0.26	2.92E+10	-0.441
355.524	49490	2.5	330765	2.5	-0.86	7.34E + 09	-0.221
355.8	77668	2.5	358725 357881	3.5	-0.97	5.65E+09 7.01E+09	0.087 0.336
355.962	0	4.5	280929	3.5	-0.98	5.53E+09	0.554
356.436	24100	3.5	304655	3.5	-0.89	6.83E + 09	-0.204
356.627	22575 77668	4.5	302980 357948	4.5	-0.93	6.14E+09 5.53E+09	-0.221
357.039	30402	2.5 5.5	310483	2.5 5.5	-0.98	1.82E+10	0.304
357.335	49490	2.5	329340	2.5	-0.57	1.43E + 10	0.318
357.368	76838	1.5	356662 310450	1.5	-0.87	7.10E+09 1.52E+10	0.165 0.376
357.883	0	4.5	279421	4.5	-0.34	2.67E+10	0.370 0.543
357.898	31823	4.5	311233	4.5	-0.65	1.17E + 10	0.23
358.022	1616	3.5	280929	3.5	-0.53	1.53E+10 1.06E+10	0.407
358.303	3528	1.5	282622	1.5	-0.78	8.63E+09	0.432
358.357	31823	4.5	310875	4.5	-0.71	1.00E + 10	0.165
358.593	30402	5.5	309269	5.5	-0.62	1.26E+10	0.185
358.856	0 0	4.5	278663	3.5	-0.92	4.75E+10	0.532
359.288	30966	2.5	309294	3.5	-0.95	5.82E + 09	0.211
359.779	31823	4.5	309772	4.5	-0.99	5.29E + 09	-0.085
359.866	2759	3.5 2.5	279497 280066	2.5 1.5	-0.23	$2.06E \pm 10$ $2.06E \pm 10$	$0.501 \\ 0.502$
360.949	1616	3.5	278663	3.5	-0.84	7.44E + 09	-0.517
361.213	3528	1.5	280373	0.5	-0.53	1.52E + 10	0.526
361.353	2759 1616	2.5 3.5	279497 278295	2.5 2.5	-0.82 -0.91	7.79E+09 6.24E+09	-0.502 -0.493
361.614	3528	1.5	280066	1.5	-0.95	5.75E + 0.09	-0.504
361.788	50072	3.5	326477	3.5	-0.89	6.53E+09	-0.146
361.836	0 30402	$4.5 \\ 5.5$	276368 305883	3.5 6.5	-0.78 -0.64	8.46E+09 1.16E±10	-0.501 -0.671
363.047	50072	3.5	325519	2.5	-0.83	7.53E+09	-0.283
363.083	49490	2.5	324909	1.5	-0.95	5.67E + 09	-0.332
363.545	31823	4.5	306892	5.5	-0.77	8.49E+09	-0.484
364.176	76838	⊿.ə 1.5	351431	⊿.ə 1.5	-0.21	$3.12E \pm 10$	0.606
365.32	49490	2.5	323222	2.5	-0.91	6.15E + 09	0.087
367.234	49490	2.5	321796	3.5	-0.75	8.73E+09	0.237
307.237 370.625	50072 49490	3.5 2.5	322376 319304	4.5 3.5	-0.9 -0.48	0.18E+09 1.61E+10	-0.224 0.38
370.896	50072	3.5	319689	4.5	-0.23	2.88E + 10	0.628
375.135	50072	3.5	316643	3.5	-0.69	9.77E+09	0.12
377.355	21066 20827	1.5 2.5	286069 285546	0.5 1.5	-0.63 -0.59	1.10E+10 1.19E±10	0.614 0.556
379.227	20827	2.5	284521	2.5	-0.22	2.78E+10	0.550 0.576
379.346	21935	0.5	285546	1.5	-0.65	1.04E + 10	-0.532

Table A6: Continued

Wavelength	Lower Level	JLow	Upper level	J_{Up}	log gf	gA	CF
379.571	21066 20827	1.5	284521 278663	2.5	-0.66	1.02E+10 7.61E+09	-0.485
933.499	256273	2.5	363397	2.5	-0.89	9.99E+08	0.434
944.552	256272	3.5	362143	3.5	-1	7.49E+08	-0.265
996.581	222401 222886	$\frac{4.5}{3.5}$	$322744 \\ 322192$	$\frac{3.5}{2.5}$	-0.99 -0.78	6.92E+08 1.09E+09	$0.238 \\ 0.552$
1026.709	234036	4.5	331435	3.5	-0.68	1.35E + 09	-0.647
1035.572	226311	5.5	322876	4.5	-0.54	1.76E + 09	-0.627
1055.302	227801	4.5 5.5	322376	3.5 4.5	-0.74 -0.72	1.07E+09 1.12E+09	0.703
1058.831	228020	3.5	322464	3.5	-1	5.87E + 08	0.532
1060.59	235053 227543	3.5	329340 321796	2.5	-0.95	6.73E+08 7 18E+08	0.488 0.455
1070.83	228048	4.5	321433	3.5	-0.83	8.59E+08	0.405
1070.914	226311	5.5	319689	4.5	-0.83	8.70E+08	0.494
1071.299 1075.631	228020 228105	$\frac{3.5}{2.5}$	321365 321074	2.5 1.5	-0.55 -0.65	1.65E+09 1.28E+09	-0.5 -0.586
1078.857	230532	2.5	323222	2.5	-0.7	1.14E+09	-0.546
1081.775	234036	4.5	326477	3.5	-0.82	8.51E+08	-0.63
1083.236	239541	3.5 4.5	331435	3.5 3.5	-0.89	1.48E+09	-0.202 0.607
1088.275	227801	5.5	319689	4.5	-0.67	1.20E + 09	-0.365
1088.714	272755	3.5 6.5	364607 311889	4.5 6.5	-0.92	6.90E+08 3.03E+09	-0.707
1091.485	227801	5.5	319419	4.5	-1	5.49E + 08	-0.739
1092.427	246477	2.5	338016	2.5	-0.41	2.17E+09	-0.555
1093.103	220623 228048	$5.5 \\ 4.5$	312106 319304	$\frac{5.5}{3.5}$	-0.57	1.51E+09 1.45E+09	-0.471 -0.616
1096.492	220938	4.5	312138	4.5	-0.72	1.06E + 09	-0.267
1097.085	239615	3.5	330765	2.5	-0.79	9.36E+08	0.716 0.741
1100.307	187779	4.5	278663	3.5	-0.52	1.66E+09	0.678
1101.307	221272	3.5	312073	3.5	-0.63	1.28E+09	-0.364
1102.972 1103.513	188833 265752	$3.5 \\ 4.5$	279497 356372	2.5 3.5	-0.9 -0.74	0.85E+08 9.95E+08	0.425 0.146
1103.63	220623	5.5	311233	4.5	-0.89	7.06E + 08	-0.207
1105.142	265886	2.5	356372	3.5	-0.84	7.84E+08	0.617
1106.23	205975 220208	3.5 6.5	310483	3.5 5.5	-0.05 -0.45	4.90E+09 1.94E+09	-0.728 -0.526
1109.6	265752	4.5	355875	4.5	0.34	1.17E + 10	-0.776
1111.079	189587 190100	2.5 1.5	279590 280066	1.5 1.5	-0.67	1.15E+09 8 43E+08	0.438
1112.168	265692	1.5	355606	2.5	-0.75	9.67E + 08	0.795
1112.225 1112.347	189587 265975	2.5	279497 355875	2.5	-0.68	1.13E+09 1.42E+09	-0.688
1113.107	226311	5.5	316149	5.5	-0.71	1.06E+09	0.151
1113.209	188833	3.5	278663	3.5	-0.85	7.64E + 08	-0.58
1114.515 1114.579	265886	$\frac{3.5}{2.5}$	355606	2.5 2.5	-0.7	1.12E+09 5.19E+09	-0.664 -0.749
1114.62	229588	3.5	319304	3.5	-0.85	7.62E + 08	0.357
1115.343 1117.453	227543 190100	4.5 1.5	317201 279590	4.5 1.5	-0.89	6.93E+08 1.67E+09	0.224
1117.694	234036	4.5	323506	5.5	-0.89	6.71E + 08	-0.478
1117.794	188833 272755	3.5	278295	2.5	-0.28	2.78E+09 1.92E+09	0.436 0.55
1121.212	190400	0.5	279590	1.5	-0.39	2.16E+09	0.811
1121.66	228048	4.5	317201	4.5	-0.06	4.58E+09	-0.617
1121.67 1121.715	205752	$\frac{4.5}{5.5}$	354905 309772	$\frac{3.5}{4.5}$	-0.22	3.19E+09 7.25E+08	-0.742 0.566
1122.269	265692	1.5	354797	1.5	-0.07	4.53E + 09	-0.805
1123.353 1124.477	265886 265975	2.5 3.5	354905 354905	$3.5 \\ 3.5$	-0.8 -0.22	8.44E+08 3.19E+09	0.52
1127.298	189587	2.5	278295	2.5	-0.36	2.26E + 09	-0.457
1127.438	222886 265886	3.5 2.5	$311582 \\ 354548$	3.5 2.5	-0.95 -0.74	5.89E + 08 9.59E + 08	0.323
1128.079	220623	5.5	309269	5.5	-0.7	1.04E+09	-0.219
1128.813	187779	4.5	276368	3.5	0.01	5.35E+09	0.5
1129.012	235053	3.5	323617	4.5	-0.45	1.31E+09	-0.567
1130.281	222401	4.5	310875	4.5	-0.82	7.85E+08	-0.417
1131.785 1131.876	220938 227801	$4.5 \\ 5.5$	$309294 \\ 316149$	$3.5 \\ 5.5$	-0.92 0.21	6.27E+08 8.45E+09	$0.205 \\ -0.783$
1132.528	221272	3.5	309570	2.5	-0.25	2.90E + 09	0.586
1133.86 1134.174	190100 235053	1.5	278295	2.5 2.5	-0.42	1.98E+09 $1.23E\pm09$	$0.805 \\ 0.524$
1134.387	265886	2.5	354039	1.5	-0.27	2.75E+09	0.736
1137.676	265692	1.5	353590	0.5	-0.51	1.57E+09	0.801
1130.212	265886	2.5	353646	3.5	-0.47	6.54E+09	-0.559
1139.479	234036	4.5	321796	3.5	-0.94	5.89E + 08	0.284
1140.356 1140.629	235053 265975	3.5 3.5	$322744 \\ 353646$	3.5 3.5	-0.81 -0.95	7.85E+08 5.68E+08	$0.747 \\ 0.338$
1140.856	239615	3.5	327268	2.5	-0.68	1.09E+09	0.738
1142.396	188833	3.5	276368	3.5	-0.41	1.99E + 09	-0.356
1143.614	220623	5.5	308065	5.5	-0.67	1.08E+09	0.728
1144.831	226889	1.5	314238	2.5	-0.64	1.17E + 09	0.673
1146.767 1147.752	220623 220938	$\frac{5.5}{4.5}$	307825 308065	$\frac{4.5}{5.5}$	-0.42 -0.78	1.91E+09 8.44E+08	-0.438 -0.289
1148.571	256272	3.5	343337	3.5	0.22	8.29E + 09	-0.735
1148.576 1148.698	256273 229588	2.5 3.5	$343337 \\316643$	$\frac{3.5}{3.5}$	-0.76 -0.91	8.74E+08 6.26E+08	$0.722 \\ -0.265$
1148.731	220938	4.5	307991	3.5	-0.46	1.73E + 09	-0.451
1149.053 1150.269	256273 239541	2.5 4.5	343301 326477	2.5 3.5	0.14	7.01E+09 7.25E+08	-0.813 0.621
1150.843	222401	4.5	309294	3.5	-0.7	9.96E+08	0.384
1150.928	220938	4.5	307825 309772	4.5 4 5	-0.44	1.80E+09	0.47
1151.677	265752	4.5	352582	4.5	-0.9	6.27E + 08	0.293
1152.216	278282	4.5	365071	3.5	-0.56	1.39E+09	0.284
1152.325 1152.827	189587 235053	$\frac{2.5}{3.5}$	276368 321796	3.5 3.5	-0.43 -0.52	1.88E+09 1.52E+09	0.828 -0.603
1153.152	221272	3.5	307991	3.5	-0.69	1.01E + 09	0.456
$1153.521 \\ 1153.521$	$278380 \\ 272801$	$\frac{3.5}{2.5}$	$365071 \\ 359492$	$\frac{3.5}{2.5}$	$0.22 \\ 0.14$	8.22E+09 6.93E+09	-0.844 -0.768
1153.595	236059	2.5	322744	3.5	-0.3	2.51E + 0.09	0.822
			168 –				_

Table A6: Continued

Wavelength	Lower Level	JLow	Upper level	JUp	log gf	gA	CF
1154.233	221272 265975	3.5	307910 352582	2.5 4.5	-0.56	1.36E+09 1.12E+09	-0.562
1155.367	221272	3.5	307825	4.5	-0.8	7.90E+08	-0.488
1155.474	236331	3.5	322876	4.5	0.32	1.04E + 10	0.85
1156.473	246477	2.5	332946	1.5	-0.49	1.55E+09	0.386
1156.002	238234	0.5 6.5	324668	0.5 5.5	-0.89	$6.49E \pm 08$ $6.98E \pm 08$	-0.799
1157.003	236040	1.5	322470	1.5	-0.77	8.45E + 08	-0.476
1157.231	236331	3.5	322744	3.5	-0.18	3.31E + 09	-0.487
1157.259	236059	2.5	322470	1.5	-0.89	6.48E + 08	-0.455
1157.538	236059	2.5	322464 324624	3.0 6.5	0.03	5.28E + 09 1 77E + 10	-0.812
1157.902	238305	5.5	324668	5.5	0.48	1.51E + 10	-0.871
1157.927	236109	0.5	322470	1.5	-0.66	1.09E + 09	0.814
1158.416	278282	4.5	364607	4.5	0.35	1.11E + 10	-0.746
1158.453	238305	1.5 5.5	332946	1.5 6.5	-0.41	1.89E+09 1.31E+09	-0.738
1158.949	187779	4.5	274065	4.5	-0.74	9.07E + 08	0.189
1159.735	278380	3.5	364607	4.5	-0.51	1.53E + 09	0.693
1159.763	187779	4.5	274004	5.5	0.52	1.63E + 10	0.9
1160.993	236059	2.5	322192	2.5	-0.39	2.04E+09	-0.268
1160.997	236331	3.5	322464	3.5	-0.85	6.92E + 08	0.464
1161.529	223477	1.5	309570	2.5	-0.33	2.31E+09	-0.771
1161.711	223214	2.5	309294 358725	3.5	-0.47	1.69E+09 7.64E+09	-0.692
1163.412	220938	4.5	306892	5.5	-0.43	1.81E + 09	-0.821
1163.94	234036	4.5	319952	5.5	-0.56	1.35E + 09	-0.585
1165.573	226311	5.5	312106	5.5	-0.73	9.08E + 08	0.152
1167.507	234036	4.5	319689	5.5 4.5	0.23 0.32	$1.02E \pm 10$	-0.83
1168.193	230532	2.5	316134	2.5	-0.95	5.57E + 08	-0.489
1168.525	226311	5.5	311889	6.5	0.21	7.86E+09	0.498
1170.075	236331 236040	3.5 1.5	321796 321443	3.5 1.5	-0.28	2.57E+09 6.08E±08	-0.782
1171.862	236109	0.5	321443	1.5	-0.43	1.82E+09	0.795
1171.988	236040	1.5	321365	2.5	-0.54	1.42E + 09	0.242
1172.174	238305	5.5	323617	4.5	0.3	9.72E+09	0.88
1172.708	∠38039 238234	⊿.ə 6.5	323506	⊿.ə 5.5	0.02	$4.91E \pm 0.09$	0.816
1172.884	220623	5.5	305883	6.5	-0.21	2.97E + 09	-0.691
1173.135	221664	1.5	306906	2.5	-0.11	3.78E + 09	0.534
1173.151	188833	3.5	274073 274065	3.5	-0.22	2.93E+09 1.17E+10	0.505
1173.511	229774	0.5	314988	1.5	-0.66	1.07E+09	0.303 0.792
1173.694	238305	5.5	323506	5.5	-0.7	9.47E + 08	0.384
1173.803	272755	3.5	357948	2.5	-0.35	2.21E+09	-0.74
1175.182	236331	3.5 1.5	321433	3.5 0.5	-0.5	1.51E+09 4.84E+08	-0.745 0.185
1175.37	199441	3.5	284521	2.5	0.09	6.02E + 09	0.808
1175.997	236040	1.5	321074	1.5	-0.33	2.25E + 09	0.833
1176.238	278380	3.5	363397	2.5	0.11	6.29E + 09 7.62E + 00	0.825
1176.952	236109	0.5	321074	1.5	-0.71	9.39E+08	0.258
1177.045	246477	2.5	331435	3.5	0.21	7.64E + 09	0.866
1177.318	222886	3.5	307825	4.5	0.08	5.82E + 09	0.782
1177.881	200648	2.5	285546	1.5	-0.19	3.14E+09 1.62E+09	0.807
1179.572	223214	2.5	307991	3.5	-0.15	3.41E+09	0.818
1180.229	246624	1.5	331354	0.5	-0.4	1.88E + 09	0.748
1181.253	201413	1.5	286069	0.5	-0.58	1.26E + 09	0.82
1181.329	229588	3.5 4.5	312138	2.5 4.5	-1	$4.78E \pm 08$	0.840 0.089
1182.552	227543	4.5	312106	5.5	0.14	6.54E + 09	0.551
1182.602	189587	2.5	274146	2.5	-0.18	3.16E + 09	0.665
1183.559	222401 189587	4.5	306892 274073	5.5	-0.59	1.22E+09 6.71E+09	0.368 0.796
1184.044	230532	2.5	314988	1.5	-0.14	3.41E+09	0.849
1184.112	221664	1.5	306116	2.5	-0.99	4.87E + 08	-0.519
1184.371	223477	1.5	307910	2.5	-0.63	1.11E + 09	0.708
1185.307	235053 227801	3.5 5.5	319419 312106	4.0 5.5	-0.43 -0.66	$1.03E \pm 09$	0.559
1186.4	246477	2.5	330765	2.5	-0.53	1.37E + 0.09	-0.293
1186.92	235053	3.5	319304	3.5	0.04	5.11E + 09	-0.631
1187.381	201850	0.5	286069 340482	0.5 1 F	-0.57	1.27E+09 2.42E-00	-0.851
1187.979	236040	1.5	320216	0.5	-0.45	1.70E+09	0.839
1188.039	226311	5.5	310483	5.5	0.27	8.88E + 09	-0.743
1188.484	246624	1.5	330765	2.5 1 F	-0.14	3.36E + 09	0.858
1188.81	201413 228020	1.5 3.5	⊿8əə46 312138	1.5 4.5	-0.46	1.05E+09 7.44E+09	-0.841 0.741
1189.195	228048	4.5	312138	4.5	-0.95	5.25E + 08	-0.123
1189.226	227801	5.5	311889	6.5	0.21	7.52E+09	0.862
1189.228	190100	1.5 4 5	274189 312106	$1.5 \\ 5.5$	-0.23	2.75E+09 4 41E+09	0.843
1189.826	190100	1.5	274146	2.5	-0.07	3.97E+09	0.807
1189.934	219203	2.5	303242	2.5	-0.53	1.40E + 09	-0.445
1190.191	222886	3.5	306906 303200	2.5	-0.96	5.26E+08 2 11E+09	0.714 0.887
1190.444	239615	3.5	323617	4.5	-0.59	1.24E+09	0.622
1190.933	228105	2.5	312073	3.5	-0.01	4.66E + 09	0.525
1190.967	239541	4.5	323506	5.5	0.25	8.48E+09	0.871
1191.546	223214 200648	$^{2.5}_{2.5}$	284521	1.5 2.5	-0.95 -0.51	0.28E+08 1.47E+09	-0.833
1192.422	278282	4.5	362145	5.5	0.5	1.47E + 10	0.897
1192.448	272801	2.5	356662	1.5	-0.48	1.55E+09	0.774
1192.449	278282	4.5 6.5	362143 304062	3.5 6.5	0.03	5.01E+09 6.47E+09	-0.822
1192.843	220623	5.5	304456	4.5	-0.98	4.91E+08	0.482
1193.068	228020	3.5	311838	2.5	-0.59	1.21E + 09	0.232
1193.184	190400	0.5	274210	0.5	-0.38	1.96E + 09 1.72E + 00	0.895
1193.485	223376	0.5	274189 307139	1.5 1.5	-0.43	1.11E+09	0.631
1193.847	278380	3.5	362143	3.5	-0.37	2.02E+09	-0.309
1194.279	228105	2.5	311838	2.5	-0.23	2.73E + 09	-0.469
1194.502	220938	4.5	304655	3.5	-0.57	1.27E + 09	0.469
			169				

Table A6: Continued

	Wavelength 1194.882	Lower Level 227543	J_{Low} 4.5	Upper level 311233	J_{Up} 4.5	log gf 0.24	gA 8.04E+09	CF -0.859
1196.156 228105 2.5 311708 1.5 -0.21 2.2887-00 0.4581-00 0.531 1196.712 228888 1.5 310450 1.5 -0.22 2.587-00 0.591 1197.347 228888 1.5 310450 1.5 -0.24 2.587+00 0.22 1197.347 22938 4.5 300492 1.5 -0.34 1.318+00 0.673 1198.43 224637 1.5 300492 1.5 -0.14 1.318+00 0.690 1198.43 224633 5.5 304092 1.5 -0.15 5.712+60 0.400 1199.443 224673 2.5 304062 1.5 -0.12 7.632+00 0.600 1199.542 246140 2.5 30466 5.5 0.5 0.51 1.5 0.12 2.4447+00 0.600 1199.542 246140 2.5 304046 5.5 0.13 3.666+00 0.638 1.666+00 0.638 1.666+00 0.638 1.666+00 0.638 1.666+00 0.643 1.666+00 0.643 1.666+00 <td>1195.062</td> <td>227543</td> <td>4.5</td> <td>311220</td> <td>3.5</td> <td>-1</td> <td>4.67E + 08 4.23E + 09</td> <td>-0.704</td>	1195.062	227543	4.5	311220	3.5	-1	4.67E + 08 4.23E + 09	-0.704
$\begin{array}{llllllllllllllllllllllllllllllllllll$	1196.158	228105	2.5	311706	1.5	-0.21	2.89E+09	$0.834 \\ 0.879$
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1196.715 1196.722	$228020 \\ 226889$	$3.5 \\ 1.5$	$311582 \\ 310450$	$\frac{3.5}{1.5}$	0 -0.26	4.68E+09 2.59E+09	-0.591 -0.596
$\begin{array}{c} 1197.83 \\ 226477 \\ 1198.044 \\ 22023 \\ 22612 \\ 2$	1197.104	228048	4.5	311582	3.5	-0.95	5.27E+08	0.183
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1197.347 1197.424	220938 223477	4.5	306989	$^{4.5}_{0.5}$	-0.38	1.05E+09 1.97E+09	0.22
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1197.83 1198.044	246477 220623	$2.5 \\ 5.5$	329961 304092	$1.5 \\ 4.5$	-0.54 -0.7	1.31E+09 9.26E+08	-0.775 0.426
$\begin{array}{llllllllllllllllllllllllllllllllllll$	1198.123	223214	2.5	306678	1.5	-0.37	2.01E+09	0.529
1199.284 221272 3.5 304655 3.5 0.91 5.71E+08 0.195 1199.692 246050 2.5 319477 1.5 0.11 3.524+09 0.641 1200.352 220023 6.5 303456 7.5 0.64 1.99E+10 0.335 1201.431 222866 5.3 305456 1.5 0.611 2.55 0.42 2.33E+09 0.345 1201.431 2328447 4.5 322748 3.5 0.27 2.33E+09 0.485 1203.152 228105 2.5 31203 3.5 -0.42 1.45E+09 -0.481 1203.152 228105 2.5 31323 3.5 -0.42 1.45E+09 -0.414 1205.642 226311 5.5 309269 5.5 -0.42 1.76E+09 0.744 1205.642 226314 4.5 322464 3.5 -0.64 1.06E+08 -0.71 1206.262 223214 4.5 322464 3.5 -0.42 2.6E+08 -0.313 1206.623 2239615 3.5 32	1198.473 1198.822	220623 265752	$\frac{5.5}{4.5}$	304062 349168	$\frac{6.5}{5.5}$	0.22 0.5	7.63E+09 1.45E+10	0.69 0.9
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1199.284	221272 236059	3.5 2.5	304655 319404	3.5	-0.91	5.71E + 08 3.53E + 09	$0.195 \\ 0.864$
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1199.952	243140	2.5	326477	3.5	0.19	7.22E+09	0.871
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1199.954 1200.352	$246624 \\ 220623$	$1.5 \\ 5.5$	$329961 \\ 303932$	$1.5 \\ 5.5$	-0.29 -0.1	2.34E+09 3.66E+09	-0.568 -0.33
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1201.221	220208	6.5 3.5	303456 306116	7.5	0.64	1.99E+10 2 34E+09	0.935 0.386
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1201.873	239541	4.5	322744	3.5	-0.27	2.53E+09	-0.86
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1201.9 1202.151	$223477 \\ 221272$	$1.5 \\ 3.5$	$306678 \\ 304456$	$1.5 \\ 4.5$	-0.51 -0.64	1.45E+09 1.07E+09	-0.863 -0.329
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1203.081	272755 228105	3.5 2.5	355875 311220	$\frac{4.5}{3.5}$	-0.58 -0.26	1.22E+09 2.51E+09	0.836
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1203.132	256273	2.5	339378	1.5	-0.51	1.45E+09	-0.813
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1204.065 1204.912	$222401 \\ 220938$	$\frac{4.5}{4.5}$	$305453 \\ 303932$	$\frac{3.5}{5.5}$	-0.28 0.13	2.46E+09 6.15E+09	$0.377 \\ 0.546$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1205.425	226311 227543	5.5	309269 310483	5.5	-0.42	1.76E+09 1.60E+09	0.214 0.748
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1205.935	239541	4.5	322464	3.5	-0.56	1.28E+09	0.534
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1206.252 1206.794	$223214 \\ 236059$	$2.5 \\ 2.5$	$306116 \\ 318923$	$2.5 \\ 2.5$	-0.24 -0.92	2.65E+09 5.59E+08	-0.813 -0.219
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1206.81	246477	2.5	329340	2.5	-0.13	3.35E + 09	-0.856
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1207.000	239541	4.5	322376	4.5	0.24	9.30E+08 8.03E+09	-0.688
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1207.33 1207.524	$228048 \\ 226889$	$\frac{4.5}{1.5}$	$310875 \\ 309703$	$\frac{4.5}{0.5}$	-0.04 -0.4	4.14E+09 1.82E+09	$0.822 \\ -0.824$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1208.293	239615	3.5	322376	4.5	-0.21	2.81E+09	0.8
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1208.7	228020 246624	3.5 1.5	329340	2.5 2.5	-0.69	9.16E+08	-0.219
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1210.563 1210.772	$234036 \\ 236331$	$4.5 \\ 3.5$	$316643 \\ 318923$	$\frac{3.5}{2.5}$	-0.02 0.12	4.35E+09 6.01E+09	$0.795 \\ 0.889$
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1211.075	265752	4.5	348324	4.5	-0.44	1.65E+09	0.861
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1211.129 1211.38	222886 229588	$3.5 \\ 3.5$	305453 312138	$\frac{3.5}{4.5}$	-0.29 -0.38	2.37E+09 1.89E+09	-0.665 0.849
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1212.018	226311 223376	5.5 0.5	308818 305844	$\frac{4.5}{1.5}$	-0.04	4.11E+09 3 34E+09	0.468
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1213.915	243140	2.5	325519	2.5	0.16	6.55E+09	-0.884
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1214.217 1214.348	220623 265975	5.5 3.5	302980 348324	$\frac{4.5}{4.5}$	-0.86 0.33	6.27E+08 9.52E+09	-0.534 0.789
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1215.677 1215.733	227543 239541	4.5	309801 321796	3.5	-0.04	4.15E+09 1.61E+09	0.721 0.697
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1215.967	223214	2.5	305453	3.5	-0.88	5.99E+08	0.835
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1216.421 1216.438	229774 221272	$0.5 \\ 3.5$	311982 303479	$0.5 \\ 2.5$	-0.41 -0.63	1.76E+09 1.05E+09	-0.859 0.77
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1216.822	239615 235053	3.5 3.5	321796 317201	$3.5 \\ 4.5$	-0.35	2.06E+09 4.60E+09	0.565 0.771
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1217.834	234036	4.5	316149	$\frac{4.5}{5.5}$	0.01	5.39E+09	0.733
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1217.962 1218.472	$272801 \\ 221664$	$2.5 \\ 1.5$	$354905 \\ 303734$	$\frac{3.5}{1.5}$	-0.63 -0.04	1.07E+09 4.05E+09	0.895 -0.891
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1218.883	220938 229588	4.5	302980 311582	$\frac{4.5}{3.5}$	-0.64	1.02E+09 1.81E+09	-0.179
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1220.444	221272	3.5	303209	3.5	-0.46	1.55E+09	-0.414
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1220.514 1220.895	$229774 \\ 265886$	$0.5 \\ 2.5$	$311706 \\ 347793$	$\frac{1.5}{3.5}$	-0.96 0.21	4.88E+08 7.20E+09	-0.524 0.789
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1221.343	219203 239615	2.5	301081	2.5	0.08	5.33E+09 5.50E+09	-0.891
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1222.223	265975	3.5	347793	3.5	-0.43	1.66E+09	0.862
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1222.6 1222.691	$272755 \\ 256272$	$3.5 \\ 3.5$	$354548 \\ 338059$	$2.5 \\ 4.5$	-0.89 0.4	5.85E+08 1.13E+10	-0.782 0.917
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1222.778	228020	3.5	309801 360058	3.5	-0.65	1.00E+09 1.27E+09	0.152
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1222.953	222886	3.5	304655	3.5	-0.38	1.86E+09	-0.41
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1222.966 1223.18	$243140 \\ 226311$	$\frac{2.5}{5.5}$	$324909 \\ 308065$	$1.5 \\ 5.5$	-0.61 -0.62	1.10E+09 1.07E+09	-0.816 0.476
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1223.185 1223.216	228048 228020	4.5	309801 309772	$3.5 \\ 4.5$	-0.39	1.80E+09 1.90E+09	0.787
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1223.342	256272	3.5	338016	2.5	-0.04	4.16E+09	0.851
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1223.593 1223.623	227543 228048	$4.5 \\ 4.5$	309269 309772	$\frac{5.5}{4.5}$	-0.97 -0.36	4.81E+08 1.96E+09	0.142 -0.733
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1223.722 1223.863	238234 221272	6.5 3.5	319952 302980	5.5 4.5	0.16 0.12	6.44E+09 5.79E+09	0.871 0.783
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1224.05	228105	2.5	309801	3.5	-1	4.42E+08	-0.418
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1224.127 1224.317	$222401 \\ 278380$	$\frac{4.5}{3.5}$	$304092 \\ 360058$	$\frac{4.5}{4.5}$	$0.2 \\ 0.35$	7.04E+09 1.00E+10	-0.722 0.794
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1224.809 1225.827	229588 221664	3.5	311233 303242	$\frac{4.5}{2.5}$	-0.7	8.89E+08 2 81E+09	0.427 0.897
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1225.935	222886	3.5	304456	4.5	-0.81	6.92E+08	-0.743
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1226.371 1226.536	230532 222401	$2.5 \\ 4.5$	$312073 \\ 303932$	$\frac{3.5}{5.5}$	-0.16 -0.27	$_{2.39E+09}^{3.06E+09}$	$0.897 \\ 0.824$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1226.58 1227.184	265692 1994/1	1.5	347219 280929	2.5 3.5	0.09	5.45E+09 8.15E+08	0.856
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1227.467	227801	5.5	309269	5.5	0.06	5.08E + 09	0.793
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1227.527 1229.513	$228105 \\ 265886$	$2.5 \\ 2.5$	$309570 \\ 347219$	$2.5 \\ 2.5$	-0.89 -0.6	5.71E+08 1.11E+09	$0.268 \\ 0.876$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1229.811	222886	3.5	304199	3.5	-0.85	6.28E+08	0.375
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1230.056	221664	$1.5^{2.3}$	302961	0.5	-0.31	2.14E+09	-0.902
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$1230.1 \\ 1230.203$	200648 229588	$2.5 \\ 3.5$	$281942 \\ 310875$	$2.5 \\ 4.5$	-0.49 -0.28	1.42E+09 2.30E+09	$0.656 \\ 0.371$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1230.388	227543	4.5	308818	4.5	-0.65	9.83E+08	0.203
1231.429 222886 3.5 304092 4.5 -0.48 1.46E+09 0.752 170	1231.395	201413	1.5	282622	1.5	-0.56	1.20E+0.09	0.787
• • • •	1231.429	222886	3.5	304092 170	4.5	-0.48	1.46E+09	0.752

Table A6: Continued

Wavelength	Lower Level	JLow	Upper level	J_{Up}	log gf	gA	CF
1231.922	238234	6.5	319408	7.5	0.63	1.88E+10	0.945
1232.839	238305	5.5	319419	4.5	-0.73	8.09E+08	-0.578
1232.865	278380	3.5	359492	2.5	-0.96	4.86E + 08	-0.771
1233.327	235053	3.5	316134	2.5	-0.14	3.21E+09	0.781
1233.371	220208	6.5 5.5	301286	5.5 4.5	-0.84	6.34E+08 4 52E+09	0.875
1236.933	272801	2.5	353646	3.5	0.23	7.37E+09	0.891
1237.501	222401	4.5	303209	3.5	-0.2	2.76E + 09	-0.672
1238.056	201850	0.5	282622	1.5	-0.13	3.25E + 09	0.904
1238.194	220623	5.5 5.5	301386	4.5 6.5	-0.07	3.72E+09 6.26E+09	0.883 0.505
1239.332	230532	2.5	311220	3.5	0.02	4.55E + 09	0.618
1239.514	229774	0.5	310450	1.5	-0.63	1.03E + 09	0.8
1239.717	220623	5.5	301286	5.5	0.22	7.12E + 09	0.846
1239.947	220938	4.5	327268	2.5	-0.09	1.81E+09	-0.859
1240.796	222886	3.5	303479	2.5	-0.32	2.07E + 09	-0.565
1241.017	222401	4.5	302980	4.5	-0.78	7.16E + 08	0.186
1241.779	201413	1.5	281942	2.5	0.08	5.19E + 09 7 55E + 08	0.902
1241.892	223214	2.5	303680	1.5	-0.47	1.47E+09	-0.87
1243.047	220938	4.5	301386	4.5	-0.19	2.76E + 0.09	0.392
1243.116	278282	4.5	358725	3.5	-0.32	2.07E + 09	-0.797
1243.617	239541	4.5	319952	5.5	0.14	6.11E+09 4.87E+09	-0.894
1244.964	220938	4.5 3.5	303209	3.5	-0.63	1.02E+09	-0.202
1245.062	220938	4.5	301255	3.5	-0.93	5.04E + 08	0.138
1245.101	221272	3.5	301587	3.5	-0.51	1.34E + 09	-0.27
1245.611	227543	4.5	307825	4.5	-1	4.23E + 08 7 80E + 00	0.161
1245.875	223214	2.5 2.5	303479	2.5	-0.41	1.66E+09	-0.299
1245.927	221272	3.5	301533	2.5	-0.35	1.90E + 09	0.636
1246.106	226889	1.5	307139	1.5	-0.54	1.24E + 09	-0.705
1246.539	230532	2.5 5.5	310754 300837	2.5 4.5	-0.45 -0.26	1.52E+09 2.35E ± 09	0.546 0.514
1246.668	229588	3.5	309801	3.5	-0.88	5.74E+08	0.318
1246.836	223477	1.5	303680	1.5	-0.24	2.49E + 09	-0.649
1246.985	220208	6.5	300401	5.5	0.32	8.96E+09	0.921
1247.124	229588 221272	3.5	309772	4.5 4.5	-0.04	3.95E+09 2.37E+09	0.627 0.318
1249.133	199441	3.5	279497	2.5	-0.49	1.39E+09	-0.9
1249.728	228048	4.5	308065	5.5	-0.47	1.45E + 09	-0.515
1249.734	226889	1.5	306906	2.5	-0.29	2.22E+09	-0.899
1249.959	223477 246477	1.5	303479 326477	2.5	-0.62	1.02E+09 6.46E+08	0.663
1250.077	223214	2.5	303209	3.5	-0.86	5.96E + 08	0.529
1250.258	221272	3.5	301255	3.5	-0.15	2.99E + 09	-0.852
1250.316	199441	3.5	279421	4.5	0.39	1.05E+10	0.906
1250.463	228020	3.5 4.5	307991	3.5 4.5	-0.5	1.35E+09 3.99E+09	0.383
1251.911	239541	4.5	319419	4.5	-0.47	1.45E+09	0.831
1252.706	272755	3.5	352582	4.5	0.32	8.95E + 09	0.886
1253.065	239615	3.5	319419	4.5	0.18	6.57E + 09	0.771
1253.709	239541	2.5 4.5	319304	2.5	-0.26	1.19E+09	-0.573
1254.601	229588	3.5	309294	3.5	-0.22	2.57E + 09	-0.637
1255.271	272755	3.5	352419	2.5	-0.11	3.33E+09	0.841
1255.293	256272	3.5	335935	3.5	-0.76	7.45E+08 $7.42E\pm09$	0.849
1256.725	226311	5.5	305883	6.5	0.13	5.72E+09	-0.662
1256.831	221272	3.5	300837	4.5	-0.53	1.24E + 09	-0.362
1258.702	246477	2.5	325923	1.5	-0.51	1.26E + 09	0.717
1259.168	200648	2.5 4.5	280066	1.5 5.5	-0.46	1.47E+09 2.85E+09	-0.906
1260.564	243140	2.5	322470	1.5	-0.52	1.26E+09	-0.809
1262.279	199441	3.5	278663	3.5	0.19	6.41E + 09	-0.879
1265.211	230532	2.5	309570	2.5	-0.94	4.78E + 08	-0.278
1265.714	238234 222401	0.5 4.5	317240	6.5 4.5	-0.62	9.92E+08 6 44E+08	0.898
1266.456	201413	1.5	280373	0.5	-0.6	1.05E+09	-0.911
1266.862	238305	5.5	317240	6.5	0.53	1.42E + 10	0.884
1267.493	238305	5.5	317201	4.5 2 5	-0.79	6.69E + 08	0.753
1268.253	200648	4.5 2.5	279497	2.5	-0.47	2.94E+09	-0.758
1268.316	228048	4.5	306892	5.5	0.22	6.88E + 09	0.637
1269.348	187779	4.5	266560	3.5	-0.1	3.33E+09	-0.918
1271.409	201413 222886	1.5 3.5	280066 301533	1.5 2.5	-0.48 -0.79	1.37E+09 $6.67E\pm08$	-0.748 0.858
1271.779	272801	2.5	351431	1.5	-0.26	2.25E+09	0.813
1273.502	201850	0.5	280373	0.5	-0.62	9.94E + 08	-0.882
1273.887	222886	3.5	301386	4.5	-0.8	6.61E+08	0.299
1274.928	222401	$^{4.0}_{4.5}$	200227 300837	$^{4.0}_{4.5}$	-0.5	1.30E+10	-0.945 0.29
1275.958	223214	2.5	301587	3.5	-0.73	7.69E + 08	-0.524
1276.003	222886	3.5	301255	3.5	-0.39	1.68E + 09	0.345
1276.826	223214	2.5	301533	2.5	-0.43	1.52E+09 9.91E-09	0.862
1278.168	229588	⊿.5 3.5	307825	4.5	-0.49	1.31E+0.09	0.330 0.441
1278.182	188833	3.5	267069	2.5	-0.04	3.76E + 09	-0.925
1278.511	201850	0.5	280066	1.5	-0.77	6.89E+08	0.596
1279.667	226311 201413	5.5 1.5	304456 279497	4.5 2.5	-0.22 -0.71	2.50E+09 $7.84E\pm08$	-0.825 0.447
1280.702	227801	5.5	305883	6.5	0.24	6.96E+09	0.541
1280.917	234036	4.5	312106	5.5	-0.94	4.69E + 08	-0.811
1281.117	223477	1.5	301533	2.5	-0.29	2.09E+09	0.553
1281.374	223214 200648	2.5 2.5	301235 278663	3.0 3.5	-0.44	1.40E+09 4.66E±08	0.309
1282.053	222401	4.5	300401	5.5	-0.21	2.50E + 09	0.693
1282.851	222886	3.5	300837	4.5	-0.41	1.57E + 09	0.253
1283.521	227543	4.5	305453	3.5	-0.67	8.73E+08	0.53
1286.149	226311	⊿.ə 5.5	207489 304062	1.0 6.5	-0.12	$3.13E \pm 09$	-0.933
1286.549	188833	3.5	266560	3.5	-0.01	3.94E+09	-0.66
1287.661	239541	4.5	317201	4.5	-0.77	7.01E + 08	-0.314
1287.686	190100	1.5	267759	0.5	-0.36	1.77E + 09	-0.942

		Table	A0: Con	tinue	a		
Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA	CF
1287.89	200648	2.5	278295	2.5	-0.71	7.77E + 08	0.881
1288.882	239615	3.5	317201	4.5	-0.73	7.61E + 08	-0.43
1290.624	189587	2.5	267069	2.5	-0.53	1.17E + 09	-0.529
1291.893	228048	4.5	305453	3.5	-0.8	6.42E + 08	-0.509
1292.09	188833	3.5	266227	4.5	-0.64	9.10E + 08	0.258
1292.36	230532	2.5	307910	2.5	-0.6	1.00E + 09	-0.296
1292.571	229774	0.5	307139	1.5	-0.76	6.94E + 08	-0.388
1296.808	227543	4.5	304655	3.5	-1	3.98E + 08	-0.207
1296.988	239541	4.5	316643	3.5	-0.77	6.99E + 08	-0.747
1297.212	190400	0.5	267489	1.5	-0.53	1.18E + 09	0.515
1299.155	189587	2.5	266560	3.5	-0.44	1.42E + 09	0.327
1299.233	190100	1.5	267069	2.5	-0.41	1.55E + 09	0.411
1299.939	199441	3.5	276368	3.5	-0.51	1.21E + 09	0.876
1304.298	226311	5.5	302980	4.5	-0.53	1.17E + 09	-0.601
1304.536	227801	5.5	304456	4.5	-0.32	1.88E + 09	0.424
1304.892	228020	3.5	304655	3.5	-0.97	4.24E + 08	-0.254
1305.355	228048	4.5	304655	3.5	-0.44	1.42E + 09	0.548
1305.362	230532	2.5	307139	1.5	-0.99	4.01E + 08	0.589
1306.341	228105	2.5	304655	3.5	-0.72	7.46E + 08	0.799
1308.101	234036	4.5	310483	5.5	-0.39	1.57E + 09	0.702
1308.287	228020	3.5	304456	4.5	-0.51	1.23E + 09	0.636
1309.087	227543	4.5	303932	5.5	-0.43	1.46E + 09	-0.496
1309.708	226889	1.5	303242	2.5	-0.34	1.78E + 09	0.438
1310.759	227801	5.5	304092	4.5	-0.82	$5.86E \pm 08$	0.43
1312.674	235053	3.5	311233	4.5	-0.6	9.67E + 08	0.78
1314.565	229774	0.5	305844	1.5	-0.76	$6.64E \pm 0.08$	0.503
1318.871	235053	3.5	310875	4.5	-0.33	1.79E + 0.09	0.797
1319.296	236040	1.5	311838	2.5	-0.98	$4.06E \pm 08$	0.521
1322.795	236109	0.5	311706	1.5	-0.89	$5.01E \pm 0.08$	0.615
1324.091	236059	2.5	311582	3.5	-0.88	5.06E + 08	0.576
1328.768	234036	4.5	309294	3.5	-0.53	$1.10E \pm 0.09$	-0.81
1329.209	234036	4.5	309269	5.5	-0.01	3.70E + 0.09	0.785
1330.143	227801	5.5	302980	4.5	-0.79	6.02E + 08	0.258
1332.134	229588	3.5	304655	3.5	-0.77	$6.41E \pm 08$	0.473
1332.142	265752	4.5	340820	3.5	0.09	4.68E + 09	0.937
1336.241	265886	2.5	340723	2.5	-0.99	$3.88E \pm 08$	-0.521
1337.832	265975	3.5	340723	2.5	-0.15	$2.64E \pm 0.09$	0.93
1338.339	235053	3.5	309772	4.5	-0.72	7.13E + 08	-0.176
1340.542	265886	2.5	340483	1.5	-0.77	6.35E + 08	0.747
1341.968	235053	3.5	309570	2.5	-0.97	3.90E + 08	-0.855
1342.415	256272	3.5	330765	2.5	-0.5	1.18E + 09	-0.868
1347.86	226889	1.5	301081	2.5	-0.64	8.29E + 08	-0.346
1348.545	265692	1.5	339846	0.5	-0.65	8.21E + 08	0.922
1349.703	226311	5.5	300401	5.5	-0.61	9.02E + 08	-0.625
1352.186	234036	4.5	307991	3.5	-0.83	5.44E + 08	-0.603
1357.075	256273	2.5	329961	1.5	-0.9	4.57E + 08	-0.736
1359.819	228048	4.5	301587	3.5	-0.5	1.13E + 09	0.506
1359.886	227801	5.5	301336	6.5	-0.43	1.34E + 09	0.375
1360.503	243140	2.5	316643	3.5	-0.42	1.40E + 09	0.648
1360.696	265886	2.5	339378	1.5	-0.61	9.04E + 08	0.572
1363.042	228020	3.5	301386	4.5	-0.99	3.67E + 08	0.225
1365.395	228048	4.5	301286	5.5	-0.76	6.20E + 08	0.28
1368.605	256272	3.5	329340	2.5	-0.79	5.86E + 08	-0.744
1372.552	235053	3.5	307910	2.5	-0.78	5.86E + 08	-0.651
1377.986	238305	5.5	310875	4.5	-1	3.54E + 08	0.68
1379.565	236331	3.5	308818	4.5	-0.76	6.24E + 08	0.744
1384.093	238234	6.5	310483	5.5	-0.81	5.35E + 08	0.857
1388.904	229588	3.5	301587	3.5	-0.93	4.05E + 08	0.477
1399.251	238305	5.5	309772	4.5	-0.93	4.00E + 08	-0.829
1407.747	238234	6.5	309269	5.5	-0.62	8.12E + 08	0.808
1420.057	234036	4.5	304456	4.5	-0.52	1.01E + 09	-0.634
1425.19	246477	2.5	316643	3.5	-0.65	7.22E + 08	0.748
1427.415	236059	2.5	306116	2.5	-0.91	4.15E + 08	0.59
1436.73	235053	3.5	304655	3.5	-0.98	3.42E + 08	-0.3
1446.715	236331	3.5	305453	3.5	-0.73	6.01E + 08	0.702
1475.775	236331	3.5	304092	4.5	-0.91	3.85E + 08	0.837
1482.815	236040	1.5	303479	2.5	-0.91	3.82E + 08	0.819
1537.151	278282	4.5	343337	3.5	-0.79	4.51E + 08	0.828

Table A6: Continued

Cu VI

Energy Levels

) 0				
Γ	E^{a}_{exp}	E^{b}_{calc}	ΔE	J	Leading components (in %) in LS coupling c
	0	-84	84	4	99 3d ^{6 5} D
	1195.8	1124	72	3	$100 \ 3d^6 \ ^5D$
	1986.8	1925	62	2	99 $3d^{6}{}^{5}D$
	2489.4	2435	54	1	99 $3d^{6}$ ⁵ D
	2733.4	2683	50	0	$99 \ 3d^{6} \ ^{5}D$
	29285	29833	-548	2	$60 \ 3d^6 \ ^3P + 38 \ 3d^6 \ ^3P$
	30417.6	30593	-175	6	99 3d ^{6 3} H
	31009.2	31085	-76	5	$95 \ 3d^6 \ {}^{3}H + 5 \ 3d^6 \ {}^{3}G$
	31287.6	31238	50	4	$78 3d^{6} {}^{3}H + 9 3d^{6} {}^{3}F + 7 3d^{6} {}^{3}G$
	32684.9	33379	-694	1	$61 \ 3d^{6} \ {}^{3}P + 37 \ 3d^{6} \ {}^{3}P$
	32756	32863	-107	4	$61 \ 3d^{6} \ {}^{3}F + 18 \ 3d^{6} \ {}^{3}F + 17 \ 3d^{6} \ {}^{3}H$
	33295.8	33384	-88	3	$74 \ 3d^{6} \ {}^{3}F + 20 \ 3d^{6} \ {}^{3}F + 6 \ 3d^{6} \ {}^{3}G$
	33739.6	33871	-131	2	$80 \ 3d^{6} \ {}^{3}F + 19 \ 3d^{6} \ {}^{3}F$
	33867.8	34556	-688	0	$59 \ 3d^6 \ ^3P + 36 \ 3d^6 \ ^3P$
	37378.1	37313	65	5	$95 \ 3d^{6} \ {}^{3}G + 5 \ 3d^{6} \ {}^{3}H$
	38468.9	38428	41	4	90 $3d^{6} {}^{3}G + 6 3d^{6} {}^{3}F$
	38907.4	38799	108	3	$93 \ 3d^6 \ {}^3G + 5 \ 3d^6 \ {}^3F$
	46405.8	46390	16	6	99 3d ⁶ ¹ I
	46714.2	46253	461	2	$97 \ 3d^{6} \ ^{3}D$
	46848.3	46295	553	1	99 3d ^{6 3} D
	47119.1	46637	482	3	99 3d ^{6 3} D
	47611.6	46790	822	4	$64 \ 3d^{6} \ {}^{1}G + 32 \ 3d^{6} \ {}^{1}G$
	53786.6	51951	1836	0	$75 \ 3d^{6} \ {}^{1}S + 21 \ 3d^{6} \ {}^{1}S$
	54747.1	56277	-1530	2	$76 \ 3d^{6} \ ^{1}D + 21 \ 3d^{6} \ ^{1}D$
	64967.6	65300	-332	3	$97 \ 3d^{6} \ {}^{1}F$
	74712	74760	-48	0	$63 \ 3d^{6} \ {}^{3}P + 37 \ 3d^{6} \ {}^{3}P$
	75774.1	75865	-91	1	$62 \ 3d^{6} \ ^{3}P + 38 \ 3d^{6} \ ^{3}P$
	77145	77096	49	2	$80 \ 3d^{6} \ {}^{3}F + 19 \ 3d^{6} \ {}^{3}F$
	77223.8	77161	63	4	$77 \ 3d^{6} \ {}^{3}F + 22 \ 3d^{6} \ {}^{3}F$
	77467.9	77433	35	3	$77 \ 3d^{6} \ {}^{3}F + 20 \ 3d^{6} \ {}^{3}F$
	77908.8	78179	-270	2	$60 \ 3d^{6} \ {}^{3}P + 39 \ 3d^{6} \ {}^{3}P$
	87505.9	87861	-355	4	$65 \ 3d^{6} \ {}^{1}G + 34 \ 3d^{6} \ {}^{1}G$
	117084.3	116858	226	2	$78 \ 3d^{6} \ ^{1}D + 22 \ 3d^{6} \ ^{1}D$
	250876.6	250877	0	3	$100 \ 3d^5(6S)4s^7S$
	265639.1	265603	36	2	$100 \ 3d^{5}(6S)4s \ 5S$
	299143	299305	-162	6	$100 \ 3d^{5}(4G)4s^{5}G$
	299250.6	299155	96	2	99 $3d^{5}(4G)4s^{5}G$
	299256	299330	-74	5	$100 \ 3d^{5}(4G)4s^{5}G$
	299282.1	299226	56	3	99 $3d^{5}(4G)4s^{5}G$
	299292.9	299293	0	4	$100 \ 3d^{5}(4G)4s^{5}G$
	308997.5	309110	-113	5	99 $3d^{5}(4G)4s^{3}G$
	309046.1	308936	110	3	49 $3d^{5}(4G)4s^{3}G + 43 3d^{5}(4D)4s^{5}D + 7 3d^{5}(4P)4s^{5}P$
	309110.8	309120	-9	4	$98 \; 3d^5(4G)4s \; {}^3G$
	322791.9	322686	106	5	$98 \ 3d^5(2I) 4s^{-3}I$
	322804.7	322780	25	6	$98 \ 3d^5(2I)4s^{-3}I$
	322877.3	322955	-78	7	$100 \ 3d^{5}(2I)4s^{3}I$

Table A7: Comparison between available experimental data and calculated even energy levels (in $\rm cm^{-1})$ in Cu VI

Table A8: Comparison between available experimental data and calculated odd energy levels (in cm⁻¹) in Cu VI

Earn	Ebala	ΔE	J	Leading components (in $\%$) in LS coupling ^{c}
342225.2	342141	84	2	$98 \; 3d^5(6S)4p \; ^7P$
343276.6	343180	97	3	$97 \ 3d^5(6S)4p^7P$
345137.1	345018	119	4	$100 \ 3d^{5}(6S)4p^{7}P$
355259.2	355237	22	3	$95 \ 3d^5 (6S) 4p^5 P$
356137.2	356133	4	2	$96 \ 3d^5 (6S) 4p^5 P$
356674	356681	$^{-7}$	1	$97 \ 3d^5(6S)4p^5P$
388191.7	388311	-119	2	$89 \ 3d^{5}(4G)4p^{5}G + 5 \ 3d^{5}(4G)4p^{3}F$
388236.1	388349	-113	3	$77 \ 3d^{5}(4G)4p^{5}G + 16 \ 3d^{5}(4G)4p^{5}H$
388312.3	388472	-160	4	$73 \ 3d^{5}(4G)4p^{5}G + 20 \ 3d^{5}(4G)4p^{5}H$
388442.1	388673	-231	5	$73 \ 3d^{5}(4G)4p^{5}G + 20 \ 3d^{5}(4G)4p^{5}H$
388707.5	389019	-312	6	78 $3d^{5}(4G)4p^{5}G + 16 3d^{5}(4G)4p^{5}H$
390618.2	390155	463	3	81 $3d^{5}(4G)4p^{5}H + 13 3d^{5}(4G)4p^{5}G$
391198.1	390846	352	4	$74 \ 3d^{5}(4G)4p^{5}H + 17 \ 3d^{5}(4G)4p^{5}G + 5 \ 3d^{5}(4G)4p^{5}F$
391691.7	391484	208	5	$63 \ 3d^{5}(4G)4p^{5}H + 19 \ 3d^{5}(4G)4p^{5}F + 12 \ 3d^{5}(4G)4p^{5}G$
391986.5	391562	425	2	$50 \ 3d^{5}(4P)4p^{5}D + 18 \ 3d^{5}(4D)4p^{5}D + 11 \ 3d^{5}(4D)4p^{5}F$
392255.1	391888	367	3	$35 3d^{5}(4P)4p {}^{5}D + 20 3d^{5}(4G)4p {}^{5}F + 14 3d^{5}(4D)4p {}^{5}F$
392516.7	392483	34	5	$65 3d^{5}(4G)4p^{5}F + 13 3d^{5}(4G)4p^{5}H + 10 3d^{5}(4G)4p^{5}G$
392593.6	392347	247	6	$80 3d^{5}(4G)4p^{5}H + 18 3d^{5}(4G)4p^{5}G$
202712.6	202570	194	4	50.30 (4G)4p = 11 + 18.30 (4G)4p = G $52.34^{5}(4C)4p = 5E + 12.24^{5}(4D)4p = 5E + 2.34^{5}(4D)4p = 5D$
202000.2	202801	280	7	$100 2d^{5}(4C)4\pi^{5}H$
393090.2	392801	- 50	2	$63 3d^5(4P)d_P {}^{5}S \pm 10 3d^5(4P)d_P {}^{3}P \pm 8 3d^5(4C)d_P {}^{5}F$
204014 7	202942	179	1	$66 2d^{5}(4C) 4p^{5}F + 18 2d^{5}(4D) 4p^{5}F + 7 2d^{5}(4F) 4p^{5}F$
394014.7	393643	120	1	50 30 (4G)4p F + 18 30 (4D)4p F + 7 30 (4F)4p F
394117.4	393965	132	3	55.50(4G)4p F + 10.50(4F)4p D + 12.50(4F)4p F
394133.8	394018	116	2	$55 3d^{\circ}(4G)4p^{\circ}F + 16 3d^{\circ}(4P)4p^{\circ}D + 10 3d^{\circ}(4P)4p^{\circ}S$
395407.1	395136	271	4	$58 3d^{\circ}(4P)4p^{\circ}D + 19 3d^{\circ}(4G)4p^{\circ}F + 17 3d^{\circ}(4D)4p^{\circ}D$
395601	395515	86	3	$38 \ 3d^{\circ}(4P)4p \ ^{\circ}P + 32 \ 3d^{\circ}(4D)4p \ ^{\circ}P + 15 \ 3d^{\circ}(4P)4p \ ^{\circ}D$
396283.7	396337	-53	2	$53 3d^{5}(4P)4p^{5}P + 26 3d^{5}(4D)4p^{5}P + 7 3d^{5}(4P)4p^{5}S$
396454.5	396408	47	2	$78 \ 3d^{3}(4G)4p \ {}^{3}F + 5 \ 3d^{3}(4G)4p \ {}^{3}G$
396523.6	396301	223	1	$68 \ 3d_{2}^{3}(4P)4p \ ^{3}P + 12 \ 3d_{3}^{3}(4D)4p \ ^{3}P + 9 \ 3d_{3}^{3}(4P)4p \ ^{3}P$
396617.1	396817	-200	3	80 3d ⁵ (4G)4p ⁵ F
396929.1	397233	-304	4	86 $3d_{5}^{\circ}(4G)4p_{7}^{\circ}F + 5 3d^{\circ}(4F)4p_{7}^{\circ}F$
397404.4	397291	113	6	91 3d ³ (4G)4p ³ H
398022.8	397796	227	5	$93 \ 3d^5(4G)4p \ ^3H$
398273.1	398215	58	2	$44 \ 3d^{5}(4P)4p \ {}^{3}P + 16 \ 3d^{5}(4D)4p \ {}^{3}P + 14 \ 3d^{5}(4P)4p \ {}^{5}S$
398376.6	398048	329	4	$94 \ 3d^5(4G)4p^{-3}H$
398722.7	398594	129	1	$44 \ 3d^{5}(4P)4p \ {}^{3}P + 16 \ 3d^{5}(4D)4p \ {}^{3}P + 9 \ 3d^{5}(4P)4p \ {}^{5}P$
399112.8	399062	51	1	$63 \ 3d^{5}(4D)4p \ {}^{5}F + 23 \ 3d^{5}(4G)4p \ {}^{5}F + 7 \ 3d^{5}(4P)4p \ {}^{3}P$
399329	399161	168	0	$61 \ 3d^{5}(4P)4p^{3}P + 20 \ 3d^{5}(4D)4p^{3}P + 12 \ 3d^{5}(4D)4p^{5}D$
399434.6	399401	34	2	$68 \ 3d^{5}(4D)4p \ {}^{5}F + 20 \ 3d^{5}(4G)4p \ {}^{5}F$
399881.3	399835	46	3	$69 \ 3d^{5}(4D)4p \ {}^{5}F + 13 \ 3d^{5}(4G)4p \ {}^{5}F$
400562.7	400563	0	4	$73 \ 3d^{5}(4D)4p^{5}F + 10 \ 3d^{5}(4G)4p^{5}F + 9 \ 3d^{5}(4P)4p^{5}D$
401264.1	401233	31	5	$89.3d^{5}(4D)4p^{5}F + 7.3d^{5}(4G)4p^{5}F$
402134 1	401793	341	3	$48 3d^{5}(4D)4p {}^{5}D + 17 3d^{5}(4P)4p {}^{5}D + 17 3d^{5}(4P)4p {}^{3}D$
402534.3	402164	370	4	$67 3d^{5}(4D)4p {}^{5}D + 20 3d^{5}(4P)4p {}^{5}D + 5 3d^{5}(4F)4p {}^{5}D$
402766.8	402492	275	2	$51 3d^{5}(4D)4p$ ⁵ D + 16 $3d^{5}(4P)4p$ ³ D + 16 $3d^{5}(4P)4p$ ⁵ D
402988.8	402492	-5	3	$87 3d^5(4G)4p^3G$
402988.8	402334	-117	4	$^{80} 3d^5(4G)4p^{-3}G$
403080.0	403204	-117	5	$^{01} 24^{5} (4C) 4p^{-3}C$
403132.9	403330	102	1	91.50(4G)4p G $4c_{2}a_{5}^{5}(4D)4=5D + 15_{2}a_{5}^{5}(4D)4=5D + 12_{2}a_{5}^{5}(4D)4=3D$
403338	403100	192	1	40.30(4D)4p D + 13.30(4F)4p D + 13.30(4F)4p D = $52.3^{5}(4D)4-^{3}D$ + 14.23 $^{5}(4D)4-^{5}D$ + 2.35(4D)4- ^{3}E
403300	403234	132	3	$55 3d^{-}(4P)4p^{-}D + 14 3d^{-}(4D)4p^{-}P + 8 3d^{-}(4D)4p^{-}F$ 51 245(4P)4- 3D + 17 245(4P)4- 5D + 6 245(4P)4- 5D
403961.1	403895	50	2	$51 3d^{\circ}(4P)4p^{\circ}D + 17 3d^{\circ}(4D)4p^{\circ}P + 6 3d^{\circ}(4P)4p^{\circ}P$
404096.2	404155	-59	1	$38 3d^{\circ}(4P)4p^{\circ}D + 34 3d^{\circ}(4D)4p^{\circ}P + 11 3d^{\circ}(4D)4p^{\circ}D$
404184	403885	299	0	$60 \ 3d^{\circ}(4D)4p^{\circ}D + 21 \ 3d^{\circ}(4P)4p^{\circ}D + 13 \ 3d^{\circ}(4P)4p^{\circ}P$
404901.7	404853	49	1	$37 3d^{\circ}(4D)4p^{\circ}P + 18 3d^{\circ}(4P)4p^{\circ}D + 17 3d^{\circ}(4D)4p^{\circ}D$
405213.5	404932	282	3	$47 \ 3d^{\circ}(4D)4p \ ^{\circ}D + 14 \ 3d^{\circ}(4D)4p \ ^{\circ}D + 12 \ 3d^{\circ}(4P)4p \ ^{\circ}P$
405505.8	405583	-77	2	$37 \ 3d^{\circ}(4D)4p \ ^{\circ}P + 19 \ 3d^{\circ}(4P)4p \ ^{\circ}P + 14 \ 3d^{\circ}(4D)4p \ ^{\circ}D$
406659.4	406340	319	2	$68 \ 3d^{\circ}(4D)4p \ 3D + 9 \ 3d^{\circ}(4D)4p \ P + 8 \ 3d^{\circ}(4F)4p \ 3D$
406752.6	406794	-41	3	$35 3d^{3}(4D)4p {}^{3}P + 29 3d^{3}(4D)4p 3D + 19 3d^{3}(4P)4p {}^{3}P$
407217.4	406829	388	1	$58 \ 3d_{2}^{\circ}(4D)4p \ 3D + 22 \ 3d_{2}^{\circ}(4P)4p \ 3D + 11 \ 3d_{2}^{\circ}(4F)4p \ 3D$
407355.9	407418	-62	4	$80 \ 3d^{2}(4D)4p \ {}^{3}F + 5 \ 3d^{3}(2G)4p \ {}^{3}F$
408177.6	408244	-66	3	$68 \ 3d_{2}^{5}(4D)4p \ {}^{3}F + 10 \ 3d_{2}^{5}(4P)4p \ 3D + 5 \ 3d_{2}^{5}(2G)4p \ {}^{3}F$
408281.7	408282	0	2	$74 \ 3d^{5}(4D)4p^{3}F + 10 \ 3d^{5}(4P)4p \ 3D + 5 \ 3d^{5}(2G)4p^{3}F$
410288.7	410132	157	1	88 3d (4P)4p S
411872.1	411571	301	6	$72 \ 3d^{\circ}(2I)4p^{\circ}K + 22 \ 3d^{\circ}(2I)4p^{\circ}I$
412326.4	412417	-91	5	$60 \ 3d_{5}^{\circ}(2I)4p_{2}^{\circ}I + 20 \ 3d_{5}^{\circ}(2I)4p_{1}^{\circ}H + 8 \ 3d_{5}^{\circ}(2I)4p_{3}^{\circ}H$
412439.9	412338	102	7	59 $3d_{5}^{\circ}(2I)4p_{7}^{\circ}K + 30 3d_{5}^{\circ}(2I)4p_{7}^{\circ}I + 9 3d_{7}^{\circ}(2I)4p_{1}K$
412469.3	412937	-468	0	$73 \ 3d_{5}^{\circ}(4D)4p_{2}^{\circ}P + 21 \ 3d_{5}^{\circ}(4P)4p_{2}^{\circ}P$
413072.5	413620	-548	1	$64 \operatorname{3d}_{5}^{\circ}(4\mathrm{D})4\mathrm{p}_{2}^{\circ}\mathrm{P} + 20 \operatorname{3d}_{5}^{\circ}(4\mathrm{P})4\mathrm{p}_{2}^{\circ}\mathrm{P} + 6 \operatorname{3d}_{2}^{\circ}(4\mathrm{P})4\mathrm{p}_{3}^{\circ}\mathrm{S}$
413692	413746	-54	2	$30 \ 3d^{5}(2F)4p^{3}F + 27 \ 3d^{5}(2D)4p^{3}F + 9 \ 3d^{5}(2D)4p^{3}F$
414203.7	414269	-65	6	$52 3d_{2}^{\circ}(2I)4p_{1}^{\circ} I + 22 3d_{2}^{\circ}(2I)4p_{1}^{\circ} H + 21 3d_{2}^{\circ}(2I)4p_{1}^{\circ} K$
414298.5	414354	-56	2	$61 \ 3d_{5}^{\circ}(4D)4p \ {}^{3}P + 23 \ 3d_{5}^{\circ}(4P)4p \ {}^{3}P + 6 \ 3d_{5}^{\circ}(2D)4p \ {}^{3}P$
415258.3	414553	705	3	$32 \ 3d^{3}(2D)4p^{3}F + 22 \ 3d^{3}(2F)4p^{3}F + 14 \ 3d^{5}(2F)4p^{3}G$
415520	415237	283	8	100 3d ^o (2I)4p ³ K
415694.4	415718	-24	7	$65 \ 3d^{2}(2I)4p^{-3}I + 35 \ 3d^{5}(2I)4p^{-3}K$
415851.8	415791	61	2	$24 \ 3d_{2}^{0}(2D)4p_{1}^{1}D + 19 \ 3d_{2}^{5}(2D)4p_{3}^{3}F + 16 \ 3d_{2}^{5}(2F)4p_{1}^{1}D$
416024.9	416303	-278	5	46 $3d^{5}(2I)4p^{-1}H + 31 3d^{5}(2I)4p^{-3}I + 7 3d^{5}(2I)4p^{-3}H$
416410.9	416685	-274	6	$67 \ 3d^{5}(2I)4p \ ^{3}H + 20 \ 3d^{5}(2I)4p \ ^{3}I$
417099.5	416822	278	4	$34 \ 3d_{2}^{0}(2D)4p_{3}^{3}F + 26 \ 3d_{2}^{5}(2F)4p_{3}^{3}F + 20 \ 3d_{2}^{5}(2F)4p_{3}^{3}G$
417221.3	417595	-374	5	73 $3d^{5}(2I)4p^{3}H + 14 3d^{5}(2I)4p^{1}H$
417267.3	416949	318	7	89 $3d^{5}(2I)4p$ 1K + 5 $3d^{5}(2I)4p$ ³ K
417511.5	417362	150	4	$70 \ 3d^5(2I)4p \ ^3H + 8 \ 3d^5(2G)4p \ ^3H$
419364.9	419479	-114	4	$37 \ 3d^5(2F)4p^{-1}G + 12 \ 3d^5(2I)4p^{-3}H + 10 \ 3d^5(2F)4p^{-3}G$
419365.2	419002	363	2	$37 \ 3d^5(2D)4p \ ^3P + 12 \ 3d^5(2D)4p \ ^3P + 11 \ 3d^5(2F)4p \ ^3D$
419605.8	419346	260	1	$33 \ 3d^{5}(2D)4p^{3}P + 25 \ 3d^{5}(2D)4p^{3}D + 10 \ 3d^{5}(2D)4p^{3}P$
419864.2	419166	698	3	$36 \ 3d^{5}(2F)4p^{3}G + 25 \ 3d^{5}(2F)4p^{3}F + 17 \ 3d^{5}(2D)4p^{1}F$
420151.2	419979	172	2	$73 \ 3d^{5}(4F)4p^{5}G + 7 \ 3d^{5}(2F)4p^{3}F$
420201.1	420068	133	3	$75 \ 3d^{5}(4F)4p^{5}G + 7 \ 3d^{5}(2F)4p^{3}G$
420355.8	420300	56	3	$34 \ 3d^{5}(2F)4p^{3}D + 30 \ 3d^{5}(2D)4p^{3}D + 11 \ 3d^{5}(2D)4p^{3}D$
420699.4	420569	130	4	$64 \ 3d^{5}(4F)4p \ {}^{5}G + 5 \ 3d^{5}(2F)4p \ {}^{1}G + 5 \ 3d^{5}(4F)4p \ {}^{5}F$
420914 7	420771	144	5	$53 3d^5(4\text{F})4\text{p} {}^5\text{G} + 9 3d^5(4\text{F})4\text{p} {}^5\text{F} + 8 3d^5(2\text{G})4\text{p} {}^3\text{H}$
421423 5	421052	372	0	$64 \ 3d^5(2D)4p^{3}P + 20 \ 3d^5(2D)4p^{3}P \pm 0 \ 3d^5(4F)4p^{5}D$
421467 7	421497	41	2	$44 3d^5(2D)4p^{-3}D + 15 3d^5(2D)4p^{-3}D + 14 3d^5(4F)4p^{-5}E$
		**	~	(PD) the price of (PD) the optimized (AL) the L
Table A8: Continued

E^{a}_{exp}	E_{calc}^{b}	ΔE	J	Leading components (in $\%$) in LS coupling ^{c}
421516.1	421296	220	1	$28 3d^5(2\text{D})4\text{p} \ {}^{3}\text{D} + 24 \ 3d^5(2\text{D})4\text{p} \ {}^{3}\text{P} + 10 \ 3d^5(2\text{D})4\text{p} \ 3\text{D}$
421622.9	421647	-24	3	$33 \ 3d^{5}(2F)4p^{3}D + 12 \ 3d^{5}(2D)4p^{3}D + 11 \ 3d^{5}(2D)4p^{3}F$
421924.7	421657	268	4	$31 \ 3d^{5}(2F)4p^{3}F + 26 \ 3d^{5}(2F)4p^{3}G + 12 \ 3d^{5}(4F)4p^{5}F$
422221.2	422297	-76	3	$55 \ 3d^{5}(4F)4p^{5}F + 23 \ 3d^{5}(4F)4p^{5}D$
422269.8	422079	191	6	$62 \ 3d^{5}(4F)4p^{5}G + 15 \ 3d^{5}(2I)4p^{-1}I + 12 \ 3d^{5}(2G)4p^{-3}H$
422425.6	422346	80	4	$32 \ 3d^{5}(4F)4p^{5}F + 22 \ 3d^{5}(4F)4p^{5}D + 16 \ 3d^{5}(2F)4p^{3}F$
422613.1	422699	-86	2	49 $3d^{5}(4F)4p^{5}F + 25 3d^{5}(4F)4p^{5}D + 8 3d^{5}(2D)4p^{3}D$
422833.7	422345	489	5	$53 \ 3d^{5}(2F)4p^{3}G + 23 \ 3d^{5}(4F)4p^{5}G + 8 \ 3d^{5}(2H)4p^{3}G$
422841.4	422565	276	4	$33 \ 3d^{5}(2G)4p^{3}H + 31 \ 3d^{5}(2H)4p^{3}H + 5 \ 3d^{5}(4F)4p^{5}F$
422858.7	422845	14	6	$63 \ 3d^{5}(2I)4p^{-1}I + 26 \ 3d^{5}(4F)4p^{-5}G + 5 \ 3d^{5}(2H)4p^{-3}H$
423078	422925	153	1	$33 3d^{5}(2F)4p ^{3}D + 25 3d^{5}(2D)4p ^{1}P + 21 3d^{5}(4F)4p ^{5}F$
423123 7	423192	-68	5	$37 3d^{5}(4F)4p^{5}F + 29 3d^{5}(2F)4p^{3}G + 9 3d^{5}(4F)4p^{5}G$
423304 7	423326	-21	1	$50 \ 3d^5(4F)4p \ {}^{5}F + 15 \ 3d^5(4F)4p \ {}^{5}D + 10 \ 3d^5(2D)4p \ {}^{3}D$
423374 7	423293	82	2	$29 3d^5(2F)4p {}^3F + 19 3d^5(2F)4p {}^3D + 16 3d^5(2D)4p {}^3F$
423403.4	420200	480	3	$\frac{17}{34^5}$ $\frac{36}{(2E)4p}$ $\frac{3}{C}$ \pm $\frac{15}{34^5}$ $\frac{36}{(2D)4p}$ $\frac{3}{E}$ \pm $\frac{13}{34^5}$ $\frac{36}{(2E)4p}$ $\frac{3}{E}$
423403.4	422525	67	5	$20.24^{5}(2C)_{4p}^{3}$ $3U + 28.24^{5}(4E)_{4p}^{5}$ $5E + 24.24^{5}(2U)_{4p}^{3}$ $3U$
423018.3	423331	207	4	$23.50(2G)4p$ II $\pm 26.50(4F)4p$ F $\pm 24.50(2H)4p$ II 16.245(2D)4p $^{3}E \pm 15.245(2H)4p$ ^{3}C
424332.3	424000	321 75	4 2	$10.50(2D)4p$ F \mp 15.50(2D)4p G 17.245(2D)4p 1E + 16.245(2E)4p 3C + 7.245(2E)4p 3C
424462.6	424000	-75	3	$17 \text{ 3d}^{-}(2D)4p \text{ F} + 10 \text{ 3d}^{-}(2F)4p \text{ G} + 7 \text{ 3d}^{-}(2F)4p \text{ G}$ $40 \text{ 2}4^{5}(2E)4-^{3}D + 10 \text{ 2}4^{5}(2D)4-^{3}D + 0 \text{ 2}4^{5}(4E)4-^{5}E$
424511.8	424603	-91	2	$40 \ 3d^{\circ}(2F)4p^{\circ}D + 10 \ 3d^{\circ}(2D)4p^{\circ}P + 9 \ 3d^{\circ}(4F)4p^{\circ}F$
424590.4	424758	-168	5	$43 3 d^{-}(2H) 4p^{-1}G + 13 3 d^{-}(2G) 4p^{-1}G + 9 3 d^{-}(2F) 4p^{-1}G$
424697.7	424804	-106	4	$24 \ 3d^{\circ}(2H)4p^{\circ}G + 10 \ 3d^{\circ}(2G)4p^{\circ}G + 7 \ 3d^{\circ}(2F)4p^{\circ}G$
425101.8	425296	-194	4	$41 \ 3d^{\circ}(4F)4p \ ^{\circ}D + 25 \ 3d^{\circ}(4F)4p \ ^{\circ}F + 5 \ 3d^{\circ}(4F)4p \ ^{\circ}G$
425544.3	425465	79	6	$30 \ 3d^{5}(2H)4p^{-5}H + 29 \ 3d^{5}(2G)4p^{-5}H + 17 \ 3d^{5}(2I)4p^{-1}I$
425599.1	425439	160	3	$25 \ 3d_{2}^{5}(2H)4p_{2}^{5}G + 14 \ 3d_{2}^{5}(2G)4p_{2}^{5}G + 6 \ 3d_{2}^{5}(2D)4p_{2}^{1}F$
425877	425993	-116	3	$57 \ 3d_{2}^{5}(4F)4p_{2}^{5}D + 21 \ 3d_{2}^{5}(4F)4p_{3}^{5}F + 5 \ 3d_{3}^{5}(4D)4p_{3}^{5}D$
425954.6	426044	-89	0	$87 \ 3d_{2}^{5}(4F)4p_{2}^{5}D + 7 \ 3d_{2}^{5}(2D)4p_{2}^{5}P_{2}$
426008.4	426107	-99	1	$73 \ 3d^{5}(4F)4p^{5}D + 10 \ 3d^{5}(4F)4p^{5}F$
426112.6	426272	-159	2	$59 \ 3d^{5}(4F)4p \ ^{5}D + 15 \ 3d^{5}(4F)4p \ ^{5}F + 6 \ 3d^{5}(2F)4p \ ^{3}D$
427330.6	426943	388	5	$80 \ 3d^{5}(2H)4p \ {}^{3}I + 9 \ 3d^{5}(2H)4p \ {}^{3}H + 5 \ 3d^{5}(2G)4p \ {}^{3}H$
427367.3	427382	-15	4	19 $3d^{5}(2F)4p {}^{1}G + 17 3d^{5}(2G)4p {}^{1}G + 16 3d^{5}(2G)4p {}^{3}G$
427940.9	427716	225	3	$29 \ 3d^5(2G)4p \ {}^3G + 22 \ 3d^5(4F)4p \ {}^3G + 9 \ 3d^5(2G)4p \ {}^3F$
428048.7	427903	146	1	$34 \ 3d^{5}(2F)4p \ 3D + 31 \ 3d^{5}(2D)4p \ ^{1}P + 8 \ 3d^{5}(2D)4p \ ^{1}P$
428386	428190	196	5	$63 \ 3d^{5}(4F)4p^{3}G + 11 \ 3d^{5}(2G)4p^{3}G + 11 \ 3d^{5}(4F)4p^{5}F$
428430.6	428144	287	6	70 $3d^{5}(2H)4p^{3}I + 11 3d^{5}(2H)4p^{1}I + 8 3d^{5}(2G)4p^{3}H$
428503.5	428561	-58	2	$47 3d^{5}(2F)4p^{-1}D + 22 3d^{5}(2D)4p^{-1}D + 9 3d^{5}(2G)4p^{-3}F$
428672.9	428362	311	4	$55 3d^{5}(4F)4p^{3}G + 13 3d^{5}(2G)4p^{3}G + 6 3d^{5}(2F)4p^{1}G$
429135.6	429119	17	3	$30 3d^{5}(4F)4p^{3}G + 26 3d^{5}(2G)4p^{3}F + 17 3d^{5}(2F)4p^{4}F$
420100.0	420110	_128	4	$46 \ 3d^5(2C)4p \ ^3F + 15 \ 3d^5(2C)4p \ ^1C + 9 \ 3d^5(2F)4p \ ^1C$
429511.5	429105	-120	-	40.30(2G)4p $P + 10.30(2G)4p$ $G + 9.30(2P)4p$ G
429037.4	429910	-208	2	51.5d (2G)4p F + 10.5d (4F)4p F + 7.5d (4D)4p F
429749.9	429467	203	2	$94.50(2\pi)4p$ 1 $40.215(2\pi)4$ 1 π + $20.215(2\pi)4$ 3 π + $(2.215(4\pi)4$ 2 π
429873.4	429616	257	3	$40 \ 3d^{-}(2F)4p^{-}F + 28 \ 3d^{-}(2G)4p^{-}F + 6 \ 3d^{-}(4F)4p^{-}3D$
431218.3	430922	296	6	$72 \ 3d^{\circ}(2H)4p^{-1} + 11 \ 3d^{\circ}(2H)4p^{-0}H + 10 \ 3d^{\circ}(2H)4p^{-0}I$
431231.7	431470	-238	2	$46 \ 3d^{\circ}(4F)4p \ ^{\circ}D + 14 \ 3d^{\circ}(2F)4p \ ^{\circ}D + 10 \ 3d^{\circ}(2F)4p \ ^{\circ}F$
431530.7	431645	-114	3	$39 \ 3d^{\circ}(4F)4p \ ^{\circ}D + 12 \ 3d^{\circ}(2F)4p \ ^{\circ}D + 12 \ 3d^{\circ}(2F)4p \ ^{\circ}F$
431766.6	432093	-326	4	$56 \ 3d^{\circ}(4F)4p \ ^{\circ}F + 25 \ 3d^{\circ}(2F)4p \ ^{\circ}F$
432272.4	432478	-206	1	$76 3d^{5}(4F)4p {}^{3}D + 7 3d^{5}(4D)4p {}^{3}D + 6 3d^{5}(2F)4p {}^{3}D$
432839.7	433122	-282	3	$57 3d^{5}(4F)4p {}^{3}F + 17 3d^{5}(4F)4p {}^{3}D + 11 3d^{5}(2F)4p {}^{3}F$
432840.8	432637	204	5	$31 \ 3d_{2}^{5}(2G)4p \ ^{3}H + 25 \ 3d_{2}^{5}(2G)4p \ ^{3}G + 21 \ 3d_{2}^{5}(2H)4p \ ^{3}H$
432939.3	432771	168	4	$38 \ 3d_{2}^{\circ}(2H)4p \ ^{3}H + 28 \ 3d_{2}^{\circ}(2G)4p \ ^{3}H + 7 \ 3d_{2}^{\circ}(2H)4p \ ^{1}G$
433257.9	433681	-423	2	$56 \ 3d_{2}^{\circ}(4F)4p \ {}^{3}F + 14 \ 3d_{2}^{\circ}(4F)4p \ {}^{3}D + 14 \ 3d_{2}^{\circ}(2F)4p \ {}^{3}F$
434063.7	433893	171	5	$24 \ 3d^{5}(2F)4p \ {}^{3}G + 21 \ 3d^{5}(2H)4p \ {}^{3}H + 18 \ 3d^{5}(2G)4p \ {}^{3}G$
434264	434216	48	3	$29 \ 3d^{5}(2F)4p \ {}^{3}G + 25 \ 3d^{5}(4F)4p \ {}^{3}G + 25 \ 3d^{5}(2G)4p \ {}^{3}G$
434286.4	434177	109	4	$25 \ 3d^5(2F)4p \ ^3G + 15 \ 3d^5(4F)4p \ ^3G + 12 \ 3d^5(2H)4p \ ^3H$
434722.8	434735	-12	6	$44 \ 3d^{5}(2G)4p \ ^{3}H + 36 \ 3d^{5}(2H)4p \ ^{3}H + 15 \ 3d^{5}(2H)4p \ ^{1}I$
434812.2	434270	542	4	$32 \ 3d^5(2F)4p \ {}^{1}G + 19 \ 3d^5(2G)4p \ {}^{3}G + 12 \ 3d^5(2G)4p \ {}^{1}G$
435369.7	435912	-542	3	$33 \ 3d^5(2G)4p \ {}^1F + 27 \ 3d^5(2F)4p \ {}^3F + 7 \ 3d^5(4F)4p \ {}^3F$
435379.2	435701	-322	2	$35 \ 3d^5(2F)4p^{-1}D + 19 \ 3d^5(4F)4p^{-3}F + 14 \ 3d^5(4F)4p \ 3D$
435676.7	435632	45	5	$51 \ 3d^5(2G)4p^{-1}H + 24 \ 3d^5(2H)4p^{-1}H + 13 \ 3d^5(2I)4p^{-1}H$
436243.7	436572	-328	3	$31 \ 3d^{5}(2G)4p^{1}F + 21 \ 3d^{5}(2F)4p^{3}F + 11 \ 3d^{5}(2G)4p^{3}F$
436475.9	436626	-150	2	$41 \ 3d^{5}(2F)4p^{3}F + 32 \ 3d^{5}(2F)4p^{1}D + 12 \ 3d^{5}(2G)4p^{3}F$
436506.5	436937	-431	4	$48 \ 3d^{5}(2F)4p^{3}F + 18 \ 3d^{5}(4F)4p^{3}F + 7 \ 3d^{5}(2F)4p^{1}G$
437233.9	437113	121	5	$63 \ 3d^{5}(2H)4p^{1}H + 27 \ 3d^{5}(2G)4p^{1}H$
438607.7	438028	580	1	$54 3d^{5}(2F)4p^{3}D + 25 3d^{5}(2S)4p^{3}P + 5 3d^{5}(2D)4p^{3}P$
439180.1	438670	510	3	$56 3d^{5}(2F)4p^{3}D + 17 3d^{5}(4F)4p^{3}D + 9 3d^{5}(2F)4p^{3}D$
439327 1	438564	763	2	$70 3d^5(2\text{F})4p ^3\text{D} + 8 3d^5(2\text{F})4p ^3\text{D} + 6 3d^5(4\text{F})4p ^3\text{D}$
439706.8	439557	150	3	$45 3d^{5}(2H)4p^{3}G + 31 3d^{5}(2F)4p^{3}G + 11 3d^{5}(2G)4p^{3}G$
439775	439309	466	1	$54 3d^{5}(2S)4p^{3}P + 27 3d^{5}(2E)4p^{3}D + 8 3d^{5}(2D)4p^{3}P$
440372.2	440206	166	4	$40 \ 3d^5(2H)4p \ ^3G + 41 \ 3d^5(2F)4p \ ^3G + 9 \ 3d^5(2G)4p \ ^3G$
440012.2	440503	303	5	45 36 $^{(21)4p}$ 3 3 41 30 $^{(21)4p}$ 3 3 45 $^{(21)4p}$ 3 3 6 48 34 5 $^{(22)4p}$ 3 3 6
440830.3	440333	208	2	$72 3d^5(2S)4p^{-3}P + 16 3d^5(2D)4p^{-3}P$
441373.8	441108	155	4	$12.3d(25)4p(1 + 10.3d(2D)4p(1 + 22.2d^{5}(2C)4p(1 + 22.2d^{5}(2C$
443432.3	443388	-100	1	42.34(21)4p + 32.34(21)4p + 32.34(20)4p +
444432.7	444620	-307	1	$(25)^{4}p^{-1} + 1850(2D)^{4}p^{-1} + 750(2D)^{4}p^{-1}$
452662.5	445801	-601	- 2	02 50 (21)4p 1 + 0 50 (21)4p 1
400000.0	445891	-601	3	$55 24^{5}(2D)4p^{3}F + 21 24^{5}(2D)4p^{2}D + 5 24^{5}(2C)4p^{3}F$
454176 2	445891 453452	-601 212	3 2 2	$55 \ 3d^5(2D)4p \ {}^3F + 31 \ 3d^5(2D)4p \ 3D + 5 \ 3d^5(2G)4p \ {}^3F$
454176.3	445891 453452 454028	-601 212 148 677	3 2 3	$ \begin{array}{c} 55 \ 3d^5(2D)4p \ ^3F + 31 \ 3d^5(2D)4p \ 3D + 5 \ 3d^5(2O)4p \ ^3F \\ 42 \ 3d^5(2D)4p \ ^3F + 33 \ 3d^5(2D)4p \ 3D + 11 \ 3d^5(2D)4p \ ^1F \\ 90 \ 2d^5(2D)4p \ ^3F \end{array} $
454176.3 454317.5	445891 453452 454028 453641	-601 212 148 677 470	3 2 3 1	$ \begin{array}{c} 55 \ 3d^5(2D)4p \ {}^3F + 31 \ 3d^5(2D)4p \ 3D + 5 \ 3d^5(2G)4p \ {}^3F \\ 42 \ 3d^5(2D)4p \ {}^3F + 33 \ 3d^5(2D)4p \ 3D + 11 \ 3d^5(2D)4p \ {}^1F \\ 89 \ 3d^5(2D)4p \ {}^3D + 20 \ 3d^5(2D)4 \\ 51 \ 2d^5(2D)4p \ {}^3D \\ 51 \ 2d^5(2D)4p \ {}^3D \\ \end{array} $
454176.3 454317.5 454921.2	445891 453452 454028 453641 454443	-601 212 148 677 478	3 2 3 1 2	$ \begin{array}{c} 55 \ 3d^5(2D)4p \ ^3F + 31 \ 3d^5(2D)4p \ 3D + 5 \ 3d^5(2G)4p \ ^3F \\ 42 \ 3d^5(2D)4p \ ^3F + 33 \ 3d^5(2D)4p \ 3D + 11 \ 3d^5(2D)4p \ ^1F \\ 89 \ 3d^5(2D)4p \ ^3D \\ 54 \ 3d^5(2D)4p \ ^3D + 30 \ 3d^5(2D)4p \ ^3F \\ 54 \ 3d^5(2D)4p \ ^3F \\ 54 \ 3d^5(2D)4p \ ^3D + 30 \ 3d^5(2D)4p \ ^3F \\ 54 \ 3d^5(2D)4p \ ^3F \ ^3F \\ 54 \ 3d^5(2D)4p \ ^3F \ ^$
$\begin{array}{r} 454176.3\\ 454317.5\\ 454921.2\\ 456264.2\\ 456545.2\end{array}$	445891 453452 454028 453641 454443 455816 456542		3 2 3 1 2 3	$ \begin{array}{l} 55 \ 3d^5(2D)4p \ ^3F + 31 \ 3d^5(2D)4p \ 3D + 5 \ 3d^5(2G)4p \ ^3F \\ 42 \ 3d^5(2D)4p \ ^3F + 33 \ 3d^5(2D)4p \ 3D + 11 \ 3d^5(2D)4p \ ^1F \\ 89 \ 3d^5(2D)4p \ ^3D \\ 54 \ 3d^5(2D)4p \ ^3D + 30 \ 3d^5(2D)4p \ ^3F \\ 54 \ 3d^5(2D)4p \ ^3D + 38 \ 3d^5(2D)4p \ ^3F \\ 54 \ 3d^5(2D)4p \ ^3D + 38 \ 3d^5(2D)4p \ ^3F \\ 60 \ 2d^5(2D)4p \ ^3F \\ 60 \ 2d^5(2D)4p \ ^3F \\ 54 \ 3d^5(2D)4p \ ^3F \ ^3F \\ 54 \ 3d^5(2D)4p \ ^3F \ ^$
$\begin{array}{r} 454176.3\\ 454317.5\\ 454921.2\\ 456264.2\\ 456545.2\\ 456545.2\end{array}$	445891 453452 454028 453641 454443 455816 456543	-601 212 148 677 478 448 2	3 2 3 1 2 3 4	$ \begin{array}{l} 55 \ 3d^5(2D)4p \ ^3F + 31 \ 3d^5(2D)4p \ 3D + 5 \ 3d^5(2G)4p \ ^3F \\ 42 \ 3d^5(2D)4p \ ^3F + 33 \ 3d^5(2D)4p \ 3D + 11 \ 3d^5(2D)4p \ ^1F \\ 89 \ 3d^5(2D)4p \ ^3D + 30 \ 3d^5(2D)4p \ ^3F \\ 54 \ 3d^5(2D)4p \ ^3D + 38 \ 3d^5(2D)4p \ ^3F \\ 54 \ 3d^5(2D)4p \ ^3F + 6 \ 3d^5(2D)4p \ ^3F \\ 90 \ 3d^5(2D)4p \ ^3F + 6 \ 3d^5(2C)4p \ ^3F \\ 60 \ 3d^5(2D)4p \ ^3F + 6 \ 3d^5(2C)4p \ ^3F \\ 60 \ 3d^5(2D)4p \ ^3F + 6 \ 3d^5(2C)4p \ ^3F \\ \end{array} $
$\begin{array}{r} 454176.3\\ 454317.5\\ 454921.2\\ 456264.2\\ 456545.2\\ 457544.9\\ 45920222\\ \end{array}$	445891 453452 454028 453641 454443 455816 456543 456543	-601 212 148 677 478 448 2 89	$ \begin{array}{c} 3 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 4 \\ 3 \\ $	$ \begin{array}{l} 55 \ 3d^5(2D)4p \ ^3F + 31 \ 3d^5(2D)4p \ 3D + 5 \ 3d^5(2G)4p \ ^3F \\ 42 \ 3d^5(2D)4p \ ^3F + 33 \ 3d^5(2D)4p \ 3D + 11 \ 3d^5(2D)4p \ ^1F \\ 89 \ 3d^5(2D)4p \ ^3D + 30 \ 3d^5(2D)4p \ ^3F \\ 54 \ 3d^5(2D)4p \ ^3D + 38 \ 3d^5(2D)4p \ ^3F \\ 54 \ 3d^5(2D)4p \ ^3F + 6 \ 3d^5(2G)4p \ ^3F \\ 90 \ 3d^5(2D)4p \ ^3F + 6 \ 3d^5(2G)4p \ ^3F \\ 69 \ 3d^5(2D)4p \ ^1F + 12 \ 3d^5(2G)4p \ ^1F + 10 \ 3d^5(2D)4p \ ^3F \\ 64 \ 3d^5(2D)4p \ ^1F + 12 \ 3d^5(2G)4p \ ^1F \\ 64 \ 3d^5(2D)4p \ ^3F \\ \end{array}$
454176.3 454317.5 454921.2 456264.2 456545.2 456545.2 457544.9 458688.9	$\begin{array}{r} 445891 \\ 453452 \\ 453452 \\ 454028 \\ 453641 \\ 454443 \\ 455816 \\ 456543 \\ 457456 \\ 459139 \\ 450132 \end{array}$	-601 212 148 677 478 448 2 89 -450	$ \begin{array}{c} 3 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 4 \\ 3 \\ 0 \\ 2 \\ 3 \\ 2 \\ 3 \\ 4 \\ 3 \\ 0 \\ 2 \\ 3 \\ 2 \\ 3 \\ 4 \\ 3 \\ 0 \\ 2 \\ 3 \\ 2 \\ 3 \\ 4 \\ 3 \\ 0 \\ 2 \\ 3 \\ 3 \\ 2 \\ 3 \\ 3 \\ 3 \\ 2 \\ 3 \\ $	$ \begin{array}{l} 55 \ 3d^5(2D)4p \ ^3F + 31 \ 3d^5(2D)4p \ 3D + 5 \ 3d^5(2G)4p \ ^3F \\ 42 \ 3d^5(2D)4p \ ^3F + 33 \ 3d^5(2D)4p \ 3D + 11 \ 3d^5(2D)4p \ ^1F \\ 89 \ 3d^5(2D)4p \ ^3D + 30 \ 3d^5(2D)4p \ ^3F \\ 54 \ 3d^5(2D)4p \ ^3D + 38 \ 3d^5(2D)4p \ ^3F \\ 90 \ 3d^5(2D)4p \ ^3F + 6 \ 3d^5(2G)4p \ ^3F \\ 69 \ 3d^5(2D)4p \ ^1F + 12 \ 3d^5(2G)4p \ ^1F + 10 \ 3d^5(2D)4p \ ^3F \\ 84 \ 3d^5(2D)4p \ ^3P + 14 \ 3d^5(2G)4p \ ^3P + 5 \ 3d^5(2D)4p \ ^3F \\ 84 \ 3d^5(2D)4p \ ^3P + 14 \ 3d^5(2G)4p \ ^3P + 5 \ 3d^5(2D)4p \ ^3F \\ 84 \ 3d^5(2D)4p \ ^3P + 14 \ 3d^5(2G)4p \ ^3P + 5 \ 3d^5(2D)4p \ ^3F \\ \end{array} $
$\begin{array}{r} 454176.3\\ 454317.5\\ 454921.2\\ 456264.2\\ 456545.2\\ 457544.9\\ 458688.9\\ 458731.8\\ \end{array}$	$\begin{array}{c} 445891\\ 453452\\ 454028\\ 453641\\ 45443\\ 455816\\ 456543\\ 457456\\ 459139\\ 459104\end{array}$	-601 212 148 677 478 448 2 89 -450 -372	3 2 3 1 2 3 4 3 0 2	$ \begin{array}{c} 55 \ 3d^5(2D)4p \ {}^3F + 31 \ 3d^5(2D)4p \ 3D + 5 \ 3d^5(2G)4p \ {}^3F \\ 42 \ 3d^5(2D)4p \ {}^3F + 33 \ 3d^5(2D)4p \ 3D + 11 \ 3d^5(2D)4p \ {}^1F \\ 89 \ 3d^5(2D)4p \ {}^3D \\ 54 \ 3d^5(2D)4p \ {}^3D + 30 \ 3d^5(2D)4p \ {}^3F \\ 54 \ 3d^5(2D)4p \ {}^3D + 38 \ 3d^5(2D)4p \ {}^3F \\ 90 \ 3d^5(2D)4p \ {}^1F + 6 \ 3d^5(2G)4p \ {}^3F \\ 69 \ 3d^5(2D)4p \ {}^1F + 12 \ 3d^5(2G)4p \ {}^1F + 10 \ 3d^5(2D)4p \ {}^3F \\ 84 \ 3d^5(2D)4p \ {}^3P + 14 \ 3d^5(2S)4p \ {}^3P \\ 66 \ 3d^5(2D)4p \ {}^3P + 16 \ 3d^5(2S)4p \ {}^3P + 7 \ 3d^5(2D)4p \ 3D \\ 60 \ 3d^5(2D)4p \ {}^3D + 16 \ 3d^5(2S)4p \ {}^3P + 7 \ 3d^5(2D)4p \ 3D \\ 60 \ 3d^5(2D)4p \ {}^3D + 16 \ 3d^5(2S)4p \ {}^3P + 7 \ 3d^5(2D)4p \ 3D \\ 60 \ 3d^5(2D)4p \ {}^3D + 16 \ 3d^5(2S)4p \ {}^3P + 7 \ 3d^5(2D)4p \ 3D \\ 60 \ 3d^5(2D)4p \ {}^3D + 16 \ 3d^5(2S)4p \ {}^3P + 7 \ 3d^5(2D)4p \ 3D \\ 60 \ 3d^5(2D)4p \ {}^3D + 16 \ 3d^5(2S)4p \ {}^3P + 7 \ 3d^5(2D)4p \ 3D \\ 60 \ 3d^5(2D)4p \ {}^3D + 16 \ 3d^5(2S)4p \ {}^3P + 7 \ 3d^5(2D)4p \ 3D \\ 60 \ 3d^5(2D)4p \ {}^3D + 16 \ 3d^5(2S)4p \ {}^3P + 7 \ 3d^5(2D)4p \ 3D \\ 60 \ 3d^5(2D)4p \ {}^3D + 16 \ 3d^5(2D)4p \ {}^3D + 7 \ 3d^5(2D)4p \ 3D \\ 60 \ 3d^5(2D)4p \ {}^3D + 16 \ 3d^5(2D)4p \ {}^3D + 7 \ 3d^5(2D)4p \ 3D \\ 60 \ 3d^5(2D)4p \ {}^3D + 16 \ 3d^5(2D)4p \ {}^3D + 7 \ 3d^5(2D)4p \ 3D \\ 60 \ 3d^5(2D)4p \ {}^3D + 16 \ 3d^5(2D)4p \ {}^3D + 7 \ 3d^5(2D)4p \ 3D \\ 60 \ 3d^5(2D)4p \ {}^3D + 16 \ 3d^5(2D)4p \ {}^3D + 7 \ {}^$
$\begin{array}{r} 454176.3\\ 454317.5\\ 454921.2\\ 456264.2\\ 456545.2\\ 457544.9\\ 458688.9\\ 458731.8\\ 458778.9\end{array}$	$\begin{array}{r} 445891\\ 453452\\ 454028\\ 453641\\ 4554443\\ 455816\\ 456543\\ 457456\\ 459139\\ 459104\\ 459173\end{array}$	-601 212 148 677 478 448 2 89 -450 -372 -394	$ \begin{array}{c} 3 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 4 \\ 3 \\ 0 \\ 2 \\ 1 \\ \end{array} $	$ \begin{array}{l} 55\ 3d^5\ (2D)4p\ ^3F\ +\ 31\ 3d^5\ (2D)4p\ 3D\ +\ 5\ 3d^5\ (2D)4p\ ^3F\ \\ 42\ 3d^5\ (2D)4p\ ^3F\ +\ 33\ 3d^5\ (2D)4p\ 3D\ +\ 11\ 3d^5\ (2D)4p\ ^1F\ \\ 89\ 3d^5\ (2D)4p\ ^3D\ +\ 30\ 3d^5\ (2D)4p\ ^3F\ \\ 54\ 3d^5\ (2D)4p\ ^3D\ +\ 38\ 3d^5\ (2D)4p\ ^3F\ \\ 90\ 3d^5\ (2D)4p\ ^3D\ +\ 38\ 3d^5\ (2D)4p\ ^3F\ \\ 90\ 3d^5\ (2D)4p\ ^3F\ +\ 63\ 3d^5\ (2D)4p\ ^3F\ \\ 69\ 3d^5\ (2D)4p\ ^1F\ +\ 12\ 3d^5\ (2G)4p\ ^3F\ \\ 84\ 3d^5\ (2D)4p\ ^1F\ +\ 12\ 3d^5\ (2S)4p\ ^3P\ \\ 63\ d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ 3D\ \\ 72\ 3d^5\ (2D)4p\ ^3P\ +\ 15\ 3d^5\ (2S)4p\ ^3P\ +\ 5\ 3d^5\ (2D)4p\ 3D\ \\ \end{array}$
$\begin{array}{r} 454176.3\\ 454317.5\\ 454921.2\\ 456264.2\\ 456545.2\\ 457544.9\\ 458688.9\\ 458731.8\\ 458778.9\\ 460536.5\end{array}$	$\begin{array}{r} 445891\\ 453452\\ 454028\\ 453641\\ 455816\\ 456543\\ 457456\\ 459139\\ 459104\\ 459173\\ 460634 \end{array}$	-601 212 148 677 478 448 2 89 -450 -372 -394 -98	$ \begin{array}{c} 3 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 4 \\ 3 \\ 0 \\ 2 \\ 1 \\ 1 \end{array} $	$ \begin{array}{c} 55 \ 3d^5(2D)4p \ {}^3F + 31 \ 3d^5(2D)4p \ 3D + 5 \ 3d^5(2G)4p \ {}^3F \\ 42 \ 3d^5(2D)4p \ {}^3F + 33 \ 3d^5(2D)4p \ 3D + 11 \ 3d^5(2D)4p \ {}^1F \\ 89 \ 3d^5(2D)4p \ {}^3D + 30 \ 3d^5(2D)4p \ {}^3F \\ 54 \ 3d^5(2D)4p \ {}^3D + 38 \ 3d^5(2D)4p \ {}^3F \\ 54 \ 3d^5(2D)4p \ {}^3F + 6 \ 3d^5(2G)4p \ {}^3F \\ 90 \ 3d^5(2D)4p \ {}^3F + 6 \ 3d^5(2G)4p \ {}^3F \\ 69 \ 3d^5(2D)4p \ {}^3F + 12 \ 3d^5(2G)4p \ {}^3F \\ 84 \ 3d^5(2D)4p \ {}^3P + 14 \ 3d^5(2S)4p \ {}^3P \\ 66 \ 3d^5(2D)4p \ {}^3P + 16 \ 3d^5(2S)4p \ {}^3P + 7 \ 3d^5(2D)4p \ 3D \\ 72 \ 3d^5(2D)4p \ {}^3P + 15 \ 3d^5(2S)4p \ {}^3P + 5 \ 3d^5(2D)4p \ 3D \\ 70 \ 3d^5(2D)4p \ {}^1P + 16 \ 3d^5(2S)4p \ {}^1P + 7 \ 3d^5(2D)4p \ {}^3P \\ \end{array} $
$\begin{array}{c} 454176.3\\ 454317.5\\ 454921.2\\ 456264.2\\ 456545.2\\ 457544.9\\ 458688.9\\ 458731.8\\ 458778.9\\ 460536.5\\ 461609.3\end{array}$	$\begin{array}{r} 445891\\ 453452\\ 4534028\\ 453641\\ 455436\\ 455816\\ 456543\\ 457456\\ 459139\\ 459104\\ 459173\\ 460634\\ 461150\end{array}$	-601 212 148 677 478 448 2 89 -450 -372 -394 -98 459	$ \begin{array}{c} 3 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 4 \\ 3 \\ 0 \\ 2 \\ 1 \\ 1 \\ 2 \end{array} $	$ \begin{array}{c} 55 \ 3d^5 \ (2D) 4p \ ^3F + 31 \ 3d^5 \ (2D) 4p \ 3D + 5 \ 3d^5 \ (2D) 4p \ ^3F \\ 42 \ 3d^5 \ (2D) 4p \ ^3F + 33 \ 3d^5 \ (2D) 4p \ 3D + 11 \ 3d^5 \ (2D) 4p \ ^1F \\ 89 \ 3d^5 \ (2D) 4p \ ^3D + 30 \ 3d^5 \ (2D) 4p \ ^3F \\ 54 \ 3d^5 \ (2D) 4p \ ^3D + 38 \ 3d^5 \ (2D) 4p \ ^3F \\ 90 \ 3d^5 \ (2D) 4p \ ^3F + 6 \ 3d^5 \ (2D) 4p \ ^3F \\ 69 \ 3d^5 \ (2D) 4p \ ^3F + 6 \ 3d^5 \ (2G) 4p \ ^3F \\ 69 \ 3d^5 \ (2D) 4p \ ^3F + 12 \ 3d^5 \ (2G) 4p \ ^3F \\ 84 \ 3d^5 \ (2D) 4p \ ^3P + 14 \ 3d^5 \ (2S) 4p \ ^3P \\ 66 \ 3d^5 \ (2D) 4p \ ^3P + 16 \ 3d^5 \ (2S) 4p \ ^3P + 7 \ 3d^5 \ (2D) 4p \ 3D \\ 72 \ 3d^5 \ (2D) 4p \ ^1P + 16 \ 3d^5 \ (2S) 4p \ ^3P + 5 \ 3d^5 \ (2D) 4p \ ^3P \\ 82 \ 3d^5 \ (2D) 4p \ ^1P + 16 \ 3d^5 \ (2S) 4p \ ^3P + 5 \ 3d^5 \ (2D) 4p \ ^3P \\ 82 \ 3d^5 \ (2D) 4p \ ^1D + 7 \ 3d^5 \ (2D) 4p \ ^3P \\ 82 \ 3d^5 \ (2D) 4p \ ^1D + 7 \ 3d^5 \ (2D) 4p \ ^3P \\ 82 \ 3d^5 \ (2D) 4p \ ^1D + 7 \ 3d^5 \ (2D) 4p \ ^3P \\ 82 \ 3d^5 \ (2D) 4p \ ^1D + 7 \ 3d^5 \ (2D) 4p \ ^3P \\ 82 \ 3d^5 \ (2D) 4p \ ^1D + 7 \ 3d^5 \ (2D) 4p \ ^1D \\ 82 \ 3d^5 \ (2D) 4p \ ^1D \\ 82 \ 3d^5 \ (2D) 4p \ ^1D + 7 \ 3d^5 \ (2D) 4p \ ^1D \\ 82 \ 3d^5 \ (2D) 4p \ ^1D \\ 82 \ 3d^5 \ (2D) 4p \ ^1D \\ 82 \ 3d^5 \ (2D) 4p \ ^1D \\ 82 \ 3d^5 \ (2D) 4p \ ^1D \\ 82 \ 3d^5 \ (2D) 4p \ ^1D \\ 82 \ 3d^5 \ (2D) 4p \ ^1D \\ 82 \ 3d^5 \ (2D) 4p \ ^1D \\ 82 \ 3d^5 \ (2D) 4p \ ^1D \ 3d^5 \ (2D) 4p \ ^1$
$\begin{array}{c} 454176.3\\ 454317.5\\ 454921.2\\ 456264.2\\ 456545.2\\ 457544.9\\ 458688.9\\ 458731.8\\ 458778.9\\ 460536.5\\ 461609.3\\ 461609.3\\ 464741.7\end{array}$	$\begin{array}{r} 445891\\ 453452\\ 454028\\ 453641\\ 455816\\ 456543\\ 457456\\ 459139\\ 459104\\ 459173\\ 460634\\ 461150\\ 464767\end{array}$	$\begin{array}{r} -601\\ 212\\ 148\\ 677\\ 478\\ 448\\ 2\\ 89\\ -450\\ -372\\ -394\\ -98\\ 459\\ -25\\ \end{array}$	$ \begin{array}{r} 3 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 4 \\ 3 \\ 0 \\ 2 \\ 1 \\ 1 \\ 2 \\ 4 \\ 4 \end{array} $	$ \begin{array}{l} 55 \ 3d^5 \ (2D) 4p \ ^3F + 31 \ 3d^5 \ (2D) 4p \ 3D + 5 \ 3d^5 \ (2D) 4p \ ^3F \\ 42 \ 3d^5 \ (2D) 4p \ ^3F \\ 39 \ 3d^5 \ (2D) 4p \ ^3D \\ 54 \ 3d^5 \ (2D) 4p \ ^3D \\ 54 \ 3d^5 \ (2D) 4p \ ^3D + 30 \ 3d^5 \ (2D) 4p \ ^3F \\ 54 \ 3d^5 \ (2D) 4p \ ^3D + 38 \ 3d^5 \ (2D) 4p \ ^3F \\ 90 \ 3d^5 \ (2D) 4p \ ^3F \\ 69 \ 3d^5 \ (2D) 4p \ ^3F \\ 69 \ 3d^5 \ (2D) 4p \ ^3F \\ 69 \ 3d^5 \ (2D) 4p \ ^3F \\ 61 \ 3d^5 \ (2D) 4p \ ^3F \\ 61 \ 3d^5 \ (2D) 4p \ ^3F \\ 61 \ 3d^5 \ (2D) 4p \ ^3F \\ 62 \ 3d^5 \ (2D) 4p \ ^3F \\ 61 \ 3d^5 \ (2D) 4p \ ^3F \\ 71 \ 3d^5 \ (2D) 4p \ ^3F \\ 72 \ 3d^5 \ (2D) 4p \ ^3P + 16 \ 3d^5 \ (2S) 4p \ ^3P \\ 72 \ 3d^5 \ (2D) 4p \ ^3P \\ 71 \ 3d^5 \ (2D) 4p \ ^3P \\ 71 \ 3d^5 \ (2D) 4p \ ^1P + 16 \ 3d^5 \ (2S) 4p \ ^3P \\ 72 \ 3d^5 \ (2D) 4p \ ^1P \\ 71 \ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^1P \\ 71 \ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \ 3d^5 \ (2D) 4p \ ^3P \\ 73 \ 3d^5 \ (2D) 4p \ ^3P \ 3d^5 \ 3d^5 \ (2D) 4p \ ^3P \ 3d^5 \ 3$
$\begin{array}{r} 454176.3\\ 454317.5\\ 454921.2\\ 456264.2\\ 456545.2\\ 457544.9\\ 45878.9\\ 458731.8\\ 458778.9\\ 460536.5\\ 461609.3\\ 464741.7\\ 465130.4\end{array}$	$\begin{array}{r} 445891\\ 453452\\ 454028\\ 453641\\ 455816\\ 456543\\ 457456\\ 459139\\ 459104\\ 459173\\ 460634\\ 461150\\ 464767\\ 465125\end{array}$	$\begin{array}{c} -601\\ 212\\ 148\\ 677\\ 478\\ 448\\ 2\\ 89\\ -450\\ -372\\ -394\\ 459\\ -25\\ 5\end{array}$	$ \begin{array}{r} 3 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 4 \\ 3 \\ 0 \\ 2 \\ 1 \\ 1 \\ 2 \\ 4 \\ 4 \\ 4 \end{array} $	$ \begin{array}{c} 55\ 3d^5\ (2D)4p\ ^3F\ +\ 31\ 3d^5\ (2D)4p\ 3D\ +\ 5\ 3d^5\ (2D)4p\ ^3F\ \\ 42\ 3d^5\ (2D)4p\ ^3F\ +\ 33\ 3d^5\ (2D)4p\ 3D\ +\ 5\ 11\ 3d^5\ (2D)4p\ ^1F\ \\ 89\ 3d^5\ (2D)4p\ ^3D\ +\ 30\ 3d^5\ (2D)4p\ ^3F\ \\ 54\ 3d^5\ (2D)4p\ ^3D\ +\ 38\ 3d^5\ (2D)4p\ ^3F\ \\ 54\ 3d^5\ (2D)4p\ ^3D\ +\ 5\ 3d^5\ (2D)4p\ ^3F\ \\ 69\ 3d^5\ (2D)4p\ ^3F\ +\ 63\ 3d^5\ (2D)4p\ ^3F\ \\ 69\ 3d^5\ (2D)4p\ ^1F\ +\ 12\ 3d^5\ (2G)4p\ ^3F\ \\ 84\ 3d^5\ (2D)4p\ ^3F\ +\ 12\ 3d^5\ (2S)4p\ ^3P\ \\ 76\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ 3D\ \\ 72\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3D\ \\ 70\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \\ 82\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \\ 82\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \\ 70\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \ \\ 53\ 3d^5\ (2D)4p\ ^3P\ +\ 14\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $
$\begin{array}{r} 454176.3\\ 454317.5\\ 454921.2\\ 456264.2\\ 456545.2\\ 457544.9\\ 458688.9\\ 458731.8\\ 458778.9\\ 460536.5\\ 461609.3\\ 464741.7\\ 465130.4\\ 465460\\ \end{array}$	$\begin{array}{r} 445891\\ 453452\\ 454028\\ 453641\\ 454433\\ 455816\\ 456543\\ 457456\\ 459139\\ 459104\\ 459173\\ 460634\\ 461150\\ 466767\\ 465125\\ 465330\\ \end{array}$	$\begin{array}{c} -601\\ 212\\ 148\\ 677\\ 478\\ 448\\ 2\\ 89\\ -450\\ -372\\ -394\\ -98\\ 459\\ -25\\ 5\\ 130\\ \end{array}$	$ \begin{array}{r} 3 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 4 \\ 3 \\ 0 \\ 2 \\ 1 \\ 1 \\ 2 \\ 4 \\ 4 \\ 5 \\ 5 \end{array} $	$ \begin{array}{c} 55\ 3d^5\ (2D)4p\ ^3F\ +\ 31\ 3d^5\ (2D)4p\ 3D\ +\ 5\ 3d^5\ (2D)4p\ ^3F\ \\ 42\ 3d^5\ (2D)4p\ ^3F\ +\ 33\ 3d^5\ (2D)4p\ 3D\ +\ 11\ 3d^5\ (2D)4p\ ^1F\ \\ 89\ 3d^5\ (2D)4p\ ^3D\ +\ 33\ 3d^5\ (2D)4p\ ^3F\ \\ 54\ 3d^5\ (2D)4p\ ^3D\ +\ 38\ 3d^5\ (2D)4p\ ^3F\ \\ 54\ 3d^5\ (2D)4p\ ^3D\ +\ 38\ 3d^5\ (2D)4p\ ^3F\ \\ \\ 90\ 3d^5\ (2D)4p\ ^3D\ +\ 38\ 3d^5\ (2D)4p\ ^3F\ \\ \\ 69\ 3d^5\ (2D)4p\ ^3F\ +\ 6\ 3d^5\ (2G)4p\ ^3F\ \\ \\ 84\ 3d^5\ (2D)4p\ ^3P\ +\ 14\ 3d^5\ (2S)4p\ ^3P\ \\ \\ 84\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ 3D\ \\ \\ 72\ 3d^5\ (2D)4p\ ^3P\ +\ 15\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \\ \\ \\ 82\ 3d^5\ (2D)4p\ ^1P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \\ \\ \\ 82\ 3d^5\ (2D)4p\ ^1P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 5\ 3d^5\ (2D)4p\ ^3P\ \\ \\ \\ \\ 82\ 3d^5\ (2D)4p\ ^1P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \\ \\ \\ \\ \\ \\ \ 5\ 3d^5\ (2G)4p\ ^3F\ +\ 17\ 3d^5\ (2G)4p\ ^3F\ +\ 17\ 3d^5\ (2G)4p\ ^3G\ \ \\ \\ \\ \ 73\ 3d^5\ (2G)4p\ ^3F\ +\ 16\ 3d^5\ (2G)4p\ ^3G\ +\ 8\ 3d^5\ (2G)4p\ ^1H\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $
$\begin{array}{r} 454176.3\\ 454317.5\\ 454921.2\\ 456264.2\\ 456545.2\\ 457544.9\\ 458688.9\\ 458731.8\\ 458778.9\\ 460536.5\\ 461609.3\\ 464741.7\\ 465130.4\\ 465460\\ 465803.6\end{array}$	$\begin{array}{r} 445891\\ 453452\\ 454028\\ 453641\\ 454443\\ 455816\\ 456543\\ 457456\\ 459139\\ 459104\\ 459173\\ 460634\\ 461150\\ 4664767\\ 465125\\ 465330\\ 465969\end{array}$	$\begin{array}{r} -601\\ 212\\ 148\\ 677\\ 478\\ 448\\ 2\\ 89\\ -450\\ -372\\ -394\\ -98\\ 459\\ -25\\ 5\\ 5\\ 130\\ -165\\ \end{array}$	$ \begin{array}{c} 3 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 4 \\ 3 \\ 0 \\ 2 \\ 1 \\ 1 \\ 2 \\ 4 \\ 4 \\ 5 \\ 3 \end{array} $	$ \begin{array}{l} 55\ 3d^5\ (2D)4p\ ^3F\ +\ 31\ 3d^5\ (2D)4p\ 3D\ +\ 5\ 3d^5\ (2D)4p\ ^3F\ \\ 42\ 3d^5\ (2D)4p\ ^3F\ +\ 33\ 3d^5\ (2D)4p\ 3D\ +\ 11\ 3d^5\ (2D)4p\ ^1F\ \\ 89\ 3d^5\ (2D)4p\ ^3D\ +\ 33\ 3d^5\ (2D)4p\ ^3F\ \\ 54\ 3d^5\ (2D)4p\ ^3D\ +\ 38\ 3d^5\ (2D)4p\ ^3F\ \\ 54\ 3d^5\ (2D)4p\ ^3D\ +\ 38\ 3d^5\ (2D)4p\ ^3F\ \\ \\ 90\ 3d^5\ (2D)4p\ ^3D\ +\ 83\ 3d^5\ (2D)4p\ ^3F\ \\ \\ 69\ 3d^5\ (2D)4p\ ^3P\ +\ 6\ 3d^5\ (2G)4p\ ^3F\ \\ \\ 69\ 3d^5\ (2D)4p\ ^3P\ +\ 14\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3F\ \\ \\ 84\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3D\ \\ \\ 72\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \\ \\ \\ 72\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 5\ 3d^5\ (2D)4p\ ^3P\ \\ \\ \\ 82\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 5\ 3d^5\ (2D)4p\ ^3P\ \\ \\ \\ \\ 82\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 5\ 3d^5\ (2D)4p\ ^3P\ \\ \\ \\ \\ \ 73\ 3d^5\ (2G)4p\ ^3H\ +\ 16\ 3d^5\ (2G)4p\ ^3H\ +\ 5\ 3d^5\ (2G)4p\ ^1G\ \\ \\ \ 73\ 3d^5\ (2G)4p\ ^3H\ +\ 16\ 3d^5\ (2G)4p\ ^3H\ +\ 5\ 3d^5\ (2G)4p\ ^1G\ \ \\ \\ \ 73\ 3d^5\ (2G)4p\ ^3F\ +\ 10\ 3d^5\ (2G)4p\ ^3H\ +\ 16\ 3d^5\ (2G)4p\ ^3H\ +\ 5\ 3d^5\ (2G)4p\ ^1H\ \ 16\ 3d^5\ (2G)4p\ ^3H\ +\ 5\ 3d^5\ (2G)4p\ ^1H\ \ 16\ 3d^5\ (2G)4p\ ^3H\ +\ 5\ 3d^5\ (2G)4p\ ^1H\ \ 16\ 3d^5\ (2G)4p\ ^3H\ +\ 5\ 3d^5\ (2G)4p\ ^1H\ \ 16\ 3d^5\ (2G)4p\ ^3H\ +\ 5\ 3d^5\ (2G)4p\ ^1H\ \ 16\ 3d^5\ (2G)4p\ ^3H\ +\ 5\ 3d^5\ (2G)4p\ ^1H\ \ 16\ 3d^5\ (2G)4p\ ^3H\ +\ 16\ 3d^5\ (2G)4p\ ^3H\ +\ 16\ 3d^5\ (2G)4p\ ^3H\ \ 3d^5\ \ 3d$
$\begin{array}{r} 454176.3\\ 454317.5\\ 454921.2\\ 456264.2\\ 456545.2\\ 455754.9\\ 458731.8\\ 458778.9\\ 460536.5\\ 461609.3\\ 464741.7\\ 465130.4\\ 465460\\ 465803.6\\ 467531.5\\ \end{array}$	$\begin{array}{r} 445891\\ 453452\\ 454028\\ 453641\\ 455816\\ 456543\\ 457456\\ 459139\\ 459104\\ 459173\\ 460634\\ 461150\\ 464767\\ 465125\\ 465330\\ 465969\\ 467729\\ \end{array}$	$\begin{array}{r} -601\\ 212\\ 148\\ 677\\ 478\\ 448\\ 2\\ 89\\ -450\\ -372\\ -398\\ 459\\ -25\\ 5\\ 130\\ -165\\ -198\end{array}$	$ \begin{array}{c} 3 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 4 \\ 3 \\ 0 \\ 2 \\ 1 \\ 1 \\ 2 \\ 4 \\ 4 \\ 5 \\ 3 \\ 2 \end{array} $	$ \begin{array}{l} 55\ 3d^5\ (2D)4p\ ^3F\ +\ 31\ 3d^5\ (2D)4p\ 3D\ +\ 5\ 3d^5\ (2D)4p\ ^3F\ \\ 42\ 3d^5\ (2D)4p\ ^3F\ \\ 33\ d^5\ (2D)4p\ ^3D\ \\ 54\ 3d^5\ (2D)4p\ ^3F\ \\ 54\ 3d^5\ (2D)4p\ ^3P\ \\ 54\ 3d^5\ (2D)4p\ ^3F\ \\ 53\ 3d^5\ (2D)4p\ ^3F\ \\ 53\ 3d^5\ (2G)4p\ ^3F\ \\ 53\ 3d^5\ (2G)4p\ ^3F\ \\ 54\ 3d^5\ (2G)4p\ ^3F\ \ \\ 54\ 3d^5\ (2G)4p\ ^3F\ \ \\ 54\ 3d^5\ (2G)4p\ ^3F\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $
$\begin{array}{r} 454176.3\\ 454317.5\\ 454921.2\\ 456264.2\\ 456545.2\\ 457544.9\\ 458638.9\\ 458731.8\\ 458778.9\\ 460536.5\\ 461609.3\\ 464741.7\\ 465130.4\\ 465460\\ 465803.6\\ 467531.5\\ 46759.8\end{array}$	$\begin{array}{r} 445891\\ 453452\\ 454028\\ 453641\\ 455816\\ 456543\\ 457456\\ 459139\\ 459104\\ 459173\\ 460634\\ 461150\\ 464767\\ 465125\\ 465300\\ 465969\\ 467729\\ 467392\end{array}$	$\begin{array}{c} -601\\ 212\\ 148\\ 677\\ 478\\ 448\\ 2\\ 89\\ -450\\ -372\\ -394\\ 459\\ -25\\ 5\\ 130\\ -165\\ -198\\ 208\\ \end{array}$	$ \begin{array}{c} 3 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 4 \\ 3 \\ 0 \\ 2 \\ 1 \\ 1 \\ 2 \\ 4 \\ 4 \\ 5 \\ 3 \\ 2 \\ 6 \\ 6 \\ \end{array} $	$ \begin{array}{c} 55\ 3d^5\ (2D)4p\ ^3F\ +\ 31\ 3d^5\ (2D)4p\ 3D\ +\ 5\ 3d^5\ (2D)4p\ ^3F\ \\ 42\ 3d^5\ (2D)4p\ ^3F\ +\ 33\ 3d^5\ (2D)4p\ 3D\ +\ 11\ 3d^5\ (2D)4p\ ^1F\ \\ 89\ 3d^5\ (2D)4p\ ^3D\ +\ 33\ 3d^5\ (2D)4p\ ^3F\ \\ 54\ 3d^5\ (2D)4p\ ^3D\ +\ 38\ 3d^5\ (2D)4p\ ^3F\ \\ 54\ 3d^5\ (2D)4p\ ^3D\ +\ 38\ 3d^5\ (2D)4p\ ^3F\ \\ 90\ 3d^5\ (2D)4p\ ^3D\ +\ 12\ 3d^5\ (2D)4p\ ^3F\ \\ 90\ 3d^5\ (2D)4p\ ^1F\ +\ 12\ 3d^5\ (2G)4p\ ^3F\ \\ 63\ d^5\ (2D)4p\ ^1F\ +\ 12\ 3d^5\ (2G)4p\ ^3F\ \\ 84\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ 3D\ \\ 72\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3D\ \\ 70\ 3d^5\ (2D)4p\ ^1P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \\ 82\ 3d^5\ (2D)4p\ ^1D\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ +\ 5\ 3d^5\ (2D)4p\ ^3D\ \\ 70\ 3d^5\ (2D)4p\ ^3F\ +\ 24\ 3d^5\ (2G)4p\ ^3F\ +\ 17\ 3d^5\ (2D)4p\ ^3G\ \\ 54\ 3d^5\ (2G)4p\ ^3F\ +\ 33\ 3d^5\ (2G)4p\ ^3H\ +\ 5\ 3d^5\ (2G)4p\ ^1G\ \\ 73\ 3d^5\ (2G)4p\ ^3F\ +\ 40\ 3d^5\ (2G)4p\ ^3G\ +\ 8\ 3d^5\ (2G)4p\ ^1H\ \\ 50\ 3d^5\ (2G)4p\ ^3F\ +\ 40\ 3d^5\ (2G)4p\ ^3F\ \\ 89\ 3d^5\ (2G)4p\ ^3F\ +\ 7\ 3d^5\ (2G)4p\ ^3F\ \\ 89\ 3d^5\ (2G)4p\ ^3F\ +\ 7\ 3d^5\ (2G)4p\ ^3F\ \ \\ 89\ 3d^5\ (2G)4p\ ^3F\ +\ 7\ 3d^5\ (2G)4p\ ^3F\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $
$\begin{array}{r} 454176.3\\ 454317.5\\ 454921.2\\ 456264.2\\ 456545.2\\ 457544.9\\ 458688.9\\ 458731.8\\ 458778.9\\ 460536.5\\ 461609.3\\ 465460\\ 465803.6\\ 467531.5\\ 467599.8\\ 46759.8\\ 467819.2\end{array}$	$\begin{array}{r} 445891\\ 453452\\ 454028\\ 453641\\ 454443\\ 455816\\ 456543\\ 457456\\ 459139\\ 459104\\ 459173\\ 460634\\ 461150\\ 4664767\\ 465125\\ 465330\\ 465969\\ 467729\\ 467729\\ 467954\end{array}$	$\begin{array}{c} -601\\ 212\\ 148\\ 677\\ 478\\ 448\\ 2\\ 89\\ -450\\ -394\\ 459\\ -25\\ 5\\ 130\\ -165\\ -198\\ 208\\ -135\\ \end{array}$	$ \begin{array}{c} 3 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 4 \\ 3 \\ 0 \\ 2 \\ 1 \\ 1 \\ 2 \\ 4 \\ 5 \\ 3 \\ 2 \\ 6 \\ 3 \end{array} $	$ \begin{array}{l} 55\ 3d^5\ (2D)4p\ ^3F\ +\ 31\ 3d^5\ (2D)4p\ 3D\ +\ 5\ 3d^5\ (2D)4p\ ^3F\ \\ 42\ 3d^5\ (2D)4p\ ^3F\ +\ 33\ 3d^5\ (2D)4p\ 3D\ +\ 11\ 3d^5\ (2D)4p\ ^1F\ \\ 89\ 3d^5\ (2D)4p\ ^3D\ +\ 33\ 3d^5\ (2D)4p\ ^3F\ \\ 54\ 3d^5\ (2D)4p\ ^3D\ +\ 38\ 3d^5\ (2D)4p\ ^3F\ \\ 54\ 3d^5\ (2D)4p\ ^3D\ +\ 38\ 3d^5\ (2D)4p\ ^3F\ \\ 89\ 3d^5\ (2D)4p\ ^3D\ +\ 14\ 3d^5\ (2G)4p\ ^3F\ \\ 84\ 3d^5\ (2D)4p\ ^3P\ +\ 14\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \\ 84\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3D\ \\ 72\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3D\ \\ 72\ 3d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3D\ \\ 72\ 3d^5\ (2D)4p\ ^1P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \\ 73\ 3d^5\ (2D)4p\ ^1P\ +\ 7\ 3d^5\ (2D)4p\ ^3F\ +\ 7\ 3d^5\ (2D)4p\ ^3F\ \\ 82\ 3d^5\ (2D)4p\ ^1D\ +\ 7\ 3d^5\ (2D)4p\ ^3F\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \\ 82\ 3d^5\ (2D)4p\ ^1D\ +\ 7\ 3d^5\ (2D)4p\ ^3F\ +\ 7\ 3d^5\ (2D)4p\ ^3F\ \\ 83\ 3d^5\ (2G)4p\ ^3F\ +\ 16\ 3d^5\ (2G)4p\ ^3F\ +\ 7\ 3d^5\ (2G)4p\ ^3F\ +\ 7\ 3d^5\ (2G)4p\ ^3F\ +\ 7\ 3d^5\ (2D)4p\ ^3F\ \ \\ 89\ 3d^5\ (2G)4p\ ^3F\ +\ 7\ 3d^5\ (2D)4p\ ^3F\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $
$\begin{array}{r} 454176.3\\ 454317.5\\ 454921.2\\ 456246.2\\ 456545.2\\ 457544.9\\ 458688.9\\ 458731.8\\ 458778.9\\ 460536.5\\ 461609.3\\ 4654741.7\\ 465130.4\\ 465460\\ 465803.6\\ 467531.5\\ 467599.8\\ 467819.2\\ 468335.2\end{array}$	$\begin{array}{r} 445891\\ 453452\\ 454028\\ 453641\\ 454443\\ 455816\\ 456543\\ 457456\\ 459139\\ 459104\\ 459173\\ 460634\\ 461150\\ 4664767\\ 465125\\ 465330\\ 465969\\ 467729\\ 467392\\ 467954\\ 468448\end{array}$	$\begin{array}{c} -601\\ 212\\ 148\\ 677\\ 478\\ 448\\ 2\\ 89\\ -450\\ -372\\ -398\\ 459\\ -25\\ 5\\ 130\\ -165\\ -198\\ 208\\ -135\\ -113 \end{array}$	$ \begin{array}{c} 3 \\ 2 \\ 3 \\ 1 \\ 2 \\ 3 \\ 4 \\ 3 \\ 0 \\ 2 \\ 1 \\ 1 \\ 2 \\ 4 \\ 4 \\ 5 \\ 3 \\ 2 \\ 6 \\ 3 \\ 4 \\ 4 \\ 5 \\ 3 \\ 2 \\ 6 \\ 3 \\ 4 \\ 4 \\ 5 \\ 3 \\ 2 \\ 6 \\ 3 \\ 4 \\ 4 \\ 5 \\ 3 \\ 2 \\ 6 \\ 3 \\ 4 \\ 4 \\ 5 \\ 3 \\ 2 \\ 6 \\ 3 \\ 4 \\ 4 \\ 5 \\ 3 \\ 2 \\ 6 \\ 3 \\ 4 \\ 5 \\ 3 \\ 5 \\ 3 \\ 4 \\ 5 \\ 3 \\ 4 \\ 5 \\ 3 \\ 5 \\ 3 \\ 4 \\ 5 \\ 3 \\ 4 \\ 5 \\ 3 \\ 4 \\ 5 \\ 3 \\ 4 \\ 5 \\ $	$ \begin{array}{l} 55\ 3d^5\ (2D)4p\ ^3F\ +\ 31\ 3d^5\ (2D)4p\ 3D\ +\ 5\ 3d^5\ (2D)4p\ ^3F\ \\ 42\ 3d^5\ (2D)4p\ ^3F\ +\ 33\ 3d^5\ (2D)4p\ 3D\ +\ 11\ 3d^5\ (2D)4p\ ^1F\ \\ 89\ 3d^5\ (2D)4p\ ^3D\ +\ 33\ 3d^5\ (2D)4p\ ^3F\ \\ 54\ 3d^5\ (2D)4p\ ^3D\ +\ 38\ 3d^5\ (2D)4p\ ^3F\ \\ 54\ 3d^5\ (2D)4p\ ^3D\ +\ 38\ 3d^5\ (2D)4p\ ^3F\ \\ \\ 69\ 3d^5\ (2D)4p\ ^3D\ +\ 38\ 3d^5\ (2D)4p\ ^3F\ \\ \\ 69\ 3d^5\ (2D)4p\ ^3F\ +\ 6\ 3d^5\ (2D)4p\ ^3F\ \\ \\ 69\ 3d^5\ (2D)4p\ ^3F\ +\ 6\ 3d^5\ (2D)4p\ ^3F\ \\ \\ 69\ 3d^5\ (2D)4p\ ^3P\ +\ 14\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \\ \\ \\ 63\ d^5\ (2D)4p\ ^3P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \\ \\ \\ 72\ 3d^5\ (2D)4p\ ^1P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \\ \\ \\ \\ 82\ 3d^5\ (2D)4p\ ^1P\ +\ 16\ 3d^5\ (2S)4p\ ^3P\ +\ 7\ 3d^5\ (2D)4p\ ^3P\ \\ \\ \\ \\ \ 73\ 3d^5\ (2G)4p\ ^3H\ +\ 24\ 3d^5\ (2G)4p\ ^3F\ +\ 17\ 3d^5\ (2G)4p\ ^1G\ \\ \\ \\ \ 73\ 3d^5\ (2G)4p\ ^3F\ +\ 7\ 3d^5\ (2D)4p\ ^3F\ \\ \\ \\ \ 89\ 3d^5\ (2G)4p\ ^3F\ +\ 7\ 3d^5\ (2D)4p\ ^3F\ \\ \\ \ 89\ 3d^5\ (2G)4p\ ^3F\ +\ 7\ 3d^5\ (2D)4p\ ^3F\ \\ \\ \ 89\ 3d^5\ (2G)4p\ ^3F\ +\ 7\ 3d^5\ (2D)4p\ ^3F\ \\ \\ \ 89\ 3d^5\ (2G)4p\ ^3F\ +\ 7\ 3d^5\ (2D)4p\ ^3F\ \\ \\ \ 89\ 3d^5\ (2G)4p\ ^3F\ +\ 7\ 3d^5\ (2D)4p\ ^3F\ \ \ 3d^5\ (2G)4p\ ^3F\ \ \ 3d^5\ \ \ \ 3d^5\ \ \ \ 3d^5\ \ \ \ \ 3d^5\ \ \ \ 3d^5\ \ \ \ \ 3d^5\ \ \ \ 3d^5\ \ \ \ 3d^5\ \ \ \ \ 3d^5\ \ \ \ \ 3d^5\ \ \ \ \ \ 3d^5\ \ \ \ 3d^5\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $

Table A8: Continued

			Τa	
E^{a}_{exp}	E^b_{calc}	ΔE	J	Leading components (in %) in LS coupling c
471595.2	471450	145	5	$88 \ 3d^5(2G)4p^{-1}H + 5 \ 3d^5(2G)4p^{-3}G$
471769.3	471973	-204	4	91 $3d^{5}(2G)4p$ ¹ G
473212.1	473441	-229	3	76 $3d^{5}(2G)4p^{-1}F + 10 3d^{5}(2D)4p^{-1}F + 5 3d^{5}(2D)4p^{-1}F$
481411.7	481292	120	0	$74 \ 3d^{5}(2P)4p \ ^{3}P + 21 \ 3d^{5}(2D)4p \ ^{3}P$
481793.2	481612	181	1	$72 \ 3d^5(2P)4p \ ^3P + 22 \ 3d^5(2D)4p \ ^3P$
483006.9	482815	192	2	$70 \ 3d^5(2P)4p \ ^3P + 24 \ 3d^5(2D)4p \ ^3P$
488810.3	488641	169	2	$55 \ 3d^5(2P)4p \ ^3D + 28 \ 3d^5(2P)4p \ ^1D + 6 \ 3d^5(2D)4p \ ^1D$
488869.4	488819	50	1	$88 \ 3d^5(2P)4p \ ^3D + 6 \ 3d^5(2D)4p \ ^3D$
491155.1	491019	136	3	$87 \ 3d^5(2P)4p \ ^3D + 8 \ 3d^5(2D)4p \ ^3D$
491878.9	491764	115	2	$46 \ 3d^{5}(2P)4p^{1}D + 34 \ 3d^{5}(2P)4p^{3}D + 12 \ 3d^{5}(2D)4p^{1}D$
493316.5	493517	-201	1	$80 \ 3d^5(2P)4p \ {}^3S + 14 \ 3d^5(2P)4p \ {}^1P$
495292.7	494929	364	1	$59 \ 3d^{5}(2P)4p \ ^{1}P + 17 \ 3d^{5}(2P)4p \ ^{3}S + 16 \ 3d^{5}(2D)4p \ ^{1}P$
502689	502588	101	2	$61 \ 3d^{5}(2D)4p \ {}^{3}F + 19 \ 3d^{5}(2D)4p \ {}^{3}F + 8 \ 3d^{5}(2D)4p \ {}^{3}D$
503114.1	502969	145	3	$58 \ 3d^5(2D)4p \ {}^3F + 18 \ 3d^5(2D)4p \ {}^3F + 9 \ 3d^5(2D)4p \ {}^3D$
504630.2	504513	117	1	$70 \ 3d^{5}(2D)4p^{3}D + 21 \ 3d^{5}(2D)4p^{3}D + 7 \ 3d^{5}(2P)4p^{3}D$
505107.8	504938	170	4	71 $3d^{5}(2D)4p^{3}F + 23 3d^{5}(2D)4p^{3}F + 6 3d^{5}(2G)4p^{3}F$
507108.1	507066	42	3	$58 \ 3d^5(2D)4p \ ^3D + 18 \ 3d^5(2D)4p \ ^3D + 10 \ 3d^5(2D)4p \ ^3F$
507132.9	507310	-177	2	41 $3d^{5}(2D)4p^{1}D + 17 3d^{5}(2P)4p^{1}D + 14 3d^{5}(2D)4p^{1}D$
509325.1	509521	-196	2	41 $3d^{5}(2D)4p^{3}P + 21 3d^{5}(2P)4p^{3}P + 15 3d^{5}(2D)4p^{3}P$
509967.2	509818	149	3	$68 3d^5(2D)4p {}^1F + 21 3d^5(2D)4p {}^1F + 6 3d^5(2G)4p {}^1F$
510178.2	510388	-210	1	$54 \ 3d^5(2D)4p \ {}^{3}P + 25 \ 3d^5(2P)4p \ {}^{3}P + 19 \ 3d^5(2D)4p \ {}^{3}P$
510942.6	511192	-249	0	$55 \ 3d^{5}(2D)4p \ {}^{3}P + 24 \ 3d^{5}(2P)4p \ {}^{3}P + 19 \ 3d^{5}(2D)4p \ {}^{3}P$

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ſ	Wavelength	Lower Level	J_{low}	Upper Level	J_{up}	log gf	gA	CF		
	228.143	30418	6	468739	5	-0.8	2.02E+10	0.354		
	228.662	31009	5	468335	4	-0.96	1.39E + 10	0.286		
	231 825	37378	5	468739	5	-0.93	$1.45E \pm 10$	-0.2		
	201.020	77994	4	507109	2	-0.50	2 12 - 10	0.256		
	232.021	11224	4	307108	3	-0.0	3.13E+10	0.250		
	232.91	38469	4	467819	3	-1	1.22E+10	-0.341		
	232.992	77909	2	507108	3	-0.98	1.27E + 10	0.515		
	233.926	77145	2	504630	1	-0.79	1.96E + 10	0.376		
	234.241	64968	3	491879	2	-0.98	1.26E + 10	-0.286		
	235.189	46406	6	471595	5	-0.27	6.42E + 10	-0.424		
	235.238	0	4	425102	4	-0.64	2.80E + 10	-0.265		
	235.471	1196	3	425877	3	-0.77	$2.06E \pm 10$	-0.256		
	235 937	64968	3	488810	2	-0.92	$1.43E \pm 10$	-0.439		
	236 708	87506	4	500067	3	0.3	$5.95E \pm 10$	0.306		
	230.100	1100	-4	409406	3	-0.5	1.45 ± 10	0.050		
	237.4	1190	3	422420	4	-0.91	$1.43E \pm 10$	-0.273		
	237.962	1987	2	422221	3	-0.81	1.84E + 10	-0.282		
	238.025	2489	1	422613	2	-0.95	1.31E + 10	-0.29		
	238.568	37378	5	456545	4	-0.93	1.39E + 10	-0.201		
	239.228	47119	3	465130	4	-0.98	1.22E + 10	-0.352		
	240.727	77909	2	493317	1	-0.62	2.79E + 10	-0.777		
	241.306	77468	3	491879	2	-0.75	$2.03E \pm 10$	-0.659		
	241 586	77224	4	491155	3	-0.24	$6.56E \pm 10$	0.73		
	242.881	77145	2	188860	1	0.61	$2.77E \pm 10$	0.749		
	242.001	77469	2	400009	1	-0.01	$2.77E \pm 10$ $2.94E \pm 10$	0.749		
	243.100	11408	3	400010	2	-0.7	$2.24E \pm 10$	0.471		
	244.244	47119	3	456545	4	-1	1.13E + 10	-0.5		
	244.412	47119	3	456264	3	-0.99	1.14E + 10	-0.228		
	245.56	75774	1	483007	2	-0.96	1.22E + 10	0.703		
	245.783	54747	2	461609	2	-0.75	1.93E + 10	-0.28		
	245.851	53787	0	460537	1	-0.95	1.24E + 10	-0.491		
	246 611	31009	5	436507	4	-0.9	$1.37E \pm 10$	-0.382		
	246.854	77000	2	483007	2	0.56	$3.00E \pm 10$	0.643		
	240.004	21000	5	424812	4	-0.50	3.00E + 10	0.566		
	247.040	31009	5	404012	4	-0.71	2.09E+10	0.300		
	247.742	30418	6	434064	5	-0.11	$8.45E \pm 10$	-0.656		
	247.968	31009	5	434286	4	-0.43	4.05E+10	-0.413		
	248.153	31288	4	434264	3	-0.4	4.35E + 10	-0.461		
	248.426	0	4	402534	4	-0.1	8.51E + 10	-0.872		
	248.495	30418	6	432841	5	-0.47	3.68E + 10	0.622		
	248.673	0	4	402134	3	-0.96	$1.19E \pm 10$	-0.278		
	248 86	31009	5	432841	5	-0.78	$1.81E \pm 10$	-0.239		
	240.00	21288	4	422041	4	0.01	1.22E 10	0.120		
	248.972	31200	4	452939	4	-0.91	1.55E+10	-0.122		
	249.022	1196	3	402767	2	-0.97	1.16E + 10	-0.285		
	249.166	1196	3	402534	4	-0.85	1.51E+10	0.648		
	249.212	0	4	401264	5	-0.64	2.46E + 10	-0.503		
	249.415	1196	3	402134	3	-0.71	2.10E + 10	-0.362		
	249.827	2489	1	402767	2	-0.84	1.54E + 10	0.57		
	249.908	1987	2	402134	3	-0.71	2.09E + 10	0.581		
	250.396	1196	3	400563	4	-0.73	$1.97E \pm 10$	-0.424		
	250 418	30418	õ	429750	7	-0.62	$2.57E \pm 10$	-0.81		
	200.410	20756	4	421767		0.02	1.14E+10	0.001		
	250.02	1106	-4	200881	-4-	-0.97	$1.14E \pm 10$ $1.97E \pm 10$	-0.085		
	250.824	1196	3	399881	3	-0.92	1.27E+10	-0.406		
	250.898	31009	5	429578	4	-0.98	1.10E + 10	-0.542		
	251.248	30418	6	428431	6	-0.91	1.29E + 10	-0.639		
	251.276	30418	6	428386	5	-0.59	2.68E+10	-0.2		
	251.323	1987	2	399881	3	-0.98	1.10E + 10	-0.252		
	251.352	31288	4	429136	3	-0.81	1.62E + 10	-0.145		
	251.399	38469	4	436244	3	-0.79	1.71E + 10	-0.255		
	251.459	47612	4	445291	3	-0.81	$1.63E \pm 10$	0.114		
	251 469	31009	5	428673	4	-0.85	$1.48E \pm 10$	-0.127		
	251.500	28007	2	426476	-1	0.07	1.19E 10	0.207		
	251.529	21000	5	430470	6	-0.97	$1.12E \pm 10$ $1.12E \pm 10$	-0.297		
	251.022	31009	5	426431	0	-0.97	1.12E + 10	-0.402		
	251.671	37378	5	434723	6	-0.43	3.93E + 10	-0.82		
	251.924	2489	1	399435	2	-0.96	1.16E + 10	-0.419		
	251.947	37378	5	434286	4	-0.47	3.60E + 10	0.602		
	252.002	32756	4	429578	4	-0.75	1.87E + 10	-0.17		
	252.089	37378	5	434064	5	-0.67	2.27E + 10	0.211		
	252.117	64968	3	461609	2	-0.3	5.19E + 10	-0.772		
	252.157	33296	3	429873	3	-0.73	1.97E + 10	-0.323		
	252.225	38907	3	435379	2	-0.72	1.99E + 10	-0.393		
	252 284	2733	õ	300113	1	1	$1.04E \pm 10$	0.68		
	252 307	38460	4	434812	4	0.87	1.01E + 10 1.40E + 10	0.206		
	202.001	21000	-1	407221	-1	0.01	1.40E + 10	0.607		
	252.52	2480	1	427331	1	-0.89	$1.34E \pm 10$ $1.14E \pm 10$	-0.097		
	202.011	2469	1	398723	1	-0.90	1.14E + 10	-0.821		
	252.498	31288	4	427331	5	-1	1.04E + 10	-0.326		
	252.578	33740	2	429657	2	-0.63	2.48E + 10	-0.242		
	252.627	33296	3	429136	3	-0.8	1.68E + 10	-0.162		
	252.642	38469	4	434286	4	-0.84	1.52E + 10	0.176		
	252.656	38469	4	434264	3	-0.71	2.05E + 10	0.604		
	252 78	0	4	395601	3	-0.15	$7.46E \pm 10$	-0.673		
	252 784	38460	4	434064	5	0.62	$2.40E \pm 10$	0.438		
	252.764	38409	-4 E	434004	4	-0.02	$2.49E \pm 10$ 1.96E ± 10	-0.438		
	404.0UD	31318	5	432939	4	-0.92	1.20E + 10	-0.34		
	252.868	37378	5	432841	5	-0.65	2.34E + 10	-0.267		
	252.922	38907	3	434286	4	-0.93	1.22E + 10	-0.404		
	252.936	38907	3	434264	3	-0.51	3.25E + 10	0.492		
	253.083	30418	6	425544	6	-0.51	3.25E + 10	-0.448		
	253.108	1196	3	396284	2	-0.32	4.99E + 10	-0.831		
	253.382	46714	2	441376	2	-0.66	2.27E + 10	-0.62		
	253 414	32756	4	427367	4	-0.94	$1.20E \pm 10$	-0.11		
	200.414	1007	-± 0	206524	1	0.94	204E + 10	-0.11		
	200.402	1301	4	495544	L C	-0.71	2.04E+10 1.42E+10	-0.00		
	253.463	31009	5	425544	6	-0.86	1.43E+10	0.524		
	253.546	1196	3	395601	3	-0.98	1.08E+10	0.176		
	253.557	37378	5	431767	4	-0.79	1.67E + 10	0.215		
	253.568	38469	4	432840	3	-0.84	1.50E + 10	0.169		
	253.568	38469	4	432841	5	-0.92	1.26E + 10	-0.216		
	253.607	31288	4	425599	3	-0.81	1.59E + 10	-0.146		
	253.616	1987	2	396284	2	-0.74	1.90E + 10	0.428		
	253.642	47119	3	441376	2	-0.39	4.28E + 10	0.505		
	253.042	1106	2	205/07	2 /	-0.39 _0 K9	3.07E.10	-0.456		
	200.071	1190	3	393407	4	-0.03	3.07E+10	-0.430		
l	⊿03.091	ააბსბ	U	420049	1	-0.94	1.105-10	0.218	J	

Table A9: Computed oscillator strengths and transition probabilities in Cu VI.

Table A9: Continued

Wavelength	Lower Level	JLow	Upper level	J _{Up}	log gf	gA	CF
253.696	30418	6	424590	5	-0.7	2.08E+10 1.09E+10	-0.133
253.785	2489	4	396524	1	-0.83	1.52E+10 1.52E+10	0.233 0.567
253.787	38907	3	432939	4	-0.83	$1.52E{+}10$	-0.365
254.008	31009	5	424698	4	-0.47	3.54E+10	-0.378
254.050	38469	4	431767	4	-0.94	$1.20E \pm 10$ $1.08E \pm 10$	-0.431 -0.228
254.5	46848	1	439775	1	-0.51	3.19E + 10	-0.76
254.504	1196	3	394117	3	-0.46	3.56E + 10	-0.429
254.529	117084	2	509967 302713	3	-0.72	1.97E+10 2.30E+10	0.691
254.643	30418	6	423124	5	-0.49	3.35E+10	0.579
254.704	46714	2	439327	2	-0.59	2.66E + 10	-0.363
254.706	31009	5	423618	5	-0.56	2.85E + 10	-0.534
254.760	29285	4 2	421623	э 3	-0.52	3.08E+10	-0.762
254.936	0	4	392255	3	-0.82	1.57E + 10	0.385
254.945	117084	2	509325	2	-0.96	1.14E + 10	0.597
254.967	47119	3	439327	2	-0.63	2.41E+10 2.70E+10	-0.755
255.006	1987	2	429578 394134	2	-0.57	2.79E+10 2.21E+10	-0.33
255.017	1987	2	394117	3	-0.51	3.16E + 10	-0.346
255.062	47119	3	439180	3	-0.2	6.44E+10	-0.607
255.171	46714 32756	2	438608 424590	1	-0.49	3.35E+10 4 19E+10	-0.803
255.215	32685	1	424512	2	-0.41	3.93E + 10	0.699
255.303	0	4	391692	5	-0.53	3.06E + 10	0.791
255.334	2489	1	394134	2	-0.7	2.03E+10	-0.363
255.393	31288	4	424355 422841	4	-0.33	4.83E+10	-0.23 0.573
255.411	2489	1	394015	1	-0.83	1.53E + 10	-0.553
255.417	1196	3	392713	4	-0.26	5.58E + 10	-0.439
255.418	77224	4	468739 420873	5	-0.43	3.80E+10 1.36E+10	0.729 0.183
255.492	33296	3	424698	4	-0.92	1.24E+10	-0.155
255.571	2733	0	394015	1	-0.92	1.22E + 10	-0.401
255.682	77224	4	468335	4	-0.67	2.18E+10	0.765
255.708	29285	2	420356 424333	3	-0.27	2.15E+10	0.668
255.841	77468	3	468335	4	-0.68	2.16E + 10	0.412
255.867	46406	6	437234	5	-0.94	1.17E + 10	-0.049
255.918	38907	3	429657	2	-0.8	1.61E+10 1.78E+10	-0.143
256.156	77145	2	467532	2	-0.26	5.54E+10	0.739
256.179	77468	3	467819	3	-0.33	4.72E + 10	0.745
256.234	1987	2	392255	3	-0.94	1.16E + 10	0.16
256.358	29285 32756	2	419365 422834	2	-0.39	$4.09E \pm 10$ 1.82E \pm 10	-0.554 0.465
256.378	117084	2	507133	2	-0.41	3.93E+10	0.665
256.417	37378	5	427367	4	-0.84	1.48E + 10	-0.176
256.617	54747 22756	2	444433	1	-0.21	6.22E+10 1.62E+10	0.867 0.475
256.631	33740	4 2	422420	4	-0.79	$1.96E \pm 10$	-0.475
256.65	33740	2	423375	$\tilde{2}$	-0.47	3.44E + 10	0.617
256.659	47612	4	437234	5	-0.46	3.49E + 10	0.515
256.676	38907 47119	3	428504 436507	2	-0.85	1.42E + 10 1.74E + 10	-0.558
256.891	46406	6	435677	5	0.45	2.82E+11	0.959
256.931	33868	0	423078	1	-0.76	1.74E + 10	0.643
256.958	32756	4	421925	4	-0.75	1.80E + 10	0.223
257.137	31288	4	420356 427367	3	-0.87	1.38E+10 2.22E+10	-0.426 0.214
257.157	32756	4	421623	3	-0.99	1.04E + 10	-0.127
257.181	32685	1	421516	1	-0.8	1.60E + 10	-0.546
257.242	32685 77145	1	421424 465804	03	-0.96	1.11E+10 2.80E+10	-0.67
257.313	47612	4	436244	3	-0.46	3.51E+10	0.491
257.35	31288	4	419864	3	-0.86	1.39E + 10	-0.23
257.509	77468	3	465804	3	-0.52	3.05E+10	0.384
257.794	55296 77224	4	465130	4	-0.25	$6.58E \pm 10$	-0.843 0.748
257.881	33740	2	421516	1	-0.56	2.72E + 10	-0.844
257.893	47612	4	435370	3	-0.59	2.62E+10	0.43
257.998	32756 77224	4	420356 464742	3	-0.25	$5.67E \pm 10$ 2.32E \pm 10	0.588 0.454
258.215	77468	3	464742	4	-0.81	1.57E + 10	-0.645
258.256	37378	5	424590	5	0.01	1.03E+11	-0.739
258.264	47612 37378	4 5	434812 424333	4 4	-0.48 -0.73	3.35E+10 1.85E+10	$0.264 \\ 0.378$
258.451	32685	1	419606	1	-1	9.82E+09	-0.327
258.604	38907	3	425599	3	-0.23	5.88E + 10	-0.683
258.688	29285	2	415852	2	-0.94	1.14E + 10	0.547
258.010	40406 38469	ю 4	432841 424698	э 4	-0.81	$1.04E \pm 10$ $5.91E \pm 10$	0.595 -0.584
258.917	31288	4	417512	4	-0.22	6.03E + 10	-0.405
258.925	31009	5	417221	5	-0.01	9.77E+10	-0.69
259.058	38469	4	424483	3	-0.97	1.06E+10 1.66EJ 11	-0.241
259.157	33740	2	419606	1	-0.83	1.46E+10	0.573
259.238	37378	5	423124	5	-0.66	2.18E + 10	0.38
259.265	87506	4	473212	3	0.03	1.06E+11	0.746
259.353	38907 47612	3 4	424483 432939	3 4	-0.82 -0.55	1.51E+10 2.83E+10	-0.266 -0.657
259.554	30418	6	415694	7	-0.28	5.17E + 10	-0.797
259.73	31009	5	416025	5	-0.74	1.82E + 10	0.565
259.784	38469	4	423403	3	-0.73	1.86E+10 9.03E-10	0.335
259.905	32756	4	417512	4	-0.85	1.39E+10	-0.248
260.047	37378	5	421925	4	-0.72	1.88E + 10	-0.288
260.1	38907	3	423375	2	-0.69	2.00E+10	-0.425
260.238	87506 87506	4 4	471769 471505	4	0.12	1.30E+11 2.25E ± 10	0.764 0.574
260.472	47612	4	431531	3	-0.74	1.81E + 10	-0.449
260.913	32756	4	416025	5	-0.95	1.10E + 10	0.349
261.227	46848	1	429657	2	-0.77	1.69E + 10 1.54E + 10	0.411
201.430	32730	4	415258 170	3	-0.8	1.04E+10	0.252
			110				

Table A9: Continued

Wavelength	Lower Level	JLow	Upper level	J_{Up}	log gf	gA	CF
261.466	47119	3	429578	4	-0.7	1.96E+10	0.468
261.601	47612	4	429130	3	-0.04	8.97E+10	-0.631
261.765	30418	6	412440	7	-0.64	2.24E + 10	0.646
261.789	37378	5	419365	4	-1	9.75E + 09	0.324
261.803	47612	4	429578 436476	4	-0.38	4.10E + 10 1.20E + 10	0.575
262.107	47612	4	429136	3	-0.76	1.71E + 10	0.345
262.126	54747	2	436244	3	-0.88	1.27E + 10	-0.218
262.425	47612	4	428673	4	-0.88	1.27E + 10	-0.449
262.44	31288	4	412326	э 1	-0.33	4.55E+10 4.40E+10	-0.552
262.539	38469	4	419365	4	-0.99	9.91E+09	-0.225
262.562	31009	5	411872	6	-0.87	1.30E + 10	0.483
262.589	77909	2	458732	2	-0.53	2.88E+10	-0.735
262.721	54747 54747	2	435379 435370	2	-0.94	1.10E + 10 1.54E + 10	-0.301
262.93	47612	4	427941	3	-0.66	2.10E+10	-0.323
262.934	64968	3	445291	3	0.02	1.02E + 11	0.74
262.986	47119	3	427367	4	-0.99	9.93E+09	0.495
263 756	46406	4 6	427507	4 6	-0.5	$5.08E \pm 10$ $5.72E \pm 10$	-0.345
263.829	37378	5	416411	6	-0.32	4.61E + 10	0.388
264.025	38469	4	417221	5	-0.4	3.78E + 10	0.411
264.128	38907	3	417512	4	-0.48	3.14E+10	0.383
264.302	77909	2	456264	3	-0.92	1.15E+10	-0.567
264.404	117084	2	495293	1	-0.11	7.46E + 10	-0.806
264.828	32685	1	410289	1	-0.8	1.50E + 10	-0.363
265.191	47612	4	424698	4	-0.89	1.23E+10 1.44E+10	-0.333
265.637	46406	6	422859	6	0.19	$1.44E \pm 10$ $1.47E \pm 11$	0.438 0.711
265.768	77909	$\tilde{2}$	454176	3	-0.98	9.88E + 09	0.585
265.793	117084	2	493317	1	-0.85	1.33E + 10	0.757
266.054	46406	6	422270	6	-0.54	2.69E + 10 2.50E + 10	-0.697
266.805	47119	∠ 3	429013	3 4	-0.87	$1.27E \pm 10$	0.651
267.192	53787	õ	428049	1	-0.56	2.62E + 10	0.864
267.382	32756	4	406753	3	-0.84	1.37E + 10	-0.27
267.554	54747 54747	2	428504	2	-0.27	4.93E+10 1.01E+10	-0.525
268.301	30418	6	403133	5	0.14	1.01E + 10 1.28E + 11	-0.300 0.575
268.761	31009	$\tilde{5}$	403087	4	0.04	1.01E + 11	0.515
268.761	31288	4	403366	3	-0.79	1.50E + 10	-0.412
269.033	31288	4	402989	3	-0.15	6.55E+10 1.57E+10	0.426 0.18
269.642	46406	6	430244 417267	7	-0.36	4.04E+10	-0.18 0.821
269.785	33296	3	403961	2	-0.54	2.66E + 10	0.332
269.825	32756	4	403366	3	-0.54	2.62E + 10	0.253
269.977	64968 22756	3	435370	3	-0.28	4.80E + 10 2.72E + 10	-0.717
270.01	33740	2	403133	1	-0.33	1.45E+10	0.367
270.1	32756	4	402989	3	-0.82	1.40E + 10	0.265
270.242	87506	4	457545	3	-0.91	1.13E+10	-0.111
270.286	37378 64968	5 3	407356 434812	4	-0.2	5.71E+10 3.01E+10	-0.372
270.423	33296	3	403087	4	-0.57	2.48E+10	-0.457
270.483	38469	4	408178	3	-0.35	4.10E + 10	-0.312
270.549	46406	6	416025	5	-0.96	9.98E + 09	0.076
270.556	38907	4 3	417221 408282	2	-0.85	3.13E+10	-0.282
270.789	53787	õ	423078	1	-0.93	1.07E + 10	-0.464
270.82	33740	2	402989	3	-0.61	2.24E+10	-0.573
271.011	29285	2	398273	2 5	-0.52	2.71E+10 3.67E+10	0.519
272.346	47012 47119	3	414299	2	-0.39	3.81E+10 3.81E+10	0.488 0.458
272.414	31288	4	398377	4	-0.46	3.13E + 10	0.346
272.469	31009	5	398023	5	-0.33	4.21E+10	0.358
272.489	30418 46714	2	397404 413073	1	-0.25	$1.96E \pm 10$	0.377
273.027	64968	3	431232	2	-0.91	1.10E + 10 1.10E + 10	-0.38
273.407	37378	5	403133	5	-0.33	4.16E + 10	0.378
274.187	47612	4	412326	5	-0.92	1.08E + 10	0.271
274.20	32756	4	396929	4	-0.30	$2.40E \pm 10$ $3.29E \pm 10$	-0.345
274.664	38907	3	402989	3	-0.73	1.65E + 10	0.218
274.804	74712	0	438608	1	-0.99	8.97E+09	0.458
274.973	77224 75774	4	440896 439327	5	-0.59	2.27E+10 2.08E+10	-0.313 0.415
275.076	64968	3	428504	2	-0.98	9.17E+09	0.29
275.128	77909	2	441376	2	-0.8	1.41E + 10	0.6
275.238	33296	3	396617	3	-0.6	2.24E+10	-0.265
275.699	77408 33740	3 2	440372 396455	4 2	-0.05	$1.90E \pm 10$ $1.76E \pm 10$	-0.299 -0.315
275.815	77145	2	439707	3	-0.73	1.64E + 10	0.298
276.276	77224	4	439180	3	-0.75	1.56E + 10	-0.272
276.8	77909 3737°	2 5	439180	3	-0.32	4.16E+10 1.79EJ 10	0.398 0.614
277.82	46714	2	406659	2	-0.73	1.63E+10	0.323
278.061	47119	3	406753	3	-0.7	1.73E + 10	0.524
278.122	38469	4	398023	5	-0.84	1.24E+10	0.498
278.125	37378 38907	5 3	396929 398377	4 4	-0.7	1.74E+10 9.37E+09	0.252 0.5
278.332	77224	4	436507	4	-0.4	3.41E + 10	-0.294
278.522	77468	3	436507	4	-0.98	9.11E + 09	0.305
278.726	77468	3	436244	3	-0.56	2.37E + 10 2.62E + 10	-0.343
279.214	38469	4	396617	2 3	-0.98	9.06E+09	0.148
279.256	47119	3	405214	3	-0.67	1.81E + 10	0.348
279.498	87506	4	445291	3	-0.49	2.77E+10	0.376
279.673	74712 77994	0	432272 434286	1	-0.94	9.86E+09 1.13E±10	-0.36 0.42
280.798	117084	2	473212	3	-0.07	7.25E+10	-0.661
280.81	77145	2	433258	2	-0.69	1.74E + 10	0.231
280.956	87506	4	443433	4	-0.13	6.25E+10	-0.469
281.005	((408	3	433208	2	-0.09	1.11E+10	0.406
			119				

Table A9: Continued

Wavelength 281 202	Lower Level 77224	J _{Low}	Upper level 432840	JUP	log gf -0.57	gA 2 28E+10	CF 0.406
281.328	75774	1	431232	2	-1	8.54E+09	-0.226
281.395 281.485	0	3 4	432840 355259	3	-0.51 -0.07	2.63E+10 7.19E+10	-0.63
281.589 281.737	77145	2	432272	1	-0.71	1.64E+10 3.65E+10	0.382 0.596
281.745	77909	2	432840	3	-0.97	9.02E+09	-0.37
281.939 282.053	1987 77224	2 4	$356674 \\ 431767$	1 4	-0.79 -0.31	1.36E+10 4.13E+10	-0.574 0.366
282.241	77224	4	431531	3	-0.93	9.77E+09	0.111
282.339 282.366	$2489 \\ 1987$	$\frac{1}{2}$	$356674 \\ 356137$	$\frac{1}{2}$	-0.68 -0.57	1.74E+10 2.26E+10	$0.581 \\ 0.593$
282.435	1196	3	355259	3	-0.66	1.83E+10	0.617
282.436	77468	3	431531 431232	3 2	-0.83	1.24E+10 9.63E+09	0.162
282.788 285.794	77909 46714	2	431531	3	-0.87	1.11E+10 1.41E+10	-0.149
285.869	47119	3	396929	4	-0.59	2.09E+10	-0.363
285.936 286.036	$87506 \\ 46848$	4	$437234 \\ 396455$	$\frac{5}{2}$	-0.54 -0.93	2.34E+10 9.52E+09	-0.365 -0.336
287.215	87506	4	435677	5	-0.39	3.28E + 10	0.579
290.255 297.274	117084 77909	$\frac{2}{2}$	$461609 \\ 414299$	2 2	-0.71 -0.88	1.53E+10 9.95E+09	$0.302 \\ 0.169$
935.694	322877	7	429750	7	-0.88	1.00E+09	0.753
956.584 979.23	299143	о 6	427331 401264	э 5	-0.94 -0.76	8.29E+08 1.20E+09	-0.599
987.102	299256	5	400563	4	-0.76	1.20E+09	-0.574
998.477	299282	3	399435	2	-0.67	1.20E+09 1.42E+09	-0.701
1001.38 1017.694	299251 299143	2	399113 397404	1 6	-0.7 -0.95	1.32E+09 7 23E+08	-0.859 0.87
1023.473	309046	3	406753	3	-0.68	1.33E+09	-0.701
$1035.486 \\ 1039.853$	322792 309046	5	$419365 \\ 405214$	4	-0.57 -0.78	1.70E+09 1.02E+09	0.677 0.367
1040.03	299256	5	395407	4	-0.48	2.04E+09	-0.638
1040.429 1053.927	299293 299251	4	$395407 \\ 394134$	$\frac{4}{2}$	-0.94 -0.72	7.02E+08 1.16E+09	$0.69 \\ 0.892$
1054.277	299282	3	394134	2	-0.26	3.28E+09	-0.72
1054.46 1054.58	299282 299293	3 4	394117 394117	3	-0.55 -0.17	1.68E+09 4 05E+09	0.753
1055.252	299251	2	394015	1	-0.28	3.14E+09	-0.895
1055.748	322792 322805	5	417512 417267	4 7	0.25	1.07E+10 1.41E+09	-0.925 0.654
1058.992	322792	5	417221	5	-0.75	1.07E+09	0.914
1059.136 1059.434	$322805 \\ 322877$	6 7	$417221 \\ 417267$	5 7	0.3	1.19E+10 9.26E+08	-0.816 0.941
1060.89	250877	3	345137	4	0.38	1.41E + 10	-0.942
1062.3 1062.822	308998 308998	5 5	$403133 \\ 403087$	$\frac{5}{4}$	$0.41 \\ -0.71$	1.51E+10 1.14E+09	$0.875 \\ 0.884$
1064.104	309111	4	403087	4	0.26	1.08E + 10	0.802
1064.428 1064.479	$299143 \\ 309046$	6 3	$393090 \\ 402989$	7	0.59	2.28E+10 4.35E+09	-0.925 0.7
1065.212	309111	4	402989	3	-0.79	9.50E + 08	0.791
$1067 \\ 1068.159$	309046 322792	3 5	$402767 \\ 416411$	2 6	-0.69 -0.66	1.20E+09 1.30E+09	-0.582 -0.788
1068.305	322805	6	416411	6	0.02	6.16E + 09	0.771
1069.135 1070.015	322877 299256	7 5	$416411 \\ 392713$	6 4	0.29	1.13E+10 5.66E+09	-0.665 -0.599
1070.084	299143	6	392594	6	-0.96	6.34E+08	0.074
1070.314 1070.438	299282 299293	3 4	392713 392713	$\frac{4}{4}$	-0.7	1.15E+09 2.24E+09	-0.829 0.54
1070.965	299143	6	392517	5	0.15	8.26E+09	-0.584
1071.38	299256 299256	э 5	$392594 \\ 392517$	5	-0.33	1.85E+10 2.70E+09	0.363
1072.582	322792	5	416025	5	0	5.88E+09	-0.848
1072.729	322805	4 6	416025	5	-0.17	6.66E + 08	-0.89 0.245
1074.252	309046	3	402134	3	-0.62	1.39E+09	-0.388
1075.706	299293	4	392255	3	-0.59	1.46E+09	0.629
1076.546 1077.388	322805 322877	6	415694	7	0.27	1.06E+10 1.15E+10	-0.887
1079.416	322877	7	415520	8	0.64	2.50E+10	-0.935
1080.512 1082.251	299143 250877	6	391692 343277	5	-0.19	3.68E+09 1.01E+10	0.698
1082.265	299293	4	391692	5	0.31	1.15E+10	-0.82
1087.641 1087.95	299256 299282	5	391198 391198	4	-0.7 0.3	1.11E+09 1.12E+10	$0.478 \\ -0.851$
1092.698	309046	3	400563	4	-0.08	4.70E + 09	0.816
1094.48 1094.708	299251 250877	2	390618 342225	$\frac{3}{2}$	0.22	9.14E+09 7.06E+09	-0.887 -0.942
1098.48	265639	2	356674	1	-0.12	4.24E+09	-0.935
1100.895 1104.996	$309046 \\ 265639$	3	$399881 \\ 356137$	3 2	-0.95 0.1	6.12E+08 6.86E+09	$0.243 \\ -0.936$
1115.633	322805	6	412440	7	0.25	9.45E + 09	-0.592
$1115.821 \\ 1116.514$	$265639 \\ 299143$	2 6	355259 388708	3 6	$0.24 \\ 0.49$	9.21E+09 1.65E+10	-0.933 0.948
1116.537	322877	7	412440	7	0.21	8.60E + 09	-0.945
1116.888 1117.048	322792 322805	5	412326 412326	5 5	-0.19	8.23E+09 2.81E+09	$0.736 \\ 0.928$
1119.438	309046	3	398377	4	0.05	5.94E+09	-0.926
1119.832 1121.251	299143 299256	ь 5	388442 388442	ь 5	-0.34 0.34	$_{2.43E+09}$ 1.18E+10	$0.934 \\ 0.792$
1122.584	322792	5	411872	6	0.3	1.05E + 10	-0.664
$1122.745 \\ 1122.885$	322805 299256	6 5	$411872 \\ 388312$	6 4	0.05 -0.29	2.73E+09	-0.852 0.933
1123.351	299293	4	388312	4	0.23	8.91E+09	0.761
1123.661 1124.177	322877 299282	7 3	411872 388236	ь З	-0.98 0.1	5.46E + 08 6.67E + 09	-0.926 0.77
1124.313	299293	4	388236	3	-0.35	2.34E+09	0.936
1124.34 1124.708	299251 309111	2 4	398023	$\frac{2}{5}$	-0.04 0.39	4.83E+09 1.29E+10	0.815 -0.907
1124.738	299282	3	388192	2	-0.56	1.47E + 09 1.57E + 10	0.938
1131.133	308998 308998	о 5	397404 396929	ю 4	$0.48 \\ 0.27$	1.07E+10 9.66E+09	-0.937 -0.886
1138.715	309111	4	396929	4	-0.74	9.42E + 08	0.866

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	Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA	CF
l	1142.775	309111	4	396617	3	0.12	6.78E + 09	-0.867
	1144.055	309046	3	396455	2	-0.18	3.40E + 09	-0.923
	1146.295	309046	3	396284	2	-0.87	6.90E + 08	0.378
	1157.93	309046	3	395407	4	-1	4.96E + 08	-0.234
	1201.793	309046	3	392255	3	-1	4.55E + 08	0.189
	1254.548	308998	5	388708	6	-0.93	5.05E + 08	0.848

Table A9: Continued

Cu VII

Energy Levels

E^a_{exp}	E^{b}_{calc}	ΔE	J	Leading components (in %) in LS coupling c
0	-13	13	2.5	$100 \ 3d^{5} \ {}^{6}S$
46442.7	46565	-122	5.5	$100 \ 3d^5 \ ^4G$
46515.3	46383	132	2.5	$99 \ 3d^5 \ ^4G$
46575	46604	-29	4.5	$100 \ 3d^{5} \ {}^{4}G$
46578.2	46520	58	3.5	$99 \ 3d^5 \ ^4G$
50731.7	50742	-10	2.5	$86 \ 3d^5 \ ^4P + 12 \ 3d^5 \ ^4D$
51066.6	51059	8	1.5	$89 \ 3d^5 \ ^4P + 10 \ 3d^5 \ ^4D$
51406.6	51420	-13	0.5	96 3d ^{5 4} P
55742.2	55792	-50	3.5	99 3d ^{5 4} D
56209.9	56168	42	0.5	96 3d ^{5 4} D
56427.2	56473	-46	2.5	$87 \ 3d^5 \ ^4D + 12 \ 3d^5 \ ^4P$
56428.5	56434	-6	1.5	$89 \ 3d^5 \ ^4D + 10 \ 3d^5 \ ^4P$
67757.3	67660	97	5.5	98 3d ^{5 2} I
67917.9	67993	-75	6.5	$100 \ 3d^5 \ ^2I$
70875.6	70762	114	2.5	$49 \ 3d^5 \ ^2D + 32 \ 3d^5 \ ^2F + 15 \ 3d^5 \ ^2D$
72226.8	72213	14	1.5	$68 \ 3d^5 \ ^2D + 21 \ 3d^5 \ ^2D + 11 \ 3d^5 \ ^4F$
74407.6	74668	-260	3.5	$92 \ 3d^5 \ {}^2F + 5 \ 3d^5 \ {}^4F$
75930.5	75980	-50	4.5	$93 \ 3d^5 \ ^4F + 6 \ 3d^5 \ ^2G$
76019	76095	-76	2.5	$73 \ 3d^5 \ {}^4F + 22 \ 3d^5 \ {}^2F$
76349.1	76277	72	3.5	91 $3d^{5} {}^{4}F + 6 3d^{5} {}^{2}F$
76886	76876	10	1.5	$89 \ 3d^5 \ ^4F + 9 \ 3d^5 \ ^2D$
77529.3	77389	140	2.5	$44 \ 3d^5 \ {}^2F + 24 \ 3d^5 \ {}^2D + 23 \ 3d^5 \ {}^4F$
80717	80653	64	4.5	$71 \ 3d^5 \ ^2H + 25 \ 3d^5 \ ^2G$
81954.4	81992	-38	5.5	97 3d ⁵ ² H
82745.5	82790	-45	3.5	$97 \ 3d^5 \ ^2G$
83910.4	83935	-25	4.5	$68 \ 3d^5 \ ^2G + 28 \ 3d^5 \ ^2H$
87979.2	88025	-46	2.5	97 3d ^{5 2} F
88279.7	88128	152	3.5	97 3d ^{5 2} F
95875.4	95932	-57	0.5	$100 \ 3d^5 \ ^2S$
106957	106878	79	1.5	100 3d ⁵ ² D
107130.6	107135	-4	2.5	99 3d ^{5 2} D
119534	119545	-11	4.5	$100 \ 3d^{5} \ ^{2}G$
119605.4	119648	-43	3.5	$99 \ 3d^5 \ ^2G$
143933.7	143910	24	1.5	99 3d ⁵ ² P
144077.2	144131	-54	0.5	100 3d ⁵ ² P
156224.4	156181	43	2.5	$77 \ 3d^5 \ ^2D + 23 \ 3d^5 \ ^2D$
156373.6	156377	-3	1.5	$76 \ 3d^5 \ ^2D + 23 \ 3d^5 \ ^2D$

Table A10: Comparison between available experimental data and calculated odd energy levels (in $\rm cm^{-1})$ in Cu VII

a: Experimental energies from [105] b: This work c: Only the components \geq to 5% are given

Table A11: Comparison between available experimental data and calculated odd energy levels (in cm⁻¹) in Cu VII

E^a_{exp}	E^b_{calc}	ΔE	J	Leading components (in $\%$) in LS coupling ^{c}
497624	497489	135	1.5	$90 \ 3d^4(5D)4p \ ^6P + 7 \ 3d^4(5D)4p \ 4P$
497863	497657	206	2.5	93 3d ⁴ (5D)4p ⁶ P
498317	498057	260	3.5	$98 \ 3d^4(5D)4p^{-6}P$
498775	499069	-294	0.5	$65 \ 3d^4(5D)4p \ ^4P + 32 \ 3d^4(5D)4p \ ^6D$
500706	500802	-96	1.5	$51 \ 3d^4(5D)4p \ {}^4P + 36 \ 3d^4(5D)4p \ {}^6D + 10 \ 3d^4(5D)4p \ {}^6P$
502909	502882	27	2.5	$58 \ 3d^{4}(5D)4p \ ^{6}D + 34 \ 3d^{4}(5D)4p \ 4P + 6 \ 3d^{4}(5D)4p \ ^{6}P$
504338	504276	62	0.5	$68 \ 3d^4(5D)4p \ ^6D + 31 \ 3d^4(5D)4p \ 4P$
504729	504631	98	1.5	$60 \ 3d^4(5D)4p \ ^6D + 38 \ 3d^4(5D)4p \ ^4P$
505447	505280	167	2.5	$59 \ 3d^4(5D)4p \ ^4P + 38 \ 3d^4(5D)4p \ ^6D$
508524	508408	116	1.5	$94 \ 3d^{+}(5D)4p^{+}F$
508877	508703	174	2.5	$92 3d^{+}(5D)4p^{+}F$
509418	509167	251	3.5	$89 \ 3d^{4}(5D)4p^{4}F + 5 \ 3d^{4}(5D)4p^{6}D$
510250	509928	322	4.5	$81 3d^{-}(5D)4p^{-}F + 14 3d^{-}(5D)4p^{-}D$
51/84/	518055	-208	0.5	$90 3d^{-}(5D)4p^{-}D$
518282	518443	-101	1.5	$90 3d^{-}(5D)4p^{-}D$
510415	510500	-115	2.0	90 30 (3D)4p D $96 2d^4(5D)4p ^4D$
528404	519509	- 94	3.0 2.5	50 50 (5D)4p D $74 2d^4(2H)4p 4H + 21 2d^4(2C)4p 4H$
520027	520068	-12	4.5	4 3d (3f)4p fi \pm 2f 3d (3G)4p fi 60 2d ⁴ (2H)4p ⁴ H \pm 10 2d ⁴ (2C)4p ⁴ H \pm 8 2d ⁴ (2H)4p ⁴ I
529027	520884	-41	4.0	$70 3d^{4}(3H)4p^{4}H + 17 3d^{4}(3G)4p^{4}H + 11 3d^{4}(3H)4p^{4}H$
531047	531008	39	6.5	$76 3d^{4}(3H)4p^{4}H + 13 3d^{4}(3G)4p^{4}H + 9 3d^{4}(3H)4p^{4}I$
532460	532075	385	2.5	$40 \ 3d^4(3P)4p \ ^4D + 26 \ 3d^4(3P)4p \ ^4D + 17 \ 3d^4(3F)4p \ ^4D$
533066	533079	-13	3.5	$27 3d^{4}(3F)4p {}^{4}G + 17 3d^{4}(3G)4p {}^{4}G + 14 3d^{4}(3F)4p {}^{4}G$
533103	532965	138	4.5	$58 3d^{4}(3H)4p^{4}I + 8 3d^{4}(3H)4p^{4}H + 7 3d^{4}(3H)4p^{2}G$
533685	533587	98	0.5	$41 \ 3d^4(3P)4p^4P + 22 \ 3d^4(3P)4p \ 4P + 15 \ 3d^4(3P)4p^2S$
534128	533733	395	4.5	$29 \ 3d^4(3H)4p^4I + 14 \ 3d^4(3F)4p^4G + 13 \ 3d^4(3H)4p^4G$
534204	533796	408	3.5	$31 \ 3d^4(3F)4p^4D + 25 \ 3d^4(3P)4p^4D + 16 \ 3d^4(3P)4p^4D$
534912	534654	258	5.5	$67 \ 3d^4(3H)4p \ ^4I + 11 \ 3d^4(3H)4p \ ^4G + 11 \ 3d^4(3H)4p \ ^4H$
535632	535162	470	5.5	$38 \ 3d^4(3H)4p \ ^4G + 25 \ 3d^4(3G)4p \ ^4G + 19 \ 3d^4(3H)4p \ ^4I$
536229	536291	-62	1.5	$55 \ 3d^4(3P)4p \ ^4P + 29 \ 3d^4(3P)4p \ ^4P$
536650	536534	116	4.5	$31 \ 3d^4(3H)4p^2G + 20 \ 3d^4(3F)4p^2G + 14 \ 3d^4(3G)4p^4G$
537169	537180	-11	2.5	$33 \ 3d^4(3H)4p \ ^4G + 27 \ 3d^4(3F)4p \ ^4G + 14 \ 3d^4(3G)4p \ ^4G$
537802	537633	169	3.5	$46 \ 3d^{4}(3H)4p \ {}^{4}G + 32 \ 3d^{4}(3F)4p \ {}^{4}G + 14 \ 3d^{4}(3G)4p \ {}^{4}G$
537874	537807	67	2.5	44 $3d^4(3F)4p \ {}^4F + 11 \ 3d^4(3F)4p \ {}^2D + 9 \ 3d^4(3H)4p \ {}^4G$
538144	537939	205	4.5	$42 \ 3d^{4}(3F)4p \ {}^{4}G + 36 \ 3d^{4}(3H)4p \ {}^{4}G + 7 \ 3d^{4}(3F)4p \ {}^{4}G$
538624	538331	293	2.5	$54 \ 3d^4(3P)4p \ ^4P + 28 \ 3d^4(3P)4p \ 4P + 5 \ 3d^4(3P)4p \ ^2D$
538749	538777	-28	3.5	$60 \ 3d^{4}(3F)4p \ {}^{4}F + 11 \ 3d^{4}(3F)4p \ {}^{4}F + 10 \ 3d^{4}(3G)4p \ {}^{4}F$
539041	538800	241	5.5	$60 \ 3d^{4}(3F)4p \ {}^{4}G + 18 \ 3d^{4}(3H)4p \ {}^{4}G + 13 \ 3d^{4}(3F)4p \ {}^{4}G$
539146	539272	-126	4.5	$54 \ 3d^{4}(3F)4p \ {}^{4}F + 15 \ 3d^{4}(3G)4p \ {}^{4}F + 10 \ 3d^{4}(3F)4p \ {}^{4}F$
539640	539940	-300	2.5	$14 \ 3d^{4}(3F)4p^{2}D + 14 \ 3d^{4}(3G)4p^{4}F + 12 \ 3d^{4}(3G)4p^{2}F$
540086	540131	-45	1.5	21 $3d^{4}(3F)4p^{2}D + 21 3d^{4}(3F)4p^{4}F + 9 3d^{4}(3D)4p^{2}D$
540915	540877	38	1.5	$37 \ 3d^{4}(3F)4p^{4}D + 13 \ 3d^{4}(3F)4p^{4}D + 10 \ 3d^{4}(3G)4p^{4}F$
540925	540904	21	3.5	$22 \ 3d^{4}(3G)4p \ {}^{4}F + 22 \ 3d^{4}(3P)4p \ {}^{4}D + 14 \ 3d^{4}(3P)4p \ {}^{4}D$
541444	541807	-363	2.5	$27 \ 3d^{4}(3G)4p^{2}F + 14 \ 3d^{4}(3D)4p^{2}F + 12 \ 3d^{4}(3F)4p^{4}D$
541457	541680	-223	4.5	$31 3d^{4}(3H)4p^{2}H + 26 3d^{4}(3G)4p^{4}H + 12 3d^{4}(3G)4p^{2}H$
541509	540981	528 120	0.0	$82 3d^{-}(3H)4p^{-1} + 11 3d^{-}(3G)4p^{-H}$
541884	541745	139	3.5	69.3d (3G)4p H + 21.3d (3H)4p H $40.24^4(2C)4z 4E + 18.24^4(2E)4z 4E + 0.24^4(2E)4z 4E$
542239	542259	-20	4.0	49 50 (5G)4p $F + 18 50 (5F)4p F + 9 50 (5D)4p F$ 16 24 ⁴ (2C)4p ² F + 16 24 ⁴ (2D)4p ² F + 16 24 ⁴ (2C)4p ⁴ F
542302	542070	261	1.5	10 30 30 4 5 $^{+}$ 10 30 30 4 10 10 30 30 4 10 $^$
542394 542776	542133	-125	2.5	21.50(3G)4p F + 14.50(3F)4p F $37.3d^4(3G)4p$ 4F + 15.3d ⁴ (3F)4p 4F + 15.3d ⁴ (3F)4p 4D
543188	543060	128	5.5	$36 3d^4(3G)4p 4H + 26 3d^4(3H)4p 2H + 16 3d^4(3G)4p 2H$
543217	543139	78	3.5	$24 \ 3d^4(3F)4p^4D + 19 \ 3d^4(3G)4p^4F + 10 \ 3d^4(3F)4p^4F$
543244	543002	242	1.5	$22 \ 3d^4(3G)4p^4F + 19 \ 3d^4(3P)4p^2P + 14 \ 3d^4(3F)4p^4D$
543574	543293	281	4.5	$48 \ 3d^4(3G)4p^4H + 23 \ 3d^4(3H)4p^2H + 11 \ 3d^4(3H)4p^4H$
544873	544242	631	1.5	$36 \ 3d^4(3P)4p^2D + 23 \ 3d^4(3P)4p^2D + 9 \ 3d^4(3G)4p^4F$
546268	545746	522	2.5	$41 \ 3d^{4}(3P)4p^{2}D + 26 \ 3d^{4}(3P)4p^{2}D + 5 \ 3d^{4}(3P)4p \ 4P$
546771	546378	393	2.5	$55 \ 3d^4(3F)4p^2F + 20 \ 3d^4(3G)4p^2F + 5 \ 3d^4(3P)4p^2D$
546881	546990	-109	3.5	$26 \ 3d^4(3F)4p^2G + 15 \ 3d^4(3F)4p^2G + 14 \ 3d^4(3H)4p^2G$
547090	547235	-145	5.5	$38 \ 3d^{4}(3G)4p^{2}H + 18 \ 3d^{4}(3H)4p^{2}H + 16 \ 3d^{4}(3G)4p^{4}G$
547381	547495	-114	4.5	$23 \ 3d^{4}(3F)4p^{2}G + 12 \ 3d^{4}(3F)4p^{2}G + 12 \ 3d^{4}(3G)4p^{2}G$
547565	547500	65	3.5	$50 \ 3d^4(3F)4p^2F + 30 \ 3d^4(3G)4p^2F$
548001	547913	88	2.5	$52 \ 3d^4(3G)4p \ ^4G + 32 \ 3d^4(3H)4p \ ^4G + 5 \ 3d^4(3F)4p \ ^2F$
548491	548364	127	3.5	49 $3d^{4}(3G)4p {}^{4}G + 24 3d^{4}(3H)4p {}^{4}G + 6 3d^{4}(3F)4p {}^{2}G$
549249	549135	114	4.5	$40 \ 3d^4(3G)4p \ ^4G + 18 \ 3d^4(3H)4p \ ^4G + 13 \ 3d^4(3G)4p \ ^2H$
550007	549870	137	5.5	46 3d ⁺ (3G)4p ⁺ G + 21 3d ⁺ (3G)4p ⁻ H + 18 3d ⁺ (3H)4p ⁺ G
550053	550667	-614	2.5	$51 3a^{-}(3D)4p^{-}P + 26 3d^{-}(3D)4p^{-}D + 5 3d^{+}(3P)4p^{-}P$
551508	552407	-899	3.5	$75 3d^{-}(3D)4p^{-}D + 7 3d^{-}(3D)4p^{-}F + 5 3d^{-}(3G)4p^{-}F$
551743	552463	-720	2.5	48 3d (3D)4p D + 20 3d (3D)4p P + 8 3d (3D)4p F
551903	551648	200	0.0	$60 \ 3d^{-}(11)4p^{-1} + 34 \ 3d^{-}(11)4p^{-K} + 6 \ 3d^{-}(3H)4p^{-1}$
552250	552167	-855	3.0 5.5	40.50 (1G)4p F + 20.50 (1G)4p F + 18.50 (5G)4p G 88.24 ⁴ (11)4p ² I
552120	552410	192	0.0 1 5	$\begin{array}{c} 88 \ 50 \ (11)^{4}\text{P} & 1 \\ 60 \ 2d^{4}(2\text{D})^{4}\text{P} & 4\text{P} + 11 \ 2d^{4}(2\text{D})^{4}\text{P} & \frac{4}{2}\text{D} + 7 \ 2d^{4}(2\text{D})^{4}\text{P} & \frac{4}{2}\text{F} \end{array}$
553490	553853	-363	4.5	$51 3d^4(3G)4p^2G + 21 3d^4(3H)4p^2G + 11 3d^4(1G)4p^2G$
553703	553770	-67	3.5	$49 \ 3d^4(3G)4p^2G + 17 \ 3d^4(3H)4p^2G + 9 \ 3d^4(1G)4p^2F$
553950	554244	-294	0.5	$87 3d^4(3\text{D})4\text{p} \ ^4\text{P} + 7 3d^4(3\text{P})4\text{p} \ ^4\text{P}$
554123	554268	-145	4.5	$47 \ 3d^4(1G)4p^2H + 21 \ 3d^4(1G)4p^2H + 10 \ 3d^4(3G)4p^2H$
554201	555068	-867	0.5	$39 \ 3d^4(3D)4p^2P + 35 \ 3d^4(1S)4p^2P + 9 \ 3d^4(3D)4p^4D$
555069	555490	-421	5.5	$54 \ 3d^4(1G)4p^2H + 18 \ 3d^4(1G)4p^2H + 11 \ 3d^4(1I)4p^2H$
555137	556274	-1137	1.5	$62 \ 3d^4(3D)4p^2P + 19 \ 3d^4(1S)4p^2P + 6 \ 3d^4(3D)4p^4D$
555295	554827	468	6.5	$64 \ 3d^4(1I)4p^2K + 35 \ 3d^4(1I)4p^2I$
555314	555863	-549	2.5	49 3d ⁴ (1G)4p ${}^{2}F$ + 23 3d ⁴ (1G)4p ${}^{2}F$ + 6 3d ⁴ (3G)4p ${}^{2}F$
555395	555919	-524	3.5	63 3d ⁴ (3D)4p ⁴ F + 19 3d ⁴ (3G)4p ⁴ F + 12 3d ⁴ (3D)4p ⁴ D
555800	556340	-540	4.5	76 $3d_{4}^{4}(3D)4p_{2}^{4}F + 19 3d_{4}^{4}(3G)4p_{2}^{4}F$
558348	559260	-912	3.5	45 $3d^{4}(1G)4p^{2}G + 30 3d^{4}(1G)4p^{2}G + 9 3d^{4}(3G)4p^{2}G$
559339	560050	-711	4.5	42 $3d_{4}^{*}(1G)4p_{2}^{2}G + 32 3d_{4}^{4}(1G)4p_{2}^{2}G + 18 3d_{4}^{4}(3G)4p_{2}^{2}G$
560328	560307	21	1.5	$34 \ 3d^{+}(1D)4p^{-2}D + 18 \ 3d^{+}(1S)4p^{-2}P$
560658	560942	-284	5.5	$333^{4}(11)4p + 1333^{4}(1G)4p + 933^{4}(3G)4p + 14$
561271	561860	-589	0.5	$40 \ 3a^{-}(3D)4p^{-}P + 29 \ 3d^{-}(1S)4p^{-}P + 12 \ 3d^{+}(1D)4p^{-}P$
561005	561500	-321	4.5	ou ou (11)4p H + 10 3d ⁻ (3G)4p ⁻ H + 8 3d ⁻ (1G)4p ² H 47 2d ⁴ (1D)4p ² D + 10 2d ⁴ (2D)4- ² D + 17 2d ⁴ (1D)4- ² D
562178 562178	562508	309 _420	⊿.0 3.5	$(1D)^{4}p D + 13 30 (3D)^{4}p D + 17 30 (1D)^{4}p D$ 62 3d ⁴ (3D)4p ² F + 10 3d ⁴ (3C)4p ² F + 7 3d ⁴ (1F)4p ² F
004110	002090	-440	0.0	$\sim \sim $

			Ta	ble AII: Continued
E^a_{exp}	E^{b}_{calc}	ΔE	J	Leading components (in %) in LS coupling c
562816	563160	-344	2.5	49 $3d^4(3D)4p {}^2F + 19 3d^4(1F)4p {}^2F + 16 3d^4(3G)4p {}^2F$
563705	564030	-325	1.5	$25 \ 3d^{4}(1D)4p^{2}D + 24 \ 3d^{4}(1S)4p^{2}P + 12 \ 3d^{4}(3D)4p^{2}P$
565170	565169	1	1.5	$70 \ 3d^{4}(3D)4p^{2}D + 15 \ 3d^{4}(3F)4p^{2}D + 5 \ 3d^{4}(1D)4p^{2}D$
565670	565238	432	2.5	$35 \ 3d^4(1D)4p \ {}^2F + 20 \ 3d^4(3D)4p \ {}^2D + 16 \ 3d^4(3D)4p \ {}^2F$
567069	566385	684	2.5	$35 \ 3d^4(3D)4p^2D + 18 \ 3d^4(1D)4p^2F + 16 \ 3d^4(1D)4p^2D$
567778	566943	835	3.5	49 $3d^4(1D)4p {}^2F + 28 3d^4(1F)4p {}^2F + 12 3d^4(1D)4p {}^2F$
572310	571556	754	2.5	$61 \ 3d^4(1F)4p \ ^2F + 12 \ 3d^4(1G)4p \ ^2F + 11 \ 3d^4(1D)4p \ ^2F$
573402	573064	338	0.5	$68 \ 3d^4(1D)4p \ ^2P + 14 \ 3d^4(1D)4p \ ^2P + 9 \ 3d^4(1S)4p \ ^2P$
573463	572399	1064	3.5	$46 \ 3d^{4}(1F)4p^{2}F + 23 \ 3d^{4}(1D)4p^{2}F + 10 \ 3d^{4}(1G)4p^{2}F$
574043	573284	759	1.5	56 $3d^4(1D)4p {}^2P + 16 3d^4(1S)4p {}^2P + 12 3d^4(1G)4p {}^2P$
575709	575410	299	3.5	$84 \ 3d^4(1F)4p^2G + 6 \ 3d^4(1F)4p^2F$
578193	577847	346	4.5	$90 \ 3d^4(1F)4p^2G$
582101	582247	-146	2.5	59 $3d^4(3F)4p \ {}^4F + 11 \ 3d^4(3P)4p \ {}^4D + 8 \ 3d^4(3F)4p \ {}^4F$
582434	582473	-39	3.5	$65 \ 3d^4(3F)4p \ ^4F + 8 \ 3d^4(3F)4p \ ^4D + 8 \ 3d^4(3F)4p \ ^4F$
582632	582763	-131	1.5	$37 \ 3d^4(3F)4p \ ^4F + 13 \ 3d^4(1F)4p \ ^2D + 11 \ 3d^4(3P)4p \ ^4D$
583223	583285	-62	4.5	$82 \ 3d^4(3F)4p \ ^4F + 9 \ 3d^4(3F)4p \ ^4F$
583496	583891	-395	1.5	20 $3d^4(3P)4p \ ^4P + 16 \ 3d^4(3P)4p \ ^4D + 16 \ 3d^4(3F)4p \ ^4F$
583853	583914	-61	2.5	23 $3d^4(3P)4p {}^4D + 21 3d^4(3F)4p {}^4F + 12 3d^4(3P)4p {}^4D$
584627	584697	-70	3.5	$32 \ 3d^4(3P)4p \ ^4D + 19 \ 3d^4(3F)4p \ ^4D + 16 \ 3d^4(3F)4p \ ^4F$
586361	586509	-148	2.5	29 $3d^4(3F)4p \ ^4G + 17 \ 3d^4(3P)4p \ ^4P + 13 \ 3d^4(3F)4p \ ^2F$
587400	587450	-50	3.5	$37 \ 3d^4(3F)4p \ ^4G + 28 \ 3d^4(3F)4p \ ^2F + 12 \ 3d^4(3F)4p \ ^4G$
588525	588525	0	2.5	$26 \ 3d^4(1F)4p \ ^2D + 19 \ 3d^4(3P)4p \ ^2D + 13 \ 3d^4(3P)4p \ ^2D$
589098	589136	-38	3.5	$39 \ 3d^4(3F)4p \ ^2F + 31 \ 3d^4(3F)4p \ ^4G + 10 \ 3d^4(3F)4p \ ^4G$
589132	589220	-88	1.5	$33 \ 3d^4(1F)4p \ ^2D + 21 \ 3d^4(3P)4p \ ^2D + 17 \ 3d^4(3F)4p \ ^2D$
596473	596393	80	4.5	$70 \ 3d^4(3F)4p^2G + 20 \ 3d^4(3F)4p^2G$
596790	597023	-233	1.5	$61 \ 3d^4(3P)4p \ ^2P + 25 \ 3d^4(3P)4p \ ^2P + 7 \ 3d^4(3D)4p \ ^2P$
597774	597560	214	3.5	$72 \ 3d^4(3F)4p^2G + 22 \ 3d^4(3F)4p^2G$
599993	599594	399	4.5	$40 \ 3d^4(1G)4p \ ^2H + 22 \ 3d^4(1G)4p \ ^2G + 19 \ 3d^4(1G)4p \ ^2H$
600555	600479	76	3.5	$51 \ 3d^4(1G)4p \ ^2G + 31 \ 3d^4(1G)4p \ ^2G + 7 \ 3d^4(1G)4p \ ^2F$
601692	601391	301	0.5	$54 \ 3d^4(3P)4p^2S + 41 \ 3d^4(3P)4p^2S$
603569	603112	457	4.5	$37 \ 3d^4(1G)4p^2G + 23 \ 3d^4(1G)4p^2H + 22 \ 3d^4(1G)4p^2G$
604021	603515	506	5.5	$65 \ 3d^4(1G)4p^2H + 31 \ 3d^4(1G)4p^2H$
604655	604594	61	3.5	$53 \ 3d^4(1G)4p^2F + 16 \ 3d^4(1G)4p^2F + 8 \ 3d^4(1G)4p^2G$
605306	605304	2	2.5	$58 \ 3d^4(1G)4p \ ^2F + 18 \ 3d^4(1G)4p \ ^2F + 9 \ 3d^4(1D)4p \ ^2F$
608598	608701	-103	2.5	49 $3d^4(3F)4p^2D + 18 3d^4(3F)4p^2D + 16 3d^4(3P)4p^2D$
609072	609176	-104	1.5	$44 \ 3d^{4}(3F)4p^{2}D + 21 \ 3d^{4}(3P)4p^{2}D + 18 \ 3d^{4}(3F)4p^{2}D$
634888	634813	75	3.5	72 $3d^4(1D)4p$ ² F + 19 $3d^4(1D)4p$ ² F + 5 $3d^4(1G)4p$ ² F

Table A11. Continued

a: Experimental energies from [105] b: This work c: Only the components \geq to 5% are given

10010 1112.	Comput		101 501	<u>unguns an</u>			ii probai	7110105	m Ou
	Wavelength	Lower Level	J_{low}	Upper Level	J_{up}	log gf	gA	CF	1
	180.290	40445	2.5	584627	4.0 9.5	-0.89	$2.47E \pm 10$ $2.18E \pm 10$	-0.023	1
	101 546	81054 81054	5.0 5.5	604021	5.5	-0.95	$2.18E \pm 10$ $2.02E \pm 10$	0.374	1
	191.540	81954	5.5	603569	4.5	-0.51	$5.58E \pm 10$	0.152	1
	192.368	80717	4.5	600555	3.5	-0.85	2.53E+10 2.53E+10	0.176	1
	193.402	80717	4.5	597774	3.5	-0.67	3.80E + 10	-0.14	1
	194.041	119534	4.5	634888	3.5	-0.44	6.50E + 10	-0.391	1
	194.164	82746	3.5	597774	3.5	-1	1.75E + 10	0.355	1
	194.356	81954	5.5	596473	4.5	-0.58	4.67E + 10	-0.118	1
	194.604	83910	4.5	597774	3.5	-0.92	2.11E + 10	0.162	1
	196.581	75931	4.5	584627	3.5	-0.08	1.44E + 11	-0.682	1
	197.043	76349	3.5	583853	2.5	-0.32	8.17E + 10	-0.549	1
	197.053	76019	2.5	583496	1.5	-0.86	2.40E + 10	0.359	1
	197.125	75931	4.5	583223	4.5	-0.17	1.17E + 11	0.529	1
	197.288	76349	3.5	583223	4.5	-0.91	2.09E + 10	-0.506	1
	197.595	76349	3.5	582434	3.5	-0.29	8.83E+10	0.477	1
	197.596	76019	2.5	582101	2.5	-0.45	6.11E+10	0.522	1
	197.041	76996	2.5	583490	1.5	-0.99	$1.74E \pm 10$ $4.21E \pm 10$	0.372	1
	197.720	2010	1.5	587400	2.5	-0.0	$4.31E \pm 10$ $1.74E \pm 10$	0.000	1
	198.014	87979	2.5	589132	1.5	-0.99	$3.41E \pm 10$	-0.324	1
	199 902	88280	3.5	588525	2.5	-0.59	4.32E+10	-0.336	1
	200.272	50732	2.5	550053	2.5	-0.62	$3.98E \pm 10$	0.351	1
	200.675	0	2.5	498317	3.5	0.13	2.24E + 11	0.984	1
	200.858	õ	2.5	497863	2.5	-0.01	1.61E + 11	0.983	1
	200.955	0	2.5	497624	1.5	-0.2	1.04E + 11	0.982	1
	200.995	107131	2.5	604655	3.5	-0.87	2.25E + 10	-0.224	1
	200.996	56429	1.5	553950	0.5	-0.77	2.78E + 10	-0.663	1
	201.015	80717	4.5	578193	4.5	-0.91	2.04E + 10	-0.468	
	201.209	46578	3.5	543574	4.5	-0.79	2.68E + 10	-0.54	
	201.328	56427	2.5	553130	1.5	-0.46	5.73E + 10	-0.611	1
	201.364	46575	4.5	543188	5.5	-0.67	3.55E + 10	-0.791	1
	201.516	81954	5.5	578193	4.5	-0.49	5.26E + 10	0.618	1
	201.613	55742	3.5	551743	2.5	-0.57	4.44E + 10	-0.521	1
	201.708	55742 46515	3.5	551508	3.5	-0.6	4.12E + 10 2.76E + 10	-0.24	1
	201.87	40515	2.5	541884	3.5	-0.64	$3.76E \pm 10$ $1.07E \pm 10$	-0.639	1
	202.07	40378	3.0	540025	4.0	-0.92	$1.97E \pm 10$ $1.62E \pm 10$	-0.739	1
	202.280	55749	4.5	550053	2.5	-1	$1.02E \pm 10$ $3.15E \pm 10$	0.266	1
	202.302	83910	4.5	578193	4.5	-0.62	$3.92E \pm 10$	-0.488	1
	202.462	67757	5.5	561677	4.5	-0.21	1.01E+11	-0.507	1
	202.583	56427	2.5	550053	2.5	-0.91	1.99E + 10	0.158	1
	202.605	46515	2.5	540086	1.5	-0.63	3.80E + 10	0.749	1
	202.814	46578	3.5	539640	2.5	-0.46	5.66E + 10	-0.799	1
	202.855	82746	3.5	575709	3.5	-0.59	4.21E + 10	-0.483	1
	202.947	67918	6.5	560658	5.5	-0.42	6.10E + 10	-0.203	1
	202.962	46443	5.5	539146	4.5	0.12	2.15E + 11	-0.912	
	203.005	46443	5.5	539041	5.5	0.05	1.82E + 11	-0.956	1
	203.052	50732	2.5	543217	3.5	-0.87	2.18E + 10	0.169	1
	203.18	46575	4.5	538749	3.5	0.01	1.65E + 11	-0.851	1
	203.315	75931	4.5	567778	3.5	-0.99	1.63E + 10	-0.661	1
	203.335	83910	4.5	575709	3.5	-0.77	2.74E + 10	-0.403	1
	203.43	46575	4.5	538144	4.5	0.12	2.11E + 11 5.87E + 10	-0.883	1
	203.317	40313	2.0	562179	2.0	-0.44	$3.87E \pm 10$ $2.00E \pm 10$	0.802	1
	203.541	46578	2.5	537874	2.5	-0.53	$4.73E \pm 10$	-0.392	1
	203.540	46575	4.5	537802	3.5	-0.00	$1.61E \pm 10$	0.37	1
	203.573	46578	3.5	537802	3.5	0.08	1.01E + 10 1.91E + 11	0.885	1
	203.621	70876	2.5	561985	2.5	-0.74	2.90E + 10	0.215	1
	203.81	46515	2.5	537169	2.5	-0.18	1.06E + 11	0.662	1
	203.836	46578	3.5	537169	2.5	-0.6	4.04E + 10	0.884	1
	203.837	72227	1.5	562816	2.5	-0.8	2.55E + 10	0.526	1
	204.001	50732	2.5	540925	3.5	-0.62	3.84E + 10	0.467	1
	204.05	46575	4.5	536650	4.5	-0.63	3.74E + 10	0.328	
	204.145	51067	1.5	540915	1.5	-0.64	3.65E + 10	0.373	1
	204.224	107131	2.5	596790	1.5	-0.52	4.82E + 10	-0.401	1
	204.263	82746	3.5	572310	2.5	-0.85	2.27E + 10	-0.135	
	204.31	70876	2.5	560328	1.5	-0.42	6.04E + 10 1.26E + 11	-0.498	1
	204.42	40443	5.5	535032	0.5 0.5	-0.07	1.30E + 11	0.494	1
	∠04.48 204.791	12221	1.0 5.5	534019	0.0 5.5	-0.57	$2.87E \pm 10$	-0.37	1
	204.721	46575	4.5	534912	5.5	-0.82	$2.07E \pm 10$ 2.40E ± 10	0.685	1
	204.111	72227	1.5	560328	1.5	-0.66	$3.46E \pm 10$	0.664	1
	204.870	50732	2.5	538624	2.5	-0.82	2.43E+10 2.43E+10	0.04	1
	205.05	46443	5.5	534128	4.5	-0.73	2.94E + 10	0.541	1
	205.05	76019	2.5	563705	1.5	-0.86	2.20E + 10	-0.638	1
	205.096	74408	3.5	561985	2.5	-0.18	1.04E + 11	0.648	1
	205.104	51067	1.5	538624	2.5	-0.93	1.84E + 10	-0.496	1
	205.139	55742	3.5	543217	3.5	-0.32	7.64E + 10	-0.728	1
	205.18	67918	6.5	555295	6.5	-0.19	1.02E + 11	-0.929	1
	205.275	67918	6.5	555069	5.5	0.35	$3.53E{+}11$	-0.947	
	205.313	80717	4.5	567778	3.5	-0.67	3.40E + 10	0.376	
	205.417	56429	1.5	543244	1.5	-0.94	1.81E + 10	0.37	
	205.427	56427	2.5	543217	3.5	-0.7	3.14E + 10	-0.22	1
	205.551	55742	3.5	542239	4.5	-0.08	1.31E + 11	0.83	1
	205.554	46575	4.5	533066	3.5	-0.92	1.90E + 10	0.375	
	205.607	67757	5.5	554123	4.5	0.15	2.24E+11	-0.779	
	205.614	56427	2.5	542776	2.5	-0.54	4.53E+10	0.553	
	205.614	56429 F6010	1.5	542776	2.5	-0.62	3.76E+10	0.331	1
	205.683	20210	0.5	56270F	1.5	-0.94	1.805+10	0.585	
	203.087	11029	2.0 2.5	000700 542362	1.0	-0.28	0.29±+10 3 37F±10	-0.472	
	205.169	119605	2.0	605306	0.0 9.5	-0.07	$1.07E \pm 11$	0.762	1
	205.974	50732	2.5	536229	1.5	-0.53	4.65E + 10	0.675	1
	206.108	88280	3.5	573463	3.5	-0.13	1.17E + 11	-0.606	
	206.134	119534	4.5	604655	3.5	-0.08	1.32E + 11	0.777	
	206.172	82746	3.5	567778	3.5	-0.91	1.93E + 10	-0.551	1

Table A12: Computed oscillator strengths and transition probabilities in Cu VII.

Table A12: Continued

Wavelength	Lower Level	JLow	Upper level	J_{Up}	log gf	gA	CF
206.215	$74408 \\ 51407$	$3.5 \\ 0.5$	559339 536229	$\frac{4.5}{1.5}$	-0.82 -0.97	2.38E+10 1.67E+10	0.185
206.311	56210	0.5	540915	1.5	-0.86	2.16E + 10	0.451
206.335	77529	2.5	562178	3.5	-0.98	1.64E + 10	0.278
206.354	46443	5.5 5.5	531047 552350	6.5 5.5	-0.31	7.63E+10 2 71E+11	0.528 0.848
206.399	56427	2.5	540925	3.5	-0.65	3.47E+10	0.327
206.404	119534	4.5	604021	5.5	-0.69	$3.19E{+}10$	0.711
206.404	56429	1.5	540915	1.5	-0.88	2.09E+10	-0.291
206.425	70876 87979	2.5 2.5	555314 572310	2.5 2.5	-0.85	2.23E+10 1.02E+11	-0.16
206.474	82746	3.5	567069	2.5	-0.64	3.59E + 10	-0.576
206.549	67757	5.5	551903	6.5	-0.66	3.45E + 10	0.771
206.597	119534	4.5	603569 551002	4.5	-0.47	5.23E + 10 2.20E + 11	0.42
206.668	83910	4.5	567778	3.5	-0.05	1.37E+11	0.746
206.837	50732	2.5	534204	3.5	-0.22	9.29E + 10	0.744
206.904	46575	4.5	529891	5.5	-0.47	5.32E + 10	0.432
207.072	55742	3.5	538624	2.5 2.5	-0.24	6.05E+10	0.028 0.607
207.203	51067	1.5	533685	0.5	-0.89	2.00E + 10	0.619
207.276	46578	3.5	529027	4.5	-0.57	4.13E+10	0.393
207.384 207.394	56427 106957	2.5	538624 589132	2.5	-0.78 -0.58	2.60E+10 4.09E+10	-0.359 0.505
207.478	46515	2.5	528494	3.5	-0.62	3.69E + 10	0.408
207.702	70876	2.5	552334	3.5	-0.83	2.31E + 10	0.174
207.73	107131 51067	2.5	588525 532460	2.5	-0.43	$5.76E \pm 10$ 2.86E ± 10	0.548 0.557
207.917	80717	4.5	561677	4.5	-0.73	9.85E+10	0.337 0.617
207.922	119605	3.5	600555	3.5	-0.19	9.96E + 10	0.793
208.134	119534	4.5	599993	4.5	-0.59	3.92E + 10	-0.576
208.165	75931	3.5 4.5	599993 555800	4.5 4.5	-0.78	2.58E+10 3.01E+10	0.659
208.454	81954	5.5	561677	4.5	-0.99	1.58E + 10	0.542
208.497	67757	5.5	547381	4.5	-0.51	4.70E + 10	0.454
208.64	76019	2.5	555314	2.5	-0.82	2.34E+10 1.70E+10	-0.289
208.748	76349	3.5	555395	3.5	-0.90	$1.64E \pm 10$	-0.298
208.798	82746	3.5	561677	4.5	-0.64	3.53E + 10	-0.307
208.86	88280	3.5	567069	2.5	-0.12	1.15E+11	0.698
208.898	81954 156224	5.5 2.5	560658 634888	5.5 3.5	-1	2.26E + 11 1.53E + 10	0.873
209.131	119605	3.5	597774	3.5	-0.32	7.31E+10	0.589
209.132	95875	0.5	574043	1.5	-0.47	5.21E + 10	-0.845
209.237	74408	3.5	552334	3.5	-0.08	1.28E + 11 7.52E + 10	0.678
209.299	83910	2.5 4.5	561677	2.5 4.5	-0.31	7.32E+10 5.32E+10	-0.594
209.367	80717	4.5	558348	3.5	-0.1	1.22E + 11	-0.741
209.412	95875	0.5	573402	0.5	-0.75	2.72E + 10	-0.844
209.472	88280 81954	3.5 5.5	565670 559339	2.5 4.5	-0.49	4.90E+10 1 36E+11	0.478
209.56	87979	2.5	565170	1.5	-0.13	1.30E+11 1.13E+11	0.82
209.67	119534	4.5	596473	4.5	-0.09	1.25E + 11	0.761
209.755	83910	4.5	560658	5.5	-0.82	2.31E+10	-0.176
210.105	82746	3.5	558348	4.5	-0.48	5.80E+10 5.80E+10	-0.338
210.271	75931	4.5	551508	3.5	-0.84	2.19E + 10	-0.317
210.337	83910	4.5	559339	4.5	-0.23	9.01E+10	-0.552
210.353	70876 67918	2.5	546268 543188	2.5	-0.81	2.35E+10 1 14E+11	0.186
210.456	76349	3.5	551508	3.5	-0.86	2.08E+10	0.476
210.756	67757	5.5	542239	4.5	-0.83	2.21E + 10	0.356
210.936	75931 70876	4.5 2.5	550007 544873	5.5 1.5	-0.42	5.73E+10 1.93E+10	-0.468 0.153
211.104	67757	5.5	541457	4.5	-0.26	8.29E+10	0.135 0.275
211.153	67918	6.5	541509	6.5	-0.21	9.12E + 10	0.36
211.264	81954	5.5	555295	6.5	-0.77	2.54E+10	0.684
211.428	76349	3.5	549249	4.5	-0.75	4.74E+10	-0.485
211.518	80717	4.5	553490	4.5	-0.86	2.08E + 10	-0.157
211.575	72227	1.5	544873	1.5	-0.81	2.32E + 10	0.401
211.653	76019 74408	2.5	548491 546771	3.5	-0.7	2.95E+10 1.61E+10	-0.326 0.252
211.789	81954	5.5	554123	4.5	-0.64	3.44E + 10	0.388
211.872	76019	2.5	548001	2.5	-0.95	1.66E + 10	-0.524
211.927 212.025	74408 80717	3.5 4.5	552359	⊿.ə 5.5	-0.34 -0.73	0.81E+10 2.78E+10	-0.318 0.331
212.081	70876	2.5	542394	1.5	-0.59	3.78E + 10	0.475
212.095	70876	2.5	542362	3.5	-0.95	1.68E + 10	-0.196
212.242	75931	4.5	547090 548001	5.5	-0.48	4.90E+10 4.64E+10	0.673
212.202	77529	2.5	548491	3.5	-0.85	2.08E+10	-0.337
212.333	82746	3.5	553703	3.5	-0.59	3.81E + 10	-0.182
212.376	76019	2.5	546881	3.5	-0.74	2.68E+10	-0.386
212.67	83910	4.5	554123	4.5	-0.53	4.36E+10	0.42
212.69	72227	1.5	542394	1.5	-0.98	1.53E + 10	0.289
212.789	81954	5.5	551903	6.5	-0.97	1.57E+10	0.213
212.952	02/40 119534	3.5 4.5	002334 589098	3.5 3.5	-0.86	2.04E+10 4.80E+10	0.246 0.334
213.121	72227	1.5	541444	2.5	-0.74	2.69E + 10	0.448
213.327	70876	2.5	539640	2.5	-0.66	3.21E + 10	-0.322
213.338	77529 80717	2.5 4.5	546268 549249	2.5 4.5	-0.66	3.23E+10 2.17E+10	0.283
213.681	76886	1.5	544873	1.5	-0.00	1.44E+10	0.55
213.696	74408	3.5	542362	3.5	-0.81	2.28E + 10	0.153
213.736	119534	4.5 2 5	587400 544972	3.5	-0.56	3.99E+10 2.17E+10	0.37
213.979	87979	$^{2.0}_{2.5}$	555314	2.5	-0.85	2.09E+10	0.205
214.173	107131	2.5	574043	1.5	-0.56	3.95E + 10	-0.574
214.202	80717	4.5	547565	3.5	-0.39	5.89E+10	0.425
214.245 214.287	119605 80717	3.5 4.5	547381	2.5 4.5	-0.98 -0.78	1.51E+10 $2.44E\pm10$	0.357 0.146
214.354	74408	3.5	540925	3.5	-1	1.44E+10	0.204
214.388	106957	1.5	573402	0.5	-0.94	1.66E + 10	-0.524
214.45	75931	4.5	542239	4.5	-0.68	3.05E + 10	-0.293

		<u> Table</u>	<u>A12: U01</u>	<u>atinue</u>	<u>ea</u>		
Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA	CF
214.517	80717	4.5	546881	3.5	-0.39	5.96E + 10	0.217
214.548	83910	4.5	550007	5.5	-0.72	2.75E + 10	-0.548
214.72	87979	2.5	553703	3.5	-0.56	3.94E + 10	-0.577
214.857	81954	5.5	547381	4.5	-0.17	9.81E + 10	0.325
214.957	88280	3.5	553490	4.5	-0.46	5.06E + 10	-0.659
214 991	81954	5.5	547090	5.5	-0.66	3.19E + 10	-0.171
215.056	144077	0.5	609072	1.5	-0.85	$2.04E \pm 10$	-0.472
215.000	77520	2.5	540260	2.5	0.00	1.79E + 10	0.205
215.151	142024	2.5	042302	3.5	-0.92	$1.72E \pm 10$	-0.205
215.209	143934	1.5	608598	2.5	-0.58	3.76E + 10	-0.425
215.454	82746	3.5	546881	3.5	-0.64	3.30E + 10	0.223
215.492	88280	3.5	552334	3.5	-0.86	2.02E+10	0.231
215.505	82746	3.5	546771	2.5	-0.51	4.48E + 10	0.238
215.607	46443	5.5	510250	4.5	-0.03	1.35E + 11	-0.529
215.669	55742	3.5	519415	3.5	-0.4	5.73E + 10	-0.457
215.678	83910	4.5	547565	3.5	-0.6	3.61E + 10	0.155
215.763	83910	4.5	547381	4.5	-0.91	1.76E + 10	0.088
215.882	75931	4.5	539146	4.5	-0.72	2.71E + 10	-0.202
215.899	83910	4.5	547090	5.5	-1	$1.45E \pm 10$	-0.187
215 988	56427	2.5	519415	3.5	-0.78	$2.37E \pm 10$	0.522
215 996	83910	4.5	546881	3.5	-0.67	$3.09E \pm 10$	-0.168
216.040	80717	4.5	549574	4.5	0.80	1.82E 10	0.246
210.049	40717	4.5	545574	4.5	-0.89	$1.03E \pm 10$	-0.240
216.056	40575	4.5	509418	3.5	-0.11	1.11E+11	-0.502
216.246	56427	2.5	518863	2.5	-0.89	1.82E+10	-0.216
216.247	56429	1.5	518863	2.5	-0.8	2.25E+10	0.517
216.263	76349	3.5	538749	3.5	-0.91	1.76E + 10	-0.155
216.31	46578	3.5	508877	2.5	-0.22	8.51E + 10	-0.485
216.337	74408	3.5	536650	4.5	-0.63	3.31E + 10	0.386
216.446	46515	2.5	508524	1.5	-0.35	6.35E + 10	-0.478
216.546	76349	3.5	538144	4.5	-0.96	1.55E + 10	0.153
216.81	81954	5.5	543188	5.5	-0.88	1.89E + 10	0.125
217.086	107131	2.5	567778	3.5	-0.69	2.86E + 10	-0.575
217 42	107131	2.5	567069	2.5	-0.4	$5.56E \pm 10$	0 449
217 532	75931	4.5	535632	5.5	-0.9	1.79E + 10	-0 144
217.602	81054	55	541509	6.5	0.6	$3.53E \pm 10$	0.688
217.002	88280	35	547565	3.5	0.78	$2.33E \pm 10$	0.000
217.73	05200	3.5	547505	3.5	-0.78	$2.33E \pm 10$ 2.44E ± 10	-0.29
217.741	95875	0.5	535157	1.5	-0.01	$3.44E \pm 10$	0.780
217.964	87979	2.5	546771	2.5	-0.94	1.62E + 10	-0.209
218.002	82746	3.5	541457	4.5	-0.93	1.65E + 10	-0.504
218.084	107131	2.5	565670	2.5	-0.92	1.67E + 10	0.288
218.239	106957	1.5	565170	1.5	-0.5	4.47E + 10	0.559
218.346	88280	3.5	546268	2.5	-0.83	2.05E+10	0.209
218.456	143934	1.5	601692	0.5	-0.5	4.44E + 10	0.746
218.524	144077	0.5	601692	0.5	-0.95	1.56E + 10	-0.458
219.366	106957	1.5	562816	2.5	-0.67	2.98E + 10	0.429
219.757	107131	2.5	562178	3.5	-0.94	1.60E + 10	0.204
219.918	50732	2.5	505447	2.5	-0.88	$1.84E \pm 10$	-0.29
220 112	106957	1.5	561271	0.5	-0.9	1.74E + 10	0.35
220.224	88280	3.5	542362	3.5	-0.92	$1.65E \pm 10$	0.19
220.224	110524	4.5	579469	2.5	0.00	1.20E 10	0.162
220.299	142024	4.5	506700	1.5	-0.99	$1.39E \pm 10$ $2.17E \pm 10$	-0.102
220.021	156974	1.5	600079	1.5	-0.8	2.17 ± 10 6.44 \E + 10	0.565
220.696	150574	1.5	009072	1.5	-0.33	$0.44E \pm 10$	-0.047
221.056	156224	2.5	608598	2.5	-0.14	1.00E+11	-0.654
221.129	156374	1.5	608598	2.5	-0.74	2.50E + 10	0.69
222.235	50732	2.5	500706	1.5	-0.95	1.53E + 10	-0.432
222.368	55742	3.5	505447	2.5	-0.75	2.42E + 10	-0.471
222.677	156224	2.5	605306	2.5	-0.88	1.77E + 10	-0.721
222.751	156374	1.5	605306	2.5	-0.46	4.64E + 10	-0.469
223	156224	2.5	604655	3.5	-0.27	7.25E + 10	-0.675
223.03	88280	3.5	536650	4.5	-0.92	1.62E + 10	-0.238
224.691	144077	0.5	589132	1.5	-0.7	2.63E + 10	-0.596
224.926	143934	1.5	588525	2.5	-0.63	3.08E + 10	-0.532
225.058	156224	2.5	600555	3.5	-0.98	1.40E + 10	0.702
225 487	75931	4.5	519415	3.5	-0.18	8.77E + 10	-0.592
225.626	110605	3.5	562816	2.5	0.20	$2.08E \pm 10$	0.169
220.020	76240	2.5	510415	2.0	0.01	1.60E 10	0.105
220.7	76010	3.5	E100C2	3.5	-0.91	$1.00E \pm 10$ $1.27E \pm 10$	0.475
440.010 005.015	110524	2.0	010000	2.0	-0.90	2.0512+10	0.497
225.915	119534	4.5	502178	3.5	-0.61	3.25E+10	0.179
225.982	10349	3.5	518863	2.5	-0.38	5.42E+10	-0.486
226.11	76019	2.5	518282	1.5	-0.67	2.80E + 10	-0.468
226.208	119605	3.5	561677	4.5	-0.5	4.16E + 10	-0.485
226.694	119534	4.5	560658	5.5	-0.6	3.28E + 10	-0.317
226.777	76886	1.5	517847	0.5	-0.8	2.06E + 10	-0.485
226.981	156224	2.5	596790	1.5	-0.52	3.90E + 10	-0.477
227.049	107131	2.5	547565	3.5	-0.67	2.75E + 10	-0.418
227.369	106957	1.5	546771	2.5	-0.9	1.62E + 10	-0.325
227.373	119534	4.5	559339	4.5	-0.97	1.39E + 10	0.076
229,603	119534	4.5	555069	5.5	-0,96	1.38E + 10	-0.19
230.245	75931	4.5	510250	4.5	-0.64	$2.87E \pm 10$	-0.395
230 363	110605	35	553703	35	-0.57	$3.34E \pm 10$	0.221
230.429	110594	4 5	559400	4.5	0.41	4 80F 10	0.247
230.430	76940	-1.J 2 K	500419	9 K	0.41	1.68E 10	0.247
430.91	10349	5.5	009410	5.5	-0.07	1.005+10	-0.200

Table A12: Continued

In IV-VII

In IV

Energy Levels

Table A13: Comparison between available experimental data and calculated even energy levels (in $\underline{cm^{-1}}$) in In IV

/				
E^{a}_{exp}	E^{b}_{calc}	ΔE	J	Leading components (in %) in LS coupling ^c
0	0	0	0	99.3 $4d^{10}$ (¹ S) ¹ S
128641.4	128681	-39.6	3	$99.4 \ 4d^{9}5s(^{2}D)^{-3}D$
130879.2	130833	46.2	2	$72.7 4d^95s (^2\text{D}) ^3\text{D} + 26.7 4d^95s (^2\text{D}) ^1\text{D}$
135791.4	135781	10.4	1	$99.4 \ 4d^{9}5s \ (^{2}D) \ ^{3}D +$
138662.1	138679	-16.9	2	72.6 $4d^{9}5s$ (^{2}D) $^{1}D + 26.7 4d^{9}5s$ (^{2}D) ^{3}D
277340.2	277373	-32.8	4	$94.2.4d^85s^2$ (³ F) ³ F
283497.2	283379	118.2	3	$93.9.4d^{8}5s^{2}$ (³ F) ³ F
284985.4	285120	134.6	2	$65.2 4d^85c^2 (^3\text{F}) \ ^3\text{F} \pm 21.3 \ 4d^85c^2 (^1\text{D}) \ ^1\text{D} \pm 5.4d^85c^2 (^3\text{P}) \ ^3\text{P}$
285046.0	285016	30.0	1	$781 4d^{9}5d (^{2}D) ^{3}S \pm 18 4d^{9}5d (^{2}D) ^{3}P$
288732.1	288772	30.0	2	$62.6 \ 4d^{9}5d \ (^{2}D) \ ^{3}P + 18.8 \ 4d^{9}5d \ (^{2}D) \ ^{3}D + 10.3 \ 4d^{8}5c^{2} \ (^{3}P) \ ^{3}P$
280011.5	280026	-33.5	4	$(1)^{1}$
289011.0	289030	-24.5	4 E	40.940 J J J J J J J J
269432.9	289421	11.9	1	99.5 40 50 (D) G + $48.0 439 \pm 3 (2D) 1D + 94 \pm 439 \pm 3 (2D) 3D + 99.2 439 \pm 3 (2D) 3D$
269515.2	289349	-33.8	1	48.9 40 50 (D) F + 24.3 40 50 (D) F + 22.3 40 50 (D) D
290845.9	290863	-17.1	3	$(8.9 40.50 (D)^{-}D + 17.3 40.50 (D)^{-}F$
291474.8	291422	52.8	2	$33.9 \ 40^{\circ} 50 \ (^{-}D) \ ^{\circ}D \ + \ 30.5 \ 40^{\circ} 50 \ (^{-}D) \ ^{\circ}D \ + \ 12.2 \ 40^{\circ} 5s^{-} \ (^{\circ}F) \ ^{\circ}F$
291620.6	291661	-40.4	3	$48 4d^{\circ}5d (^{\circ}D) {}^{\circ}F + 23.2 4d^{\circ}5d (^{\circ}D) {}^{\circ}G + 20.1 4d^{\circ}5d (^{\circ}D) {}^{\circ}F$
292068.6	291950	118.6	0	$84.7 \ 4d^{\circ} 5d \ (^{-}D) \ ^{\circ}P + 11.2 \ 4d^{\circ} 5s^{-} \ (^{\circ}P) \ ^{\circ}P$
292221.8	292195	26.8	4	$74.2 \ 4d^{\circ}5d \ (^{\circ}D) \ ^{\circ}F + 15.8 \ 4d^{\circ}5d \ (^{\circ}D) \ ^{\circ}G + 7.6 \ 4d^{\circ}5d \ (^{\circ}D) \ ^{\circ}G$
293229.7	293267	-37.3	2	$41 4d^{\circ}5s^{\circ} (^{\circ}P) ^{\circ}P + 16.6 4d^{\circ}5s^{\circ} (^{\circ}D) ^{\circ}D + 16.1 4d^{\circ}5d (^{\circ}D) ^{\circ}P$
294544.8	294629	-84.2	1	$36.6 \ 4d^{3}5d^{(2}D)^{3}P + 29.1 \ 4d^{3}5d^{(2}D)^{4}P + 17 \ 4d^{3}5d^{(2}D)^{3}S$
296394.7	296359	35.7	3	74 4d 9 5d (² D) 3 G + 18.1 4d 9 5d (² D) 1 F + 7.2 4d 9 5d (² D) 3 F
296723.8	296782	-58.2	1	$69.6 \ 4d^95d \ (^2D) \ ^3D + 19.2 \ 4d^95d \ (^2D) \ ^1P + 8.8 \ 4d^85s^2 \ (^3P) \ ^3P$
296993.7	296970	23.7	4	$40.3 4d^{9}5d (^{2}\text{D}) ^{3}\text{G} + 31.4 4d^{9}5d (^{2}\text{D}) ^{1}\text{G} + 22.2 4d^{9}5d (^{2}\text{D}) ^{3}\text{F}$
297086.6	297157	-70.4	2	$35.4 4d^95d (^2\text{D}) ^1\text{D} + 27.2 4d^95d (^2\text{D}) ^3\text{D} + 11.5 4d^95d (^2\text{D}) ^3\text{P}$
297850.5	297864	-13.5	0	79.3 $4d^{\circ}5s^{2}$ (³ P) ³ P + 11.3 $4d^{9}5d$ (² D) ³ P + 5.7 $4d^{\circ}5s^{2}$ (¹ S) ¹ S
298619.5	298588	31.5	1	70.1 $4d^85s^2$ (³ P) ³ P + 18.8 $4d^95d$ (² D) ³ P + 6.6 $4d^95d$ (² D) ³ D
298643.9	298650	-6.1	3	99.8 $4d^{9}6s$ (² D) ³ D
298925.8	298873	52.8	2	$69.2 4d^95d (^2\text{D}) \ ^3\text{F} + 18.4 \ 4d^95d (^2\text{D}) \ ^3\text{D}$
299322.9	299316	6.9	2	$50.9 4d^96s (^2D) \ ^1D + 47.6 \ 4d^96s (^2D) \ ^3D$
299325.2	299330	-4.8	3	51.8 $4d^{9}5d(^{2}D)^{3}F + 33.1 4d^{9}5d(^{2}D)^{1}F + 13.3 4d^{9}5d(^{2}D)^{3}D$
301456.6	301363	93.6	2	$43.3 \ 4d^85s^2 \ (^{1}D) \ ^{1}D + 21.7 \ 4d^85s^2 \ (^{3}P) \ ^{3}P + 13.7 \ 4d^95d \ (^{2}D) \ ^{1}D$
302457.9	302459	-1.1	4	$88.7 4d^85s^2 (^{1}\text{G}) ^{1}\text{G} + 5.3 4d^95d (^{2}\text{D}) ^{1}\text{G}$
305793.7	305788	5.7	1	99.9 $4d^{9}6s$ (² D) ³ D
306290.2	306296	-5.8	2	51.8 $4d^{9}6s$ (² D) ³ D + 48 $4d^{9}6s$ (² D) ¹ D
309455.8	309459	-3.2	0	$88.7 4d^95d (^2\text{D}) \ ^1\text{S} + 5.5 \ 4d^96d (^2\text{D}) \ ^1\text{S}$
356718.8	356766	-47.2	1	$67.3 4d^96d (^2\text{D}) \ ^3\text{S} + 27.2 \ 4d^96d (^2\text{D}) \ ^3\text{P}$
357807.8	357815	-7.2	4	$47.1 \ 4d^{9}6d \ (^{2}D) \ ^{1}G + 51.1 \ 4d^{9}6d \ (^{2}D) \ ^{3}G$
357968.8	357879	89.8	2	$63.7 4d^96d (^2\text{D}) ^3\text{P} + 33.6 4d^96d (^2\text{D}) ^3\text{D}$
357920.8	357890	30.8	5	$99.9 \ 4d^{9}6d \ (^{2}D) \ ^{3}G$
358005.8	357974	31.8	1	$53.5 4d^96d (^2\text{D}) ^1\text{P} + 26.8 4d^96d (^2\text{D}) ^3\text{D} + 18 4d^96d (^2\text{D}) ^3\text{P}$
358397.6	358406	-8.4	3	$68.9 4d^96d (^2\text{D}) \ ^3\text{D} + 28.5 \ 4d^96d (^2\text{D}) \ ^3\text{F}$
358745.8	358760	-14.2	3	$56.3 4d^96d (^2\text{D}) {}^1\text{F} + 18.5 4d^96d (^2\text{D}) {}^3\text{F} + 13.5 4d^96d (^2\text{D}) {}^3\text{D}$
358841	358843	-2	2	$54.3 4d^96d (^2\text{D}) \ ^1\text{D} + 17.4 \ 4d^96d (^2\text{D}) \ ^3\text{D} + 17 \ 4d^96d (^2\text{D}) \ ^3\text{F}$
358944.4	358937	7.4	4	$85.2 \ 4d^{9}6d \ (^{2}D) \ ^{3}F + 11.9 \ 4d^{9}6d \ (^{2}D) \ ^{1}G$
360739.1	360859	-119.9	0	$88.2 \ 4d^{9}6d \ (^{2}D) \ ^{3}P + 10.2 \ 4d^{9}6d \ (^{2}D) \ ^{1}S$
360971.5	360980	-8.5	3	$99.8 \ 4d^97s$ (² D) ³ D
361238.1	361230	8.1	2	56.9 $4d^{9}7s$ (² D) ¹ D + 42.9 $4d^{9}7s$ (² D) ³ D
364509.3	364477	32.3	1	$39.6 \ 4d^{9}6d^{(2}D)^{3}P + 30.1 \ 4d^{9}6d^{(2}D)^{3}S + 28.8 \ 4d^{9}6d^{(2}D)^{1}P$
364917.7	364912	5.7	3	$85.8 \ 4d^{9}6d \ (^{2}D) \ ^{3}G + 10.2 \ 4d^{9}6d \ (^{2}D) \ ^{1}F$
365226.7	365217	9.7	1	$71.2 \ 4d^{9}6d \ (^{2}D) \ ^{3}D + 14.9 \ 4d^{9}6d \ (^{2}D) \ ^{3}P + 13.1 \ 4d^{9}6d \ (^{2}D) \ ^{1}P$
365353.4	365347	6.4	4	$46.1 \ 4d^{9}6d \ (^{2}D) \ ^{3}G + 40.9 \ 4d^{9}6d \ (^{2}D) \ ^{1}G + 12.9 \ 4d^{9}6d \ (^{2}D) \ ^{3}F$
365644.3	365625	19.3	2	$45.1 \ 4d^{9}6d \ (^{2}D) \ ^{3}D + 28.1 \ 4d^{9}6d \ (^{2}D) \ ^{1}D + 24.8 \ 4d^{9}6d \ (^{2}D) \ ^{3}P$
365914.3	365942	-27.7	2	$78.8 \text{ 4d}^9 \text{6d} (^2\text{D}) \ ^3\text{F} + 17 \ \text{4d}^9 \text{6d} (^2\text{D}) \ ^1\text{D}$
366067 7	366091	-23.3	3	$49 4d^{9}6d (^{2}D) {}^{3}F + 33.2 4d^{9}6d (^{2}D) {}^{1}F + 17.2 4d^{9}6d (^{2}D) {}^{3}D$
368163	368152	11	1	$99.8 4d^97 \text{ s} (^2\text{D})^{-3}\text{D}$
368320 4	368331	-10.6	2	$56.9 4d^97s$ (² D) ³ D + 42.9 4d ⁹ 7s (² D) ¹ D
370640.4	370624	16.4	õ	$76.8 4d^{9}6d (^{2}D) ^{1}S + 11.5 4d^{9}6d (^{2}D) ^{3}P + 7.9 4d^{9}7d (^{2}D) ^{1}S$
391586 5	391246	340.5	2	$60.4 \ 4d^97d \ (^2D) \ ^3P + 33.8 \ 4d^97d \ (^2D) \ ^3D$
391446 1	391258	188 1	3	$94 \ 1 \ 4d^9 \ 8s \ (^2D) \ ^3D$
00 1 1 TO. 1	001400	100.1	9	

a: From Swapni [32] and Ryabtsev [33]
b: This work
c: Only the component ≥ 5% are given

Table A14: Comparison between available experimental data and calculated odd energy levels (in cm^{-1}) in In IV

E^{a}_{exp}	E^{b}_{calc}	ΔE	J	Leading components (in $\%$) in LS coupling ^{c}
193894.2	193941	-46.8	2	$87.3 \ 4d^95p \ (^2D) \ ^3P + 9.9 \ 4d^95p \ (^2D) \ ^3D$
196599.7	196561	38.7	3	57.7 $4d^{9}5p$ (² D) ³ F + 32.5 $4d^{9}5p$ (² D) ¹ F + 9.3 $4d^{9}5p$ (² D) ³ D
200553.1	200542	11.1	1	$88.9 \ 4d^95p \ (^2D) \ ^3P + 8.5 \ 4d^95p \ (^2D) \ ^3D$
201051.4	201090	-38.6	4	99.6 $4d^{9}5p$ (² D) ³ F
202024.6	202009	15.6	2	$83.4 \ 4d^95p \ (^2D) \ ^3F + 10.8 \ 4d^95p \ (^2D) \ ^3D$
204947.6	204887	60.6	0	$99.5 \text{ 4d}^95_{\text{p}} (^2\text{D})^3\text{P}$
205252.2	205287	-34.8	2	$65.8 \ 4d^95p \ (^2D) \ ^1D + 19.3 \ 4d^95p \ (^2D) \ ^3D + 9.1 \ 4d^95p \ (^2D) \ ^3F$
205848.9	205789	59.9	3	71.6 4d ⁹ 5p (² D) ³ D + 27.5 4d ⁹ 5p (² D) ¹ F
208598.5	208599	-0.5	1	76.1 4d ⁹ 5p (² D) ¹ P + 23.4 4d ⁹ 5p (² D) ³ D
209781.2	209856	-74.8	3	$39.5 4d^{9}5p (^{2}D) {}^{1}F + 41.6 4d^{9}5p (^{2}D) {}^{3}F + 18.5 4d^{9}5p (^{2}D) {}^{3}D$
211546.8	211541	5.8	1	$67.6 4d^95p (^2D) ^3D + 21.3 4d^95p (^2D) ^1P + 10.6 4d^95p (^2D) ^3P$
212679.6	212674	5.6	2	$59.4 \ 4d^95p \ (^2D) \ ^3D + 31.1 \ 4d^95p \ (^2D) \ ^1D + 6.4 \ 4d^95p \ (^2D) \ ^3F$
201515.5	212074	194 5	2	33.4 4d $3p(D)$ $D + 31.1$ 4d $3p(D)$ $D + 0.4$ 4d $3p(D)$ P
321015.5	321001	65.2	2	52.9 4d 6p (D) 1^{+} + 14.5 4d 6p (D) 1^{-} D $50.6 4d^{9}6p (^{2}D) ^{3}F + 38.9 4d^{9}6p (^{2}D) ^{1}F + 10.1 4d^{9}6p (^{2}D) ^{3}D$
222452.0	222520	-05.2	4	30.0 4d $6p(D)$ $F + 38.3$ 4d $6p(D)$ $F + 10.1$ 4d $6p(D)$ D
222402.2	323330	-11.0	4	$99.4 40 \text{ op} (D) = 7 \pm 0.2 40 41 (D) = 7$ $45.7 439c_{-} (2D) 3D = 44.7 439c_{-} (2D) 1D = 7.6 439c_{-} (2D) 3D$
323692.6	323699	-0.2	1	45.740 op (D) $F + 44.740$ op (D) $F + 7.040$ op (D) D
324424	324483	-59	2	$51.14d^{\circ} \text{ op}(D) D + 20.34d^{\circ} \text{ op}(D) D + 11.14d^{\circ} \text{ op}(D)^{\circ} \text{ F}$
324925.2	324907	18.2	3	$79.8 4d^{\circ} 6p (^{-}D) + 19.4 4d^{\circ} 6p (^{-}D) + F$
327893.1	327832	61.1	0	91.2 4d 4f (-D) $P + 7.6$ 4d 6p (-D) P
328547.4	328596	-48.6	1	$79.2 \text{ 4d}^{\circ} 4f(^{\circ}D) ^{\circ}P + 8.7 \text{ 4d}^{\circ} 4f(^{\circ}D) ^{\circ}D + 8.6 \text{ 4d}^{\circ} 6p(^{\circ}D) ^{\circ}P$
328806.5	328921	-114.5	2	$80 4d^{\circ} \text{op} (^{2}\text{D}) ^{\circ}\text{F} + 18.8 4d^{\circ} \text{op} (^{2}\text{D}) ^{4}\text{D}$
329330.2	329309	21.2	1	$43 4d^{\circ}6p (^{2}D) ^{1}P + 32.7 4d^{\circ}6p (^{2}D) ^{0}P + 11.8 4d^{\circ}6p (^{2}D) ^{0}D$
329640.5	329756	-115.5	2	$64.6 \ 4d^{\circ}4f(^{2}D) \ ^{\circ}P + 21.3 \ 4d^{\circ}4f(^{2}D) \ ^{\circ}D + 12.6 \ 4d^{\circ}4f(^{2}D) \ ^{\circ}D$
329773.4	329817	-43.6	0	92.1 4d ⁹ 6p (² D) ^{3}P + 7.5 4d ⁹ 4f (² D) ^{3}P
330512.3	330543	-30.7	6	99.7 4d ⁹ 4f (² D) ³ H
330858.3	330829	29.3	5	51.9 $4d^{9}4f(^{2}D)^{3}H + 47.3 4d^{9}4f(^{2}D)^{1}H$
331003.1	330953	50.1	3	$40.5 \ 4d^96p \ (^2D) \ ^1F + 47.4 \ 4d^96p \ (^2D) \ ^3F + 9.4 \ 4d^96p \ (^2D) \ ^3D$
331368.5	331309	59.5	1	78.3 $4d^{9}6p$ (² D) ³ D + 19.2 $4d^{9}6p$ (² D) ³ P
331916.2	331886	30.2	2	55.9 $4d^{9}6p$ (² D) ³ D + 27.6 $4d^{9}6p$ (² D) ¹ D + 7.4 $4d^{9}6p$ (² D) ³ F
332072.4	331952	120.4	2	$37.6 \ 4d^{9}4f \ (^{2}D) \ ^{1}D + 34.1 \ 4d^{9}4f \ (^{2}D) \ ^{3}F + 23.3 \ 4d^{9}4f \ (^{2}D) \ ^{3}D$
331945.4	332009	-63.6	3	$57.8 \text{ 4d}^9 \text{4f} (^2\text{D}) \ ^3\text{D} + 34.4 \ \text{4d}^9 \text{4f} (^2\text{D}) \ ^3\text{F}$
332541.6	332532	9.6	4	$62.2 \ 4d^{9}4f \ (^{2}D) \ ^{3}F + 30.6 \ 4d^{9}4f \ (^{2}D) \ ^{3}G$
332743.2	332743	0.2	4	$48.4 \ 4d^{9}4f(^{2}D)^{-1}G + 19.8 \ 4d^{9}4f(^{2}D)^{-3}H + 16.2 \ 4d^{9}4f(^{2}D)^{-3}F$
332819.1	332809	10.1	5	$75.4 \ 4d^{9}4f(^{2}D) \ ^{3}G + 14 \ 4d^{9}4f(^{2}D) \ ^{1}H + 8.8 \ 4d^{9}4f(^{2}D) \ ^{3}H$
333233.6	333228	5.6	3	$47.5 \ 4d^{9}4f(^{2}D)^{1}F + 22.2 \ 4d^{9}4f(^{2}D)^{3}G + 19 \ 4d^{9}4f(^{2}D)^{3}F$
333972.3	333970	2.3	1	78 4d ⁹ 4f (² D) ³ D + 11.4 4d ⁹ 4f (² D) ¹ P + 5.9 4d ⁹ 4f (² D) ³ P
335865.5	335838	27.5	3	$69.1 4d^{8}5s5p ({}^{3}F) {}^{5}D + 10.9 4d^{8}5s5p ({}^{3}F) {}^{5}F + 9.2 4d^{8}5s5p ({}^{3}P) {}^{5}D$
337003.8	336981	22.8	2	$^{381} 4d^94f(^2D)^{3}D + ^{33}54d^94f(^2D)^{3}P + ^{26}64d^94f(^2D)^{1}D$
337978 7	337829	149.7	4	$60.4 \ 4d^{9}4f \ (^{2}D) \ ^{3}H + 12.5 \ 4d^{8}5s5p \ (^{3}F) \ ^{5}G + 7.3 \ 4d^{9}4f \ (^{2}D) \ ^{1}G$
338146.8	338216	60.2	5	$38 4d^9 4f (^2D) ^{1}H + 38 6 4d^9 4f (^2D) ^{3}H + 22 3 4d^9 4f (^2D) ^{3}G$
228200 7	229255	-09.2	4	$42 + 448_{555} + (3_{\rm E}) = 5C + 14 + 4494 + (2_{\rm E}) = 34 + 11 + 448_{555} + (3_{\rm E}) = 5E$
338200.7	220082	-104.5	4	43.3 40 3sp(F) G + 14.8 40 41(D) H + 1140 3sp(F) F
339093.2	339083	10.2	2	62.74041(D)F + 21.34041(D)D + 14.34041(D)D
339567.8	339446	121.8	3	$42.3 4d^{-}4I(-D)^{-}F + 27.5 4d^{-}4I(-D)^{-}D + 10.5 4d^{-}4I(-D)^{-}F$
339881.9	339853	28.9	2	$68.8 4d^{\circ} 5s5p (^{\circ}F) ^{\circ}D + 14.8 4d^{\circ} 5s5p (^{\circ}P) ^{\circ}D + 7.7 4d^{\circ} 5s5p (^{\circ}F) ^{\circ}F$
339794.6	340105	-310.4	4	$42.4 \ 4d^{\circ}4f \ (^{2}D) \ ^{\circ}G + 36 \ 4d^{\circ}4f \ (^{2}D) \ ^{\circ}G + 20 \ 4d^{\circ}4f \ (^{2}D) \ ^{\circ}F$
340333.8	340131	202.8	3	$52.5 4d^{\circ}4i(-D) \circ G + 30 4d^{\circ}4i(-D) \circ F + 7.5 4d^{\circ}55p(\circ F) \circ G$
340919.3	341024	-104.7	3	$62.4 \ 4d^{\circ} 5s5p (^{\circ}F) \ ^{\circ}G + 12.2 \ 4d^{\circ} 5s5p (^{\circ}F) \ ^{\circ}F + 8.2 \ 4d^{\circ} 4f (^{\circ}D) \ ^{\circ}G$
341920.7	342117	-196.3	2	$65 \ 4d^{\circ}5s5p \ (^{\circ}F) \ ^{\circ}G \ + \ 10.4 \ 4d^{\circ}5s5p \ (^{\circ}D) \ ^{\circ}F \ + \ 10.3 \ 4d^{\circ}5s5p \ (^{\circ}F) \ ^{\circ}F$
342526.8	342504	22.8	1	$69.6 \ 4d^{\circ}5s5p \ (^{\circ}F) \ ^{\circ}D + 19.6 \ 4d^{\circ}5s5p \ (^{\circ}P) \ ^{\circ}D + 5 \ 4d^{\circ}5s5p \ (^{\circ}F) \ ^{\circ}F$
343003	342991	12	1	$77.6 \text{ 4d}^9 \text{4f} (^2\text{D}) ^1\text{P} + 10.1 \text{ 4d}^9 \text{4f} (^2\text{D}) ^3\text{D}$
344718.3	344490	228.3	4	55 4d ⁸ 5s5p (³ F) ⁵ F + 10.8 4d ⁸ 5s5p (³ F) ³ G + 9 4d ⁸ 5s5p (³ F) ¹ G
344859	344847	12	2	$27.7 \ 4d^85s5p \ (^{3}P) \ ^{5}P + 17.7 \ 4d^85s5p \ (^{3}F) \ ^{5}G + 15 \ 4d^85s5p \ (^{1}D) \ ^{3}D$
345259	345176	83	1	$34.1 \ 4d^{\circ}5s5p \ (^{3}F) \ ^{3}F + 30 \ 4d^{\circ}5s5p \ (^{1}D) \ ^{3}D + 7.3 \ 4d^{\circ}5s5p \ (^{3}F) \ ^{3}D$
345738.5	345866	-127.5	3	23.3 $4d^85s5p({}^{3}F) {}^{3}D + 19.3 4d^85s5p({}^{3}F) {}^{3}F + 10.6 4d^85s5p({}^{3}F) {}^{5}D$
346271.9	346187	84.9	3	$32.6 \ 4d^85s5p \ ({}^{3}F) \ {}^{5}F + 15.4 \ 4d^85s5p \ ({}^{3}P) \ {}^{5}P + 11.6 \ 4d^85s5p \ ({}^{1}D) \ {}^{3}D$
346388.9	346613	-224.1	4	$16.5 \ 4d^85s5p \ ({}^3F) \ {}^3G + 32.6 \ 4d^85s5p \ ({}^3F) \ {}^5G + 19.5 \ 4d^85s5p \ ({}^3F) \ {}^1G$
348130.4	348046	84.4	2	54.2 $4d^85s5p({}^{3}F){}^{5}F + 9 4d^85s5p({}^{3}F){}^{5}D + 7.1 4d^85s5p({}^{3}P){}^{5}P$
348955.6	348673	282.6	3	$38.8 \ 4d^{8}5s5p \ (^{3}P) \ ^{5}P + 18.8 \ 4d^{8}5s5p \ (^{3}F) \ ^{3}D + 9.7 \ 4d^{8}5s5p \ (^{3}F) \ ^{5}F$
349088.8	348976	112.8	2	$22.2 \ 4d^{8}5s5p \ ({}^{3}F) \ {}^{3}D + 34.9 \ 4d^{8}5s5p \ ({}^{3}P) \ {}^{5}P + 11.8 \ 4d^{8}5s5p \ ({}^{3}F) \ {}^{3}D$
350304.6	350402	-97.4	3	$37.5 \ 4d^85s5p \ (^3F) \ ^3G + 19.9 \ 4d^85s5p \ (^3F) \ ^3G + 19.1 \ 4d^85s5p \ (^3P) \ ^5P$
351714.5	351987	-272.5	4	$35.9 \ 4d^85s5p \ (^3F) \ ^3F + 30.7 \ 4d^85s5p \ (^3F) \ ^3F + 17.8 \ 4d^85s5p \ (^3F) \ ^5F$
352253.3	352066	187.3	3	$17 \ 4d^85s5p \ (^3F) \ ^3F + 26.3 \ 4d^85s5p \ (^3F) \ ^1F + 16.6 \ 4d^85s5p \ (^3F) \ ^5F$
352173.1	352149	24.1	1	5.1 $4d^85s5p$ (¹ D) ³ P + 32 $4d^85s5p$ (³ F) ⁵ F + 22.9 $4d^85s5p$ (³ F) ³ D
354150.4	353660	490.4	2	43.6 4d ⁸ 5s5p (³ F) ¹ D + 14.5 4d ⁸ 5s5p (³ F) ³ F + 12.4 4d ⁸ 5s5p (¹ D) ³ D
354111.7	353770	341.7	4	$27.1 \ 4d^85s5p \ (^{3}F) \ ^{1}G + 36.4 \ 4d^85s5p \ (^{1}D) \ ^{3}F + 17 \ 4d^85s5p \ (^{3}P) \ ^{5}D$
354929.1	354803	126.1	2	$35 \ 4d^85s5p \ (^1D) \ ^3F + 14 \ 4d^85s5p \ (^3F) \ ^3D + 10 \ 4d^85s5p \ (^3F) \ ^5G$
356138.3	356388	-249.7	2	19.5 4d ⁸ 5s5p (³ F) ³ F + 17.7 4d ⁸ 5s5p (³ F) ³ F + 15.1 4d ⁸ 5s5p (³ F) ¹ D
356309	356392	-83	3	22.4 $4d^{8}5s5p$ (¹ D) ³ D + 16 $4d^{8}5s5p$ (³ P) ⁵ P + 14.2 $4d^{8}5s5p$ (³ F) ¹ F
356582.8	356720	-137.2	3	$18.3 \ 4d^85s5p \ (^3F) \ ^1F + 28.1 \ 4d^85s5p \ (^3P) \ ^5D + 13.7 \ 4d^85s5p \ (^1D) \ ^3F$
358034.5	357868	166.5	1	21.3 $4d^{8}5s5p(^{3}F)^{3}D + 22.3 4d^{8}5s5p(^{3}P)^{3}P + 10.8 4d^{8}5s5p(^{3}F)^{3}D$
358628.7	358718	-89.3	0	$62.9 \ 4d^85s5p \ (^{3}P) \ ^{5}D + 25.4 \ 4d^85s5p \ (^{3}F) \ ^{5}D$
358751.6	358897	-145.4	4	$47.5 \ 4d^85s5p \ (^{3}P) \ ^{5}D + 22.6 \ 4d^85s5p \ (^{3}F) \ ^{1}G + 11.2 \ 4d^85s5p \ (^{3}F) \ ^{3}G$
358922.3	358942	-19.7	1	$63.3 \ 4d^85s5p \ (^{3}P) \ ^{5}D + 19.4 \ 4d^85s5p \ (^{3}F) \ ^{5}D$
359563.3	359447	116.3	2	$20.1 \ 4d^85s5p \ (^{3}P) \ ^{3}P + 24.5 \ 4d^85s5p \ (^{3}P) \ ^{5}D + 19.9 \ 4d^85s5p \ (^{1}D) \ ^{3}D$
360307	360039	268	2	$36.2 4d^85s5p (^{3}P) ^{5}D + 14.5 4d^85s5p (^{1}D) ^{3}F + 10.8 4d^85s5p (^{3}F) ^{5}D$
360330.7	360148	182.7	4	$60.5 \ 4d^85s5p \ (^1G) \ ^3F + 11.5 \ 4d^85s5p \ (^3P) \ ^5D + 10.9 \ 4d^85s5p \ (^1G) \ ^3H$
360831.9	360388	443.9	1	$32.5 \ 4d^85s5p \ (^1D) \ ^3D + 22.9 \ 4d^85s5p \ (^1D) \ ^3P + 14.6 \ 4d^85s5p \ (^3P) \ ^1P$
360920.3	361014	-93.7	4	82 4d ⁸ 5s5p (¹ G) ³ H + 8.2 4d ⁸ 5s5p (¹ G) ³ F + 6.2 4d ⁸ 5s5p (³ F) ¹ G
361284.1	361033	251.1	3	$33.2 4d^85s5p (^1G) ^3F + 30 4d^85s5p (^3P) ^5D + 14.7 4d^85s5p (^1D) ^3F$
362115.9	361961	154.9	2	$38.3 \ 4d^85s5p \ (^1D) \ ^3P + 12.3 \ 4d^85s5p \ (^3P) \ ^3D + 12.3 \ 4d^85s5p \ (^3F) \ ^1D$
362278.5	362942	-663.5	3	7.2 $4d^85s5p(^{1}D)^{3}F + 31.2 4d^85s5p(^{1}D)^{3}D + 26.2 4d^85s5p(^{3}F)^{1}F$
362948.8	363323	-374.2	2	20.6 4d ⁸ 5s5p (¹ D) ³ D + 18 4d ⁸ 5s5p (³ P) ³ P + 11.2 4d ⁸ 5s5p (³ P) ³ P
363895.5	364303	-407.5	1	$33.7 \ 4d^{8}5s5p \ (^{3}P) \ ^{3}D + 18.7 \ 4d^{8}5s5p \ (^{1}D) \ ^{3}P + 15.7 \ 4d^{8}5s5p \ (^{3}P) \ ^{3}P$
364988.4	365408	-419.6	3	$14.2 \ 4d^85s5p \ (^{3}P) \ ^{5}D + 28 \ 4d^85s5p \ (^{1}G) \ ^{3}F + 19.1 \ 4d^85s5p \ (^{3}P) \ ^{3}D$
366418.6	365691	727.6	2	$8.3 \ 4d^85s5p \ (^{3}P) \ ^{3}D + 31.7 \ 4d^85s5p \ (^{1}G) \ ^{3}F + 11.5 \ 4d^85s5p \ (^{3}P) \ ^{3}P$
366197.3	365776	421.3	1	$7.3 \ 4d^85s5p \ (^3P) \ ^3P + 29.8 \ 4d^85s5p \ (^3P) \ ^1P + 16.5 \ 4d^85s5p \ (^3P) \ ^3D$
367240.2	367501	-260.8	Ô	$43.4 \ 4d^85s5p(^1D) \ ^3P + 29.8 \ 4d^85s5p(^3P) \ ^3P + 14.2 \ 4d^85s5p(^3P) \ ^1S$
367621.3	001001	200.0		-101 - 1000 p (-2) - 1 - 2000 q (-000 p (-1) - 1 - 14.2 + 0.000 p (-1) - 0.000
001041.0	367617	4.3	- 2	(0.140°) as $(2P)^{\circ}$ $(2P$
368048 7	367617 368260	4.3 -211 3	2 4	$(^{0.1} 4d^{\circ} 5sp (^{\circ}P) ^{\circ}S + 11.4 4d^{\circ} 5sp (^{\circ}D) ^{\circ}P + 5.9 4d^{\circ} 5sp (^{\circ}G) ^{\circ}F$ $50.5 4d^{8} 5sp (^{1}D) ^{3}F + 15.4 4d^{8} 5sp (^{1}G) ^{3}F + 14.7 4d^{8} 5sp (^{3}D) ^{5}D$
368048.7 368820-4	367617 368260 368709	4.3 -211.3 111.4	2 4 2	$\begin{array}{c} \text{(10.1 4d}^{\circ} \text{ssp} \ (^{\circ} \text{P}) \ ^{\circ} \text{F} + 13.4 \ ^{\circ} \text{ssp} \ (^{\circ} \text{D}) \ ^{\circ} \text{P} + 5.9 \ ^{\circ} \text{4d}^{\circ} \text{ssp} \ (^{\circ} \text{G}) \ ^{\circ} \text{F} \\ \text{50.5 } 4d^8 \text{5s5p} \ (^{\circ} \text{D}) \ ^{\circ} \text{F} + 15.4 \ ^{\circ} \text{4d}^8 \text{5s5p} \ (^{\circ} \text{G}) \ ^{\circ} \text{F} + 14.7 \ ^{\circ} \text{4d}^8 \text{5s5p} \ (^{\circ} \text{P}) \ ^{\circ} \text{D} \\ \text{37 } 34d^8 \text{5s5p} \ (^{\circ} \text{C}) \ ^{\circ} \text{3F} + 12.7 \ ^{\circ} \text{4d}^8 \text{5s5p} \ (^{\circ} \text{P}) \ ^{\circ} \text{D} + 11 \ ^{\circ} \text{4d}^8 \text{5s5p} \ (^{\circ} \text{D}) \ ^{\circ} \text{T} \end{array}$
368048.7 368820.4 368857.8	367617 368260 368709 368848	4.3 -211.3 111.4 9.8	2 4 2 3	$\begin{array}{c} \text{(10.1 } 4d^{\circ} \text{ssp} \ (^{\circ} \text{P}) \ ^{\circ} \text{S} + 11.4 \ ^{\circ} \text{ssp} \ (^{\circ} \text{D}) \ ^{\circ} \text{P} + 5.9 \ ^{\circ} \text{4} \text{C} \ ^{\circ} \text{ssp} \ (^{\circ} \text{G}) \ ^{\circ} \text{F} \\ \text{50.5 } 4d^{\otimes} \text{5sp} \ (^{\circ} \text{D}) \ ^{\circ} \text{F} + 15.4 \ ^{\circ} \text{4} d^{\otimes} \text{5sp} \ (^{\circ} \text{G}) \ ^{\circ} \text{F} + 14.7 \ ^{\circ} \text{4} d^{\otimes} \text{5sp} \ (^{\circ} \text{P}) \ ^{\circ} \text{D} \\ \text{37.3 } 4d^{\otimes} \text{5sp} \ (^{\circ} \text{G}) \ ^{\circ} \text{F} + 12.7 \ ^{\circ} \text{4} d^{\otimes} \text{5sp} \ (^{\circ} \text{P}) \ ^{\circ} \text{D} + 11 \ ^{\circ} \text{4} d^{\otimes} \text{5sp} \ (^{\circ} \text{D}) \ ^{\circ} \text{F} \\ \text{30.1 } 4d^{\otimes} \text{5sp} \ (^{\circ} \text{D}) \ ^{\circ} \text{D} + 13 \ ^{\circ} \text{6} d^{\otimes} \text{6sp} \ ^{\circ} \text{1} \text{D} \ ^{\circ} \text{F} + 12.2 \ ^{\circ} \text{4} d^{\otimes} \text{5sp} \ ^{\circ} \text{3} \text{D} \\ \end{array}$
368048.7 368820.4 368857.8 370001 4	367617 368260 368709 368848 369992	4.3 -211.3 111.4 9.8 9.4	2 4 2 3 1	$\begin{array}{l} \text{(10.1 } 4d^{2} \text{ssp} \ (^{2}\text{P}) \ ^{2}\text{S} + 11.4 \ ^{4} \text{ssp} \ (^{2}\text{D}) \ ^{2}\text{P} + 5.9 \ ^{4} \text{d}^{2} \text{ssp} \ (^{2}\text{G}) \ ^{3}\text{F} \\ \text{50.5 } 4d^{8} \text{5s5p} \ (^{1}\text{D}) \ ^{3}\text{F} + 15.4 \ ^{4} d^{8} \text{5s5p} \ (^{1}\text{G}) \ ^{3}\text{F} + 14.7 \ ^{4} d^{8} \text{5s5p} \ (^{3}\text{P}) \ ^{5}\text{D} \\ \text{37.3 } 4d^{8} \text{5s5p} \ (^{1}\text{G}) \ ^{3}\text{F} + 12.7 \ ^{4} d^{8} \text{5s5p} \ (^{3}\text{P}) \ ^{3}\text{D} + 11 \ ^{4} d^{8} \text{5s5p} \ (^{1}\text{D}) \ ^{3}\text{F} \\ \text{30.1 } 4d^{8} \text{5s5p} \ (^{3}\text{P}) \ ^{3}\text{D} + 13.6 \ ^{4} d^{8} \text{5s5p} \ (^{1}\text{D}) \ ^{3}\text{F} + 12.2 \ ^{4} d^{8} \text{5s5p} \ (^{3}\text{F}) \ ^{3}\text{D} \\ \text{34 } dd^{8} \text{5s5p} \ (^{3}\text{P}) \ ^{1}\text{P} + 12.7 \ ^{4} d^{8} \text{5s5p} \ (^{1}\text{D}) \ ^{3}\text{P} + 9.0 \ ^{4} d^{8} \text{5s5p} \ (^{3}\text{P}) \ ^{3}\text{P} \\ \end{array}$

Table A14: Continued

E^a_{exp}	E^{b}_{calc}	ΔE	J	Leading components (in $\%$) in LS coupling ^{c}
370806.6	371118	-311.4	2	56.7 4d ⁸ 5s5p (³ P) ¹ D + 6.7 4d ⁹⁵ F (² D) ¹ D + 5.6 4d ⁸ 5s5p (³ P) ³ D
371525.5	371494	31.5	2	$69.6 4d^97 \text{p} (^2\text{D}) \ ^3\text{P} + 17.8 \ 4d^97 \text{p} (^2\text{D}) \ ^3\text{D}$
371915.9	371845	70.9	3	$43.6 \ 4d^97p \ (^2D) \ ^1F + 47.5 \ 4d^97p \ (^2D) \ ^3F + 6.3 \ 4d^97p \ (^2D) \ ^3D$
371655.4	372017	-361.6	1	$27.9 \ 4d^85s5p \ (^{3}P) \ ^{3}S + 29.5 \ 4d^85s5p \ (^{3}P) \ ^{3}S + 19.2 \ 4d^{95}F \ (^{2}D) \ ^{3}P$
372145.7	372246	-100.3	1	$56.2 \ 4d^{95}F(^{2}D) \ ^{3}P + 9.6 \ 4d^{95}F(^{2}D) \ ^{3}D + 8.2 \ 4d^{8}5s5p(^{3}P) \ ^{3}S$
372549.3	372629	-79.7	4	77.3 $4d^{9}7p$ (² D) ³ F + 8.3 $4d^{95}F$ (² D) ³ F + 5.4 $4d^{95}F$ (² D) ³ G
372701.4	372717	-15.6	1	$47.5 \ 4d^97p \ (^2D) \ ^1P + 32.1 \ 4d^97p \ (^2D) \ ^3P + 8.4 \ 4d^97p \ (^2D) \ ^3D$
373535.4	373294	241.4	6	$98.5 \ 4d^{95}F \ (^{2}D) \ ^{3}H$
374448.1	374712	-263.9	4	79.4 4d ⁸ 5s5p (¹ G) ³ G + 6.1 4d ⁹⁵ F (² D) ³ G

a: From Swapnil [32] and Ryabtsev [33] b: This work c: Only the component ≥ 5% are given

Wavelength	Lower Level ^a	JLow	Upper level ^a	JUp	log gf	gA	CF	1
291.543	0	0	343003	ĩ	-0.13	5.77E + 10	0.335	
299.426	0	0	333972	1	-0.89	9.61E + 09	0.374	
416.361	128681	3	368858	3	-0.6	9.68E + 09 4.57E + 00	0.146	
420.033	120001	2	366419	2	-0.91	4.57E+09 3.79E+09	0.200	
427.151	130879	2	364988	3	-0.67	7.89E + 09	0.275	
428.386	128681	3	362116	2	-0.98	3.80E + 09	0.255	
429.131	135791	1	368820	2	-0.59	9.29E + 09	0.396	
430.591	128681	3	360920	4	-0.92	4.29E + 09	0.922	
431.687	128681	3	360331	4	-0.02	3.39E + 10	0.925	
431.731	128081	3	360307	2	-1	3.58E+09	0.713	
432.266	138662	2	370001	1	-0.47	1.22E+10	0.536 0.586	
433.122	128681	3	359563	2	-0.34	1.62E + 10	0.767	
433.6	135791	1	366419	2	-0.87	4.77E + 09	0.218	
434.017	135791	1	366197	1	-0.73	6.54E + 09	0.337	
434.018	130879	2	361284	3	-0.51	1.09E + 10	0.575	
434.072	135701	2	363806	1	-0.98	$5.00E \pm 09$ $5.18E \pm 09$	0.22	
439.065	138662	2	366419	2	-0.45	1.23E+10	0.595	
439.314	128681	3	356309	3	-0.9	4.40E + 09	0.342	
440.227	130879	2	358035	1	-0.69	7.09E + 09	0.381	
441.84	138662	2	364988	3	-0.89	4.46E + 09	0.331	
441.844	135791	1	362116	2	-0.87	4.56E + 09	0.876	
441.995	128681	3	354112	4	-0.97	$4.07E \pm 09$	0.529	
447.194	138662	2	362279	3	-0.7	6.75E+09	0.301	
447.283	128681	3	352253	3	-0.33	1.54E + 10	0.789	
447.52	138662	2	362116	2	-0.52	1.01E + 10	0.611	
447.886	130879	2	354150	2	-0.17	2.26E+10	0.709	
448.364	128681	3	351715	4	-0.46	1.16E+10	0.381	
449.192	138002	2	358025	3 1	-0.9	4.14E+09 4.51E⊥00	0.497	
451.724	130879	2	352253	3	-0.79	5.29E+09	0.220 0.233	
453.98	128681	3	348956	3	-0.38	1.34E + 10	0.694	
458.275	130879	2	349089	2	-0.51	9.82E + 09	0.412	
458.883	138662	2	356583	3	-0.93	3.77E + 09	0.365	
459.579	128681	3	346272	3	-0.89	4.04E+09	0.189	
459.821	138662	2	356138	2	-0.64	7.18E + 09	0.413	
462.146	135791	1	352173	1	-0.03	$3.68E \pm 09$	0.31 0.267	
464.062	138662	2	354150	2	-0.67	6.54E + 09	0.177	
465.421	130879	2	345739	3	-0.82	4.69E + 09	0.246	
472.709	0	0	211547	1	-0.73	5.62E + 09	0.733	
479.39	0	0	208598	1	-0.18	1.93E + 10	0.735	
525.225	201051	4	391446	3	-0.95	2.69E + 09 2.82E + 00	0.612	
598.525 607 392	195694	2	361238	2	-0.82	2.83E+09 2.70E+09	0.558	
620.316	196600	3	357808	4	-0.93	2.05E+09	0.393	
625.312	201051	4	360972	3	-0.57	4.60E + 09	0.696	
630.759	209781	3	368320	2	-0.7	3.35E + 09	0.755	
637.473	201051	4	357921	5	-0.77	2.80E + 09	0.384	
641.084	205252	2	361238	2	-0.96	1.79E + 09 1.60E + 00	0.503	
642.505	212680	2	365353	2	-0.98	1.69E+09 2.07E+09	0.504	
644.652	205849	3	360972	3	-0.87	2.07E+09 2.15E+09	0.664	
945.742	200553	1	306290	2	-0.74	1.36E + 09	0.401	
954.656	193894	2	298644	3	-0.06	6.40E + 09	0.754	
959.089	202025	2	306290	2	-0.71	1.42E + 09	0.5	
963.678	202025	2	305794	1	-0.36	3.14E + 09	0.418	
973.489	196600	3	299323	2	-0.05	0.24E+09 2.74E+09	0.593	
989.727	205252	2	306290	2	-0.93	$8.07E \pm 0.08$	0.109	
991.499	208598	1	309456	0	-0.36	2.97E + 09	0.522	
991.61	204948	0	305794	1	-0.77	1.15E + 09	0.751	
994.614	205252	2	305794	1	-0.68	1.41E + 09	0.892	
1012.455	200553	1	299323	2	-0.46	2.24E+09	0.724	
1023.028	206598 201051	1	298644	2	-0.48	2.09E+09 1.01E±10	0.730	
1024.793	193894	2	291475	2	-0.52	1.92E + 09	0.358	
1027.766	202025	2	299323	2	-0.57	1.71E + 09	0.668	
1028.857	208598	1	305794	1	-0.98	6.65E + 08	0.945	
1031.441	193894	2	290846	3	0.07	7.37E + 09	0.455	
1031.979	202025	2	298926	2	-0.26	3.48E+09	0.272	
1035.911	200553	1	297087	2	-0.52	1.87E + 09 7 10E + 00	0.232	
1039.818	200553	1	296724	1	-0.56	1.69E+09	0.309	
1045.795	193894	2	289515	1	-0.56	1.68E + 09	0.338	
1050.32	277340	4	372549	4	-0.81	9.49E + 08	0.448	
1051.945	202025	2	297087	2	-0.81	9.37E + 08	0.182	
1052.4	196600	3	291621	3	0.04	6.55E+09	0.52	
1054.017	196600	3	291475	2	-0.55	1.695+09	0.595	
1054.45	202025	2	296724	1	-0.85	8.39E+08	0.336	
1059.658	202025	2	296395	3	0.33	1.28E + 10	0.53	
1061.043	211547	1	305794	1	-0.37	2.50E + 09	0.909	
1061.051	196600	3	290846	3	-0.24	3.40E + 09	0.425	
1063.029	205252	2	299323	2	-0.15	4.19E + 09	0.586	
1063.924	200553	1	294545	1	-0.72	1.14E+09 6.62E+09	0.205	
1067 556	204948	0	298620	2 1	-0.95	$1.18E \pm 0.09$	0.526	
1068.255	212680	2	306290	2	-0.17	3.96E + 09	0.696	
1069.816	205849	3	299323	2	-0.48	1.93E + 09	0.596	
1073.951	212680	2	305794	1	-0.58	1.54E + 09	0.905	
1076.912	208598	1	301457	2	-0.78	9.46E + 08	0.335	
1077.645	205849	3	298644	3	-0.07	4.90E + 09	0.893	1

Table A15: Computed oscillator strengths and transition probabilities in In IV.

Table A15: Continued

Wavelength 1079.02	Lower Level 209781	J_{Low}	Upper level 302458	J_{Up}_4	log gf -0.71	gA 1.11E+09	CF 0.354
1079.021	200553	1	293230	2	-0.77	9.83E+08	0.486
1082.113	196600	3	288732	2	-0.72	1.09E+09	0.613
$1086.334 \\ 1089.608$	$193894 \\ 204948$	2 0	$285947 \\ 296724$	1	0.19 -0.5	8.63E+09 1.78E+09	$0.802 \\ 0.676$
1092.686	277340	4	368858	3	-0.13	4.18E+09	0.538
1092.712 1096.429	200553	$\frac{1}{2}$	292069 293230	$\frac{0}{2}$	-0.28 -0.65	1.25E+09	0.811 0.599
1096.847	201051 205252	4	292222 296395	4	0.18 0.24	8.46E+09 9.71E+09	$0.743 \\ 0.883$
1099.848	200553	1	291475	2	-0.37	2.33E+09	0.47
1107.085 1113.654	208598 201051	4	298926 290846	2 3	-0.28 -0.44	2.82E+09 1.96E+09	0.867 0.632
1116.107	204948 202025	0	294545 291621	1	-0.38 0.16	2.25E+09 7 80E+09	$0.81 \\ 0.582$
1116.77	209781	3	299325	3	-0.03	5.03E+09	0.389
1117.94 1122.938	202025 283497	2 3	$291475 \\ 372549$	2 4	-0.73 -0.96	1.00E+09 5.85E+08	$0.237 \\ 0.22$
1124.074 1126.418	200553 212680	$\frac{1}{2}$	289515 301457	$\frac{1}{2}$	-0.19 -0.74	3.43E+09 9.56E+08	0.657 0.259
1130.096	208598	1	297087	2	-0.47	1.76E + 09	0.348
1131.458 1134.748	201051 208598	4	289433 296724	$^{5}_{1}$	-0.82	3.43E+10 3.86E+09	0.91 0.89
1136.654 1136.879	205252 201051	2 4	293230 289011	2 4	-0.69 -0.55	1.06E+09 1.46E+09	0.283
1140.925	277340	4	364988	3	-0.87	6.92E+08	0.306
1142.979 1144.44	$202025 \\ 211547$	2 1	289515 298926	$\frac{1}{2}$	-0.97 0.17	5.49E+08 7.50E+09	0.327 0.758
1145.405 1146.624	209781 209781	3	297087 296994	2 4	-0.82 0.71	7.70E+08 2.57E+10	0.23
1148.465	211547	1	298620	1	-0.89	6.59E+08	0.417
1154.127 1154.555	212680 209781	2 3	299325 296395	3	$0.47 \\ -0.55$	1.48E+10 1.41E+09	0.874 0.303
1157.771 1157.83	205849 205252	3	292222 291621	4	0.55 0.12	1.78E+10 6.57E+09	0.873
1159.789	205252	2	291475	2	-0.07	4.18E+09	0.458
1163.517 1165.886	$208598 \\ 205849$	$\frac{1}{3}$	$294545 \\ 291621$	$\frac{1}{3}$	-0.73 -0.6	9.26E+08 1.24E+09	0.335 0.212
1169.047	211547 200553	1	297087 285947	2	-0.48	1.61E + 09 0.01E + 08	0.258
1176.513	200333 205849	3	290846	3	0.26	8.77E+08	0.838
1184.737 1186.76	$212680 \\ 205252$	$\frac{2}{2}$	$297087 \\ 289515$	2 1	$0.06 \\ -0.57$	5.45E+09 1.27E+09	0.544 0.358
1189.025	289433 212680	5	373535	6	-0.25	2.63E+09 6 22E+08	0.597
1194.528	212680	2	296395	3	-0.91	5.76E + 08	0.082
1202.465 1203.132	$205849 \\ 289433$	3 5	$289011 \\ 372549$	$\frac{4}{4}$	-0.45 -0.76	1.64E+09 8.01E+08	0.297 0.53
1204.848	211547 289011	1	294545 371916	1	-0.26	2.52E+09 5.48E+08	0.844
1206.517	205849	3	288732	2	-0.19	2.95E+09	0.448
1206.617 1221.52	$208598 \\ 212680$	$\frac{1}{2}$	$291475 \\ 294545$	2 1	-0.52 -0.66	1.38E+09 9.73E+08	0.324 0.434
1223.939	290846	3	372549	4	-0.96	4.94E+08	0.514
1235.838	208598	1	289515	1	-0.41	1.71E+0.09	0.353
1267.395 1282.571	$130879 \\ 211547$	2 1	$209781 \\ 289515$	$\frac{3}{1}$	-0.71 -0.85	8.16E+08 5.78E+08	0.087 0.117
1295.882	128681 135701	3	205849	3	0.08	4.80E+09 1.58E+09	0.727
1320.038	135791	1	212030	1	-0.22	2.29E+09	0.746
1322.26 1333.871	$293230 \\ 130879$	$\frac{2}{2}$	$368858 \\ 205849$	3 3	-0.96 -0.39	4.17E+08 1.52E+09	$0.087 \\ 0.56$
1344.573	130879 138662	2	205252	2	-0.19	2.39E+09 2.92E+09	0.464
1373.494	135791	1	208598	1	-0.87	4.73E+08	0.398
1381.788 1398.772	$128681 \\ 205849$	3 3	$201051 \\ 277340$	$\frac{4}{4}$	$0.37 \\ -0.94$	8.26E+09 3.91E+08	$0.848 \\ 0.806$
1405.572	130879	2	202025	2	-0.25	1.89E+09 5.24E+09	0.799
1400.093	321152	2	391587	2	-0.7	6.48E+08	0.385
1422.584 1429.872	$321152 \\ 138662$	$\frac{2}{2}$	$391446 \\ 208598$	$\frac{3}{1}$	-0.81 -0.24	5.10E+08 1.86E+09	0.371 0.781
1435.256	130879	2	200553	1	-0.2	2.03E+09 3.18E+08	0.83
1439.662	135791	1	205252	2	-0.56	8.78E+08	0.801
1446.002 1470.72	$135791 \\ 323452$	$\frac{1}{4}$	$204948 \\ 391446$	0 3	-0.59 -0.49	8.26E + 08 9.89E + 08	0.849 0.611
1472.357 1488.387	$128681 \\ 138662$	3	196600 205849	3	-0.31 -0.72	1.50E+09 5.77E+08	0.783
1501.725	138662	2	205252	2	-0.49	9.59E+08	0.24
1503.287 1509.818	$324925 \\ 135791$	3 1	$391446 \\ 202025$	$\frac{3}{2}$	-0.63 -0.24	6.92E+08 1.70E+09	$0.626 \\ 0.416$
1521.594 1533.442	130879 128681	2	196600 193894	3	$0.06 \\ 0.07$	3.29E+09 3.36E+09	0.578
1802.489	277340	4	332819	5	-0.69	4.22E + 08	0.722
1869.586 2062.975	289515 294545	1	$343003 \\ 343003$	1	-0.62 -0.33	$^{4.57E+08}_{7.38E+08}$	$0.176 \\ 0.568$
2071.953 2160 119	284985 296724	2	333234 343003	3 1	-0.67 -0.36	3.33E+08 6 20E+08	0.622
2248.663	289515	1	333972	1	-0.1	1.06E + 09	0.616
2275.172 2285.962	296395 289011	3 4	$340334 \\ 332743$	3 4	-0.28 -0.12	9.76E + 08	0.549 0.767
2287.962 2296.554	285947 289011	1 4	329640 332542	$\frac{2}{4}$	-0.03 -0.54	1.20E+09 3.63E+08	0.397
2304.175	289433	5	332819	5	0.06	1.45E+09	0.959
2304.326 2306.615	285947 288732	1 2	329330 332072	1 2	-0.71	2.43E+08 4.31E+08	0.204 0.382
2311.574 2313.394	297087 288732	$\frac{2}{2}$	$340334 \\ 331945$	3 3	-0.05 0.21	1.11E+09 2.04E+09	0.716 0.573
2319.008	289433	5	332542	4	-0.8	1.98E+08	0.711
2335.089	290994 285947	4	328547	4 1	-0.16	1.13E+08	0.475
2349.062 2353.26	289515 297087	$\frac{1}{2}$	$332072 \\ 339568$	2 3	$0.1 \\ 0.17$	1.52E+09 1.77E+09	$0.586 \\ 0.553$
·			192				

Table A15: Continued

Wavelength 2354 494	Lower Level 294545	JLow	Upper level 337004	JUP	log gf	gA 2.10E±09	CF 0.856
2359.472	296724	1	339093	2	0.25	2.16E+09 2.16E+09	0.937
2379.849 2380.595	297087 298926	2 2	$339093 \\ 340919$	2 3	-0.42 -0.68	4.50E+08 2.50E+08	$0.36 \\ 0.578$
2383.283	285947	1	327893	0	-0.4	4.70E + 08	0.511
2385.696	292069 289011	$0 \\ 4$	333972 330858	1 5	-0.17 0.8	7.92E+08 7 40E+09	0.835
2391.271	296395	3	338201	4	0.11	1.53E+09	0.866
2393.974	291475 290846	2	333234	3	0.32	2.46E+09 3.74E+09	0.802
2402.365	291621	3	333234	3	0.07	1.34E+09	0.644
2404.038	296395 289433	3	337979 330858	4	0.58 0.76	4.36E+09 2 00E+08	0.923
2414.258	298926	2	340334	3	0.1	1.44E+09	0.689
2419.974	329330	1	370640	0	-0.26	6.19E+08	0.46
2429.216	296994	4	338147	5	0.79	6.99E+09	0.949
2431.016	291621	3	332743	4	0.64	4.88E + 09	0.892
2432.382 2433.575	289433	5	330512	6	0.27	2.09E+09 8.57E+09	0.932
2437.77	299325	3	340334	3	-0.37	4.78E + 08	0.571
2459.765	298926	2	339568	3	0.01	2.04E+09	0.818
2462.457	291475	2	332072	2	-0.06	9.49E+08	0.526
2467.085	292222	4	332743	4	-0.91	1.36E+09	0.885
2469.996	298620	1	339093	2	-0.66	2.42E+08	0.741
2470.258 2479.425	299325 292222	3 4	339795 332542	4	0.66	1.57E+09	0.969
2484.176	299325	3	339568	3	-0.25	6.11E + 08	0.297
2488.831 2491.445	298926 289515	2	329640	2	-0.53	2.62E+08	0.235 0.186
2499.003	293230	2	333234	3	-0.24	6.07E + 08	0.63
2504.429 2510.545	297087 321152	2	337004 360972	2	-0.31 0.16	5.17E+08 1.50E+09	0.363
2510.844	288732	2	328547	1	-0.4	4.18E + 08	0.585
2516.639 2529.994	$292222 \\ 328807$	4	$331945 \\ 368320$	3 2	-0.53 -0.3	3.11E+08 5.16E+08	0.679
2542.116	328807	2	368132	1	-0.01	9.96E + 08	0.857
2542.969 2560.334	$321926 \\ 321926$	3	$361238 \\ 360972$	2	$0.14 \\ -0.24$	1.42E+09 5.85E+08	0.633
2563.978	329330	1	368320	2	-0.14	7.31E + 08	0.788
2571.43 2576 909	301457 290846	2	$340334 \\ 329640$	3	-0.3 -0.51	5.00E+08 3.13E+08	0.611
2582.161	293230	2	331945	3	-0.67	2.15E + 08	0.348
2604.457	298620 320773	1	337004 368132	2	-0.5 0.58	3.12E + 08 2.58E + 08	0.636
2625.407	298926	2	337004	2	-0.96	1.07E+08	0.259
2656.198	301457	2	339093	2	-0.78	1.57E + 08	0.505
2676.918	323452 323893	4	361238	2	-0.14	6.76E+08	0.879
2678.926	331003	3	368320	2	0.26	1.69E + 09	0.867
2694.048	328807	$\frac{2}{2}$	365914	2	0.2	1.45E+09 1.35E+09	0.429
2694.843	328547	1	365644	2	-0.97	9.77E+07	0.164
2712.583	321920	2	358006	1	-0.33	3.35E+08	0.395
2713.364	323893	1	360737	0	-0.16	6.25E+08	0.706
2714.838 2715.111	321926	3	358746	3	-0.93	1.05E+08 1.19E+09	0.425 0.46
2715.31	321152	2	357969	2	0.45	2.50E + 09	0.619
2715.546 2719.283	324424 331369	2	368132	2	-0.1	1.34E+09 7.14E+08	0.917
2732.619	329330	1	365914	2	-0.2	5.68E + 08	0.537
2741.033 2744.917	321926 328807	3 2	365227	3 1	-0.78	1.12E+09 1.46E+08	0.629
2745.63	293230	2	329640	2	-0.63	2.08E + 08	0.5
2746.124 2752.937	331916 329330	$\frac{2}{1}$	$368320 \\ 365644$	$\frac{2}{2}$	-0.03 -0.14	8.29E+08 6.45E+08	$0.625 \\ 0.316$
2753.028	324925	3	361238	2	-0.28	4.65E+08	0.817
2760.41 2762.145	$331916 \\ 288732$	$\frac{2}{2}$	$368132 \\ 324925$	1 3	-0.37 -0.63	3.71E+08 2.06E+08	$0.835 \\ 0.544$
2768.406	328807	2	364918	3	0.73	4.66E + 09	0.934
2773.391 2773.645	324925 321926	3	360972 357969	3 2	$0.11 \\ -0.47$	1.11E+09 2.89E+08	0.777
2779.9	328547	1	364509	1	-0.93	1.01E + 08	0.114
2783.629 2784.965	289011 329330	4 1	324925 365227	3 1	-0.84 -0.18	1.25E+08 5.68E+08	0.357
2786.091	321926	3	357808	4	0.84	5.98E + 09	0.912
2801.166 2810.743	302458 321152	4	338147 356719	5	-0.58 0.34	2.22E+08 1.81E+09	$0.563 \\ 0.775$
2816.691	323452	4	358944	4	0.37	1.95E+09	0.858
2819.782 2837 769	329773 294545	0	365227 329773	1	-0.12 -0.86	6.41E+08 1 15E+08	0.723
2839.704	285947	1	321152	2	-0.25	4.67E + 08	0.556
2841.761	329330 331003	1	364509 366068	1	0.01	8.49E+08 1.25E+09	0.49
2860.538	323893	1	358841	2	0.17	1.20E+09 1.20E+09	0.692
2860.767	323452	4	358398	3	-0.39	3.34E+08	0.486
2863.768	289515	1	324424	2	-0.94	9.30E+07	0.255
2870.274	297087	2	331916	2	-0.34	3.66E + 08	0.277
2878.021	294545 329773	1 0	329330 364509	1	-0.81	1.23E+08 3.74E+08	0.171
2885.598	296724	1	331369	1	-0.88	1.06E + 08	0.219
2885.89 2888.622	331003 296395	3 3	365644 331003	23	-0.84 -0.97	1.16E+08 8.54E+07	0.161 0.198
2893.86	331369	1	365914	2	0.26	1.44E + 09	0.759
2900.341 2902.688	$323452 \\ 289011$	4 4	$357921 \\ 323452$	$\frac{5}{4}$	0.96 -0.87	7.19E+09 1.07E+08	0.939
2904.69	324424	2	358841	2	0.36	1.81E + 09	0.659
2908.021 2909.881	289515 323452	1 4	$323893 \\ 357808$	1 4	-0.37 -0.33	3.34E+08 3.66E+08	0.506
2910.33	331003	3	365353	4	0.87	5.80E + 09	0.942
2912.747 2916.656	324424 331369	2	358746 365644	3 2	$0.59 \\ 0.11$	3.05E+09 1.01E+09	0.834 0.847

Table A15: Continued

Wavelength 2927.272	Lower Level 331916	J_{Low}	Upper level 366068	J_{Up}	log gf 0.61	gA 3.19E+09	CF 0.902
2930.576	323893	1	358006	1	0.18	1.18E+09	0.709
2933.474 2938.65	290846 289433	3 5	$324925 \\ 323452$	3 4	-0.01 0.46	7.49E+08 2.24E+09	0.899 0.868
2938.657	324925	3	358944	4	0.71	3.98E + 09	0.956
2939.507 2940.481	$296994 \\ 331916$	4	$331003 \\ 365914$	3 2	0.33	1.66E+09 9.40E+07	0.831
2940.721	332072	2	366068	3	-0.85	1.11E + 08	0.308
2947.721	331003 331369	3	364918 365227	3	-0.45 -0.13	2.76E+08 5.70E+08	0.349
2955.914	324925	3	358746	3	-0.17	5.13E + 08	0.358
2964.021 2976.934	331916 324424	2	$365644 \\ 358006$	2	0.26	1.37E+09 3.63E+08	0.518
2980.008	309456	0	343003	1	-0.1	5.92E+08	0.583
2986.665	324925 331945	3	358398 365353	3	0.43	2.02E+09 0.19E+07	0.878
3001.717	291621	3	324925	3	-0.91	9.06E+07	0.265
3016.55	331369 296724	1	364509 320773	1	-0.45	2.58E + 08 9.65E + 07	0.439
3025.424	324925	3	357969	2	0.02	7.51E+08	0.856
3029.283	331916	2	364918	3	-0.59	1.89E+08	0.165
3037.306	289011	4	321926	3	0.3	1.45E+09	0.430
3040.237	324925	3	357808	4	-0.46	2.49E + 08 1.25E + 08	0.279
3045.48	291621	3	324424	$\frac{1}{2}$	0.07	8.41E+08	0.797
3056.898	292222	4	324925	3	0.19	1.10E + 09	0.896
3066.001	290724 290846	3	323452	4	-0.55	7.24E+07	0.498
3067.243	331916	2	364509	1	-0.46	2.43E+08	0.316
3081.463	299325 298926	3 2	331916 331369	2	-0.07	6.03E+08	0.775
3083.681	288732	2	321152	2	-0.14	5.17E + 08	0.586
3083.811 3084.397	291475 296395	2	323893 328807	1 2	-0.48 0.2	2.34E+08 1.11E+09	0.573 0.872
3095.575	324424	2	356719	1	-0.88	9.18E + 07	0.174
3100.486	297087 292069	2	329330 323893	1	-0.51 -0.69	2.14E+08 1.41E+08	0.328
3155.857	299325	3	331003	3	-0.29	3.43E + 08	0.435
3160.013 3183.154	289515 329330	1	$321152 \\ 360737$	2	-0.9 -0.98	8.40E+07 6.98E+07	0.339
3201.084	292222	4	323452	4	-0.09	5.35E + 08	0.955
3204.791 3216.584	293230 290846	2	324424 321926	2	-0.62 -0.56	1.56E+08 1.80E+08	0.716 0.544
3260.312	293230	2	323893	1	-0.8	1.00E + 00 1.00E + 08	0.805
3283.02	291475 290846	2	321926 321152	3	-0.93	7.31E+07 2.71E+08	0.579
3298.818	291621	3	321926	3	-0.33	2.88E+08	0.601
3345.681	298926	2	328807	2	-0.56	1.67E+08	0.648
3502.213	302458	$\frac{2}{4}$	331003	3	-0.78	9.00E+07	0.874
3529.026	329640	2	357969	2	-0.89	6.82E+07	0.198
3586.6	301457	$\frac{1}{2}$	329330	1	-0.93	6.11E+07	0.248
3617.254	343003	1	370640	0	-0.95	5.78E + 07	0.092
3647.458	330512	6	357921	5	0.16	7.23E+08	0.669
3674.531	338147	5	365353	4	0.1	6.23E+08	0.76
3709.586	330858	5	357808	4	0.08	5.86E+08	0.264
3711.033	337979	4	364918	3	-0.14	3.55E+08	0.694
3734.655	332072	2	355914 358841	2	-0.92	$5.76E \pm 07$ $5.83E \pm 07$	0.383
3735.272	333972	1	360737	0	-0.8	7.62E+07	0.461
3779.329	331945	4 3	358398	3	-0.62 -0.54	1.13E+08 1.34E+08	0.664 0.431
3786.396	332542	4	358944	4	-0.61	1.15E + 08	0.551
3805.084	298644 339795	3 4	324925 366068	3	-0.02	4.33E+08	0.89
3825.421	339093	2	365227	1	-0.4	1.84E + 08	0.844
3826.614 3827.034	332819 305794	5 1	$358944 \\ 331916$	$\frac{4}{2}$	0.04 -0.11	3.53E+08	0.858 0.952
3833.783	339568	3	365644	2	-0.19	2.97E + 08	0.847
3841.604 3844.683	331945 332743	3 4	357969 358746	2 3	-0.41 -0.05	4.00E+08	0.828
3854.935	332072	2	358006	1	-0.56	1.23E + 08	0.424
3901.185	332542 306290	$\frac{4}{2}$	331916	3 2	-0.16	6.84E+08	0.664
3904.02	333234	3	358841	2	-0.21	2.68E + 08	0.741
3904.805 3908.124	299323 340334	2	324925 365914	3	-0.03 -0.28	4.07E+08 2.33E+08	0.894 0.861
3908.995	305794	1	331369	1	0.14	6.05E + 08	0.939
3911.428 3918.588	$339795 \\ 333234$	4	$365353 \\ 358746$	4	-0.8 -0.67	6.67E+07 9.35E+07	$0.533 \\ 0.434$
3982.659	332819	5	357921	5	-0.64	9.63E + 07	0.916
3982.775 3988.567	299323 332743	2 4	$324424 \\ 357808$	2 4	0.38 -0.81	1.01E+09 6 44E+07	0.907
4029.772	298644	3	323452	4	0.63	1.78E + 09	0.982
4045.33 4066.558	306290 340334	2	331003 364918	3	0.5 -1	1.29E+09 4.11E+07	0.967
4068.885	299323	2	323893	1	0.13	5.38E + 08	0.87
4159.686	333972 305794	1	358006 320772	1	-0.62	9.18E+07	0.509
4293.976	298644	3	321926	3	-0.06	3.20E+08	0.902
4339.062	306290	2	329330	1	0.06	4.02E+08	0.921
4422.985	299323	2	321926	2 3	0.18	7.36E+08	0.902
4425.828	368858	3	391446	3	-0.69	6.92E + 07	0.757
4439.984 4441.699	298644	23	328807 321152	2	-0.15 0.34	2.40E+08 7.48E+08	0.937
4491.672	306290	2	328547	1	-0.92	3.95E + 07	0.877
4498.439 4648.499	343003 343003	1	365227 364509	1	-0.99 -0.63	$3.40E \pm 07$ $7.21E \pm 07$	0.392 0.587
4810.998	370807	2	391587	2	-0.58	7.16E + 07	0.371
4983.406 5018.529	371526 371526	2	391587 391446	3	0.55	9.27E+08 2.59E+08	0.588

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Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA	CF
5030.203	309456	0	329330	1	-0.62	6.32E + 07	0.751
5118.849	371916	3	391446	3	-0.06	2.19E + 08	0.729
5142.388	372146	1	391587	2	-0.71	4.66E + 07	0.227
5290.429	372549	4	391446	3	0.36	5.33E + 08	0.62
6007.839	357808	4	374448	4	-0.82	2.89E + 07	0.731
6228.608	358398	3	374448	4	-0.34	8.18E + 07	0.722
6255.074	356719	1	372701	1	-0.39	6.93E + 07	0.314
6366.729	358746	3	374448	4	-0.72	3.25E + 07	0.265
6402.476	357921	5	373535	6	1.01	1.64E + 09	0.952
6448.287	358944	4	374448	4	-0.93	1.95E + 07	0.424
6480.393	356719	1	372146	1	-0.08	1.33E + 08	0.475
6663.582	343003	1	358006	1	-0.81	2.31E + 07	0.381
6693.116	356719	1	371655	1	-0.49	5.06E + 07	0.663
6751.835	356719	1	371526	2	-0.1	1.15E + 08	0.482
6781.698	357808	4	372549	4	-0.32	7.04E + 07	0.831
6802.88	358006	1	372701	1	-0.23	8.48E + 07	0.376
6834.085	357921	5	372549	4	0.52	4.76E + 08	0.686
6924.751	309456	0	323893	1	-0.99	1.43E + 07	0.533
7051.784	357969	2	372146	1	-0.28	7.25E + 07	0.568
7064.341	358398	3	372549	4	-0.87	1.83E + 07	0.063
7070.236	358006	1	372146	1	-0.7	2.73E + 07	0.237
7086.173	357808	4	371916	3	0.53	4.48E + 08	0.861
7212.811	358841	2	372701	1	-0.11	9.94E + 07	0.593
7304.404	357969	2	371655	1	-0.78	2.23E + 07	0.675
7348.268	358944	4	372549	4	0.36	2.86E + 08	0.965
7374.395	357969	2	371526	2	0.21	2.02E + 08	0.653
7394.577	358006	1	371526	2	-0.93	1.45E + 07	0.18
7395.343	358398	3	371916	3	-0.26	6.59E + 07	0.657
7590.867	358746	3	371916	3	-0.13	8.54E + 07	0.551
7615.268	358398	3	371526	2	-0.28	5.96E + 07	0.279
7646.137	358841	2	371916	3	-0.92	1.37E + 07	0.314
7787.354	357969	2	370807	2	-0.6	2.96E + 07	0.52
7809.863	358006	1	370807	2	-0.64	2.63E + 07	0.5
8355.483	360737	0	372701	1	-0.57	2.53E + 07	0.43
8634.847	360972	3	372549	4	0.63	3.89E + 08	0.938
8721.096	361238	2	372701	1	0.2	1.40E + 08	0.911
8762.45	360737	0	372146	1	-0.94	9.87E + 06	0.179
9134.586	360972	3	371916	3	-0.07	6.78E + 07	0.881
9165.404	361238	2	372146	1	-0.9	1.02E + 07	0.768
9362.656	361238	2	371916	3	0.48	2.27E + 08	0.769
9472.482	360972	3	371526	2	0.41	1.90E + 08	0.958
9557.425	358398	3	368858	3	-0.83	1.08E + 07	0.733
10164.878	360972	3	370807	2	-0.99	7.04E + 06	0.867
12676.749	360972	3	368858	3	-0.95	4.61E + 06	0.785

Table A15: Continued

a: Experimental values from: [33, 32]

In V

Energy Levels

\mathbf{F}^{a}	\mathbf{F}^{b}	ΔF	T	Leading components (in $\%$) in LS coupling ^c
\Box_{exp}	^L calc	 _	0	Leading components (in 70) in LS coupling
0	0	0	2.5	99.5 4d ^o (² D) ² D
7171.8	7172	-0.2	1.5	$9954d^9(^2D)^2D$
100400.0	100410	10.0	1.0	
160428.2	160412	16.2	4.5	$98.5 \text{ 4d}^{\circ} 5s (^{\circ}\text{F})^{-}\text{F}$
163979.7	163935	44.7	3.5	$82.4 4d^8 5s (^{3}\text{F}) ^{4}\text{F} + 16.2 4d^8 5s (^{3}\text{F}) ^{2}\text{F}$
167760.8	167718	12.8	25	91 7 4d ⁸ 5e (3 E) 4E \pm 5 4d ⁸ 5e (1 D) 2D
101100.0	107710	42.0	2.5	31.7 40 38 (P) P + 040 38 (D) D
169230.4	169174	56.4	1.5	$81.4 \text{ 4d}^{\circ} \text{ 5s} (^{\circ}\text{F}) + F + 16.6 \text{ 4d}^{\circ} \text{ 5s} (^{\circ}\text{D}) + D$
171289.7	171358	-68.3	3.5	$81.5 \text{ 4d}^8 5 \text{ 5s} ({}^3\text{F}) {}^2\text{F} + 17 \text{ 4d}^8 5 \text{ 5s} ({}^3\text{F}) {}^4\text{F}$
172270.0	179410	41.1	0.5	$26.9 \pm 18.5 \pm (3.5) \pm 10.4 \pm 18.5 \pm (1.5) \pm 25.4 \pm 0.0 \pm 418.5 \pm (3.5) \pm 25.5$
173370.9	1/3412	-41.1	2.5	$36.8 \text{ 4d}^{-} \text{ 5s} (^{-}\text{P}) \text{ P} + 31.9 \text{ 4d}^{-} \text{ 5s} (^{-}\text{D}) \text{ D} + 29.6 \text{ 4d}^{-} \text{ 5s} (^{-}\text{F}) \text{ F}$
177669.8	177782	-112.2	2.5	$52.7 \text{4d}^8 \text{5s} (^3\text{F}) ^2\text{F} + 43.9 \text{4d}^8 \text{5s} (^3\text{P}) ^4\text{P}$
178288 8	178203	4.9	15	54.2 4d ⁸ 5c $({}^{3}P)$ 4P + 23 4d ⁸ 5c $({}^{1}D)$ 2D + 12.2 4d ⁸ 5c $({}^{3}P)$ 2P
170200.0	170233	-4.2	1.5	0 = 2 = 40 = 0.5 (1) = 1 = 2.5 = 40 = 0.5 (1) = 1 = 12.2 = 40 = 0.5 (1) = 1
180492.8	180552	-59.2	0.5	$97.1 \text{ 4d}^{\circ} \text{ 5s} (^{\circ}\text{P}) \stackrel{\text{\tiny 4}}{=} \text{P}$
182194	182182	12	1.5	$33.3 \text{ 4d}^8 \text{ 5s} (^1\text{D}) ^2\text{D} + 44.7 \text{ 4d}^8 \text{ 5s} (^3\text{P}) ^4\text{P} + 15.3 \text{ 4d}^8 \text{ 5s} (^3\text{P}) ^2\text{P}$
195600 1	195659	20.0	0 5	$(3 \pm 4.18 \pm (1 \pm 2.15))$ 2 $\pm 1.17.8 + 4.18 \pm (3 \pm 2.15)$ 4 $\pm 1.12.2 + 4.18 \pm (3 \pm 2.15)$ 2 $\pm 1.17.8 \pm 1.18$ 2 ± 1.1
183022.1	185052	-29.9	2.5	62.5 4 d $3s$ (D) D + 17.8 4 d $3s$ (F) F + 15.5 4 d $3s$ (F) F
188396.3	188434	-37.7	4.5	$98.4 \text{ 4d}^{\circ} 5s (^{1}\text{G})^{-2}\text{G}$
188575 1	188537	38.1	3.5	$97.4 4d^8 5s (^1C) ^2C$
100010.1	100001	-0.1	0.0	
188639.6	188563	76.6	0.5	$97.6 \text{ 4d}^{\circ} \text{ 5s} (^{\circ}\text{P}) \stackrel{\text{-}}{=} \text{P}$
188649.1	188583	66.1	1.5	$70.9 \text{4d}^8 \text{5s} (^{3}\text{P}) ^2\text{P} + 26.6 \text{4d}^8 \text{5s} (^{1}\text{D}) ^2\text{D}$
220602.6	220604	0.4	0.5	$05.2 448 5_{0}$ (1S) 2S + 2.2 448 5_{0} (3P) 4P
220035.0	220034	-0.4	0.5	33.240 35 (3) 5 ± 2.340 35 (1) 1
349273.3	349350	-76.7	3.5	$79.6 \text{ 4d}^{\circ} \text{ 5d} ({}^{\circ}\text{F}) {}^{\circ}\text{D} + 13.7 \text{ 4d}^{\circ} \text{ 5d} ({}^{\circ}\text{F}) {}^{\circ}\text{F}$
349569.3	349576	-6.7	2.5	$41.3 \text{ 4d}^8 \text{ 5d} ({}^3\text{F}) {}^4\text{D} + 48.3 \text{ 4d}^8 \text{ 5d} ({}^3\text{F}) {}^4\text{P}$
251020.0	251082	42.0	E E	40 = 438 = 372 $211 + 200 = 438 = 372$ $411 + 76 = 438 = 3737$ 472
301039.2	201083	-43.8	0.0	30.3 40 30 (F) = H + 33.3 40 30 (F) = H + (.0.40 30 (F) = G
351397.5	351294	103.5	6.5	98.2 4d° 5d (°F) ⁴ H
351761.9	351678	83.9	1.5	$40.4 \text{ 4d}^8 \text{ 5d} ({}^{3}\text{F}) {}^{2}\text{P} + 27.8 \text{ 4d}^8 \text{ 5d} ({}^{3}\text{F}) {}^{4}\text{D}$
050400.0	001010	05.0	4 5	$20.0 4.18 \pm 1.(3\pi) 4 \alpha + 20.0 4.18 \pm 1.(3\pi) 2 \alpha + 20.0 4.18 \pm 1.(3\pi) 4 \pi$
352433.9	352336	97.9	4.5	$39.8 \ 4d^{\circ} \ 5d \ (^{\circ}F) \ ^{\circ}G + 29.3 \ 4d^{\circ} \ 5d \ (^{\circ}F) \ ^{\circ}G + 9.9 \ 4d^{\circ} \ 5d \ (^{\circ}F) \ ^{\circ}F$
352548.2	352438	110.2	5.5	78.2 4d ⁸ 5d (³ F) ⁴ G + 19 4d ⁸ 5d (³ F) ² H
251571 7	252572	1000.2	25	42.4 4.48 5.4 $(3E)$ $2E$ $+$ 21.4 4.48 5.4 $(3E)$ $4E$ $+$ 11.7 4.47 5.2 $(4E)$ $4E$
331371.7	332372	-1000.3	5.5	42.4 4u $5u$ (F) F + 21.4 4u $5u$ (F) F + 11.7 4u $5s$ (F) F
353886.1	353681	205.1	2.5	$41.2 4d^{\circ} 5d ({}^{3}\text{F}) {}^{4}\text{P} + 20.7 4d^{\circ} 5d ({}^{3}\text{F}) {}^{4}\text{D} + 12 4d^{\circ} 5d ({}^{3}\text{F}) {}^{4}\text{F}$
353631.9	354257	-625.1	4.5	$45.6 4d^8 5d ({}^{3}\text{F}) {}^{4}\text{F} + 25.4d^8 5d ({}^{3}\text{F}) {}^{2}\text{G} + 16.7 4d^7 5s^2 ({}^{4}\text{F}) {}^{4}\text{F}$
25000010	256102	20.0	1.0	
356232.8	320193	39.8	1.5	$46.2 \ 4d^{\circ} \ 5d \ (^{\circ}F) \ -P \ + \ 43.7 \ 4d^{\circ} \ 5d \ (^{\circ}F) \ -D$
356617.7	356477	140.7	0.5	$73.3 \text{ 4d}^8 \text{ 5d} ({}^3\text{F}) {}^4\text{D} + 13 \text{ 4d}^8 \text{ 5d} ({}^3\text{F}) {}^4\text{P} + 8 \text{ 4d}^8 \text{ 5d} ({}^3\text{F}) {}^2\text{P}$
357392.6	356714	678.6	2.5	$42.7 4d^7 5s^2 ({}^{4}\text{F}) {}^{4}\text{F} + 25.7 4d^8 5d ({}^{3}\text{F}) {}^{4}\text{F} + 12.4d^8 5d ({}^{3}\text{F}) {}^{4}\text{D}$
057552.0	055700	145.0	2.0	
357537.3	357392	145.3	4.5	$62.4 4d^{\circ} 5d (^{\circ} \text{F})^{-} \text{H} + 18.9 4d^{\circ} 5d (^{\circ} \text{F})^{-} \text{G} + 15.8 4d^{\circ} 5d (^{\circ} \text{F})^{-} \text{H}$
358493.2	357859	634.2	1.5	$34.4 \text{ 4d}^8 \text{ 5d} ({}^{3}\text{F}) {}^{4}\text{F} + 33.7 \text{ 4d}^7 \text{ 5s}^2 ({}^{4}\text{F}) {}^{4}\text{F} + 14 \text{ 4d}^8 \text{ 5d} ({}^{1}\text{D}) {}^{2}\text{D}$
357050 5	357004	46.5	35	40.3 4d ⁸ 5d $({}^{3}\text{F})$ 4C \pm 33.8 4d ⁸ 5d $({}^{3}\text{F})$ 4H \pm 18 4d ⁸ 5d $({}^{3}\text{F})$ 2F
337930.3	337904	40.5	3.5	40.54 40.54 50 (F) $G + 55.64$ 50 (F) $H + 1640$ 50 (F) F
358242.2	357927	315.2	5.5	$58.1 \text{ 4d}^{\circ} \text{ 5d} (^{\circ}\text{F}) ^{4}\text{H} + 28.5 \text{ 4d}^{\circ} \text{ 5d} (^{\circ}\text{F}) ^{2}\text{H} + 12.9 \text{ 4d}^{\circ} \text{ 5d} (^{\circ}\text{F}) ^{4}\text{G}$
358748.1	358004	744.1	1.5	$67.6 \ 4d^8 \ 5d \ (^{3}F) \ ^{4}P + 5.5 \ 4d^8 \ 5d \ (^{3}F) \ ^{4}F + 5.1 \ 4d^8 \ 5d \ (^{3}F) \ ^{4}D$
250142 7	259595	201.2	0 5	(3E) $(3E)$
338143.7	338323	-361.5	2.5	$50.4 \ 4d^{-} \ 5d^{-} \ F + 11.5 \ 4d^{-} \ 5d^{-} \ 5d^{-} \ F + 11.5 \ 4d^{-} \ 5d^{-} \ 5d^{-} \ F + 11.5 \ 4d^{-} \ 5d^{-} \ 5d^{-} \ F + 11.5 \ 4d^{-} \ 5d^{-} \ 5d^{-} \ F + 11.5 \ 4d^{-} \ 5d^{-} \ 5d^{-} \ F + 11.5 \ 4d^{-} \ 5d^{-} \ 5d^{-} \ F + 11.5 \ 4d^{-} \ 5d^{-} \ 5d^{-} \ F + 11.5 \ 4d^{-} \ 5d^{-} \ 5d^{-} \ F + 11.5 \ 4d^{-} \ 5d^{-} \ 5d^{-} \ F + 11.5 \ 4d^{-} \ 5d^{-} \ 5d^{-} \ F + 11.5 \ 4d^{-} \ 5d^{-} \ 5d^{-} \ F + 11.5 \ 4d^{-} \ 5d^{-} \ 5d^{-} \ 5d^{-} \ F + 11.5 \ 4d^{-} \ 5d^{-} \ 5d^{-} \ F + 11.5 \ 4d^{-} \ 5d^{-} \ 5d^{-} \ F + 11.5 \ 4d^{-} \ 5d^{-} \ 5$
359123.8	358823	300.8	4.5	$13.3 \text{ 4d}^{\circ} \text{ 5d} (^{\circ}\text{F}) \ ^{2}\text{G} + 37.6 \text{ 4d}^{\circ} \text{ 5d} (^{\circ}\text{F}) \ ^{4}\text{G} + 29.1 \text{ 4d}^{\circ} \text{ 5d} (^{\circ}\text{F}) \ ^{2}\text{H}$
358748	359102	-354	3.5	$30.24d^85d({}^{3}F){}^{4}H + 24.24d^85d({}^{3}F){}^{4}F + 13.94d^85d({}^{3}F){}^{2}F$
050501 5	000102	050 5	0.0	
359561.7	359285	276.7	0.5	$51.6 \ 4d^{\circ} \ 5d \ (^{\circ}F) \ ^{\circ}P \ + \ 17.5 \ 4d^{\circ} \ 5d \ (^{\circ}F) \ ^{\circ}P \ + \ 16.6 \ 4d^{\circ} \ 5d \ (^{\circ}F) \ ^{\circ}D$
359254.2	359451	-196.8	2.5	$63.7 4d^8 5d ({}^{3}\text{F}) {}^{4}\text{G} + 15.7 4d^8 5d ({}^{1}\text{D}) {}^{2}\text{F} + 7.8 4d^7 5s^2 ({}^{4}\text{F}) {}^{4}\text{F}$
360579.9	360090	489.9	3.5	$27.1 4d^8 5d(^3\text{F}) ^4\text{F} + 19.8 4d^8 5d(^3\text{F}) ^4\text{C} + 18.8 4d^8 5d(^3\text{F}) ^4\text{H}$
000010.0	000000	405.5	0.0	
360413.7	360346	67.7	0.5	$61.8 4d^{\circ} 5d (^{\circ}\text{F}) \ ^{\circ}\text{P} + 22.6 \ ^{\circ}\text{4}d^{\circ} \ ^{\circ}\text{5}d (^{\circ}\text{F}) \ ^{\circ}\text{P} + 11.8 \ ^{\circ}\text{4}d^{\circ} \ ^{\circ}\text{5}d (^{\circ}\text{D}) \ ^{\circ}\text{S}$
359377.3	360422	-1044.7	2.5	$32.3 \text{ 4d}^8 \text{ 5d} ({}^{3}\text{F}) {}^{4}\text{F} + 23.8 \text{ 4d}^7 \text{ 5s}^2 ({}^{4}\text{F}) {}^{4}\text{F} + 14.5 \text{ 4d}^8 \text{ 5d} ({}^{3}\text{F}) {}^{2}\text{D}$
250400 6	260760	1250.4	15	$28544752^{2}(4F)4F + 10244854(3F)2D + 16644854(1D)2D$
339409.0	300709	-1359.4	1.5	26.5 4 d $38 (1) 1 + 19.3 4 d$ $34 (1) D + 10.0 4 d$ $34 (D) D$
360937.3	360789	148.3	4.5	$36 \ 4d^{\circ} \ 5d \ (^{3}F)^{-2}H + 16.2 \ 4d^{\circ} \ 5d \ (^{3}F)^{-4}G + 15.4 \ 4d^{\circ} \ 5d \ (^{1}D)^{-2}G$
361097.4	360922	175.4	3.5	$54.5 \text{ 4d}^8 \text{ 5d} ({}^{3}\text{F}) {}^{2}\text{G} + 23.4 \text{ 4d}^8 \text{ 5d} ({}^{1}\text{D}) {}^{2}\text{F} + 7.2 \text{ 4d}^8 \text{ 5d} ({}^{3}\text{F}) {}^{4}\text{G}$
362171 7	363111	020.2	1 5	14.0 448 54 (3 2
302171.7	303111	-939.3	1.5	14.9 4 d 3 d (F) = D + 30.7 4 d 3 d (F) = F + 20.3 4 d 3 s (F) = 10.7 4 d 3 d (F) = 10.7 4
364260.1	363911	349.1	2.5	$34.1 \text{ 4d}^{\circ} \text{ 5d} (^{\circ}\text{F}) \ ^{2}\text{D} + 14.1 \text{ 4d}^{\circ} \text{ 5d} (^{\circ}\text{F}) \ ^{2}\text{F} + 10.8 \text{ 4d}^{\circ} \text{ 5d} (^{3}\text{F}) \ ^{4}\text{F}$
365556.5	366198	-641.5	0.5	$57.4 4d^8 5d (^{3}\text{P}) ^{4}\text{D} + 20.5 4d^8 5d (^{1}\text{D}) ^{2}\text{P} + 10.1 4d^8 5d (^{3}\text{P}) ^{4}\text{P}$
266225 0	266271	195 1	2 5	62 6 4 d8 5 d (3 p) 4 p + 12 7 4 d8 5 J (3 p) 2 c + 6 4 4 J8 5 J (1 p) 2 p
300233.9	300371	-130.1	3.5	0.0.4 u Ju (F) $D + 12.74$ u Ju (F) $G + 0.44$ u Ju (D) F
366978.4	366401	577.4	1.5	25.7 4d' 5s ² ("P) "P + 16.5 4d" 5d ("P) "D
368135-1	367155	980-1	1.5	$39 4d^8 5d ({}^{3}P) {}^{4}D + 18.8 4d^8 5d ({}^{3}P) {}^{2}D + 14.8 4d^8 5d ({}^{3}F) {}^{2}D$
267200.0	2001100	647.0	2.5	20×10^{10} cm (13×10^{10}) cm $(13 \times $
307398.2	308040	-047.8	5.5	38.740° $30(-F)$ $F + 30.240^{\circ}$ $30(-D)$ $G + 13.840^{\circ}$ $30(-F)$ F
368096.6	368509	-412.4	4.5	55.3 4d° 5d (°P) ${}^{4}F$ + 26.8 4d ⁸ 5d (${}^{1}D$) ${}^{2}G$ + 8.3 4d ⁸ 5d (${}^{3}F$) ${}^{2}H$
369302.5	368531	771 5	0.5	$32 4d^8 5d ({}^{3}\text{P}) {}^{4}\text{P} + 21 7 4d^8 5d ({}^{1}\text{D}) {}^{2}\text{S} + 21 1 4d^7 5s^2 ({}^{4}\text{P}) {}^{4}\text{P}$
260552.4	260605	010.4	1 5	2 = 0.417 = 2.40 + 40 + 0.20 + 0.48 = 1.430 + 20 + 10.0418 = 1.430 + 40.0418 = 1.4
309553.4	308035	918.4	1.5	33.6 4 a $3s$ (P) $P + 23.3 4 a$ $3d$ (P) $D + 10.6 4 d$ $5d$ (P) D
368011.6	368947	-935.4	2.5	$30.2 \text{ 4d}^{\circ} \text{ 5d} ({}^{3}\text{P}) {}^{2}\text{D} + 20.8 \text{ 4d}^{\circ} \text{ 5d} ({}^{3}\text{P}) {}^{4}\text{D} + 17.9 \text{ 4d}^{\circ} \text{ 5d} ({}^{1}\text{G}) {}^{2}\text{D}$
371725.9	372061	-335 1	0.5	$27.4 \text{ 4d}^8 \text{ 5d} ({}^{3}\text{P}) {}^{2}\text{P} + 19.2 \text{ 4d}^8 \text{ 5d} ({}^{3}\text{P}) {}^{4}\text{D} + 18.6 \text{ 4d}^7 \text{ 5s}^2 ({}^{4}\text{P}) {}^{4}\text{P}$
272251 7	272766	414.9	0.5	2326438 = 3(3D) 4E + 10.0 438 = 3(1D) 2E + 167 438 = 3(3D) 2D
312351.7	3/2/00	-414.3	2.5	$23.0 40^{\circ}$ $30 (^{\circ}P)^{\circ}F + 19.2 40^{\circ} 30 (^{\circ}D)^{\circ}F + 10.7 40^{\circ} 50 (^{\circ}P)^{\circ}D$
372497.9	372792	-294.1	1.5	$21.5 \text{ 4d}^{\circ} \text{ 5d} (^{3}\text{P}) ^{4}\text{P} + 23.1 \text{ 4d}^{\circ} \text{ 5d} (^{3}\text{P}) ^{4}\text{F} + 17.1 \text{ 4d}^{\circ} \text{ 5d} (^{3}\text{P}) ^{4}\text{D}$
373780.9	373258	522.9	2.5	$27.5 4d^8 5d (^{1}D) ^{2}D + 23.5 4d^8 5d (^{3}P) ^{4}F + 16.5 4d^8 5d (^{3}P) ^{4}D$
070100.0	010200	100.0	1.0	2,3,5,1,4,5,1,5,1
373670.2	373262	408.2	1.5	32.4 4d ad bd (P) F + 25.8 4d bd (P) F + 13.7 4d bd (P) 2D
373176.7	373447	-270.3	3.5	$24.3 \text{ 4d}^8 \text{ 5d} (^1\text{D}) {}^2\text{F} + 26.9 \text{ 4d}^8 \text{ 5d} (^3\text{P}) {}^4\text{F} + 22.3 \text{ 4d}^8 \text{ 5d} (^3\text{P}) {}^4\text{D}$
375218	374948	970	25	$32.7 4d^8 5d(^{1}D)^{2}E \pm 27.6 4d^8 5d(^{3}D)^{4}E \pm 13.5 4d^{8}Ed(^{3}D)^{2}E$
070410	074240	310	2.0	$32.1 \pm 0.0 \pm 0.0 \pm 1.0 \pm 0.0 \pm 0.0$
374804.6	374589	215.6	5.5	97.9 4d 5d (*G) *1
374412.7	374610	-197.3	1.5	$8.2 \text{ 4d}^8 \text{ 5d} (^{3}\text{P}) \ ^{2}\text{D} + 28.6 \text{ 4d}^8 \text{ 5d} (^{3}\text{P}) \ ^{4}\text{F} + 19.3 \text{ 4d}^8 \text{ 5d} (^{3}\text{P}) \ ^{2}\text{P}$
374263 1	374654	_300.0	35	$45.24d^8.5d(^{3}P)$ $^{4}F \pm 30.44d^8.5d(^{1}D)$ $^{2}F \pm 7.64d^8.5d(^{1}C)$ ^{2}F
314203.1	574034	-390.9	5.5	-10.2 -10 -10 -1 -10.4 -10 $-$
375734.5	375305	429.5	6.5	98.2 4d° 5d (1G) ² I
375831.9	375375	456.9	2.5	$49.7 \ 4d^8 \ 5d \ (^{3}P) \ ^{2}F + 13.1 \ 4d^8 \ 5d \ (^{3}P) \ ^{4}P + 11.4 \ 4d^8 \ 5d \ (^{3}P) \ ^{4}F$

Table A16: Comparison between available experimental data and calculated even energy levels (in $\rm cm^{-1}$) in In V

Table A16: Continued

375279.5	375724	-444.5	3.5	$37.9 \text{ 4d}^8 \text{ 5d} (^1\text{D}) \ ^2\text{G} + 42.3 \text{ 4d}^8 \text{ 5d} (^3\text{P}) \ ^2\text{F} + 8.6 \text{ 4d}^8 \text{ 5d} (^1\text{G}) \ ^2\text{G}$
376554.5	376060	494.5	1.5	$18.8 \text{ 4d}^8 \text{ 5d} (^1\text{G}) ^2\text{D} + 15.7 \text{ 4d}^8 \text{ 5d} (^3\text{P}) ^4\text{P} + 15.3 \text{ 4d}^8 \text{ 5d} (^3\text{P}) ^2\text{P}$
377152.5	377629	-476.5	3.5	83.8 4d ⁸ 5d (¹ G) 2 F + 6.1 4d ⁸ 5d (¹ D) 2 F
378144.6	377928	216.6	2.5	$82.3 \text{ 4d}^8 \text{ 5d} (^1\text{G}) ^2\text{F} + 7 \text{ 4d}^8 \text{ 5d} (^1\text{D}) ^2\text{F}$
377971.2	378218	-246.8	3.5	$62.9 4d^7 5s^2 (^2\text{G}) \ ^2\text{G} + 29.7 \ 4d^8 5d (^1\text{G}) \ ^2\text{G}$
377994.7	378354	-359.3	0.5	$35.5 \text{ 4d}^8 \text{ 5d} (^1\text{D}) ^2\text{S} + 34.2 \text{ 4d}^8 \text{ 5d} (^3\text{P}) ^2\text{P} + 10.4 \text{ 4d}^8 \text{ 5d} (^3\text{P}) ^4\text{P}$
379358.2	378999	359.2	4.5	98.9 $4d^8$ 6s (³ F) ⁴ F
380026.2	380383	-356.8	3.5	57.3 4d ⁸ 6s (³ F) ² F + 39.2 4d ⁸ 6s (³ F) ⁴ F
381614.9	381547	67.9	4.5	70.5 4d ⁸ 5d (¹ G) ² G + 11 4d ⁸ 5d (¹ G) ² H + 8.6 4d ⁸ 5d (¹ D) ² G
			a:	From Swapnil [34] and Ryabtsev [35]
				b: This work
			c:	Only the component $\geq 5\%$ are given

Table A17: Comparison between available experimental data and calculated odd energy levels (in $\rm cm^{-1})$ in In V

	E^{a}_{exp}	E^b_{calc}	ΔE	J	Leading components (in %) in LS coupling c
	235384.1	235446	-61.9	3.5	76.5 $4d^85p ({}^{3}F) {}^{4}D + 11.2 4d^85p ({}^{3}F) {}^{4}F$
	238629.2	238589	40.2	4.5	$35.9 \ 4d^85p \ ({}^3F) \ {}^2G + 41.1 \ 4d^85p \ ({}^3F) \ {}^4G + 21.4 \ 4d^85p \ ({}^3F) \ {}^4F$
	241510.9	241550	-39.1	2.5	$69.7 \ 4d^{\circ}5p \ (^{3}F) \ ^{4}D + 11.1 \ 4d^{\circ}5p \ (^{3}P) \ ^{4}D + 10.4 \ 4d^{\circ}5p \ (^{3}F) \ ^{4}F$
	243798.3	243766	32.3	3.5	$65.9 \ 4d^{\circ}5p \ (^{\circ}F) \ ^{\circ}G + 15 \ 4d^{\circ}5p \ (^{\circ}F) \ ^{\circ}F + 13.3 \ 4d^{\circ}5p \ (^{\circ}F) \ ^{\circ}G$
	244282.5 245121.7	244197	80.0	0.0 9.5	98.2 4d 5p (F) G + 1.5 4d 5p (G) H 55.7 4d ⁸ 5p (³ F) ^{4}C + 12.0 4d ⁸ 5p (¹ D) ^{2}F + 12.5 4d ⁸ 5p (³ F) ^{4}F
	245121.7	245150	-14.5	2.5	35.740 5p (F) G + 12.940 5p (D) F + 12.540 5p (F) F $34.4d^{8}5p$ (³ F) ⁴ D + 21.64d ⁸ 5p (³ F) ⁴ F + 12.74d ⁸ 5p (¹ D) ² D
	246721.8	246823	-101.2	1.5	$16.8 \ 4d^85p \ (^1D) \ ^2D + 36.9 \ 4d^85p \ (^3F) \ ^4D + 17.8 \ 4d^85p \ (^3P) \ ^4D$
	247254.7	247177	77.7	4.5	71.1 4d ⁸ 5p (³ F) ⁴ F + 25.4 4d ⁸ 5p (³ F) ² G
	248164.6	248173	-8.4	0.5	$63.5 \ 4d^85p \ (^3F) \ ^4D + 24.2 \ 4d^85p \ (^3P) \ ^4D + 7.6 \ 4d^85p \ (^1D) \ ^2P$
	248507.3	248555	-47.7	3.5	54.6 $4d^{8}5p({}^{3}F) {}^{2}F + 21.9 4d^{8}5p({}^{3}F) {}^{4}F + 10.2 4d^{8}5p({}^{3}F) {}^{4}D$
	249639.7	249672	-32.3	2.5	$36 \ 4d^85p \ ({}^{3}F) \ {}^{2}D + 24.1 \ 4d^85p \ ({}^{3}F) \ {}^{4}G + 16.3 \ 4d^85p \ ({}^{3}F) \ {}^{4}F$
	251868.1	251852	16.1	4.5	$56.6 \text{ 4d}^{\circ}\text{5p} (^{\circ}\text{F}) ^{4}\text{G} + 36.7 \text{ 4d}^{\circ}\text{5p} (^{\circ}\text{F}) ^{2}\text{G} + 6.3 \text{ 4d}^{\circ}\text{5p} (^{\circ}\text{F}) ^{4}\text{F}$
	252621.8	252542	79.8	1.5	$47.6 \ 4d^{\circ}5p \ (^{\circ}P) \ ^{\circ}P + 26.2 \ 4d^{\circ}5p \ (^{\circ}F) \ ^{\circ}F + 5.9 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}P$
	252090.0	252059	58.7	2.5	$35 4d^{3} \text{ p}(^{2} \text{ r}) = r + 21.7 4d^{3} \text{ p}(^{2} \text{ r}) = r + 14.2 4d^{3} \text{ p}(^{2} \text{ r}) = D$ $86 3 4d^{8} \text{ sp}(^{3} \text{ P}) = 4 \text{ P}$
	253871.2	253842	29.2	2.5	$46.6 4d^85p ({}^{3}P) {}^{4}P + 29.8 4d^85p ({}^{3}F) {}^{2}D + 6.1 4d^85p ({}^{3}P) {}^{4}D$
	253926.3	253959	-32.7	3.5	42.2 4d ⁸ 5p (³ F) ⁴ F + 25.7 4d ⁸ 5p (³ F) ² F + 24.8 4d ⁸ 5p (³ F) ² G
l	254804.6	254877	-72.4	3.5	$38.3 \ 4d^85p \ ({}^{3}F) \ {}^{2}G + 24.8 \ 4d^85p \ ({}^{1}D) \ {}^{2}F + 16.4 \ 4d^85p \ ({}^{3}F) \ {}^{4}G$
	257128.6	257306	-177.4	2.5	38.7 4d ⁸ 5p (³ F) ² F + 19.8 4d ⁸ 5p (¹ D) ² F + 17.3 4d ⁸ 5p (³ P) ² D
	257290.6	257336	-45.4	1.5	$42.6 \ 4d^{8}5p \ ({}^{3}F) \ {}^{4}F + 26.3 \ 4d^{8}5p \ ({}^{3}F) \ {}^{2}D + 14.1 \ 4d^{8}5p \ ({}^{3}P) \ {}^{4}P$
	258597.9	258502	95.9	2.5	21.7 4d ⁸ 5p (¹ D) ² F + 26.1 4d ⁸ 5p (³ P) ⁴ P + 13.6 4d ⁸ 5p (³ F) ⁴ G
	261208.1	261157	51.1	0.5	$35.1 \ 4d^{\circ}5p \ (^{\circ}P) \ ^{\circ}P + 38 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}P + 9 \ 4d^{\circ}5p \ (^{\circ}P) \ ^{\circ}P$
	261262.6	261226	36.6	3.5	$25.3 \ 4d^{\circ}5p \ (^{\circ}G) \ ^{\circ}F + 23 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}F + 20.9 \ 4d^{\circ}5p \ (^{\circ}P) \ ^{\circ}F$
	262089.3	261902	187.3	1.5	19.3 4d 5p (F) D + 30.5 4d 5p (F) P + 20.1 4d 5p (F) F 02.2 4d ⁸ 5p (¹ C) ² H + 5.8 4d ⁸ 5p (¹ C) ² C
	263009.8	262404	195.8	4.5 0.5	$62.3 4d^{8}5p (^{3}P) ^{4}D + 23.2 4d^{8}5p (^{3}F) ^{4}D + 5.2 4d^{8}5p (^{3}P) ^{2}P$
	262965.5	263145	-179.5	2.5	$18 4d^{8}5p (^{3}P) {}^{4}D + 24.8 4d^{8}5p (^{3}P) {}^{2}D + 22.5 4d^{8}5p (^{1}D) {}^{2}D$
	263558.6	263449	109.6	1.5	$33.8 \ 4d^{8}5p \ (^{3}P) \ ^{4}D + 22.6 \ 4d^{8}5p \ (^{3}F) \ ^{2}D + 12.4 \ 4d^{8}5p \ (^{1}D) \ ^{2}D$
l	264126.5	264038	88.5	3.5	$42.8 \ 4d^85p \ (^{3}P) \ ^{4}D + 46 \ 4d^85p \ (^{1}G) \ ^{2}F + 5.5 \ 4d^85p \ (^{3}F) \ ^{2}F$
	265905.4	265811	94.4	1.5	54 4d ⁸ 5p (¹ D) ² P + 17.7 4d ⁸ 5p (¹ D) ² D + 7.8 4d ⁸ 5p (³ P) ² D
	266067.6	265965	102.6	2.5	$30.4 \ 4d^85p \ (^1D) \ ^2D + 21.1 \ 4d^85p \ (^1G) \ ^2F + 18 \ 4d^85p \ (^3P) \ ^4D$
	268230.5	268146	84.5	1.5	$55.8 \text{ 4d}^{\circ}\text{5p} (^{\circ}\text{P}) ^{2}\text{P} + 19.9 \text{ 4d}^{\circ}\text{5p} (^{1}\text{D}) ^{2}\text{D} + 8.5 \text{ 4d}^{\circ}\text{5p} (^{\circ}\text{P}) ^{2}\text{D}$
	268861.1	268841	20.1	2.5	$43 4d^{\circ}5p (^{\circ}P) ^{2}D + 36.3 4d^{\circ}5p (^{\circ}P) ^{2}D + 11.3 4d^{\circ}5p (^{\circ}G) ^{2}F$
	208957	200920	37 181 0	0.0 1.5	98.140 5p (G) H 66.8 $4d^{8}$ 5p (³ P) ² D + 12.0 $4d^{8}$ 5p (³ P) ⁴ D + 5.3 $4d^{8}$ 5p (¹ D) ² P
	270201.1	270383 271154	-308.5	0.5	$70.7 4d^85p (^{3}P) ^{2}S + 16.2 4d^85p (^{3}P) ^{2}P + 5 4d^85p (^{3}P) ^{4}D$
	271234.4	271173	61.4	3.5	$49 \ 4d^85p \ (^1D) \ ^2F + 24.4 \ 4d^85p \ (^3P) \ ^4D + 11.1 \ 4d^85p \ (^1G) \ ^2F$
	272573.9	272602	-28.1	2.5	56.2 4d ⁸ 5p (¹ G) ² F + 12.1 4d ⁸ 5p (¹ D) ² F + 9.8 4d ⁸ 5p (¹ D) ² D
	272846.4	272655	191.4	1.5	86.3 $4d^{8}5p$ (³ P) ⁴ S
	275318.1	275486	-167.9	0.5	$39.9 \ 4d^85p \ (^1D) \ ^2P + 34.4 \ 4d^85p \ (^3P) \ ^2P + 18.6 \ 4d^85p \ (^3P) \ ^2S$
	276576.3	276605	-28.7	3.5	$87.7 \text{ 4d}^{\circ}5p(^{1}\text{G}) ^{2}\text{G} + 9.6 \text{ 4d}^{\circ}5p(^{1}\text{G}) ^{2}\text{F}$
	277481.7	277509	-27.3	4.5	$92.6 \ 4d^{\circ}5p \ (^{\circ}G) \ ^{\circ}G + 5.6 \ 4d^{\circ}5p \ (^{\circ}G) \ ^{\circ}H$
	298294.7	298294 305343	0.7	0.5	91.2 4d $^{\circ}$ p (S) P 03.2 4d 8 5p (¹ S) 2 P
	382835	382781	54	3.5	$49.8 \ 4d^84f \ (^{3}F) \ ^{4}D + 38.1 \ 4d^84f \ (^{3}F) \ ^{4}F + 6.3 \ 4d^84f \ (^{3}P) \ ^{4}F$
	385365	385403	-38	0.5	$24.9 \ 4d^84f \ (^3F) \ ^2S + 26.7 \ 4d^84f \ (^3F) \ ^4P + 25.4 \ 4d^84f \ (^3F) \ ^4D$
l	386795	386890	-95	3.5	22.1 4d ⁸ 4f (³ F) ⁴ F + 39.9 4d ⁸ 4f (³ F) ⁴ D + 11.5 4d ⁸ 4f (³ P) ⁴ F
	386943	386896	47	2.5	$34.1 \ 4d^84f \ ({}^3F) \ {}^4F + 31.2 \ 4d^84f \ ({}^3F) \ {}^4P + 14.1 \ 4d^84f \ ({}^3P) \ {}^4F$
	387648	387677	-29	1.5	$24.4 4d^{8}4f ({}^{3}\text{F}) {}^{4}\text{S} + 21.8 4d^{8}4f ({}^{3}\text{F}) {}^{4}\text{P} + 20.8 4d^{8}4f ({}^{3}\text{F}) {}^{4}\text{F}$
	390542	390635	-93	2.5	$39.6 \ 4d^84f \ (^{3}F) \ ^{4}P + 32.7 \ 4d^84f \ (^{3}F) \ ^{4}D + 7.9 \ 4d^84f \ (^{1}D) \ ^{2}F$
	390542	390723	-181	1.5	45.6 4d ⁴ 4f (³ F) ⁴ F + 16.9 4d ⁴ 4f (³ F) ⁴ F + 16.5 4d ³ 4f (³ F) ⁴ D 62.0 4d ⁸ 4f (³ F) ⁴ D + 15.7 4d ⁸ 4f (³ F) ² C + 10.4 4d ⁸ 4f (³ F) ² D
ļ	391882	303336	-21 52	0.0	$305 4d^84f(^3F)^4H \pm 241 4d^84f(^3F)^4C \pm 108 4d^84f(^3F)^2C$
ļ	393914	393592	322	2.5	$38 4d^84f ({}^{3}F) {}^{4}G + 26 4d^84f ({}^{1}D) {}^{2}F + 118 4d^84f ({}^{3}F) {}^{4}F$
	393573	393788	-215	1.5	$26 4d^84f (^3\text{F}) ^4\text{P} + 39.6 4d^84f (^3\text{F}) ^4\text{S} + 9.4 4d^84f (^3\text{F}) ^4\text{D}$
	394157	394331	-174	1.5	$37.7 \ 4d^{8}4f \ ({}^{3}F) \ {}^{2}P + 13.6 \ 4d^{8}4f \ ({}^{1}G) \ {}^{2}P + 12.5 \ 4d^{8}4f \ ({}^{3}F) \ {}^{4}D$
	394644	394375	269	3.5	$3.8 4d^84f \left({}^{1}\text{D}\right) {}^{2}\text{F} + 28 4d^84f \left({}^{3}\text{F}\right) {}^{4}\text{H} + 27 4d^84f \left({}^{3}\text{F}\right) {}^{2}\text{G}$
ļ	396177	396020	157	1.5	7.3 4d ⁸ 4f (¹ G) ² D + 26.7 4d ⁸ 4f (¹ D) ² D + 16.1 4d ⁸ 4f (³ F) ² D
	396509	396670	-161	2.5	2.9 4d ⁸ 4f (¹ D) ² F + 34.3 4d ⁸ 4f (³ F) ⁴ G + 21.3 4d ⁸ 4f (³ F) ² F
ļ	399348	399231	117	3.5	$35.3 \text{ 4d}^{\circ} 4f (^{\circ}P) = F + 20.4 \text{ 4d}^{\circ} 4f (^{\circ}F) = F + 14.8 \text{ 4d}^{\circ} 4f (^{\circ}F) = H$
ļ	399533 400952	399687 400622	-154	2.5	25.3 4 a^{-4t} ("F) $^{-}$ D + 13.4 4 a^{-4t} ("G) $^{-}$ D + 11.7 4 a^{-4t} ("D) $^{-2}$ F 51.7 4 a^{8} Af (3D) 4F \pm 15.7 4 a^{8} Af (3E) 4F \pm 6 4 a^{8} Af (3E) 2D
ļ	401318	401189	129	2.5 1.5	53.6
	401352	401403	-51	3.5	$58.5 4d^86p (^3F) ^4D + 9.9 4d^86p (^3F) ^4F + 6.1 4d^84f (^3F) ^2G$
ļ	401957	401559	398	3.5	19 4d ⁸ 4f (³ F) ² G + 20 4d ⁸ 6p (³ F) ⁴ D + 13.9 4d ⁸ 4f (³ F) ² F
ļ	403631	403746	-115	2.5	$20.5 4d^84f({}^{3}\text{F}) {}^{2}\text{F} + 27.5 4d^84f({}^{3}\text{P}) {}^{2}\text{F} + 16.7 4d^84f({}^{1}\text{G}) {}^{2}\text{D}$
ļ	404022	403894	128	3.5	24.7 4d ⁸ 4f (³ P) ² F + 23.5 4d ⁸ 4f (³ P) ⁴ F + 16.7 4d ⁸ 4f (¹ D) ² F
ļ	405584	404321	1263	2.5	$50.7 \text{ 4d}^{\circ}6p ({}^{3}\text{F}) {}^{2}\text{D} + 30.4 \text{ 4d}^{\circ}6p ({}^{3}\text{F}) {}^{4}\text{D}$
ļ	403778	404401	-623	1.5	$35.8 \text{ 4d}^{\circ}4f (^{\circ}\text{D}) ^{\circ}\text{P} + 38 \text{ 4d}^{\circ}4f (^{\circ}\text{P}) ^{4}\text{D} + 14 \text{ 4d}^{\circ}4f (^{\circ}\text{P}) ^{2}\text{D}$
ļ	405917	404931	986	3.5 2 =	$25.8 4 a^{-} op (^{-}F)^{-}F + 17.6 4 d^{-} op (^{-}F)^{-}F + 11.8 4 d^{-} op (^{-}F)^{-}D$ $42.7 4 d^{8} 4 f (^{1}D)^{-} 2 C + 12.4 d^{8} 4 f (^{3}D)^{-} 2 E + 10.4 d^{8} 4 f (^{3}D)^{-} 2 E$
ļ	407004	407340	∠04 119	3.3 25	42.7 + 40 + 41 (D) + 12.4 + 40 + 41 (P) + 10 + 40 + 41 (P) = F $44.9 + 4d^8 + 40 + 15.1 + 4d^8 + 40 + 10 + 4d^8 + 41 + 10 + 4d^8 $
	408470	408354	116	3.5	$53.8 \text{4} \text{d}^8 \text{4} \text{f} (^3\text{P}) \ ^4\text{G} + 11.8 \text{4} \text{d}^8 \text{6} \text{p} \ (^3\text{F}) \ ^4\text{G} + 7.7 \text{4} \text{d}^8 \text{4} \text{f} \ (^3\text{F}) \ ^4\text{G}$
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Table 1	TT1 •	Commutu	

I	E_{exp}^{a}	E_{calc}^{o}	ΔE	J	Leading components (in %) in LS coupling
	408756	408731	25	2.5	39.1 $4d^{8}4f$ (³ P) ⁴ G + 12.9 $4d^{8}4f$ (³ P) ⁴ D + 10.3 $4d^{8}4f$ (³ P) ² F
	409094	408909	185	1.5	$23.4 \text{ 4d}^84 \text{f} (^3\text{P}) \ ^4\text{D} + 14.7 \ 4\text{d}^84 \text{f} (^3\text{P}) \ ^2\text{D} + 14.7 \ 4\text{d}^84 \text{f} (^1\text{D}) \ ^2\text{D}$
	409016	409117	-101	3.5	52.9 $4d^{8}4f(^{3}P) {}^{4}D + 8.9 4d^{8}6p(^{3}F) {}^{4}G + 6.3 4d^{8}4f(^{3}P) {}^{2}G$
	409174	409379	-205	2.5	39.1 $4d^{8}6p$ (³ F) ⁴ D + 33.7 $4d^{8}6p$ (³ F) ² D + 11.3 $4d^{8}6p$ (³ F) ⁴ F
I	409843	410000	-157	3.5	$37 4d^{8}6p (^{3}\text{F}) \ ^{4}\text{G} + 21.1 \ 4d^{8}4f (^{3}\text{P}) \ ^{4}\text{G} + 13.7 \ 4d^{8}6p (^{3}\text{F}) \ ^{2}\text{F}$
	410603	410711	-108	2.5	$36 \ 4d^86p \ (^3F) \ ^4G + 19.4 \ 4d^86p \ (^3F) \ ^4F + 10.7 \ 4d^86p \ (^1D) \ ^2F$
	410331	410853	-522	1.5	59.2 $4d^{8}6p$ (³ F) ⁴ D + 17.8 $4d^{8}6p$ (³ F) ⁴ F + 9.4 $4d^{8}6p$ (¹ D) ² P
	410963	411107	-144	3.5	$65 4d^84f (^{3}P) \ ^{2}G + 12.1 \ 4d^84f (^{3}P) \ ^{4}D + 8.3 \ 4d^84f (^{1}G) \ ^{2}G$
	411211	411138	73	2.5	27.6 $4d^{8}4f(^{3}P)^{2}D + 19 4d^{8}4f(^{1}G)^{2}F + 12.4 4d^{8}4f(^{3}P)^{4}G$
	411257	411963	-706	1.5	$26.6 4d^{8}4f (^{1}\text{D}) \ ^{2}\text{D} + 26 4d^{8}4f (^{3}\text{P}) \ ^{4}\text{D} + 22.7 4d^{8}4f (^{1}\text{G}) \ ^{2}\text{D}$
	411182	412001	-819	3.5	49.7 4d ⁸ 6p (³ F) ⁴ F + 24.1 4d ⁸ 6p (³ F) ² G + 9.6 4d ⁸ 6p (³ F) ² F
	412353	412158	195	2.5	$33.9 4d^86p {\binom{3}{F}} {}^{4}F + 24 4d^86p {\binom{3}{F}} {}^{2}F + 10.8 4d^86p {\binom{1}{D}} {}^{2}F$
	412518	412271	247	2.5	41.5 $4d^{8}4f(^{1}D)^{2}D + 21.9 4d^{8}4f(^{3}P)^{4}D + 8 4d^{8}4f(^{3}P)^{2}D$
	412912	412608	304	0.5	$28.1 \ 4d^{8}4f \ (^{1}D) \ ^{2}P + 28.5 \ 4d^{8}6p \ (^{3}F) \ ^{4}D + 24.8 \ 4d^{8}4f \ (^{3}P) \ ^{4}D$
	413816	412999	817	2.5	$28.3 4d^{8}6p ({}^{3}\text{F}) {}^{2}\text{F} + 21.4 4d^{8}6p ({}^{1}\text{D}) {}^{2}\text{D} + 18.2 4d^{8}6p ({}^{3}\text{P}) {}^{4}\text{P}$
	413151	413044	107	3.5	$36.9 \ 4d^84f ({}^{1}G) \ {}^{2}F + 17.2 \ 4d^84f ({}^{1}D) \ {}^{2}F + 10.2 \ 4d^86p \ ({}^{3}F) \ {}^{2}G$
	413916	413330	586	3.5	19.7 4d ⁸ 6p (³ F) ² G + 21.7 4d ⁸ 6p (¹ D) ² F + 13 4d ⁸ 6p (³ F) ⁴ G
	412646	413528	-882	1.5	29.4 4d ⁸ 6p (³ F) 4 F + 29.5 4d ⁸ 6p (³ F) 2 D + 10.7 4d ⁸ 6p (¹ D) 2 P
	414465	414364	101	2.5	43.5 4d ⁸ 4f (¹ G) ${}^{2}F$ + 28.2 4d ⁸ 4f (³ P) ${}^{2}D$ + 10.8 4d ⁸ 4f (¹ D) ${}^{2}F$
	414310	414736	-426	1.5	42.9 4d°4f (³ P) ^{2}D + 32.7 4d°4f (¹ D) ^{2}P + 8.2 4d°4f (³ F) ^{2}D
	415880	416248	-368	1.5	$45.1 \ 4d^{\circ}6p \ (^{3}P) \ ^{4}P + 19.8 \ 4d^{\circ}6p \ (^{3}F) \ ^{2}D + 11.5 \ 4d^{\circ}6p \ (^{3}F) \ ^{4}F$
	417549	416899	650	2.5	20.3 4d°6p (³ P) ^{2}D + 21.3 4d°6p (³ P) ^{4}P + 17.9 4d°6p (³ F) ^{2}F
	417225	417140	85	3.5	$79.4 \ 4d^{\circ}4f \ (^{1}G) \ ^{2}G + 9.1 \ 4d^{\circ}4f \ (^{3}P) \ ^{2}G$
	417679	417608	71	0.5	$20.5 \ 4d^{\circ}6p \ (^{\circ}P) \ ^{2}P + 40.1 \ 4d^{\circ}6p \ (^{\circ}P) \ ^{4}P + 15 \ 4d^{\circ}6p \ (^{\circ}F) \ ^{4}D$
	417629	418384	-755	1.5	$48.4 \ 4d^{\circ}6p \ (^{\circ}P) \ ^{\circ}P + 13.6 \ 4d^{\circ}6p \ (^{\circ}F) \ ^{\circ}F + 8.7 \ 4d^{\circ}4f \ (^{\circ}G) \ ^{\circ}P$
	420075	419292	783	2.5	$59.6 \text{ 4d'} 5s5p ({}^{4}\text{F}) {}^{6}\text{F} + 22.5 \text{ 4d'} 5s5p ({}^{4}\text{F}) {}^{6}\text{D} + 9.1 \text{ 4d'} 5s5p ({}^{4}\text{F}) {}^{6}\text{G}$
	420008	420646	-638	0.5	51.8 4d ⁶ 6p (³ P) ^{4}P + 27.1 4d ⁶ 6p (³ P) ^{2}P + 9.9 4d ⁶ 6p (³ P) ^{2}S
	421670	421908	-238	1.5	$45.9 \ 4d^{\circ}6p \ (^{\circ}P) \ ^{\circ}D + 23.6 \ 4d^{\circ}6p \ (^{\circ}P) \ ^{\circ}D + 5.9 \ 4d^{\circ}6p \ (^{\circ}F) \ ^{\circ}D$
	422872	423004	-132	0.5	$81.4 \text{ 4d} 5s5p (^{+}F) \circ F + 6.2 \text{ 4d} 5s5p (^{+}F) \circ D$
	424036	423519	517	2.5	$18.9 \text{ 4d}^{\circ} \text{5s5p} (^{\circ}\text{F}) ^{\circ}\text{D} + 31.7 \text{ 4d}^{\circ} \text{5s5p} (^{\circ}\text{F}) ^{\circ}\text{G} + 17.8 \text{ 4d}^{\circ}\text{6p} (^{\circ}\text{P}) ^{\circ}\text{D}$
	423531	424095	-564	0.5	$48.3 44^{\circ}6p (^{\circ}P) ^{2}S + 17.5 44^{\circ}6p (^{\circ}P) ^{2}D + 9.5 44^{\circ}6p (^{\circ}P) ^{2}P$
	423896	424224	-328	1.5	$15.7 4d^{\circ}0p(^{\circ}P)^{-5} + 24.5 4d^{\circ}41(^{\circ}G)^{-7}P + 15.1 4d^{\circ}0p(^{\circ}P)^{-7}P$
	424800	424507	293	3.5	$9.0 4 d^{-4} d^{-4} f^{-1} F^{-1} = 30.8 4 d^{-4} d^{-4} f^{-1} F^{-1} = 18.5 4 d^{-4} d^{-4} f^{-1} G^{-1} F^{-1} = 418 c^{-4} G^{-1} G^{-1} G^{-1} = 418 c^{-4} G^{-1} G^{-1} G^{-1} G^{-1} = 418 c^{-4} G^{-1} G^{-1} G^{-1} G^{-1} = 418 c^{-4} G^{-1} G^{-1$
	425311	424891	420	1.5	40.4 4d $^{\circ}$ op ('P) D + 30.3 4d $^{\circ}$ op ('P) S + 7.3 4d $^{\circ}$ op ('P) D 27.0 47 E = (4E) 6D + 22.7 47 E = (4E) 6E + 20.2 47 E = (4D) 6D
	427028	420907	1071	1.0	27.940 $353p$ (F) $D + 22.740$ $353p$ (F) $F + 20.240$ $353p$ (F) $D25.4475-5-(4E)$ $6C + 29.14475-5-(4E)$ $6E + 14.74475-5-(4E)$ $6D$
	423949	420971	-22	2.0	3540 355p(F) G + 28.140 355p(F) F + 14.740 555p(F) D 20.04486p(1D) 2F + 14.24486p(1C) 2F + 104486p(3D) 2D
	420392	420420	215	2.5	30.9 40 op (12) F + 14.2 40 op (3) F + 10 40 op (1) D $40.5 4d^{8}4f (^{1}\text{C}) ^{2}\text{P} + 18.5 4d^{8}4f (^{3}\text{F}) ^{2}\text{P} + 13.3 4d^{8}6p (^{3}\text{P}) ^{2}\text{S}$
	427070	426855	210	1.5	40.5 44 4f(G) 1 + 10.5 44 4f(F) 1 + 10.5 44 0p(F) 5 $30.4 4d^{8}6p(^{1}D) ^{2}D + 12.7 4d^{8}6p(^{3}P) ^{2}P + 8.2 4d^{8}6p(^{3}F) ^{4}F$
	427133	420000	248	3.5	$23.6 \ 4d^75e^{5p} \ (^4F) \ ^4F \ + 20.7 \ 4d^75e^{5p} \ (^4F) \ ^4D \ + 11.5 \ 4d^75e^{5p} \ (^4F) \ ^4F$
	421121	421303	291	2.5	25.0 4d $350p$ (1) 1 + 20.1 4d $350p$ (1) D + 11.0 4d $350p$ (1) 1 47.3 4d ⁸ 6p (¹ D) ² D + 24.6 4d ⁸ 6p (¹ C) ² E + 7.5 4d ⁸ 6p (³ P) ⁴ P
	420240	420013	221	1.5	41.3 40 op (D) D + 24.0 40 op (G) P + 7.5 40 op (P) P $51.4 4d^86p (D) ^{2}P + 10.4 4d^86p (^{3}P) ^{4}S + 0.7 4d^86p (^{1}D) ^{2}D$
	429414	429170	-17	2.5	$11 1 4d^84f (^{3}P) ^{2}F \pm 27.6 4d^86p (^{1}D) ^{2}F \pm 12.6 4d^86p (^{1}G) ^{2}F$
	429575	429943	-368	3.5	$46.8 4d^{8}6p (^{1}D) ^{2}F + 25.6 4d^{8}6p (^{1}G) ^{2}F + 13.5 4d^{8}6p (^{3}P) ^{4}D$
	430484	430603	-119	0.5	$57.2 4d^86p (^1D) ^2P + 12.8 4d^86p (^3P) ^2S + 12.2 4d^86p (^3P) ^2P$
	430469	430661	-192	1.5	$23.3 4d^84f ({}^{3}\text{F}) {}^{2}\text{D} + 19.5 4d^84f ({}^{1}\text{G}) {}^{2}\text{D} + 11.1 4d^86n ({}^{1}\text{D}) {}^{2}\text{D}$
	431126	431081	45	2.5	$26.6 \ 4d^7 \ 5s5p \ (^4F) \ ^4F + 16.8 \ 4d^7 \ 5s5p \ (^4F) \ ^4D + 14.3 \ 4d^7 \ 5s5p \ (^4F) \ ^4F$
	432769	433336	-567	3.5	$30.6 \ 4d^{7}5s5p(^{4}F) \ ^{4}G + 18.9 \ 4d^{7}5s5p(^{4}F) \ ^{4}G + 14.4 \ 4d^{7}5s5p(^{4}F) \ ^{4}D$

a: From Swapni [34] and Ryabtsev [35]
b: This work
c: Only the component ≥ 5% are given

 Wavelength	Lower Level ^a	JLow	Upper level ^a	Jun	log gf	gA	CF	1
Å	cm^{-1}	• L0w	cm^{-1}	0 <i>0 p</i>	108 81	s ⁻¹	01	
204.985	0	2.5	487840	3.5	-0.73	2.92E + 10	0.213	
209.781	0	2.5	476687	3.5	-0.88	2.02E + 10	0.267	
210.637	0	2.5	474750	2.5	-0.92	1.83E + 10	0.116	
214.361	0	2.5	466502	1.5	-0.97	1.58E + 10	0.181	
223.995	0	2.5	446439	3.5	-0.77	2.26E + 10	0.196	
227.108	7172	1.5	447491	2.5	-0.43	4.81E + 10	0.32	
234.083	0	2.5	427199	1.5	-0.89	1.58E + 10	0.333	
234.410	0	2.5	420592	2.5	-0.54	$3.52E \pm 10$	0.321	
235.405	0	2.5	424800	1.5	0.33	$2.37E \pm 10$ 7 30E ± 10	0.309	
236.232	7172	1.5	430484	0.5	-0.9	1.52E+10	0.483	
236.241	7172	1.5	430469	1.5	0.18	1.82E + 11	0.475	
236.965	7172	1.5	429175	2.5	-0.11	9.23E + 10	0.308	
237.152	0	2.5	421670	1.5	-1	1.20E + 10	0.326	
238.08	7172	1.5	427199	1.5	-0.8	1.87E + 10	0.15	
238.153	7172	1.5	427070	0.5	-0.26	6.49E + 10	0.508	
238.424	7172	1.5	426592	2.5	-1	1.17E + 10	0.065	
337.028	185622	2.5	482333	3.5	-0.9	7.42E+09	0.339	
340.209	188396	4.5	482333	3.5	-0.23	3.41E + 10 1.00E + 10	0.011	
345.979	182194	1.5	471229	2.5	-0.70	$9.47E \pm 09$	0.212	
346 713	178289	1.5	466712	2.5	-0.79	9.04E+09	0.28	
349.586	171290	3.5	457343	3.5	-0.98	5.71E + 0.09	0.174	
350.132	185622	2.5	471229	2.5	-0.69	1.11E + 10	0.351	
357.561	177670	2.5	457343	3.5	-0.93	6.20E + 09	0.314	
367.187	160428	4.5	432769	3.5	-0.57	1.34E + 10	0.528	
367.842	188575	3.5	460431	3.5	-0.71	9.62E + 09	0.635	
368.025	185622	2.5	457343	3.5	-0.51	1.52E+10	0.414	
370.095	U 199900	2.5	270201	1.5	-0.82	7.37E+09	0.441	
372 814	198330	4.0	407343	3.0 1.5	-0.85	0.77E+09 1.89E±10	0.342	
372.931	7172	1.5	275318	0.5	-0.33	$2.24E \pm 10$	0.841	
375.844	0	2.5	266068	2.5	-0.77	8.03E + 09	0.478	
376.074	0	2.5	265905	1.5	-0.64	1.08E + 10	0.539	
376.787	7172	1.5	272574	2.5	-0.12	3.61E + 10	0.49	
378.606	0	2.5	264127	3.5	-0.1	3.71E + 10	0.715	
379.159	163980	3.5	427721	3.5	-0.52	1.40E + 10	0.219	
379.257	7172	1.5	270846	0.5	-1	4.68E + 09	0.669	
379.701	167761	2.5	431126	2.5	-0.73	8.57E + 09 7.42E + 00	0.158	
381 540	0	2.0	262900	2.5	-0.79	$7.43E \pm 10$ $2.21E \pm 10$	0.202	
382 133	7172	1.5	268861	2.5	-0.83	6.77E+09	0.333 0.437	
382.757	0	2.5	261263	3.5	-0.33	2.11E+10	0.711	
383.056	7172	1.5	268230	1.5	-0.23	2.69E + 10	0.697	
386.256	7172	1.5	266068	2.5	-0.97	4.79E + 09	0.242	
386.701	0	2.5	258598	2.5	-0.69	9.19E + 09	0.317	
388.91	0	2.5	257129	2.5	-0.29	2.27E + 10	0.625	
390.036	7172	1.5	263559	1.5	-0.52	1.33E + 10	0.362	
390.94	7172	1.5	262966	2.5	-0.64	9.93E + 09	0.53	
392.264	0	2.5	254805	3.5	-0.55	$7.53E \pm 09$	0.205 0.722	
393.901	0	2.5	253871	2.5	-0.3	2.15E+10	0.464	
395.741	õ	2.5	252691	2.5	-0.85	5.98E + 09	0.224	
399.81	7172	1.5	257291	1.5	-0.73	7.78E + 09	0.285	
400.069	7172	1.5	257129	2.5	-0.91	5.13E + 09	0.157	
400.577	0	2.5	249640	2.5	-0.35	1.84E + 10	0.324	
402.403	0	2.5	248507	3.5	-0.58	1.08E + 10	0.31	
694.567	235384	3.5	379359	4.5	0.15	1.92E + 10 1.56E + 10	0.802	
710 584	238620	4.5	370350	3.0 4.5	0.07	$1.50E \pm 10$ $1.04E \pm 10$	0.582	
719.514	349273	3.5	488256	3.5	-0.43	4.81E+09	0.442	
721.05	349569	2.5	488256	3.5	-1	1.28E + 09	0.154	
721.942	241511	2.5	380026	3.5	-0.35	5.68E + 09	0.67	
734.064	243798	3.5	380026	3.5	-0.47	4.25E + 09	0.657	
740.323	244283	5.5	379359	4.5	0.35	2.70E + 10	0.87	
753.173	247255	4.5	380026	3.5	-0.14	8.56E + 09	0.828	
760.98	247200 248507	4.0 3 5	380036	4.0 3 5	0.06	1.33E+10 1.28E±10	0.784	
766.95	249640	2.5	380020	3.5	-0.84	$1.28E \pm 10$ $1.66E \pm 09$	0.020 0.251	
785.326	252691	2.5	380026	3.5	-0.92	1.31E+09	0.149	
792.675	253871	2.5	380026	3.5	-0.45	3.76E + 09	0.647	
794.362	241511	2.5	367398	3.5	-0.82	1.64E + 09	0.188	
795.989	246722	1.5	372352	2.5	-0.91	1.31E + 09	0.059	
796.777	248165	0.5	373670	1.5	-0.94	1.19E + 09	0.142	
804.29	248165	0.5	372498	1.5	-0.93	1.22E + 09	0.174	
810.145	252691	2.0	274262	2.0	-0.7	$1.90E \pm 0.00$	0.209	
823 633	232091	2.5	368135	1.5	-0.89	$1.29E \pm 09$ 1.16E ± 09	0.128	
830.759	253298	0.5	373670	1.5	-0.62	2.31E+09	0.28	
836.215	241511	2.5	361097	3.5	-0.96	1.04E + 09	0.139	
838.477	257291	1.5	376555	1.5	-0.84	1.35E + 09	0.198	
838.929	253298	0.5	372498	1.5	-0.49	3.08E + 09	0.291	
841.505	246722	1.5	365557	0.5	-0.77	1.61E + 09	0.314	
842.417	245554	1.5	364260	2.5	-0.69	1.90E + 09	0.145	
845.682	235384	3.5 ⊿ ⊑	353632	4.5 2 F	-0.56	2.58E+09 1.17E+00	0.112	
847.441	300937 351579	4.0 25	479120 460574	3.3 3 K	-0.9 -0.8¤	1.175+09	0.447	
847.978	257291	1.5	375218	2.5	-0.6	$2.29E \pm 09$	0.28	
848.419	241511	2.5	359377	2.5	-0.47	3.21E+09	0.384	
849.196	249640	2.5	367398	3.5	-0.65	2.09E + 09	0.164	
851.148	264127	3.5	381615	4.5	-0.96	1.02E + 09	0.059	
852.54	366978	1.5	484275	1.5	-0.41	3.53E + 09	0.211	
852.97	241511	2.5	358748	3.5	-0.19	5.91E+09	0.383	
852.972	241011 258509	2.5	338748	1.5	-0.55	2.30E+09 9.07E-09	0.146	
004.000	±00000	4.0	010004	4.0	- 1	0.010+00	0.140	J

Table A18: Computed oscillator strengths and transition probabilities in In V.

Table A18: Continued

Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA	CF
853.81 854.337	257291 235384	$1.5 \\ 3.5$	374413 352434	$1.5 \\ 4.5$	-0.89 0.05	1.17E+09 1.02E+10	$0.245 \\ 0.603$
857.033	258598	2.5	375280	3.5	-0.42	3.48E + 09	0.189
857.04	252622	1.5	369303	0.5	-0.78	1.50E + 09	0.286
857.484	258598 249640	2.5 2.5	375218 366236	2.5	-0.88	1.19E+09 2.06E+09	$0.123 \\ 0.142$
858.815	241511	2.5	357951	3.5	-0.87	1.22E+09	0.142
860.677	235384	3.5	351572	3.5	-0.61	2.24E + 09	0.127
862.038	253298	0.5	369303	0.5	-0.64	2.02E+09	0.607
862.25	245122 261263	2.5	361097 377153	3.5	-0.68	1.87E+09 4 39E+09	0.173 0.243
863.91	248507	3.5	364260	2.5	-0.59	2.30E+09	0.188
864.565	258598	2.5	374263	3.5	-0.87	1.22E + 09	0.101
864.899	262351	4.5	377971	3.5	-0.63	2.11E+09	0.625
865.209	243798 252622	3.5 1.5	359377 368135	2.5	-0.91	1.11E+09 5.39E+09	0.278
866.115	245122	2.5	360580	3.5	-0.25	4.93E+09	0.159
866.132	243798	3.5	359254	2.5	-0.87	1.21E + 09	0.406
867.111	243798	3.5	359124	4.5	-0.93	1.03E+09 1.18E+00	0.032
870.628	245554	1.5	360414	0.5	-0.31	4.27E+09	0.799
870.801	253298	0.5	368135	1.5	-0.42	3.29E + 09	0.434
871.066	262351	4.5	377153	3.5	-0.99	9.14E+08	0.555
871.674	241511 369553	2.5	356233	1.5	-0.26	$4.86E \pm 09$ 2.08E \pm 09	0.617
871.782	252691	2.5	367398	3.5	-0.96	9.72E+08	0.190
874.458	252622	1.5	366978	1.5	-0.61	2.11E + 09	0.27
874.984	245122	2.5	359410	1.5	-0.74	1.63E + 09	0.379
875.167	253871 262966	2.5	368135 377153	1.5	-0.98	9.04E+08 1.62E+09	0.221
875.77	235384	3.5	349569	2.5	0.53	2.91E+10	0.853
876.024	243798	3.5	357951	3.5	0.23	1.46E + 10	0.826
876.175	245122	2.5	359254	2.5	0.18	1.31E + 10	0.721
877.138	248105	0.5	362172	1.5 3.5	-0.41	3.47E+09 2.29E+10	0.572
878.306	245554	1.5	359410	1.5	-0.18	5.81E + 09	0.48
878.39	264127	3.5	377971	3.5	-0.91	1.07E + 09	0.555
878.698	238629	4.5	352434	4.5	0.46	2.47E + 10	0.772
879.206	258598	2.5	357537	2.5 4.5	-0.74	$3.26E \pm 10$	0.130 0.746
879.506	245554	1.5	359254	2.5	-0.1	6.84E + 09	0.531
880.075	245122	2.5	358748	3.5	0.04	9.48E + 09	0.31
880.326	243798	3.5	357393	2.5	-0.93	1.01E+09 1.68E+00	0.159
880.848	253871	2.5	367398	3.5	-0.29	4.42E+09	0.48
882.056	245122	2.5	358493	1.5	-0.63	1.98E + 09	0.528
883.438	245554	1.5	358748	1.5	-0.34	3.83E + 09	0.329
883.947	262089 253871	1.5	375218	2.5	-0.15	5.98E+09 0.01E+08	0.419
884.752	264127	3.5	377153	3.5	-0.04	7.82E+09	0.401
884.952	261263	3.5	374263	3.5	-0.68	1.81E + 09	0.13
884.988	263559	1.5	376555	1.5	-0.81	1.30E + 09	0.194
885.406	238629 245554	4.5 1.5	351572 358493	3.5	-0.44 -0.34	3.18E+09 3.82E+09	0.377
885.468	252622	1.5	365557	0.5	-0.54	2.47E + 09	0.571
886.211	246722	1.5	359562	0.5	-0.73	1.58E + 09	0.217
886.299	245122	2.5	357951	3.5	0.28	1.62E + 10	0.475
887.662	246722	5.5 1.5	359377	$\frac{4.5}{2.5}$	-0.45	5.74E+09	0.572
888.633	246722	1.5	359254	2.5	-0.59	2.19E + 09	0.365
889.277	262351	4.5	374802	5.5	0.86	6.08E+10	0.914
889.601	238629	4.5 2.5	351039	5.5 2.5	0.81	5.50E + 10 1 45E + 10	0.848
889.959	253871	2.5	366236	3.5	0.11	1.10E + 10 1.10E + 10	0.457
890.286	262089	1.5	374413	1.5	-0.69	1.73E + 09	0.197
890.361	262966	2.5	375280	3.5	0.12	1.12E + 10	0.464
890.703	253298	2.5	365557	2.5	-0.62	1.99E+09 3.62E+09	0.205
890.847	262966	2.5	375218	2.5	-0.04	7.44E + 09	0.718
892.244	266068	2.5	378145	2.5	-0.6	2.11E + 09	0.23
892.279	248507 246722	3.5	360580 358748	3.5	-0.96	9.10E + 08 3.96E + 09	0.068
893.543	261263	3.5	373177	3.5	-0.52	2.52E+09	0.184
894.027	368012	2.5	479865	3.5	-0.87	1.10E + 09	0.097
894.146	245554	1.5	357393	2.5	-0.64	1.91E+09	0.191
895.75	252622	1.5 1.5	364260	2.5	-0.69	2.82E+09	0.240
896.211	262089	1.5	373670	1.5	-0.69	1.70E + 09	0.198
897.202	249640	2.5	361097	3.5	-0.77	1.40E + 09	0.124
897.49	246722	1.5 0 5	358144	2.5 1 5	-0.84	1.22E+09 1.40E-00	0.258
897.689	248165	0.5	359562	0.5	-0.24	4.73E+09	0.783
898.492	262966	2.5	374263	3.5	0.14	1.14E + 10	0.416
900	245122	2.5	356233	1.5	-0.52	2.47E + 09	0.64
900.384	245554 257129	1.5 2.5	368135	0.5 1.5	-0.31	$4.01E \pm 09$ $1.03E \pm 09$	0.478
901.387	249640	2.5	360580	3.5	0.2	1.30E + 10	0.799
901.852	257129	2.5	368012	2.5	-0.8	1.32E + 09	0.205
902.165	257291	1.5	368135	1.5	-1	8.13E+08	0.093
903.171	207291 377153	1.5 3.5	308012 487840	2.5 3.5	-0.57 -0.55	2.20E+09 2.24E+09	0.362
903.581	246722	1.5	357393	2.5	-0.56	2.20E + 0.09	0.321
903.666	263010	0.5	373670	1.5	-0.32	3.90E + 09	0.401
903.799	238629	4.5 2 F	349273	3.5 ⊿ ⊧	-0.2	5.19E+09	0.809
904.025	248507 261208	э.э 0.5	371726	4.0 0.5	-0.87	$4.67E \pm 0.09$	0.693
905.085	266068	2.5	376555	1.5	-0.49	2.62E + 09	0.352
905.726	262089	1.5	372498	1.5	-0.88	1.09E+09	0.132
905.888	253871 271234	2.5	364260	2.5 4 5	-0.19	5.22E+09 6.52E-00	0.376
906.383	248165	0.5	358493	4.5 1.5	-0.1	3.29E+09	0.772
906.868	257129	2.5	367398	3.5	0.29	1.60E + 10	0.725
906.872	356233	1.5	466502	1.5	-0.71	1.62E + 09	0.294
906.927	262089 241511	1.5 2.5	372352 351762	$\frac{2.5}{1.5}$	-0.25	4.64E+09 9.72E⊥00	0.227
907.258	263559	1.5	373781	2.5	-0.37	3.45E+09	0.21

Table A18: Continued

$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$0.567 \\ 0.494 \\ 0.433 \\ 0.485$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$0.434 \\ 0.433 \\ 0.485$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.485
909.952 246722 1.5 356618 0.5 -0.53 2.36E+09	
	0.41
910.468 243798 3.5 353632 4.5 -0.2 $5.11E+09$	0.455
911.265 249640 2.5 359377 2.5 -0.24 4.71E+09	0.2
911.679 257291 1.5 366978 1.5 -0.73 1.46E+09	0.331
912.827 252622 1.5 362172 1.5 -0.79 1.32E+09	0.184
913.15 246722 1.5 356233 1.5 -0.43 $2.95E+09$	0.508
913.341 263010 0.5 372498 1.5 -0.08 6.72E+09 012.4 252601 2.5 262172 1.5 0.77 1.20E+00	0.772
913.613 254805 3.5 364260 2.5 -0.97 $8.51E+08$	0.182 0.167
913.716 248507 3.5 357951 3.5 -0.54 $2.28E+09$	0.17
913.963 258598 2.5 368012 2.5 -0.66 1.77E+09	0.264
914.5 244283 5.5 353632 4.5 -0.65 $1.83E+09$	0.508
915.007 367398 3.5 476687 3.5 -0.95 $8.91E+08$	0.261
915.651 266068 2.5 375280 3.5 -0.04 7.30E+09	0.807
916.166 266068 2.5 375218 2.5 -0.9 9.83E+08	0.083
916.517 249640 2.5 358748 3.5 -0.09 6.43E+09	0.346
916.849 251868 4.5 360937 4.5 -0.67 $1.68E+09$	0.115
917.179 248507 3.5 357537 4.5 0.28 1.49 ± 10 918.617 351572 3.5 460431 3.5 -0.39 3.14 ± 09	0.91
919.115 258598 2.5 367398 3.5 0.17 $1.19E+10$	0.718
919.176 263559 1.5 372352 2.5 0.15 1.14E+10	0.694
920.171 368012 2.5 476687 3.5 -0.51 2.38E+09	0.303
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.188
921.597 205905 1.5 374413 1.5 -0.92 9.51E+08 921.625 249640 2.5 358144 2.5 -0.71 1.56E+09	0.183
922.452 252691 2.5 361097 3.5 -0.91 9.54E+08	0.063
922.676 258598 2.5 366978 1.5 -0.99 7.98E+08	0.277
922.864 358144 2.5 466502 1.5 -0.94 9.01E+08	0.243
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.639
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.288 0.037
923.648 244283 5.5 352549 5.5 0.34 $1.72E+10$	0.846
923.999 264127 3.5 372352 2.5 -1 7.90E+08	0.248
924.63 244283 5.5 352434 4.5 -0.63 1.82E+09	0.685
924.732 378145 2.5 486284 3.5 -0.19 $5.04E+09$	0.672
925.117 201208 0.5 309303 0.5 -0.92 9.24E+08 926.754 365557 0.5 473460 1.5 -0.43 2.89E+09	0.28
926.876 252691 2.5 360580 3.5 0.13 1.05 ± 10	0.464
926.994 265905 1.5 373781 2.5 0.13 1.04E+10	0.764
927.873 243798 3.5 351572 3.5 -0.24 4.58E+09	0.374
928.05 249640 2.5 357393 2.5 -0.49 2.45E+09	0.354
928.391 200008 2.5 373781 2.5 -0.55 2.10E+09 928.562 268861 2.5 376555 1.5 -0.91 9.43E+08	0.162 0.271
928.856 360414 0.5 468073 0.5 -0.73 $1.46E+09$	0.531
929.04 258598 2.5 366236 3.5 0.09 9.54E+09	0.498
929.281 351762 1.5 459372 1.5 -0.36 3.39E+09	0.421
929.356 268230 1.5 375832 2.5 -0.81 1.18E $+09$	0.172
930.117 372352 2.5 479805 3.5 -0.25 $4.51E+09$ 930.543 262089 1.5 369553 1.5 -0.99 7.78E+08	0.452 0.151
932.351 251868 4.5 359124 4.5 0.23 1.30 ± 10	0.671
932.608 253871 2.5 361097 3.5 -0.46 2.64E+09	0.37
933.088 253926 3.5 361097 3.5 -0.48 2.55E+09	0.227
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.173
933.578 375218 2.5 482333 3.5 -0.84 $1.12E+09$	0.323 0.273
933.628 266068 2.5 373177 3.5 0.4 1.94E+10	0.819
934.687 268230 1.5 375218 2.5 -0.09 6.11E+09	0.578
934.834 268861 2.5 375832 2.5 -0.35 3.36E $+09$	0.574
934.840 257291 1.5 304200 2.5 -0.50 $3.53E+09935.217$ 261208 0.5 368135 1.5 -0.87 $1.00E+09$	0.342 0.151
935.364 271234 3.5 378145 2.5 -0.93 $8.95\pm+08$	0.329
935.617 356618 0.5 463499 1.5 -0.44 2.78E+09	0.584
935.626 251868 4.5 358748 3.5 -0.74 1.39E+09	0.307
936032 308748 3.5 405025 3.5 -0.9 $9.40E+08936032$ 261263 3.5 368007 4.5 0.50 $2.06E+10$	0.122
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.926
936.709 244283 5.5 351039 5.5 -0.15 5.36E+09	0.876
936.72 252622 1.5 359377 2.5 -0.62 1.84E+09	0.427
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.223
936.884 271234 3.5 377971 3.5 -0.79 $1.31E+09$	0.687
937.31 373177 3.5 479865 3.5 -0.86 1.04E+09	0.204
937.369 366978 1.5 473660 2.5 -0.41 2.98E+09	0.333
937.004 358493 1.5 465148 2.5 -0.59 1.96E+09	0.182
937.802 25320 3.0 300000 3.0 -0.4 $3.00E+09937.802$ 252622 1.5 359254 2.5 -0.58 $2.03E+09$	0.213 0.229
937.955 368135 1.5 474750 2.5 -0.37 3.32 ± 09	0.403
938.147 249640 2.5 356233 1.5 -0.18 4.96E+09	0.599
938.152 265905 1.5 372498 1.5 -0.91 9.32E+08	0.135
938.971 353880 2.5 400431 3.5 -0.2 4.74E+09 938.957 375832 2.5 482333 3.5 0.41 2.00E+00	0.446 0.562
939.441 265905 1.5 372352 2.5 -0.56 2.12E+09	0.226
939.492 357951 3.5 464391 3.5 -0.63 1.81E+09	0.492
939.687 268861 2.5 375280 3.5 0.12 1.02E+10	0.648
940.051 247255 4.5 353632 4.5 0.35 1.70E+10	0.711
940.073 201000 4.0 306242 0.0 0.80 $0.40E+10940.108 359254 2.5 465625 3.5 -0.05 6.62E+00$	0.937
940.261 270201 1.5 376555 1.5 -0.85 $1.06E+09$	0.341
940.797 254805 3.5 361097 3.5 0.12 9.81E+09	0.582
941.197 359377 2.5 465625 3.5 -0.01 7.22E+09	0.759
942.210 254805 3.5 360937 4.5 0.75 4.24E+10 942.284 351762 1.5 457887 0.5 0.40 0.81E+00	0.927
942.663 251868 4.5 357951 3.5 -0.74 $1.37E\pm09$	0.719
942.882 252691 2.5 358748 3.5 -0.74 1.38 ± 09	0.079
942.885 252691 2.5 358748 1.5 -0.26 4.12E+09	0.534
944.088 262089 1.5 368012 2.5 -0.46 2.63E+09	0.234
944.120 271234 3.5 377153 3.5 -0.09 6.13E $+09944.342 359254 2.5 465148 2.5 0.91 4.69E\pm 0.0$	0.645
944.543 252622 1.5 358493 1.5 -0.93 $8.65E+08$	0.159
944.781 268957 5.5 374802 5.5 -0.79 $1.22E+09$	0.867
201	

Table A18: Continued

Wavelength	Lower Level	JLow	Upper level	J _{Un}	log gf	gA	CF
945.445	261208	0.5	366978	$1.5^{0.p}$	-0.66	1.61E + 09	0.374
945.52	358748	1.5	464510	0.5	-0.98	8.01E + 08	0.322
945.73	359410	1.5	465148	2.5	-0.24	4.14E + 09	0.614
945.993	270846	0.5	376555	1.5	-0.65	1.64E + 09	0.325
946.35	251868	4.5	357537	4.5	-0.44	2.71E + 09	0.279
946.413	258598	2.5	364260	2.5	-0.4	2.95E+09	0.214
946.536	368012	2.5	473660	2.5	-0.66	1.61E + 09	0.406
946.635	359562	0.5	465199	1.5	-0.84	1.10E + 09	0.567
946.693	270201	1.5	373832	2.5	0.32	1.53E + 10 1.08E + 00	0.799
940.900	374203 272574	3.0 2.5	4798000	0.0 9.5	-0.85	$1.08E \pm 09$ $1.14E \pm 10$	0.290
947.232	268230	2.5	373781	2.5	0.19	$1.14E \pm 10$ $1.38E \pm 00$	0.161
947.812	253871	2.5	359377	2.5	-0.9	9.50E + 08	0.172
947.994	353886	2.5	459372	1.5	-0.44	2.75E+09	0.36
948.289	252691	2.5	358144	2.5	0.09	9.08E + 09	0.617
948.308	253926	3.5	359377	2.5	-0.77	1.28E + 09	0.351
948.748	268861	2.5	374263	3.5	0.14	1.04E + 10	0.591
948.791	272574	2.5	377971	3.5	-0.45	2.62E + 09	0.501
948.958	248507	3.5	353886	2.5	-0.19	4.74E + 09	0.39
949.443	368135	1.5	473460	1.5	-0.67	1.60E + 09	0.322
949.72	247255	4.5	352549	5.5	0.7	3.71E + 10	0.888
950.03	252691	2.5	357951	3.5	-0.47	2.52E + 09	0.164
950.595	200920	3.0	474750	4.0	0.07	$2.72E \pm 10$ $0.08E \pm 08$	0.173
951.038	272846	1.5	377995	0.5	-0.92	8.79E±08	0.105
951.142	359254	2.5	464391	3.5	-0.49	2.44E+09	0.373
951.252	248507	3.5	353632	4.5	0	7.52E + 09	0.376
951.972	360580	3.5	465625	3.5	-0.75	1.31E + 09	0.149
952.031	276576	3.5	381615	4.5	0.19	1.13E + 10	0.803
952.623	261263	3.5	366236	3.5	-0.06	6.41E + 09	0.716
953.461	257291	1.5	362172	1.5	-0.24	4.28E + 09	0.456
953.997	253926	3.5	358748	3.5	0	7.40E + 09	0.539
954.465	252622	1.5	357393	2.5	-0.73	1.35E+09	0.268
954.646	358748	1.5	463499	1.5	-0.76	1.29E+09	0.264
955.092	252691	2.5	357393	2.5	-0.23	4.22E+09	0.363
950.218	272574	2.5	377133	3.0	-0.92	8.84E+08	0.241
950.238	203559	1.5	308135	1.5	-0.48	2.38E+09	0.241
957 369	263559	1.5	368012	2.5	-0.97	$3.01E \pm 09$	0.28
957 555	262966	2.5	367398	3.5	-0.43	2.70E+09	0.123
958.448	372352	2.5	476687	3.5	-0.27	3.87E+09	0.353
958.596	254805	3.5	359124	4.5	-0.76	1.24E + 09	0.04
958.629	268861	2.5	373177	3.5	0.09	8.99E + 09	0.477
959.533	253926	3.5	358144	2.5	-0.19	4.68E + 09	0.744
960.084	369303	0.5	473460	1.5	-0.71	1.44E + 09	0.432
960.309	277482	4.5	381615	4.5	0.42	1.90E + 10	0.616
960.419	268230	1.5	372352	2.5	-0.71	1.43E + 09	0.088
960.554	369553	1.5	473660	2.5	-0.45	2.60E + 09	0.427
960.713	359410	1.5	463499	1.5	-0.65	1.58E + 09	0.371
961.315	253926	3.5	357951	3.5	-0.71	1.41E+09	0.163
961.371	3/3/81	2.5	276555	3.5	-0.91	$9.05E \pm 0.00$	0.527
901.718	264127	2.5	368007	1.5	0.81	$1.11E \pm 0.9$ $1.32E \pm 10$	0.181
961.827	257129	2.5	361097	3.5	0.20	$1.32E \pm 10$ $1.26E \pm 10$	0.664
962.058	254805	3.5	358748	3.5	-0.43	2.71E+09	0.265
962.218	248507	3.5	352434	4.5	0	7.13E + 09	0.244
962.392	375218	2.5	479126	3.5	-0.98	7.75E + 08	0.285
962.602	264127	3.5	368012	2.5	-0.31	3.62E + 09	0.657
963.535	247255	4.5	351039	5.5	-0.32	3.46E + 09	0.154
964.245	272846	1.5	376555	1.5	-0.7	1.42E + 09	0.283
964.804	265905	1.5	369553	1.5	-0.73	1.33E + 09	0.247
965.149	253926	3.5	357537	4.5	-0.59	1.83E+09	0.121
965.439	270201	1.5	373781	2.5	-0.27	3.83E+09	0.383
966 271	268861	2.5	379359	2.5	-0.09	$1.86E \pm 0.0$	0.873
966 472	270201	1.5	373670	1.5	-0.45	2.51E+09	0.525
967.145	265905	1.5	369303	0.5	-0.82	1.06E+09	0.286
968.11	375832	2.5	479126	3.5	-0.7	1.44E + 09	0.488
968.114	361097	3.5	464391	3.5	-0.85	1.02E + 09	0.36
968.332	262966	2.5	366236	3.5	-0.44	2.59E + 09	0.315
969.563	356233	1.5	459372	1.5	-0.83	1.06E + 09	0.237
969.715	257291	1.5	360414	0.5	-0.57	1.89E + 09	0.563
970.267	248507	3.5	351572	3.5	0.27	1.34E + 10	0.524
970.003	211234	3.3 1 F	375020	3.5 ೧೯	0.22	4.29E+09	0.3/3
971.01	262179	1.5	465148	2.5	-0.51	2.10E+09	0.391
971.76	373781	2.5	476687	3.5	-0.65	$1.61E \pm 0.9$	0,205
973.657	272574	2.5	375280	3.5	-0.18	4.73E + 09	0.335
973.932	275318	0.5	377995	0.5	-0.16	4.92E + 09	0.868
975.615	258598	2.5	361097	3.5	-0.46	2.43E + 09	0.206
976.929	253871	2.5	356233	1.5	-0.51	2.17E + 09	0.379
977.699	257129	2.5	359410	1.5	-0.9	9.08E + 08	0.21
978.073	364260	2.5	466502	1.5	-0.98	7.43E+08	0.156
978.189	265905	1.5	308135	1.5	-0.89	8.79E+08	0.223
979.22	∠4904U 257201	2.0 1 F	351/02	1.0	-0.07	1.485+09	0.22
979.20	264127	3.5	366236	1.0 3.5	-0.70	$4.17E \pm 09$	0.171
980.213	247255	4.5	349273	3.5	0.07	8.12E+09	0.78
980.412	263559	1.5	365557	0.5	-0.95	7.87E + 08	0.203
980.566	258598	2.5	360580	3.5	-0.9	8.64E + 08	0.06
980.742	257291	1.5	359254	2.5	-0.59	1.78E + 09	0.168
980.947	271234	3.5	373177	3.5	-0.61	1.73E + 09	0.155
981.046	249640	2.5	351572	3.5	-0.79	1.13E + 09	0.122
981.944	272574	2.5	374413	1.5	-0.49	2.24E + 09	0.516
983.389	272574	2.5	374263	3.5	-0.77	1.18E+09	0.159
983.452	358748	3.5	460431	3.5	-0.85	9.65E+08	0.133
984.559	276576	3.5	3/8145	2.5	0 14	0.78E+09	0.612
930.243 986 001	260170 360170	3.0 1 K	463400	ა.ე 1 ≍	-0.14	1 10E- 00	0.039
987 22	262966	2.5	364260	2.5	-0.70	$1.08E \pm 09$	0.169
989,156	272574	2.5	373670	1.5	-0.93	7.93E + 08	0.385
989.384	265905	1.5	366978	1.5	-0.66	1.47E + 0.09	0.269
989.951	257129	2.5	358144	2.5	-0.71	1.33E + 0.09	0.128
991.273	270846	0.5	371726	0.5	-0.98	7.10E + 08	0.176
991.541	257291	1.5	358144	2.5	-0.52	2.07E + 09	0.398

Table A18: Continued

Wavelength	Lower Level	JLow	Upper level	J_{Up}	log gf	gA	CF
991.829	272846	1.5	373670	1.5	-0.61	1.65E + 09	0.307
991.848	257129	2.5	357951	3.5	-0.98	7.00E + 08	0.117
991.949	258598	2.5	359410	1.5	-0.92	8.39E+08	0.205
992.399	248507	2.5	349273	3.5	-0.73	$1.28E \pm 0.09$ 7 10E \pm 0.08	0.131
994.271	276576	3.5	377153	3.5	-0.3	3.38E+09	$0.124 \\ 0.652$
998.666	264127	3.5	364260	2.5	-0.97	7.21E + 08	0.166
999.851	253871	2.5	353886	2.5	-0.91	8.23E + 08	0.128
1000.102	373670	1.5	473660	2.5	-0.92	8.13E + 08	0.136
1000.76	272574	2.5	372498	1.5	-0.95	7.45E + 08	0.229
1001.491	360380	3.0	460431	3.5	-0.9	$8.27E \pm 08$	0.123
1002.194	253926	3.5	353632	4.5	-0.56	1.46E+09	0.202
1003.303	277482	4.5	377153	3.5	0.18	1.01E+10	0.86
1003.497	272846	1.5	372498	1.5	-0.64	1.52E + 09	0.315
1006.775	257291	1.5	356618	0.5	-0.72	1.26E + 09	0.447
1008.568	268861	2.5	368012	2.5	-0.38	2.81E + 09	0.522
1009.137	275318	0.5	374413	1.5	-0.67	1.40E+09	0.235
1009.375	252691	2.5	351762	1.5	-0.68	1.36E + 09 1.18E + 00	0.137
1013.138	276576	3.5	375218	2.5	-0.74	$1.18E \pm 0.09$ $1.19E \pm 0.09$	0.38 0.647
1015.829	375218	2.5	473660	2.5	-0.98	7.01E + 08	0.18
1016.728	265905	1.5	364260	2.5	-0.92	7.80E + 08	0.24
1017.041	262089	1.5	360414	0.5	-0.66	1.43E + 09	0.5
1021.548	253871	2.5	351762	1.5	-0.28	3.33E + 09	0.541
1023.536	253871	2.5	351572	3.5	-0.49	2.10E + 09	0.412
1024.616	377153	3.5	474750	2.5	-0.68	1.32E + 09 1.74E + 00	0.636
1027.539	277482	4.5	374802	0.0 3.5	-0.56	$1.74E \pm 09$ 8.78E \pm 08	0.498 0.665
1035.712	263010	0.5	359562	0.5	-0.7	1.24E+09	0.637
1036.741	272846	1.5	369303	0.5	-0.93	7.16E + 08	0.236
1043.866	167761	2.5	263559	1.5	-0.91	7.47E + 08	0.306
1050.679	177670	2.5	272846	1.5	-0.85	8.40E + 08	0.305
1057.556	178289	1.5	272846	1.5	-0.78	9.86E + 08	0.278
1066.332	169230	1.5	263010	0.5	-0.8	9.36E+08	0.596
1073.377	208098	2.5	351762	1.5	-0.87	7.80E+08	0.238
1074.380	203009 173371	1.0	265905	1.5	-0.9	1.20E+08 6.72E⊥08	0.319
1082.795	180493	0.5	272846	1.5	-0.6	1.41E+0.9	0.603
1096.596	177670	2.5	268861	2.5	-0.84	7.99E + 08	0.635
1101.861	173371	2.5	264127	3.5	-0.53	1.63E + 09	0.413
1103.115	182194	1.5	272846	1.5	-0.58	1.45E + 09	0.497
1111.771	163980	3.5	253926	3.5	-0.88	7.12E + 08	0.071
1112.453	163980	3.5	253871	2.5	-0.6	1.35E+09	0.593
1110.947	167761	2.5	257291	1.5	-0.98	$5.56E \pm 10$	0.337
1122.518	188575	4.5	277482	4.5	-0.38	$2.19E \pm 0.09$	0.039
1135.586	169230	1.5	257291	1.5	-0.56	1.43E+09	0.429
1136.348	188575	3.5	276576	3.5	0.31	1.05E + 10	0.746
1137.679	169230	1.5	257129	2.5	-0.74	9.38E + 08	0.664
1137.765	173371	2.5	261263	3.5	-0.54	1.48E + 09	0.159
1137.807	163980	3.5	251868	4.5	-0.19	3.30E + 09	0.209
1141.336	178289	1.5	265905	1.5	-0.52	1.55E+09 5.43E+08	0.451 0.271
1145.574	185622	2.5	272846	1.5	-0.98	$5.43E \pm 08$ 6.88E \pm 08	0.271
1148.848	167761	2.5	254805	3.5	-0.24	2.92E+09	0.358 0.462
1150.063	185622	2.5	272574	2.5	-0.76	8.80E + 08	0.307
1151.723	160428	4.5	247255	4.5	0.22	8.23E + 09	0.678
1153.815	188649	1.5	275318	0.5	-0.32	2.41E + 09	0.779
1153.841	182194	1.5	268861	2.5	-0.34	2.30E + 09	0.478
1156.648	177670	2.5	264127	3.5	-0.24	2.86E + 09	0.776
1168.057	185622	2.5	200920	3.5	-0.52	1.52E+09 8.23E+09	0.54
1170.787	180493	0.5	265905	1.5	-0.95	5.47E + 08	0.711
1172.748	178289	1.5	263559	1.5	-0.54	1.38E + 09	0.367
1177.443	167761	2.5	252691	2.5	-0.11	3.76E + 09	0.621
1180.962	178289	1.5	262966	2.5	-0.71	9.31E + 08	0.195
1181.326	220694	0.5 9 F	305344	1.5 9 F	0.02	5.00E+09	0.51
1100.403	103960	3.5	248507	2.5	-0.01	4.71E+09 4.67E+09	0.51
1191.543	188649	1.5	272574	2.5	-0.51	$1.45E \pm 0.09$	0.715
1191.616	173371	2.5	257291	1.5	-1	4.75E + 0.08	0.157
1192.27	182194	1.5	266068	2.5	-0.18	3.08E + 09	0.756
1192.545	160428	4.5	244283	5.5	0.52	1.54E + 10	0.89
1193.921	173371	2.5	257129	2.5	-0.5	1.48E+09	0.28
1194.081	182194	1.0	⊿03905 261263	1.0 3.5	-0.08 -0.00	9.01E+08 3.74E⊥00	0.3
1199 163	169230	2.0 1.5	252622	5.5 1.5	-0.09	$1.54E \pm 09$	0.643
1200.842	163980	3.5	247255	4.5	-0.1	3.72E + 0.09	0.854
1203.864	180493	0.5	263559	1.5	-0.5	1.44E + 09	0.667
1207.174	188396	4.5	271234	3.5	-0.55	1.30E + 09	0.668
1210.117	171290	3.5	253926	3.5	0.08	5.52E + 09	0.731
1210.531	185622	2.5	268230	1.5	-0.92	5.41E + 08	0.410
1210.925	1/1290	3.5 0 F	253871	2.5	-0.54	1.32E+09	0.419
1216 457	188640	0.5	270846	0.5	-0.34	$1.61E \pm 09$	0.783
1221.316	167761	2.5	249640	2.5	-0.93	5.25E + 08	0.153
1226.068	188640	0.5	270201	1.5	-0.14	3.21E + 09	0.821
1227.994	173371	2.5	254805	3.5	0	4.43E + 09	0.629
1228.487	171290	3.5	252691	2.5	-0.49	1.42E + 09	0.39
1235.664	177670	2.5	258598	2.5	-0.35	1.94E+09 1.67E+00	0.574
1200.444	171900	2.0 3.5	240007 251868	3.3 4 5	-0.42	1.07日十09 8.81日上00	0.723
1241.3	188396	4.5	268957	-1.5 5.5	0.51	1.39E+10	0.895
1241.382	173371	2.5	253926	3.5	-0.56	1.19E + 09	0.49
1242.233	173371	2.5	253871	2.5	-0.21	2.65E + 09	0.725
1243.077	185622	2.5	266068	2.5	-0.47	1.45E+09	0.293
1243.636	169230	1.5	249640	2.5	-0.24	2.51E+09	0.742
1245.188	178289	1.5	258598	2.5	-0.19	2.77E+09	0.725
1240.048	185622	5.0 2.5	200001 265905	2.0 1.5	-0.74	1.190+08 9.400-08	0.701
1246.697	188649	1.5	268861	2.5	-0.22	$2.58E \pm 0.9$	0.803
1251.639	182194	1.5	262089	1.5	-0.49	1.36E + 09	0.427
1252.841	163980	3.5	243798	3.5	-0.05	3.82E + 09	0.797
1255.953	177670	2.5	257291	1.5	-0.48	1.39E + 09	0.622
1256.576	188649	1.5	268230	1.5	-0.09	3.44E + 09	0.73

Table A18: Continued

Wavelength	Lower Level	JLow	Upper level	J _{Up}	log gf	gA	CF
1258.514 1260.722	$177670 \\ 173371$	$2.5 \\ 2.5$	257129 252691	$2.5 \\ 2.5$	-0.42 -0.7	1.61E+09 8.38E+08	$0.43 \\ 0.359$
1261.815	173371	2.5	252622	1.5	-0.91	5.15E + 08	0.196
1265.597	182194 167761	1.5	261208 246722	0.5	-0.49	1.34E+09 7.92E+08	0.678
1266.878	169230	2.5	248165	0.5	-0.72	1.55E+0.09	0.301
1268.395	178289	1.5	257129	2.5	-0.32	2.02E + 09	0.693
1276.323	171290 160428	3.5 4.5	249640 238629	2.5 4.5	-0.3	2.03E+09 4 03E+09	0.656
1283.096	185622	2.5	263559	1.5	-0.73	7.47E+08	0.349
1285.46	167761	2.5	245554	1.5	-0.22	2.43E+09	0.669
1288.642	220694 163980	$0.5 \\ 3.5$	298295 241511	$\frac{0.5}{2.5}$	-0.32	1.91E+09 4.56E+09	0.843
1290.447	188575	3.5	266068	2.5	-0.49	1.29E+09	0.783
1290.465	169230	1.5	246722	1.5	-0.54	1.18E+09	0.724
1291.68	188649 167761	1.5 2.5	266068 245122	2.5 2.5	-0.28	3.98E+08 2.12E+09	0.734 0.621
1292.935	185622	2.5	262966	2.5	-0.13	2.95E + 09	0.722
1295.041	171290	3.5	248507	3.5	-0.34	1.80E+09	0.216
1296.432 1307.751	185622	2.5 2.5	254805 262089	$\frac{3.5}{1.5}$	-0.34 -0.72	1.80E+09 7.46E+08	0.398
1312.312	177670	2.5	253871	2.5	-0.56	1.06E + 09	0.398
1315.141	167761 171200	2.5	243798 247255	3.5	-0.08	3.21E+09 9.56E+08	0.413
1317.673	169230	1.5	245122	2.5	-0.21	2.39E+09	0.412
1320.477	188396	4.5	264127	3.5	-0.03	3.60E + 09	0.796
1322.043	185622	2.5 2.5	$261263 \\ 248507$	3.5	-0.49 -0.87	1.23E+09 5.12E+08	0.217
1331.618	182194	1.5	257291	1.5	-0.78	6.25E+08	0.458
1333.164	178289	1.5	253298	0.5	-0.48	1.25E+09	0.758
1334.118	160428	4.5 2.5	235384 252622	$\frac{3.5}{1.5}$	-0.49	6.73E+09 1.22E+09	0.867
1334.498	182194	1.5	257129	2.5	-0.97	4.02E + 08	0.141
1339.594	163980	3.5	238629	4.5	0.07	4.35E+09	0.484
1345.598 1352.185	188649	1.5 4.5	262966 262351	2.5 4.5	-0.38	1.24E+09 1.24E+09	0.524 0.799
1354.425	171290	3.5	245122	2.5	-0.75	6.52E + 08	0.817
1355.462	188575	3.5	262351	4.5	0.32	7.66E + 09	0.771
1363.311	173371	2.5	202089 246722	1.5	-0.45	1.28E+09	0.804
1365.592	351572	3.5	424800	3.5	-0.55	9.68E + 08	0.363
1372.376	188396	4.5	261263 243708	3.5	-0.24	2.05E+09 4.08E+08	0.835
1379.140	358144	2.5	430469	1.5	-0.93	4.03E+0.08 4.17E+0.08	0.153
1385.367	173371	2.5	245554	1.5	-0.8	5.50E + 08	0.343
1386.403	180493	0.5	252622 249640	1.5	-0.84 -0.78	$5.06E \pm 08$ $5.69E \pm 08$	0.429
1393.713	173371	2.5	245122	2.5	-0.98	3.58E + 08	0.288
1395.144	182194	1.5	253871	2.5	-0.95	3.83E+08	0.166
1406.385	182194 358144	$1.5 \\ 2.5$	253298 429175	$0.5 \\ 2.5$	-1 -0.91	3.42E+08 4.14E+08	0.264
1424.07	171290	3.5	241511	2.5	-0.96	3.61E + 08	0.319
1427.444	360414	0.5	430469	1.5	-0.61	8.14E+08	0.423
1467.567	173371	2.5	240722 241511	2.5	-0.84	4.32E+08 4.32E+08	0.230
1477.72	180493	0.5	248165	0.5	-0.97	3.31E + 08	0.841
1477.908	356233 171200	1.5	423896	1.5	-0.85 0.56	4.38E+08 8.36E+08	0.41
1495.898	357951	3.5	424800	3.5	-0.86	4.07E+08	0.365
1513.968	358748	3.5	424800	3.5	-0.9	3.57E + 08	0.336
1569.795 1720.658	361097 372352	$\frac{3.5}{2.5}$	$424800 \\ 430469$	$\frac{3.5}{1.5}$	-0.84 -0.97	3.87E+08 2 42E+08	0.293
1738.629	369553	1.5	427070	0.5	-0.98	2.37E+0.00	0.441
1759.841	372352	2.5	429175	2.5	-0.82	3.24E+08	0.133
1765.421	349273 374413	3.5 1.5	405917 430484	3.5 0.5	-0.84 -0.85	2.96E+08 2.96E+08	0.203
1783.921	374413	1.5	430469	1.5	-0.89	2.68E + 08	0.169
1784.685	351572	3.5	407604	3.5	-0.97	2.14E+08	0.139
1796.225	358012 358144	2.5 2.5	423896 413816	$^{1.5}_{2.5}$	-0.33	$9.61E \pm 0.08$ $4.76E \pm 0.08$	0.464 0.302
1807.929	374263	3.5	429575	3.5	-0.77	3.43E + 08	0.21
1808.714	353886	2.5	409174	2.5	-0.68	4.29E + 08	0.146
1809.929	358748	3.5	413916	3.5	-0.43	5.70E+08	0.333
1815.95	358748	3.5	413816	2.5	-0.96	2.11E+08	0.167
1816.092	373177 357393	$\frac{3.5}{2.5}$	428240 412353	2.5 2.5	-0.51 -0.57	6.16E+08 5.53E+08	0.272
1823.244	372352	2.5	427199	1.5	-0.7	3.86E + 08	0.213
1836.24	373781	2.5	428240	2.5	-0.89	2.58E+08	0.166
1838.019	359410 351572	1.5 3.5	413816 405917	2.5 3.5	-0.98	1.90E+08 1.74E+09	0.254
1844.702	358144	2.5	412353	2.5	-0.64	4.42E + 08	0.262
1850.92	359124	4.5	413151	3.5	-0.82	2.99E+08	0.258
1852.644	351572 374263	3.5 3.5	405584 428240	2.5 2.5	-0.32 -0.27	8.50E+08 1.03E+09	0.516
1853.335	375218	2.5	429175	2.5	-0.5	6.35E + 08	0.261
1855.442	375280	3.5	429175 405584	2.5	-0.26	1.05E+09 1.79E→00	0.363
1861.736	356618	0.5	410331	$\frac{2.3}{1.5}$	-0.37	8.42E+08	0.793
1863.64	368012	2.5	421670	1.5	-0.91	2.29E + 08	0.221
1864.117 1865.501	357537 358748	$4.5 \\ 1.5$	411182 412353	$\frac{3.5}{2.5}$	-0.66 -0.96	4.37E+08 2.16E+08	0.256
1867.94	368135	1.5	421670	1.5	-0.87	2.71E + 0.00	0.254
1869.75	352434	4.5	405917	3.5	-0.13	1.38E+09	0.391
1872.947	359254 364260	2.5 2.5	412646 417629	1.5 1.5	-0.72 -0.77	3.40E+08 3.40E+08	0.255
1874.404	359562	0.5	412912	0.5	-0.78	3.15E + 08	0.396
1877.275	359377	2.5	412646	1.5	-0.76	3.27E+08	0.354
1878.425 1879.332	360580 357393	$3.5 \\ 2.5$	413816 410603	$2.5 \\ 2.5$	-0.93 -0.7	2.19E+08 3.85E+08	0.131
1885.43	358144	2.5	411182	3.5	-0.64	4.33E + 08	0.388
1887.551	360937	4.5	413916	3.5	0.3	3.66E + 09	0.862
1888.2	375280	2.5 3.5	412353 428240	$^{2.0}_{2.5}$	-0.73	5.51E+08 6.05E+08	0.26
1888.888	356233	1.5	409174	2.5	-0.22	1.13E + 09	0.571

Table A18: Continued

Wavelength	Lower Level	J _{Low}	Upper level	J_{Up}	log gf	gA 4 22E + 08	CF 0.272
1891.808	376555	1.5	429414	1.5	-0.88	4.32E+08 2.47E+08	0.372
1893.272	361097	3.5	413916	3.5	-0.27	9.86E+08	0.46
1898.12	349273	3.5 3.5	401957	3.5	-0.61	4.43E+08	0.138
1899.072	374413	1.5	427070	0.5	-0.6	4.54E + 08 1.25E + 00	0.509
1905.15	377995	0.5	430484	0.5	-0.59	4.74E+08	0.661
1907.174	358748	3.5	411182	3.5	-0.42	7.13E+08	0.353
1907.578	375832	2.5	429575 428240	2.5	-0.18	2.23E+09	0.094 0.21
1908.845	349569	2.5	401957	3.5	-0.33	8.42E+08	0.257
1910.99	357537	3.5 4.5	420392 409843	$^{2.3}_{3.5}$	0.16	2.69E+09	0.413 0.795
1912.591	353632	4.5	405917	3.5	-0.05	1.54E + 09	0.736
1914.524 1915.206	360937	$\frac{0.5}{4.5}$	412040	3.5	-0.47	6.19E + 08	0.35
1918.557	365557	0.5	417679	0.5	-0.64	4.03E + 08	0.616
1920.171 1920.927	349273 359124	$\frac{3.5}{4.5}$	401352 411182	3.5 3.5	0.01	1.84E+09 3.36E+09	$0.456 \\ 0.769$
1921.097	361097	3.5	413151	3.5	-0.86	2.51E + 08	0.136
1921.935	353886 375218	2.5 2.5	405917 427199	$\frac{3.5}{1.5}$	-0.4 -0.62	7.06E+08 4.43E+08	0.461 0.274
1927.061	357951	3.5	409843	3.5	-0.15	1.28E + 09	0.762
1928.469 1931.147	$358748 \\ 349569$	$\frac{3.5}{2.5}$	$410603 \\ 401352$	2.5 3.5	-0.26 0.05	9.77E+08 2.03E+09	$0.399 \\ 0.519$
1931.505	360580	3.5	412353	2.5	0.15	2.54E + 09	0.874
1934.315 1934 779	353886 376555	2.5 1.5	$405584 \\ 428240$	2.5 2.5	-0.18 -0.52	1.14E+09 5.39E+08	$0.591 \\ 0.474$
1936.453	373670	1.5	425311	1.5	-0.6	4.51E + 08	0.491
1938.627	358748	1.5	410331	1.5	-0.43	6.86E + 08 2.21E + 08	0.514
1942.551	357537	4.5	409016	3.5	-0.35	8.06E+08	0.787
1944.795	377995	0.5	429414	1.5	-0.89	2.23E + 08	0.363
1946.517	375218	2.5	426592	2.5	-0.93	3.30E+08	0.152
1947.465	359254	2.5	410603	2.5	-0.24	1.01E + 09	0.621
1948.82	375280	3.5 3.5	417549 426592	2.5 2.5	-0.26	$9.40E \pm 08$ $1.73E \pm 09$	0.468 0.632
1952.229	357951	3.5	409174	2.5	-0.76	3.09E+08	0.385
1952.98 1957.813	357393	2.5	408470	$^{2.3}_{3.5}$	-0.99	2.03E+08	0.428 0.246
1957.836	359254	2.5	410331	1.5	-0.69	3.58E+08	0.481
1959.616	378145 358144	2.5 2.5	429175 409174	2.5 2.5	-0.94 -0.74	$2.00E \pm 08$ $3.12E \pm 08$	0.103 0.243
1963.375	357537	4.5	408470	3.5	-0.27	9.42E+08	0.822
1965.209	373177	1.5 3.5	424036	$^{1.5}_{2.5}$	-0.79	2.73E+08 6.81E+08	0.384 0.722
1968.291	357951	3.5	408756	2.5	-0.7	3.47E+08	0.482
1974.31 1974.548	366978 376555	$1.5 \\ 1.5$	$417629 \\ 427199$	$1.5 \\ 1.5$	-0.73 -0.54	4.92E+08	0.526 0.293
1976.203	360580	3.5	411182	3.5	-0.66	3.93E+08	0.189
1981.206	362172 369553	$1.5 \\ 1.5$	412646 420008	$1.5 \\ 0.5$	-0.54 -0.9	4.93E+08 2.27E+08	0.361 0.42
1983.108	358748	1.5	409174	2.5	-0.78	2.94E + 08	0.183
1983.12 1987.143	365557	0.5	409174 415880	$^{2.5}_{1.5}$	-0.61	$4.13E \pm 08$ $3.56E \pm 08$	0.338
1993.986	367398	3.5	417549	2.5	-0.11	1.25E+09	0.61
1995.407 1996.191	373781 378145	2.5 2.5	423896 428240	$^{1.5}_{2.5}$	-0.69	2.13E+08	0.299 0.165
1996.622	361097	3.5	411182	3.5	-0.73	3.26E + 08	0.237
2002.565 2007.516	359254 359377	2.5 2.5	409174 409174	2.5 2.5	-0.98 -0.55	4.50E+08	0.33
2008.476	374263	3.5	424036	2.5	-0.86	2.19E+08	0.361
2014.77 2017.272	364260	2.5 2.5	417629 413816	2.5	-0.69	$4.38E \pm 0.08$ $3.29E \pm 0.08$	0.239
2017.761	368135	1.5	417679	0.5	-0.64	3.90E+08	0.399
2018.608 2019.322	352434 361097	$^{4.5}_{3.5}$	401957 410603	$\frac{3.5}{2.5}$	-0.89	1.78E+08	0.169 0.225
2020.404	375832	2.5	425311	1.5	0.02	1.70E+09	0.849
2023.07 2026.992	368135 372352	$1.5 \\ 2.5$	417549 421670	$^{2.5}_{1.5}$	-0.99	9.72E+08	0.322 0.571
2035.247	374413	1.5	423531	0.5	-0.66	3.61E + 08	0.349
2037.898 2043.577	352434	$^{2.5}_{4.5}$	427199 401352	1.5 3.5	-0.71	5.13E+08 5.34E+08	0.366
2044.267	366978	1.5	415880	1.5	-0.85	2.35E + 08	0.317
2066.058	364260 369303	$2.5 \\ 0.5$	$412646 \\ 417679$	$1.5 \\ 0.5$	-0.73	3.03E+08 1.94E+08	$0.269 \\ 0.574$
2070.5	371726	0.5	420008	0.5	-0.65	3.53E + 08	0.775
2079.395 2084.403	$369553 \\ 381615$	$1.5 \\ 4.5$	$417629 \\ 429575$	$1.5 \\ 3.5$	-0.96 -0.32	1.81E+08 7.55E+08	0.403 0.519
2092.423	351572	3.5	399348	3.5	-0.83	2.16E + 08	0.174
2093.799 2104.148	$368135 \\ 372498$	$1.5 \\ 1.5$	$415880 \\ 420008$	$1.5 \\ 0.5$	-0.43 -0.84	$_{0.04E+08}$ 2.20E+08	0.569
2107.244	358144	2.5	405584	2.5	-0.92	1.69E + 08	0.148
2128.052 2152.092	$376555 \\ 375218$	$1.5 \\ 2.5$	$423531 \\ 421670$	$0.5 \\ 1.5$	-1 -0.55	1.55E+08 4.27E+08	0.256 0.318
2181.799	368097	4.5	413916	3.5	-0.81	2.08E + 08	0.101
2225.79 2314.902	$364260 \\ 381615$	$\frac{2.5}{4.5}$	$409174 \\ 424800$	$\frac{2.5}{3.5}$	-0.85 -0.71	1.96E+08 2.39E+08	0.136
2414.871	357951	3.5	399348	3.5	-0.89	1.47E + 08	0.19
2446.664 2455.879	$361097 \\ 351572$	3.5 3.5	401957 392278	$3.5 \\ 3.5$	-0.96 -0.59	1.20E+08 2.70E+08	0.124 0.323
2489.555	359377	2.5	399533	2.5	-0.94	1.18E + 08	0.2
2546.759 2558.06	$377971 \\ 378145$	$\frac{3.5}{2.5}$	417225 417225	3.5 3.5	-0.3 0.01	5.09E+08 1.05E+09	0.861
2580.732	373781	2.5	412518	2.5	-0.85	1.45E + 08	0.206
2584.455 2589.141	$362172 \\ 372352$	$1.5 \\ 2.5$	400853 410963	2.5 3.5	-0.79 -0.78	1.53E+08 1.65E+08	0.368
2605.744	358144	2.5	396509	2.5	-0.28	5.13E + 08	0.659
2613.558 2625.357	$361097 \\ 349569$	$3.5 \\ 2.5$	$399348 \\ 387648$	$\frac{3.5}{1.5}$	-0.89 -0.97	1.27E+08 1.04E+08	0.388 0.109
2629.701	358493	1.5	396509	2.5	-0.86	1.39E + 08	0.214
2636.053 2637.006	$356233 \\ 376555$	$1.5 \\ 1.5$	$394157 \\ 414465$	$\frac{1.5}{2.5}$	-0.56 -0.26	2.68E+08 5.36E+08	0.553 0.789
2651.948	364260	2.5	401957	3.5	-0.48	3.10E + 08	0.241
			205 –				

Table A18: Continued

Wavelength	Lower Level	JLow	Upper level	JUP	log gf	gA	CF 0.24
2675.284	371726	0.5	409843 409094	1.5	-0.87	4.03E+08	0.24 0.812
2675.771	362172 375832	1.5	399533 413151	2.5	-0.97	9.52E+07 1.77E+08	0.243
2695.206	364260	2.5	401352	3.5 3.5	-0.85	1.32E+08	0.199
2716.616	366978	1.5	403778	1.5	-0.62	2.32E+08	0.629
2718.995	359410	1.5	396177	1.5	-0.48	2.72E+08	0.764 0.572
2719.283	377153	3.5	413916	3.5	-0.73	1.57E + 08	0.283
2724.471 2727.266	353886	3.5 2.5	$394644 \\ 390542$	$\frac{3.5}{2.5}$	-0.79	1.45E+08 1.28E+08	0.254 0.091
2731.962	364260	2.5	400853	2.5	-0.56	2.51E + 08	0.38
2737.311 2738.893	357393 358144	2.5 2.5	393914 394644	$\frac{2.5}{3.5}$	-0.75 -0.52	1.61E+08 2.60E+08	0.351
2752.46	378145	2.5	414465	2.5	-0.28	4.68E + 08	0.657
2752.846 2767.862	377995 372352	$0.5 \\ 2.5$	414310 408470	$1.5 \\ 3.5$	-0.2 -0.15	5.51E+08 5.93E+08	0.799
2775.932	358144	2.5	394157	1.5	-0.75	1.51E + 08	0.6
2776.154 2777.074	$368012 \\ 377153$	2.5 3.5	404022 413151	3.5 3.5	-0.11 -0.15	6.27E+08 5.96E+08	0.584 0.599
2779.777	376555	1.5	412518	2.5	-0.95	9.77E + 07	0.128
2785.77	$351762 \\ 360414$	1.5 0.5	387648 396177	1.5 1.5	-0.43 -0.59	3.20E+08 2.18E+08	0.517
2795.479	365557	0.5	401318	1.5	-0.47	2.76E + 08	0.704
2796.785 2798.641	375218 366236	2.5 3.5	$410963 \\ 401957$	3.5 3.5	-0.76 -0.57	1.58E+08 2.23E+08	0.221 0.364
2804.286	356233	1.5	391882	0.5	-0.69	1.75E + 08	0.764
2805.08 2806.63	$372498 \\ 368012$	1.5 2.5	408137 403631	2.5 2.5	-0.05 -0.72	7.44E+08 1.53E+08	0.729
2816.397	368135	1.5	403631	2.5	-0.21	5.51E+08	0.668
2822.369	358493	1.5	393914	2.5	-0.63	1.98E+08	0.288
2823.318 2824.842	359254	2.5	394644	3.5	-0.08	8.20E+08	0.425
2826.319	351572	3.5	386943	2.5	-1	7.95E+07	0.412
2834.204 2834.702	364260 359377	$2.5 \\ 2.5$	399533 394644	$\frac{2.5}{3.5}$	-0.61 -0.82	$2.10E \pm 08$ $1.17E \pm 08$	0.289 0.288
2835.86	372352	2.5	407604	3.5	-0.08	6.59E + 08	0.598
2837.245 2838.195	$373781 \\ 351572$	2.5 3.5	$409016 \\ 386795$	3.5 3.5	-0.45 -0.24	3.02E+08 4.55E+08	0.329 0.596
2841.597	351762	1.5	386943	2.5	-0.67	1.77E + 08	0.361
2845.644 2846.86	$375832 \\ 366236$	2.5 3.5	$410963 \\ 401352$	3.5 3.5	0.18	1.28E+09 1.31E+08	0.814 0.272
2849.148	364260	2.5	399348	3.5	-0.11	6.46E + 08	0.59
2849.318 2865.687	373670 357393	1.5 2.5	408756 392278	2.5 3.5	-0.02	7.98E+08 3.97E+08	0.809
2870.666	358748	1.5	393573	1.5	-0.82	1.30E+08	0.195
2880.792	376555	1.5	411257	1.5	-0.4	3.46E + 08	0.567
2882.553	374413	2.5	409094	1.5	-0.31	4.01E+08 7.98E+07	0.315 0.272
2884.341	359254	2.5	393914	2.5	-0.36	3.36E+08	0.626
2897.332	359410	2.5	393914	2.5	-0.66	1.89E+08 1.92E+08	0.48
2899.761	369303	0.5	403778	1.5	-0.36	3.76E + 08	0.874
2911.432 2912.263	362172 357951	1.5 3.5	396509	2.5 3.5	-0.39 -0.41	$3.10E \pm 08$ $3.04E \pm 08$	0.467
2913.817	356233	1.5	390542	2.5	-0.88	1.03E+08	0.335
2922.531 2928.748	374263 358144	$\frac{3.5}{2.5}$	408470 392278	3.5 3.5	-0.95 -0.44	$8.54E \pm 07$ $2.73E \pm 08$	0.273 0.528
2933.621	369553	1.5	403631	2.5	-0.7	1.64E + 08	0.384
2934.783 2939.34	360580 359562	$\frac{3.5}{0.5}$	$394644 \\ 393573$	$\frac{3.5}{1.5}$	-0.73	$1.46E \pm 08$ $4.35E \pm 08$	0.23 0.873
2939.858	362172	1.5	396177	1.5	-0.89	9.23E + 07	0.368
2945.044 2946.878	$368012 \\ 356618$	$2.5 \\ 0.5$	401957 390542	$\frac{3.5}{1.5}$	-0.96 -0.56	7.79E+07 2.16E+08	$0.228 \\ 0.456$
2951.202	366978	1.5	400853	2.5	-0.85	1.11E + 08	0.303
2955.696 2957.908	$373781 \\ 375218$	2.5 2.5	$407604 \\ 409016$	3.5 3.5	-0.49 -0.37	2.54E+08 3.47E+08	0.641 0.561
2961.054	353886	2.5	387648	1.5	-0.47	2.62E + 08	0.4
2964.355 2975.045	$374413 \\ 351762$	1.5 1.5	408137 385365	2.5 0.5	-0.72 -0.31	1.42E+08 3.71E+08	0.412 0.838
2978.717	349273	3.5	382835	3.5	0.06	8.49E + 08	0.631
2980.058 3005 223	$361097 \\ 349569$	$\frac{3.5}{2.5}$	394644 382835	3.5 3.5	-0.7 -0.53	1.48E+08 2.16E+08	0.334
3006.48	375218	2.5	408470	3.5	-0.59	2.01E + 08	0.292
3012.723	368135 357393	1.5 2.5	401318 390542	$1.5 \\ 2.5$	-0.63 -0.76	1.80E+08 1.34E+08	0.536
3017.178	358748	1.5	391882	0.5	-0.72	1.45E + 08	0.52
3019.137 3019.165	378145 366236	2.5 3.5	411257 399348	$1.5 \\ 3.5$	-0.89 -0.92	9.99E+07 8.58E+07	0.597 0.267
3023.337	378145	2.5	411211	2.5	-0.55	2.09E + 08	0.5
3024.206 3027 238	$353886 \\ 359254$	2.5 2.5	386943 392278	2.5	-0.16 -0.52	5.04E+08 2.17E+08	0.626
3037.808	353886	2.5	386795	3.5	-0.16	5.10E + 08	0.503
3055.542	368135	1.5	400853	2.5	-0.53	2.23E + 08	0.363
3086.877	375218	2.5	407604	3.5	-0.38	3.02E+08	0.359
3092.731	375280	3.5	407604	3.5	-0.67	1.44E + 08	0.472
3119.016	371726	⊿.5 0.5	403137	$^{2.0}_{1.5}$	-0.98	7.27E+07	0.233
3119.337	358493	1.5	390542	2.5	-0.67	1.53E+08	0.759
3129.003 3144.347	307398 358748	$3.5 \\ 1.5$	399348 390542	3.5 2.5	-0.82 -0.31	3.44E+07	0.446
3144.347	358748	1.5	390542	1.5	-0.83	1.06E + 08	0.307
3170.052 3182.252	381615 356233	$^{4.5}_{1.5}$	$\frac{413151}{387648}$	3.5 1.5	-0.82 -1	1.00E+08 6.69E+07	0.358 0.234
3288.407	352434	4.5	382835	3.5	-0.96	6.78E+07	0.537
3305.806 3334.642	$373781 \\ 369553$	2.5 1.5	404022 399533	$\frac{3.5}{2.5}$	-0.46 -0.68	2.20E+08 1.35E+08	0.41
3343.867	364260	2.5	394157	1.5	-1	6.11E + 07	0.271
3359.374	374263 357393	$\frac{3.5}{2.5}$	404022 386795	3.5 3.5	-0.49 -0.79	1.83E + 08 9.86E + 07	0.604
3423.312	353632	4.5	382835	3.5	-0.83	8.06E + 07	0.588
3473.604 3516.22	373177 377153	3.5	401957 405584	3.5 2.5	-0.96	5.76E+07 5.22E+07	0.17
3564.477	358748	3.5	386795	3.5	-0.99	5.30E+07	0.153

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Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA	CF
3813.513	360580	3.5	386795	3.5	-0.96	5.28E + 07	0.187
3861.296	380026	3.5	405917	3.5	0.43	1.09E + 09	0.948
3911.607	380026	3.5	405584	2.5	0.27	7.16E + 08	0.91
4235.252	380026	3.5	403631	2.5	-0.98	3.82E + 07	0.898
4423.85	379359	4.5	401957	3.5	-0.18	2.26E + 08	0.98
4545.544	379359	4.5	401352	3.5	0.29	6.49E + 08	0.989

Table A18: Continued

a: Experimental values from [35, 34]

In VI

Energy Levels

/				
E^{a}_{exp}	E^b_{calc}	ΔE	J	Leading components (in $\%$) in LS coupling ^{c}
0	-10	10	4	$98.3 \text{ 4d}^8 ({}^3\text{F}) {}^3\text{F}$
6465.3	6473	-7.7	3	99.7 4d ⁸ $({}^{3}F)$ ${}^{3}F$
8154	8151	3	2	$68.3 \text{ 4d}^8 ({}^{3}\text{F}) {}^{3}\text{F} + 25.7 \text{ 4d}^8 ({}^{1}\text{D}) {}^{1}\text{D} + 5.7 \text{ 4d}^8 ({}^{3}\text{P}) {}^{3}\text{P}$
15160.7	15180	-19.3	2	$59.5 \text{ 4d}^8 ({}^{3}\text{P}) {}^{3}\text{P} + 22.9 \text{ 4d}^8 ({}^{3}\text{F}) {}^{3}\text{F} + 17.3 \text{ 4d}^8 ({}^{1}\text{D}) {}^{1}\text{D}$
20606.8	20618	-11.2	0	95.6 4d ⁸ (³ P) ³ P
20649.2	20629	20.2	1	99.6 4d ⁸ (^{3}P) ³ P
23255.1	23251	4.1	2	56.6 4d ⁸ (^{1}D) $^{1}D + 34.5$ 4d ⁸ (^{3}P) $^{3}P + 8.6$ 4d ⁸ (^{3}F) ^{3}F
25865.9	25866	-0.1	4	$98.3 \text{ 4d}^8 (^1\text{G}) ^1\text{G}$
58627.3	58627	0.3	0	$95.5 \text{ 4d}^8 (^1\text{S})^{-1}\text{S}$
201884	201914	-30	5	$95.3 \text{ 4d}^7 \text{5s} (^4 \text{F}) ^5 \text{F}$
205958	205952	6	4	$90.7 \ 4d^75s \ (^4F) \ ^5F + 6 \ 4d^75s \ (^4F) \ ^3F$
209225.9	209217	8.9	3	$95.1 \ 4d^75s \ (^4F) \ ^5F$
211177.7	211163	14.7	2	93.7 $4d^75s$ (⁴ F) ⁵ F
212336.5	212317	19.5	1	91.8 $4d^75s$ (⁴ F) ⁵ F + 5.5 $4d^75s$ (² D) ³ D
214364.3	214368	-3.7	4	$84.7 \ 4d^75s \ (^4F) \ ^3F + 7.6 \ 4d^75s \ (^4F) \ ^5F$
219074	218999	75	3	54.7 $4d^75s$ (⁴ P) ⁵ P + 36.9 $4d^75s$ (⁴ F) ³ F
219005.8	219042	-36.2	2	$68.5 \ 4d^75s \ (^4P) \ ^5P + 24.8 \ 4d^75s \ (^2P) \ ^3P$
220287.1	220214	73.1	3	54.1 4d ⁷ 5s (⁴ F) ${}^{3}F$ + 41.8 4d ⁷ 5s (⁴ P) ${}^{5}P$
221971.3	221971	0.3	1	$75.9 4d^75s (^4P) {}^5P + 17.8 4d^75s (^2P) {}^3P$
222582.1	222604	-21.9	2	$82.8 4d^{7}5s (^{4}F) ^{3}F + 7.3 4d^{7}5s (^{4}P) ^{5}P + 5.1 4d^{7}5s (^{2}D) ^{1}D$
225122.4	225104	18.4	5	79.5 $4d^75s$ (² G) ³ G + 12.9 $4d^75s$ (² H) ³ H
226765.2	226695	70.2	4	$61.2 4d^{7}5s (^{2}\text{G}) ^{3}\text{G} + 20.6 4d^{7}5s (^{2}\text{H}) ^{3}\text{H} + 10 4d^{7}5s (^{2}\text{G}) ^{1}\text{G}$
228283.9	228380	-96.1	1	$31.7 \ 4d^{7}5s \ (^{2}P) \ ^{1}P + 29.4 \ 4d^{7}5s \ (^{4}P) \ ^{3}P + 15 \ 4d^{7}5s \ (^{4}P) \ ^{5}P$
228806.9	228705	101.9	2	$24.3 4d^{7}5s (^{2}P) ^{3}P + 44.3 4d^{7}5s (^{4}P) ^{3}P + 11.8 4d^{7}5s (^{2}D) ^{3}D$
230497.2	230395	102.2	3	94.2 $4d^{7}5s$ (² G) ³ G
230738.1	231064	-325.9	0	59.6 4d ⁷ 5s (² P) ${}^{3}P$ + 40 4d ⁷ 5s (⁴ P) ${}^{3}P$
231741.8	231835	-93.2	6	99.7 4d $^{\prime}$ 5s (2 H) 3 H
233207.3	233171	36.3	2	$48.4 \text{ 4d}'_{5s} (^{4}\text{P}) {}^{3}\text{P} + 23.5 \text{ 4d}'_{5s} (^{2}\text{P}) {}^{3}\text{P} + 9.8 \text{ 4d}'_{5s} (^{4}\text{P}) {}^{5}\text{P}$
233167.7	233176	-8.3	4	49.8 4d' 5s (2 G) 1 G + 28.4 4d' 5s (2 G) 3 G + 16.7 4d' 5s (2 H) 3 H
233903	233924	-21	5	73 4d' 5s (² H) ³ H + 20.5 4d' 5s (² H) ¹ H + 6 4d' 5s (² G) ³ G
234615.5	234475	140.5	3	$71.2 \text{ 4d}' \text{ 5s} (^2\text{D}) ^3\text{D} + 19 \text{ 4d}' \text{ 5s} (^2\text{D}) ^3\text{D}$
234581.9	234564	17.9	1	$40.6 \ 4d' \ 5s \ (^{2}P) \ ^{3}P + 33.4 \ 4d' \ 5s \ (^{2}P) \ ^{3}P + 15.4 \ 4d' \ 5s \ (^{2}D) \ ^{3}D$
237469.8	237310	159.8	2	$40.8 \text{ 4d}' \text{ 5s} (^2\text{D}) ^3\text{D} + 23.6 \text{ 4d}' \text{ 5s} (^2\text{D}) ^3\text{D} + 8.6 \text{ 4d}' \text{ 5s} (^2\text{D}) ^3\text{D}$
237876	238092	-216	1	$35.7 \text{ 4d}^{2} \text{5s} (^{2}\text{P}) ^{3}\text{P} + 23.2 \text{ 4d}^{2} \text{5s} (^{2}\text{D}) ^{3}\text{D} + 20.3 \text{ 4d}^{2} \text{5s} (^{2}\text{P}) ^{4}\text{P}$
238975.3	238983	-7.7	4	$61.9 \text{ 4d}^{2} \text{5s} (^{2}\text{H}) ^{3}\text{H} + 31.9 \text{ 4d}^{2} \text{5s} (^{2}\text{G}) ^{3}\text{G}$
239157.9	239198	-40.1	0	$59.5 \text{ 4d}^{\circ} \text{5s} (^{\circ} \text{P}) ^{\circ} \text{P} + 40.1 \text{ 4d}^{\circ} \text{5s} (^{\circ} \text{P}) ^{\circ} \text{P}$
240989.6	241128	-138.4	5	$76 \text{ 4d}^{\circ} \text{5s} (^{2}\text{H})^{-1}\text{H} + 13.7 \text{ 4d}^{\circ} \text{5s} (^{2}\text{H})^{-0}\text{H} + 9.8 \text{ 4d}^{\circ} \text{5s} (^{2}\text{G})^{-0}\text{G}$
245366.1	245307	59.1	2	$53.6 \text{ 4d}^{2} \text{ 5s} (^{2}\text{F}) ^{\circ}\text{F} + 14.3 ^{\circ}\text{4d}^{2} ^{\circ}\text{5s} (^{2}\text{D}) ^{\circ}\text{D} + 13.8 ^{\circ}\text{4d}^{2} ^{\circ}\text{5s} (^{2}\text{D}) ^{\circ}\text{D}$
245508.9	245555	-46.1	1	$34.8 \text{ 4d}^{2} \text{5s} (^{2}\text{D}) ^{3}\text{D} + 43.7 \text{ 4d}^{2} \text{5s} (^{2}\text{P}) ^{4}\text{P} + 15.2 \text{ 4d}^{2} \text{5s} (^{4}\text{P}) ^{3}\text{P}$
245979.1	245873	106.1	2	35.740° S (D) $^{\circ}$ D + 41.940 S ($^{\circ}$ F) $^{\circ}$ F + 9.34d S ($^{\circ}$ P) $^{\circ}$ P
246405.3	246397	8.3	3	89.0 4d $\operatorname{ps}(F) = F + 5.0 4d \operatorname{ps}(F) = F$
248093.5 052270 5	248/04	-00.0	4	94.04038(F) ^T 0014 7 ^E (2E) 1E + 614 7 ^E (2E) 3E
203378.0 060705	253204	1(4.5	3 1	$30.140 \ 38 (F)^{-}F + 0.140 \ 38 (-F)^{-}F$ $00.437 E_{-}(2D)^{-}3D + 8.6437 E_{-}(2D)^{-}3D$
209703	209807	-102	1	30.40 os (D) D + 8.0.40 os (D) D $30.447 \text{ e}_{-} (2\text{ D}) 3\text{ D} + 11 \text{ e}_{-} 447 \text{ e}_{-} (2\text{ D}) 3\text{ D}$
210403 272270 F	270004	-101	2	74240 35 (D) $D + 11.040$ 35 (D) $D74240^756 (^2D) ^3D + 20240^756 (^2D) ^3D$
212210.3	276087	04.0 80	ა ი	(4.3 40 38 (D) D + 20.3 40 38 (D) D 77.2 $4d^{7}5c (^{2}D)$ ¹ D + 16.2 $4d^{7}5c (^{2}D)$ ¹ D
211010	210901	09	4	(1.2.40.08) D + $10.2.40.08$ D D

Table A19: Comparison between available experimental data and calculated even energy levels (in $\rm cm^{-1}$) in In VI

a: From Ryabtsev [37] b: This work c: Only the component $\geq 5\%$ are given

Table A20: Comparison between available experimental data and calculated odd energy levels (in cm^{-1}) in In VI

E^a	E^b .	ΔΕ	J	Leading components (in $\%$) in LS coupling ^c
-exp	-calc	1.0	4	$49.7 4^{7} t_{-} (4E) 5D + 90 t 4^{7} t_{-} (4E) 5E + 9 t 4^{7} t_{-} (4E) 3E$
280626.1	280628	-1.9	4	$48.7 4d^{2} p(F) D + 28.5 4d^{2} p(F) F + 8.5 4d^{2} p(F) F$
288303.7	288202	101.7	5	$53.3 \text{ 4d}^{-}\text{5p}(^{-}\text{F}) = F + 21.7 \text{ 4d}^{-}\text{5p}(^{-}\text{F}) = G + 19.9 \text{ 4d}^{-}\text{5p}(^{-}\text{F}) = G$
291912.1	291928	-15.9	3	$36.1 \ 4d' \ 5p \ ({}^{4}F) \ {}^{5}D + 45.6 \ 4d' \ 5p \ ({}^{4}F) \ {}^{5}F + 5.9 \ 4d' \ 5p \ ({}^{4}P) \ {}^{5}D$
294223.8	294127	96.8	4	41.4 4d' 5p (4 F) 5 G + 22.1 4d' 5p (4 F) 5 F + 15 4d' 5p (4 F) 5 D
294997.7	295016	-18.3	2	55.1 4d ⁷ 5p (⁴ F) ⁵ F + 19.4 4d ⁷ 5p (⁴ F) ⁵ D + 6.5 4d ⁷ 5p (⁴ F) ⁵ G
296630.6	296574	56.6	3	$44.1 \ 4d^{7}5p \ (^{4}F) \ ^{5}G + 14.3 \ 4d^{7}5p \ (^{4}F) \ ^{5}D + 8.7 \ 4d^{7}5p \ (^{4}F) \ ^{5}F$
296786.5	296804	-17.5	1	57.1 4d ⁷ 5p (⁴ F) ⁵ F + 12 4d ⁷ 5p (⁴ F) ⁵ D + 7.8 4d ⁷ 5p (⁴ F) ³ D
297246	297165	81	5	$34.2 \ 4d^{7}5p \ (^{4}F) \ ^{3}G + 42.3 \ 4d^{7}5p \ (^{4}F) \ ^{5}F + 16.9 \ 4d^{7}5p \ (^{4}F) \ ^{5}G$
207302 /	207325	67.4	6	$03.8 \ dd^{7}5p \ (^{4}F) \ ^{5}C + 5.8 \ dd^{7}5p \ (^{2}C) \ ^{3}H$
291392.4	291325	01.4	2	0.436 = (3E) 3E + 27.6 437 = (4E) 5C + 27.4 437 = (4E) 5C
298738.2	298767	-28.8	2	$0.4a^{-}$ ssp (°F) °F + 37.8 4a sp (°F) °S + 27.4 4a sp (°F) °G
298945.5	298955	-9.5	2	$43.8 \text{ 4d}^{-}5p(^{-}P) \circ S + 27.8 \text{ 4d}^{-}5p(^{-}F) \circ G + 6.3 \text{ 4d}^{-}5p(^{-}F) \circ D$
299666	299670	-4	2	23.3 4d' 5p (4 P) 9 D + 13.6 4d' 5p (4 F) 9 G + 12.5 4d' 5p (4 F) 9 D
299836.1	299771	65.1	4	$31.4 \ 4d^7 5p \ (^4F) \ ^3F + 22.4 \ 4d^7 5p \ (^4F) \ ^5D + 16.5 \ 4d^7 5p \ (^4F) \ ^5F$
300502.8	300556	-53.2	1	$25.5 \ 4d^75p \ (^4F) \ ^5D + 36.4 \ 4d^75p \ (^4P) \ ^5D + 17.3 \ 4d^75p \ (^4F) \ ^5F$
300850.9	300956	-105.1	0	$45.6 \ 4d^{7}5p \ (^{4}P) \ ^{5}D + 42.1 \ 4d^{7}5p \ (^{4}F) \ ^{5}D + 7.9 \ 4d^{7}5p \ (^{2}P) \ ^{3}P$
301111.2	300979	132.2	3	$22.5 4d^{7}5p ({}^{4}F) {}^{5}F + 24.6 4d^{7}5p ({}^{4}F) {}^{5}G + 13.4 4d^{7}5p ({}^{4}P) {}^{5}D$
202052.2	202056	102.2	4	22.0 44 op(1) 1 + 24.0 44 op(1) 0 + 10.4 44 op(1) D 30.0 4475 - (4E) 5E + 37.6 4475 - (4E) 3E + 14.4475 - (4E) 5C
303033.2	303030	-2.0	4	50.9 4d 5p (F) F + 27.0 4d 5p (F) F + 14 4d 5p (F) G
304156.8	304145	11.8	5	$59.1 \text{ 4d} 5p (^{1}\text{F}) ^{\circ}\text{G} + 36.3 \text{ 4d} 5p (^{1}\text{F}) ^{\circ}\text{G}$
304448.8	304630	-181.2	3	44.6 4d' 5p (${}^{4}F$) ${}^{3}D$ + 17.8 4d' 5p (${}^{4}F$) ${}^{3}F$ + 9 4d' 5p (${}^{4}F$) ${}^{3}D$
306757	306935	-178	1	$22.6 4d'_{5p} (^{2}\text{P}) {}^{3}\text{P} + 17.1 4d'_{5p} (^{4}\text{P}) {}^{3}\text{S} + 12.1 4d'_{5p} (^{2}\text{P}) {}^{3}\text{S}$
307655.3	307793	-137.7	2	29.4 $4d^{7}5p ({}^{4}F) {}^{3}D + 17.4 4d^{7}5p ({}^{4}F) {}^{5}F + 10.8 4d^{7}5p ({}^{4}F) {}^{5}D$
308184.9	308271	-86.1	4	$62 \ 4d^75p \ (^4F) \ ^3G + 23.4 \ 4d^75p \ (^4F) \ ^5G$
308432.1	308419	13.1	3	$37.5 4d^{7}5p ({}^{4}F) {}^{3}F + 16.9 4d^{7}5p ({}^{4}F) {}^{5}F + 13.1 4d^{7}5p ({}^{4}F) {}^{3}D$
200060 2	208844	24.2	2	$16.6 4d^{7}5p (^{4}F) ^{5}C + 26.4d^{7}5p (^{4}F) ^{3}F + 0.2 4d^{7}5p (^{4}F) ^{5}D$
200015	308844	24.2	4	10.0 40 5p(F) G + 20 40 5p(F) F + 9.2 40 5p(F) D
309215	309144	11	5	$37.3 4 \text{d}^{2} \text{p} (\text{G})^{-1} \text{H} + 18.6 4 \text{d}^{-2} \text{p} (\text{H})^{-1} + 18.4 \text{d}^{-2} \text{p} (\text{G})^{-1} \text{H}$
310570.9	310475	95.9	4	$27.6 \text{ 4d}^{\circ} \text{5p} (^{2}\text{G}) ^{\circ}\text{F} + 24.1 \text{ 4d}^{\circ} \text{5p} (^{2}\text{F}) ^{\circ}\text{F} + 10.5 \text{ 4d}^{\circ} \text{5p} (^{2}\text{G}) ^{\circ}\text{G}$
310899.4	310905	-5.6	3	$63.7 \text{ 4d}'_{5p} (^{4}\text{F}) ^{3}\text{G} + 7.3 \text{ 4d}'_{5p} (^{4}\text{F}) ^{3}\text{G}$
310800.6	310959	-158.4	1	$33.2 \ 4d^75p \ (^4F) \ ^3D + 16.8 \ 4d^75p \ (^2P) \ ^3D + 15.4 \ 4d^75p \ (^4F) \ ^5D$
311484.8	311430	54.8	3	$9 \text{ 4d}^7 \text{5p} (^4\text{P}) {}^5\text{P} + 19.5 \text{ 4d}^7 \text{5p} (^4\text{P}) {}^5\text{D} + 18.6 \text{ 4d}^7 \text{5p} (^4\text{F}) {}^3\text{D}$
312153	312239	-86	2	$28.2 4d^75p ({}^4F) {}^3F + 12.1 4d^75p ({}^4F) {}^3D + 11.5 4d^75p ({}^4F) {}^5D$
313493 4	313414	79.4	4	$65.9.4d^{7}5p(^{2}C)^{3}H + 9.9.4d^{7}5p(^{2}C)^{1}C + 5.3.4d^{7}5p(^{2}C)^{3}C$
214996.6	214052	10.4 024 G	1	$14.9 43^{7} = (2D)^{3} D + 15.6 43^{7} = (4D)^{3} C + 15.43^{7} = (4D)^{5} D$
314280.0	314032	234.0	1	$14.8 40 \text{ sp}(\mathbf{r}) D + 13.0 40 \text{ sp}(\mathbf{r}) S + 13.40 \text{ sp}(\mathbf{r}) \mathbf{r}$
314464.2	314662	-197.8	0	$36.8 \text{ 4d} \text{ 5p} (^{1}\text{F}) ^{\circ}\text{D} + 24.2 \text{ 4d} \text{ 5p} (^{1}\text{P}) ^{\circ}\text{D} + 14.9 \text{ 4d} \text{ 5p} (^{2}\text{P}) ^{1}\text{S}$
314565.8	315107	-541.2	0	$64 4d'_{5p} (^{2}P) {}^{3}P + 13.4 4d'_{5p} (^{2}D) {}^{3}P + 7.1 4d'_{5p} (^{4}P) {}^{3}P$
315135.6	315147	-11.4	6	59 4d' 5p (² H) ³ I + 20 4d' 5p (² H) ¹ I + 9.9 4d' 5p (² G) ³ H
315321.2	315184	137.2	2	$20.7 \ 4d^75p \ (^4P) \ ^5P + 21.9 \ 4d^75p \ (^4P) \ ^5D + 10.9 \ 4d^75p \ (^2D) \ ^3F$
315206.8	315229	-22.2	5	$80.5 \ 4d^{7}5p \ (^{2}H) \ ^{3}G + 6.4 \ 4d^{7}5p \ (^{2}F) \ ^{3}G + 5 \ 4d^{7}5p \ (^{2}H) \ ^{3}H$
316098-1	315824	274 1	4	81.6 4d ⁷ 5p (⁴ P) ⁵ D + 9.7 4d ⁷ 5p (⁴ F) ⁵ D
315985.8	315942	43.8	3	$30.1.4d^{7}5p$ (² G) ³ G + 22.6.4d ⁷ 5p (² G) ³ F + 14.4d ⁷ 5p (² G) ¹ F
216201 7	216417	25.2	1	$28 4d^{7}5p (4p) 5p + 186 4d^{7}5p (4p) 5p + 145 4d^{7}5p (4p) 3p$
310391.7	310417	-20.0	1	2840.5p(1) D + 18.040.5p(1) 1 + 14.540.5p(1) D
316277	316587	-310	2	$23.3 \text{ 4d}^{\circ} \text{ 5p} (^{-}\text{P})^{\circ}\text{P} + 26.9 \text{ 4d}^{\circ} \text{5p} (^{-}\text{F})^{\circ}\text{D} + 11.8 \text{ 4d}^{\circ} \text{5p} (^{-}\text{P})^{\circ}\text{P}$
316886.1	316888	-1.9	3	$30.4 \ 4d^{2}5p \ (^{2}P) \ ^{9}D + 18.3 \ 4d^{2}5p \ (^{4}P) \ ^{9}P + 17.3 \ 4d^{2}5p \ (^{4}P) \ ^{9}D$
317795.4	317722	73.4	6	$64.8 \ 4d' 5p \ (^2G) \ ^3H + 29.8 \ 4d' 5p \ (^2H) \ ^1I$
318711.2	318636	75.2	4	$26.8 \ 4d^75p \ (^2G) \ ^1G + 26 \ 4d^75p \ (^2G) \ ^3F + 13.4 \ 4d^75p \ (^2H) \ ^1G$
318650.7	318704	-53.3	3	21.9 $4d^{7}5p$ (² H) ³ G + 19.1 $4d^{7}5p$ (² G) ¹ F + 11.6 $4d^{7}5p$ (² F) ³ G
318954.2	318867	87.2	2	$16 4d^{7}5p (^{4}P) {}^{3}P + 20 4d^{7}5p (^{4}P) {}^{5}P + 11.8 4d^{7}5p (^{2}P) {}^{1}D$
319588	319586	2	5	$52 4d^75p (^2C) ^3C + 371 4d^75p (^2H) ^3I$
220260 7	220057	212.7	2	22 2 4 7 5 $^{(2)}$ 3
320209.7	320037	212.1	1	32.2 4d 5p (D) D + 10.3 4d 5p (D) T + 7.3 4d 5p (D) D 37.1 417r (4p) 3c + 10.0 417r (2p) 3p + 10.417r (4p) 3p
320117.5	320192	-74.5	1	$35.14d^{2}p(P)^{-5} + 16.84d^{2}p(P)^{-1}P + 104d^{2}p(P)^{-1}D$
320046.1	320270	-223.9	0	$46.1 \ 4d' \ 5p \ (^2P) \ ^2S + 21 \ 4d' \ 5p \ (^4P) \ ^0D + 13.9 \ 4d' \ 5p \ (^4P) \ ^0P$
320949.8	320766	183.8	3	$49.7 \text{ 4d}' \text{ 5p} (^{4}\text{P}) ^{3}\text{D} + 27.3 \text{ 4d}' \text{ 5p} (^{4}\text{P}) ^{3}\text{P} + 8 \text{ 4d}' \text{ 5p} (^{4}\text{P}) ^{3}\text{D}$
321145.7	321008	137.7	1	28 4d ⁷ 5p (⁴ P) ⁵ P + 14.3 4d ⁷ 5p (² P) ³ D + 11.8 4d ⁷ 5p (⁴ P) ³ S
321423.7	321263	160.7	2	$30.1 \ 4d^75p \ (^4P) \ ^3D + 19.1 \ 4d^75p \ (^2D) \ ^3P + 15.9 \ 4d^75p \ (^4P) \ ^3P$
321497.1	321545	-47.9	4	$55.5 \ 4d^75p \ (^2H) \ ^3G + 16 \ 4d^75p \ (^2G) \ ^3F + 12 \ 4d^75p \ (^2F) \ ^3G$
321946.6	322018	-71.4	5	$36.3 \ 4d^{7}5p \ (^{2}H) \ ^{3}I + 20.6 \ 4d^{7}5p \ (^{2}G) \ ^{1}H + 14.7 \ 4d^{7}5p \ (^{2}G) \ ^{3}H$
322528.8	322680	-151.2	1	$28.4 4d^{7}5p (^{2}P) ^{1}P + 24.1 4d^{7}5p (^{4}P) ^{3}P + 19.5 4d^{7}5p (^{2}P) ^{3}D$
222015 1	222000	24.0	7	20.4 4d op(1) 1 + $24.1 4d op(1)$ 1 + $15.0 4d op(1)$ D $00.7 \text{ 4d}^{7}\text{5p}(2\text{H})$ 31
222910.1	222940	-24.9	2	39.7 40 5p (11) 1 $20.7 437 z_{-} (20) 3z_{-} 16.1 437 z_{-} (20) 30 + 19.8 437 z_{-} (2z) 30$
323218.9	323120	98.9	3	$39.7 40^{-5}p(-G)^{-7}F + 10.1 40^{-5}p(-G)^{-1}G + 12.8 40^{-5}p(-F)^{-3}G$
323559.1	323456	103.1	2	$23.7 \text{ 4d} \cdot 5p (^2\text{D}) \circ F + 23.3 \text{ 4d} \cdot 5p (^2\text{G}) \circ F + 14.2 \text{ 4d} \cdot 5p (^2\text{P}) \circ P$
323562.4	323511	51.4	4	$59 \text{ 4d}' \text{ 5p} (^{2}\text{G}) ^{3}\text{G} + 17.6 \text{ 4d}' \text{ 5p} (^{2}\text{G}) ^{3}\text{H} + 12.2 \text{ 4d}' \text{ 5p} (^{2}\text{H}) ^{1}\text{G}$
324393.5	324325	68.5	5	$45.8 \ 4d^{7}5p \ (^{2}G) \ ^{1}H + 41.3 \ 4d^{7}5p \ (^{2}G) \ ^{3}H + 8.6 \ 4d^{7}5p \ (^{2}G) \ ^{3}G$
324358.9	324345	13.9	2	$42.2 \ 4d^75p \ (^2G) \ ^3F + 9.1 \ 4d^75p \ (^4P) \ ^3D + 7.2 \ 4d^75p \ (^2D) \ ^3F$
324595.7	324541	54.7	2	$9.2 \ 4d^75p \ (^2D) \ ^3D + 18.4 \ 4d^75p \ (^4P) \ ^3P + 17.1 \ 4d^75p \ (^4P) \ ^5P$
324826	324749	77	3	$9.1 \ 4d^{7}5p \ (^{4}P) \ ^{5}D + 19.3 \ 4d^{7}5p \ (^{2}D) \ ^{3}F + 15.8 \ 4d^{7}5p \ (^{2}P) \ ^{3}D$
325370 5	325297	73.5	1	$32.7 4d^{7}5p (^{2}D) ^{3}D + 20.1 4d^{7}5p (^{4}P) ^{3}D + 8.1 4d^{7}5p (^{4}F) ^{3}D$
326277 1	326115	162 1	3	$724d^{7}5p(^{2}F)^{3}D + 1584d^{7}5p(^{2}H)^{3}C + 1564d^{7}5p(^{2}C)^{3}C$
326242.0	396957	112.0	1	$36.7 4d^75_{\text{D}} (^4\text{P}) ^3\text{P} \pm 16.7 4d^75_{\text{D}} (^2\text{P}) ^3\text{C} \pm 16.7 4d^75_{\text{D}} (^2\text{P}) ^3\text$
020240.0	320337	100 -	1	$12.4 \ 417 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ D \ 40.7 \ \epsilon_{-} (2 \ D) \ 3 \ C \ 40.7 \ c_{-} (2 \ D) \ 3 \ C \ 40.7 \ c_{-} (2 \ D) \ 3 \ C \ 40.7 \ c_{-} (2 \ D) \ 3 \ C \ 40.7 \ c_{-} (2 \ D) \ 3 \ C \ 40.7 \ c_{-} (2 \ D) \ 3 \ C \ 40.7 \ c_{-} (2 \ D) \ 3 \ C \ 40.7 \ c_{-} (2 \ D) \ 3 \ C \ 40.7 \ c_{-} (2 \ D) \ 3 \ C \ 40.7 \ c_{-} (2 \ D) \ 3 \ C \ 40.7 \ c_{-} (2 \ D) \ 3 \ C \ 40.7 \ c_{-} (2 \ D) \ 40.7 \ c_{-} (2 \ C) \ 40.7 \ c_{-} (2 \ C) \ 40.7$
32/132.7	327044	108.7	2	13.4 4d $ 5p(-F)$ $(-F)$ $(-$
328090.9	327913	177.9	4	$69.7 \text{ 4d} 5p (^{-}\text{D}) F + 12.8 \text{ 4d} 5p (^{-}\text{D}) F + 5 \text{ 4d} 5p (^{-}\text{F}) F$
329406.5	329520	-113.5	6	84.2 4d'5p (² H) ³ H + 15 4d'5p (² H) ³ I
329895.2	330019	-123.8	6	49.7 4d ['] ₂ 5p (² H) ¹ ₁ I + 25.7 4d ['] ₂ 5p (² H) ³ I + 18.9 4d ⁷ 5p (² G) ³ H
330022	330059	-37	2	$20.3 4d^75p (^2P) ^3D + 16 4d^75p (^2D) ^1D + 12.5 4d^75p (^2D) ^3P$
330374.9	330424	-49.1	5	$66.1 \ 4d^75p \ (^2H) \ ^3H + 18.6 \ 4d^75p \ (^2H) \ ^1H + 6.4 \ 4d^75p \ (^2H) \ ^3G$
330633.4	330603	30.4	3	$33.6 \ 4d^{7}5p \ (^{2}G) \ ^{1}F + 10.9 \ 4d^{7}5p \ (^{2}P) \ ^{3}D + 10.2 \ 4d^{7}5p \ (^{2}D) \ ^{3}F$
330914 7	330967	-52.3	1	$23.1 \ 4d^{7}5p \ (^{2}P) \ ^{3}S + 22.8 \ 4d^{7}5p \ (^{2}P) \ ^{3}P + 21.8 \ 4d^{7}5p \ (^{2}D) \ ^{3}P$
331570 1	331550	20.1	1	$17.9 \ 4d^{7}5n \ (^{4}P) \ ^{3}D + 23.2 \ 4d^{7}5n \ (^{2}D) \ ^{1}P \pm 12.4 \ d^{7}5n \ (^{2}D) \ ^{1}D$
331000.0	221500	20.1	0	$66.8 4d^7 \text{sp} (4\text{P}) ^3\text{P} \pm 96.4 ^37 \text{sp} (2\text{P}) ^1\text{C}$
331200.2	220105	-301.8	0	$20.0 \pm 4.0 \text{ p} (\mathbf{r}) = \mathbf{r} \pm 20.40^{\circ} \text{ p} (\mathbf{r}) = 5$ $20.0 \pm 4.7 \text{ m} + (2\text{ p}) = 100 \pm 4.17 \text{ m} + (2\text{ p}) = 3 \text{ p} + 10.0 \pm 17 \text{ m} + (4\text{ p}) = 3 \text{ p}$
331952.1	002100 000400	-212.9	2	22.5 40 5p (F) $D + 22.4$ 4d 5p (F) $F + 10.2$ 4d 5p (P) $^{\circ}D$
332306.3	332463	-156.7	4	50.3 4d 5p (⁻ H) -G + 20.7 4d 5p (⁻ G) -G + 15.7 4d 5p (² H) -H
332847.9	332832	15.9	4	51.5 4d' 5p (2 H) 3 H + 22.7 4d' 5p (2 G) 1 G + 14.7 4d' 5p (2 F) 3 G
333541.4	333427	114.4	3	19.4 4d ['] 5p (² D) ${}^{1}F$ + 19.7 4d ['] 5p (² F) ${}^{3}F$ + 13 4d ⁷ 5p (² F) ${}^{3}G$
334172.8	333928	244.8	2	$0.7 \ 4d^75p \ (^4F) \ ^5D + 18.2 \ 4d^75p \ (^2P) \ ^1D + 15.9 \ 4d^75p \ (^2F) \ ^1D$
335891.7	335876	15.7	2	$18.9 \ 4d^75p \ (^2D) \ ^1D + 12.5 \ 4d^75p \ (^2F) \ ^3F + 12.3 \ 4d^75p \ (^2P) \ ^3P$
336395.2	336339	56.2	1	$50.2 \ 4d^{7}5p \ (^{2}D) \ ^{1}P + 20.7 \ 4d^{7}5p \ (^{2}P) \ ^{3}S + 9.8 \ 4d^{7}5p \ (^{2}P) \ ^{1}P$
336758 1	336610	130.1	2	$20 4d^{7}5p (^{2}F) ^{3}G \pm 24.7 4d^{7}5p (^{2}H) ^{3}G \pm 16.5 4d^{7}5p (^{2}F) ^{3}D$
227120 5	227101	100.1	4	$177 4d^{7} 5p (^{2} p) 30 + 218 4d^{7} 5p (^{2} p) 10 + 4d^{7} 5p (^{2} p) 30 + 218 4d^{7} 5p (^{2} p) 10 + 4d^{7} 5p (^{2} p) 3p$
00/102.0	337181	-40.0	4	$r_{1.1}$ + $r_{2.1}$ $r_{1.1}$ + $r_{2.1}$
338400.4	338476	-75.6	Б	(1.4 4d op (H) H + 12.8 4d op (H) $^{\circ}$ H + 5.4 4d op (G) $^{\circ}$ G
339553	339549	4	1	$37.2 \text{ 4d' 5p} (^{2}\text{D}) ^{2}\text{P} + 17.8 \text{ 4d' 5p} (^{2}\text{P}) ^{1}\text{P} + 11.5 \text{ 4d' 5p} (^{2}\text{F}) ^{3}\text{D}$
340106.5	339953	153.5	0	73.2 4d' 5p (² D) $^{\circ}P$ + 11.4 4d' 5p (² P) $^{\circ}P$ + 10.2 4d' 5p (² P) ^{1}S
341214.1	341205	9.1	3	56.7 4d' 5p (${}^{2}F$) ${}^{3}F$ + 15.5 4d' 5p (${}^{2}F$) ${}^{3}G$ + 6.9 4d' 5p (${}^{2}F$) ${}^{3}D$
341053.9	341249	-195.1	2	$31.6 \text{ 4d}' \text{ 5p} (^{2}\text{F}) ^{3}\text{F} + 20.7 \text{ 4d}' \text{ 5p} (^{2}\text{F}) ^{1}\text{D} + 18.3 \text{ 4d}^{7}\text{5p} (^{2}\text{F}) ^{3}\text{D}$
342178.7	342010	168.7	3	$11 4d^{7}5p (^{2}D) {}^{3}F + 24.3 4d^{7}5p (^{2}F) {}^{3}D + 18 4d^{7}5p (^{2}P) {}^{3}D$

Table A20: Continued

E_{exp}^{a}	E_{calc}°	ΔE	J	Leading components (in %) in LS coupling $^{\circ}$					
343271.8	342193 343174	-128.1 97.8	4	47.8 4d 5p (F) G + 55.8 4d 5p (F) G + 6 4d 5p (H) G $64.4 4d^{7}5p (^{2}F) ^{3}D + 9.9 4d^{7}5p (^{2}D) ^{3}D + 9.3 4d^{7}5p (^{2}D) ^{3}D$					
343896.6	343862	34.6	2	$47.8 \ 4d^{7}5p \ (^{2}F) \ ^{3}D + 22.2 \ 4d^{7}5p \ (^{2}F) \ ^{1}D + 6.2 \ 4d^{7}5p \ (^{2}D) \ ^{3}D$					
344138	344089	49	5	84.3 $4d^{7}5p$ (² F) ³ G + 8.2 $4d^{7}5p$ (² H) ³ G					
344200.9	344236	-35.1	4	$61.9 \text{ 4d}' \text{ 5p} (^{2}\text{F}) ^{3}\text{F} + 12.5 \text{ 4d}' \text{ 5p} (^{2}\text{F}) ^{1}\text{G} + 11.5 \text{ 4d}' \text{ 5p} (^{2}\text{F}) ^{3}\text{G}$					
355484	355523	-39	2	$69.2 \ 4d^{7}5p \ (^{2}D) \ ^{3}P + 15.3 \ 4d^{7}5p \ (^{2}D) \ ^{3}P$					
356225.6	356397	-171.4	2	71.1 $4d^{7}5p$ (² D) ³ F + 8.1 $4d^{7}5p$ (² F) ³ F + 6.9 $4d^{7}5p$ (² D) ³ F					
357557.3	357608	-50.7	1	$67.2 4d^75p (^2D) ^{3}P + 10.8 4d^75p (^2D) ^{1}P + 8.3 4d^75p (^2D) ^{3}D$					
359371.2	359296	75.2	3	$54 \ 4d^75p \ (^2D) \ ^3F + 12.4 \ 4d^75p \ (^2D) \ ^1F + 11.1 \ 4d^75p \ (^2D) \ ^3F$					
360811.4	360915	-103.6	0	90 4d' 5p (² D) ³ P 70 1 4d ⁷ 5 (² D) ³ E + 10 4d ⁷ 5 (² D) ³ E					
365630.9	365545	125.4 85.9	4	$(10.140^{-5}\text{p})(^{2}\text{D})^{-1}\text{P} + 1940^{-5}\text{p}(^{2}\text{D})^{-3}\text{D} + 18640^{7}\text{5}\text{p}(^{2}\text{D})^{-3}\text{P}$					
366355.3	366389	-33.7	3	58.6 $4d^{7}5p$ (² D) ¹ F + 20.7 $4d^{7}5p$ (² D) ³ F + 7.8 $4d^{7}5p$ (² D) ¹ F					
369896.8	369849	47.8	2	$61.6 \ 4d^75p \ (^2D) \ ^3D + 13.4 \ 4d^75p \ (^2D) \ ^3D + 12.4 \ 4d^75p \ (^2D) \ ^1D$					
370177.8	370228	-50.2	1	$40.9 \ 4d_{7}^{7}5p \ (^{2}D) \ ^{3}D + 42.9 \ 4d_{7}^{7}5p \ (^{2}D) \ ^{1}P + 7.5 \ 4d_{7}^{7}5p \ (^{2}D) \ ^{3}D$					
373995.4	373904	91.4	3	59.6 $4d^{7}5p$ (² D) ³ D + 21.2 $4d^{7}5p$ (² D) ³ D + 8.3 $4d^{7}5p$ (² D) ¹ F					
433093.2	433279	-185.8	1	$75.7 \text{ 4d} \cdot 41 (^{\circ}\text{F}) \circ \text{F} + 9.8 \text{ 4d} \cdot 41 (^{\circ}\text{P}) \circ \text{F}$ $65.2 \text{ 4d}^7 4f (^4\text{E}) \cdot ^5\text{D} + 20.2 \text{ 4d}^7 4f (4f) \cdot ^5\text{D} + 5.2 \text{ 4d}^7 4f (^4\text{D}) \cdot ^5\text{D}$					
440559.7	440621	-61.3	1	$53.2 \text{ 4d} \text{ 4f} (^{4}\text{P}) ^{5}\text{D} + 19.6 \text{ 4d}^{7}\text{4f} (^{4}\text{f}) ^{5}\text{P} + 15.2 \text{ 4d}^{7}\text{4f} (^{4}\text{F}) ^{5}\text{D}$					
441387	441600	-213	3	$10.4 4d^{7}4f (^{4}\text{F}) \ ^{3}\text{G} + 20.5 \ 4d^{7}4f (^{4}\text{f}) \ ^{5}\text{D} + 11.7 \ 4d^{7}4f (^{4}\text{F}) \ ^{3}\text{D}$					
442751.3	442904	-152.7	1	52.4 $4d^{7}4f(^{4}F)^{3}D + 12.8 4d^{7}4f(^{4}f)^{3}P + 9 4d^{7}4f(^{2}H)^{3}D$					
443097.1	443434	-336.9	1	49.3 4d ⁷ 4f (⁴ F) ⁵ D + 32.2 4d ⁷ 4f (⁴ P) ⁵ D + 7.5 4d ⁷ 4f (⁴ F) ⁵ P					
444346	443535	811	5	43.6 4d' 4f (4 F) 3 H + 13.7 4d' 4f (4 F) 3 G + 11.1 4d' 4f (2 G) 3 G					
445014	444588	426 574	3	21.2 4d 4f (F) $^{\circ}D + 32.1$ 4d 4f (F) $^{\circ}D + 9.9$ 4d 4f (F) $^{\circ}G$ 20.3 4d 7 4f (^{2}P) $^{3}F + 13.3$ 4d 7 4f (^{2}D) $^{3}F + 10.4$ d 7 4f (^{4}P) ^{5}D					
450428	451273	-845	2	23.5 4d 4f (1) F + 10.5 4d 4f (D) F + 10 4d 4f (1) D 21.1 4d ⁷ 4f (⁴ F) ³ P + 24.6 4d ⁷ 4f (² H) ¹ D + 17 4d ⁷ 4f (⁴ F) ³ D					
453642	453098	544	1	$39.3 4d^{7}4f(^{2}P) ^{3}D + 13.1 4d^{7}4f(^{4}F) ^{3}P + 8.5 4d^{7}4f(^{4}F) ^{3}S$					
454009	454778	-769	4	$17.2 4d^{7}4f (^{2}H) ^{3}G + 16.3 4d^{7}4f (^{2}H) ^{3}F + 15.6 4d^{7}4f (^{2}G) ^{3}H$					
454321	455487	-1166	2	$31.3 4d^74f (^2\text{H}) \ ^3\text{F} + 16.3 \ 4d^74f (^2\text{G}) \ ^3\text{F} + 13.6 \ 4d^74f (^4\text{P}) \ ^3\text{D}$					
456827	456867	-40	4	19.2 4d' 4f (² P) ³ F + 13.5 4d' 4f (² H) ³ G + 10.1 4d' 4f (² P) ⁴ G					
457848	457450 458581	392 522	3 4	15.1 4d 4f (H) F + 11.6 4d 4f (P) D + 8 4d 4f (P) G 14.8 $4d^{7}4f(^{2}C)$ ^{3}C + 19.5 $4d^{7}4f(^{2}P)$ ^{3}C + 12.2 $4d^{7}4f(^{4}P)$ ^{5}C					
458311	458001 459004	-693	1	29.6 $4d^{7}4f({}^{4}F){}^{3}S + 17.9 4d^{7}4f({}^{2}G){}^{3}D + 11.2 4d^{7}4f({}^{2}F){}^{3}S$					
459774	459039	735	4	25.2 $4d^{7}4f(^{2}D)$ $^{3}F + 24.1 4d^{7}4f(^{2}G)$ $^{1}G + 10.5 4d^{7}4f(^{2}D)$ ^{3}F					
460440	460262	178	4	23.2 $4d^{7}4f(^{2}H)^{3}F + 18.9 4d^{7}4f(^{2}G)^{3}F + 16.6 4d^{7}4f(^{2}H)^{3}G$					
460841	461582	-741	1	$35.9 \ 4d^7 4f \ (^2G) \ ^3D + 17.2 \ 4d^7 4f \ (^2G) \ ^3P + 9.4 \ 4d^7 4f \ (^4F) \ ^3S$					
461717	461617	100	4	12.3 4d' 4f (2 D) 3 G + 17.6 4d' 4f (2 G) 3 H + 15.4 4d' 4f (2 P) 3 F 21.2 4d ⁷ 4f (2 P) 1 D + 15.2 4d ⁷ 4f (4 P) 3 E + 12.5 4d ⁷ 4f (2 C) 3 D					
465968	464881	1087	2	$39.4 4d^74f (^4P) ^5F + 10.6 4d^74f (^2G) ^1D + 8.7 4d^74f (^2D) ^1D$					
465777	465436	341	4	$14.7 4d^7 4f (^2 \text{H}) ^3 \text{H} + 23.7 4d^7 4f (^4 \text{P}) ^3 \text{F} + 17.9 4d^7 4f (^2 \text{P}) ^1 \text{G}$					
465997	466345	-348	1	$35.9 4d^{7}4f(^{2}\text{D}) ^{1}\text{P} + 27.3 4d^{7}4f(^{2}\text{F}) ^{1}\text{P} + 9.6 4d^{7}4f(^{2}\text{G}) ^{1}\text{P}$					
468330	467632	698	3	$4.9 \ 4d^{7}4f(^{2}D) \ ^{3}D + 15 \ 4d^{7}4f(^{4}P) \ ^{5}F + 13.8 \ 4d^{7}4f(^{4}P) \ ^{3}F$					
470177	470011	166	4	22.2 4d' 4f (² P) ³ G + 12.7 4d' 4f (² D) ¹ G + 9.7 4d' 4f (² P) ¹ G					
470312	470998	-686	3	$38.7 \text{ 4d} \cdot 4f (^{2}P) \circ F + 9.5 \text{ 4d} \cdot 4f (^{2}D) \circ G + 9 \text{ 4d} \cdot 4f (^{2}P) \circ G$ 27.2 $4d^{7}4f (^{2}D) \circ 3P + 25.5 4d^{7}4f (^{2}D) \circ 3P + 11.0 4d^{7}4f (^{4}P) \circ 3P$					
471669	472484	-1331	1	33.9					
480137	478704	1433	5	51.8 $4d^{7}4f(^{2}F)^{3}I + 18.9 4d^{7}4f(^{2}H)^{3}I + 6 4d^{7}4f(^{2}H)^{1}H$					
478443	478844	-401	3	$15.5 4d^{7}4f(^{2}\text{D}) \ ^{3}\text{D} + 12.2 \ 4d^{7}4f(^{2}\text{H}) \ ^{3}\text{D} + 11.1 \ 4d^{7}4f(^{2}\text{F}) \ ^{3}\text{D}$					
480376	479822	554	2	$13.5 \text{ 4d}^{7} \text{4f} (^{2}\text{D}) ^{1}\text{D} + 13.5 \text{ 4d}^{7} \text{4f} (^{2}\text{F}) ^{3}\text{F} + 12.5 \text{ 4d}^{7} \text{4f} (^{2}\text{F}) ^{1}\text{D}$					
479867	480712	-845	3	$36.6 4d' 4f (^2F) ^3G + 22.2 4d' 4f (^2F) ^3F + 5.2 4d' 4f (^2H) ^3G$					
482000 482451	481649 481884	351 567	э 4	42.1 4d 4f (F) $G + 8.7$ 4d 4f (F) $H + 7.4$ 4d op (F) G 15.2 4d ⁷ 4f (² F) $^{3}H + 18.9$ 4d ⁷ 4f (² F) $^{1}G + 14.7$ 4d ⁷ 4f (² D) ^{3}H					
481700	482657	-957	2	$57.9 \ 4d^{7}4f(^{2}F)^{3}F + 5.7 \ 4d^{7}4f(^{2}H)^{3}F + 5 \ 4d^{7}4f(^{2}D)^{3}F$					
482984	482983	1	3	$30.7 4d^{7}4f(^{2}\text{H}) ^{3}\text{D} + 16.3 4d^{7}4f(^{2}\text{F}) ^{3}\text{F} + 7.1 4d^{7}4f(^{4}\text{F}) ^{3}\text{D}$					
485789	484606	1183	5	$28.3 4d^{7}4f (^{2}\text{F}) \overset{3}{}_{1}\text{H} + 11.8 4d^{7}4f (^{2}\text{H}) \overset{3}{}_{1}\text{H} + 11.7 4d^{7}4f (^{2}\text{D}) \overset{3}{}_{2}\text{H}$					
484659	485333	-674	2	19.6 4d ⁷ 4f (² D) ¹ D + 19.2 4d ⁷ 4f (² F) ¹ D + 17.5 4d ⁷ 4f (² F) ³ D					
492097	492563	-466	5	$3.6 \text{ 4d}^{-}4\text{f}(^{-}\text{H})^{-}\text{G} + 20.9 \text{ 4d}^{-}4\text{f}(^{-}\text{F})^{-}\text{G} + 17.6 \text{ 4d}^{-}4\text{f}(^{-}\text{P})^{-}\text{G}$					
494801	494092	266	2	$8.4 \text{ 4d}^7 \text{4f} (^2 \text{G}) ^3 \text{F} + 11.9 \text{ 4d}^7 \text{4f} (^4 \text{F}) ^3 \text{F} + 10.5 \text{ 4d}^7 \text{4f} (^2 \text{F}) ^3 \text{P}$					
495623	495868	-245	3	$28.7 4d^{7}4f (^{2}\text{H}) {}^{1}\text{F} + 10.6 4d^{7}4f (^{4}\text{F}) {}^{3}\text{F} + 8.4 4d^{7}4f (^{2}\text{G}) {}^{3}\text{F}$					
496515	497749	-1234	4	11.3 $4d^{7}4f(^{4}P)^{3}G + 14.9 4d^{7}4f(^{2}D)^{3}H + 14.3 4d^{7}4f(^{4}F)^{3}G$					
497593	497904	-311	3	$18.1 \ 4d^{7}_{4} 4f \ (^{2}_{F}) \ ^{3}_{5} D + 14.5 \ 4d^{7}_{4} 4f \ (^{2}_{F}) \ ^{1}_{F} F + 10.6 \ 4d^{7}_{4} 6p \ (^{4}_{F}) \ ^{3}_{5} D$					
498091	498710	-619	3	$37.2 \text{ 4d}' 6p ({}^{4}\text{F}) {}^{3}\text{F} + 39.6 \text{ 4d}' 6p ({}^{4}\text{F}) {}^{3}\text{D} + 5 \text{ 4d}' 6p ({}^{4}\text{F}) {}^{3}\text{F}$					
500115 504304	499643 503572	472	5	42.4 4d ⁻⁴ f(⁻ D) ^o H + 15 4d ⁻⁴ f(⁻ F) ^o H + 11.9 4d ⁻⁴ f(⁻ D) ^o H 41.7 4d ⁷ 6p (⁴ F) ⁵ F + 20.8 4d ⁷ 6p (⁴ F) ⁵ C + 13.2 4d ⁷ 6p (⁴ F) ³ C					
505151	505298	-147	4	$23.4 \ 4d^74f \ (^2D) \ ^1G + 12 \ 4d^74f \ (^2H) \ ^1G + 11.9 \ 4d^74f \ (^2G) \ ^1G$					
506788	506159	629	3	17.6 $4d^{7}4f$ (² D) ³ F + 19.3 $4d^{7}6p$ (⁴ F) ⁵ F + 15.1 $4d^{7}6p$ (⁴ F) ³ F					
506753	507197	-444	4	50.7 4d ⁷ 6p (⁴ F) 3 G + 20.8 4d ⁷ 6p (⁴ F) 5 G + 9.3 4d ⁷ 4f (² D) 3 G					
510338	509837	501	4	$34.6 \text{ 4d}' 4f (^{2}\text{D}) {}^{3}\text{F} + 14.8 \text{ 4d}' 4f (^{2}\text{D}) {}^{3}\text{F} + 14 \text{ 4d}' 4f (^{2}\text{D}) {}^{3}\text{G}$					
511308 510313	510572 512017	736	5	33.7 4d 6p (2 F) 3 G + 12.8 4d 4f (2 D) 3 G + 12.3 4d 6p (2 C) 3 C + 13.6 4d 7 4f (2 D) 3 C + 12.3 4d 7 6p (2 C) 1 H					
510313 512945	512617 512680	265	3	$28.4 4d^{7}4f^{(2)} + 16.6 4d^{7}6p^{(4F)} + 3G + 15.7 4d^{7}4f^{(2)} + 3G$					
513093	512729	364	4	25.9 $4d^{7}4f(^{2}D)^{3}G + 22 4d^{7}6p(^{2}G)^{3}F + 6.3 4d^{7}4f(^{2}D)^{3}G$					
513229	513045	184	4	$35.7 4d_{0}^{7}6p (^{2}\text{G}) ^{3}\text{F} + 16.4 4d_{0}^{7}4f (^{2}\text{D}) ^{3}\text{G} + 9 4d_{0}^{7}6p (^{2}\text{G}) ^{3}\text{G}$					
513638	513584	54	4	$62.9 \ 4d^{0}5s5p \ (^{3}D) \ 'F + 24 \ 4d^{0}5s5p \ (^{3}D) \ 'P$					
512690	513904	-1214	2	71.9 $4d^{\circ}5s5p$ (°D) 'F					
514520 515813	514458 516591	-778	3 4	$31.8 4d^{7}6p (^{2}G) ^{3}H + 30.9 4d^{7}6p (^{2}G) ^{3}G + 12.8 4d^{7}6p (^{2}G) ^{3}F$					
517431	517357	74	4	$53.9 \ 4d^{6}5s5p \ (^{5}D) \ ^{7}P + 21 \ 4d^{6}5s5p \ (^{5}D) \ ^{7}D + 18.3 \ 4d^{6}5s5p \ (^{5}D) \ ^{7}F$					
518987	520141	-1154	5	82.8 $4d^{7}6p$ (² H) ³ G + 9.2 $4d^{7}6p$ (² H) ³ H					
522188	521267	921	5	33 4d ⁷ 6p (² G) ¹ H + 35.5 4d ⁷ 6p (² G) ³ H + 5.8 4d ⁷ 4f (² F) ¹ H					
523207	522055	1152	4	38 4d $^{\circ}$ 6p ($^{\circ}$ G) $^{\circ}$ G + 32.2 4d $^{\circ}$ 6p ($^{\circ}$ G) $^{\circ}$ G + 9.5 4d $^{\circ}$ 6p ($^{\circ}$ G) $^{\circ}$ H					
524913	522979 525538	-428 -625	э 5	20.4 4u (1) $n + 10.7 4d$ (1) $n + 9 4d$ (1) $ -$					
526265	525629	636	4	$58.3 \ 4d^{7}6p \ (^{2}D) \ ^{3}F + 20.7 \ 4d^{7}6p \ (^{2}D) \ ^{3}F + 11.9 \ 4d^{7}6p \ (^{4}P) \ ^{5}D$					
526016	525900	116	2	$16.1 4d^{7}6p (^{2}\text{D}) ^{3}\text{F} + 15.4 4d^{7}6p (^{4}\text{P}) ^{3}\text{D} + 12.6 4d^{7}6p (^{2}\text{P}) ^{3}\text{P}$					
526056	526418	-362	5	45.7 $4d^{6}_{5}s5p$ $\binom{5}{2}D$ $\frac{5}{2}F$ + 36 $4d^{6}_{5}s5p$ $\binom{5}{2}D$ ^{5}F + 9.8 $4d^{6}_{5}s5p$ $\binom{5}{2}D$ ^{7}F					
527054	527469	-415	3	$30.6 \ 4d^{\circ}5s5p \ (^{\circ}D) \ ^{\circ}F + 22.2 \ 4d^{\circ}5s5p \ (^{\circ}D) \ ^{\circ}F + 10 \ 4d^{\circ}5s5p \ (^{\circ}D) \ ^{\circ}D$					
531754 537080	531989 538376	-235	5 2	52.7 4d 6p ($^{\circ}$ H) $^{\circ}$ H + 24.8 4d 6p ($^{\circ}$ H) $^{\circ}$ H + 9.4 4d 6p ($^{\circ}$ G) $^{\circ}$ G 70.3 4d 7 6p (2 F) 3 G + 7.1 4d 7 6p (2 F) 3 F + 5.2 4d 7 6p (2 F) 1 F					
538218	539206	-390	2	$22.7 \ 4d^{6}5s5p \ (^{3}F) \ ^{5}F + 16.2 \ 4d^{6}5s5p \ (^{3}D) \ ^{5}F + 8.2 \ 4d^{6}5s5p \ (^{4}F) \ ^{5}F$					
				a: From Ryabtsev [37]					
				b: This work					
			-	A THE AND A THE					
			c:	210^{10} s $^{5\%}$ are given					
0010 112	Wavelength	Lower Level ^a	.J.	Upper level ^a	Ju	log of	o A	CF	111 11
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	Å	cm ⁻¹	^o Low	cm ⁻¹	Up	105 51	s ⁻¹	01	Í
	207.046	0	4	482984	3	-0.23	9.21E + 10	0.389	l l
	207.469	õ	4	482000	5	-0.69	3.17E + 10	0.114	1
	209.011	0	4	478443	3	-0.4	6.12E + 10	0.303	Í
	209.855	6465	3	482984	3	-0.91	1.87E + 10	0.116	Í
	211.244	6465	3	479853	2	-0.88	1.98E + 10	0.194	1
	293.695	25866	4	366355	3	-0.29	3.97E + 10	0.464	1
	293.838	15161	2	355484	2	-0.89	9.87E+09	0.183	Í
	290.337	8154	2	343097	1	-0.98	$9.14E \pm 09$	0.221 0.225	1
	298.655	20649	1	355484	2	-0.68	1.58E+10	0.6	1
	299.845	25866	4	359371	3	-0.85	1.05E + 10	0.349	Í
	300.997	23255	2	355484	2	-0.78	1.22E + 10	0.298	Í
	304.794	0	4	328091	4	-0.95	8.03E + 09	0.208	1
	305.84	23255	2	350224	3	-0.67	1.53E+10	0.326	1
	307.857	25866	4	324820	3	-0.00	1.54E + 10 9.17E + 10	0.171	l l
	309.065	6465	3	3300224	2	-0.98	7.39E+09	0.313 0.145	l l
	309.196	8154	2	331573	1	-0.94	8.11E + 09	0.116	Í
	309.361	20649	1	343897	2	-0.56	1.90E + 10	0.434	Í
	309.919	20607	0	343272	1	-0.66	1.52E + 10	0.44	Í
	310.948	15161	2	336758	3	-0.23	4.03E+10	0.52	1
	311.373	0 22255	4	320950	3	-0.48	2.27E+10 1.57E+10	0.343 0.283	Í
	312.237	0	4	320270	3	-0.31	3.34E+10	0.253 0.354	l l
	312.903	õ	4	319588	5	-0.62	1.62E + 10	0.471	1
	313.031	20649	1	340107	0	-0.91	8.37E + 09	0.718	Í
	313.481	8154	2	327153	2	-0.78	$1.13E{+}10$	0.351	l l
	313.555	23255	2	342179	3	-0.41	2.63E+10	0.312	l l
	313.574	20649	1	339553	1	-0.61	1.65E + 10 2.20E + 10	0.517	1
	314.089	15161	2	333541	3	-0±/	$6.82E \pm 09$	0.113	1
	314.109	6465	3	324826	3	-0.76	1.17E + 10	0.202	1
	314.337	6465	3	324596	2	-0.43	$2.49E{+}10$	0.61	1
	314.344	8154	2	326277	3	-0.73	1.26E + 10	0.175	l l
	314.571	6465	3	324359	2	-0.62	1.62E+10	0.352	Í
	315.301	0405	3	323302	4	-0.64	1.53E + 10 1.47E + 10	0.38	1
	315.703	6465	3	323219	3	-0.2	4.20E+10	0.295 0.445	l l
	316.014	8154	2	324596	2	-0.86	9.21E+09	0.199	Í
	316.143	25866	4	342179	3	-0.32	3.20E + 10	0.56	Í
	316.158	23255	2	339553	1	-0.52	2.02E+10	0.421	l l
	316.251	8154	2	324359	2	-0.16	4.58E+10	0.428	l l
	316.47	0	4	315986	3	-0.81	1.03E + 10 1.47E + 10	0.434	l l
	317 053	8154	2	323559	2	-0.76	$1.47E \pm 10$ $1.16E \pm 10$	0.310 0.239	1
	317.216	20649	1	335892	2	-0.72	1.26E + 10	0.684	Í
	317.252	0	4	315207	5	0.24	1.16E + 11	0.75	Í
	317.395	8154	2	323219	3	-0.98	7.02E + 09	0.158	l l
	317.428	6465	3	321497	4	0.1	8.29E+10	0.749	1
	317.502	6465 15161	3	321424	2	-0.44	2.38E + 10 5 10E + 10	0.499	Í
	318 092	8154	2	322529	2	-0.11	$2.98E \pm 10$	0.625	l l
	318.67	6465	3	320270	3	-0.81	1.02E + 10	0.227	Í
	318.986	0	4	313493	4	-0.65	1.46E + 10	0.469	Í
	319.346	23255	2	336395	1	-0.2	4.13E + 10	0.506	i i
	319.697	8154	2	320950	3	-0.92	7.79E + 09	0.376	1
	319.86	23255	2	335892	2 5	-0.55	1.86E+10 6.74E+10	0.22	l l
	320.26	6465	3	318711	4	-0.7	1.31E+10	0.33 0.29	Í
	320.322	6465	3	318651	3	-0.27	3.53E + 10	0.654	1
	320.394	8154	2	320270	3	-0.46	2.24E + 10	0.509	Í
	320.521	15161	2	327153	2	-0.89	8.33E + 09	0.15	1
	321.423	15161	2	326277	3	-0.41	2.51E+10	0.44	Í
	321.458	15161	2	326244	1	-0.44	2.36E + 10 2.40E + 10	0.381	1
	321.988	23255	4	310571	4	0.27	1.07E+11	0.402 0.636	l l
	322.065	8154	2	318651	3	-0.43	2.40E + 10	0.231	Í
	322.776	6465	3	316277	2	-0.75	1.14E + 10	0.214	Í
	322.929	15161	2	324826	3	-0.98	6.71E+09	0.203	1
	323.08	6465 15161	3	315986	3	-0.67	1.36E + 10	0.2	1
	324 22	0	4	308432	3	-0.26	$3.48E \pm 10$	$0.111 \\ 0.466$	1
	324.853	8154	2	315986	3	-0.63	1.47E + 10	0.204	l l
	325.018	25866	4	333541	3	-0.71	1.23E + 10	0.278	Í
	325.332	23255	2	330633	3	-0.08	5.27E + 10	0.623	1
	325.752	25866	4	332848	4	-0.2	3.99E+10	0.622	l l
	325.98	23255	2	330022	2	-0.77	1.06E + 10	0.15	l l
	327.131	6465	3	312153	2	-0.71	1.22E+10	0.092 0.273	ĺ
	327.915	15161	2	320118	1	-0.66	1.37E + 10	0.184	1
	328.119	25866	4	330633	3	-0.7	1.25E + 10	0.577	l
	328.123	20607	0	325371	1	-0.73	1.14E + 10	0.369	1
	328.398	25866	4	330375	5	-0.48	2.04E+10	0.713	1
	328.462	U 9154	4	304449	3	-0.42	2.34E+10 0.36E+00	0.199	1
	320.948 329.005	0104 20649	1	312133 324596	2	-0.82	9.30E+09 7.32E+09	0.133	1
	329.975	0	4	303053	$\frac{2}{4}$	-0.63	1.45E+10	0.159	l i
	330.045	23255	2	326244	1	-1	6.19E + 09	0.138	ĺ
	330.418	8154	2	310801	1	-0.68	1.27E+10	0.287	1
	331.162	6465	3	308432	3	-0.82	9.15E+09	0.091	1
	332.016	6465	3	307655	2	-0.82	9.16E + 09	0.122	1
	332.103	10101	4	301111	2 3	-0.00	$7.32E \pm 09$	0.234 0.197	
	332.542	8154	2	308868	2	-0.89	7.77E + 0.09	0.12	ĺ
	333.516	0	4	299836	4	-0.37	2.57E + 10	0.32	ĺ
	333.925	20649	1	320118	1	-0.61	1.46E + 10	0.314	j –

Table A21: Computed oscillator strengths and transition probabilities in In VI.

Table A21: Continued

Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA	CF
334.977	25866	4	324394	5	-0.69	1.21E+10 1.06E+10	0.641
335.589	6465	3	304449	3	-0.66	1.29E+10 1.29E+10	0.435
335.913	25866	4	323562	4	-0.91	7.22E + 09	0.173
337.468	15161	2	311485	3	-0.97	6.24E+09	0.196
337.502	8154	2	304449	3 5	-0.92	7.05E+09 1.20E+10	0.214
340.981	15161	2	308432	3	-0.84	8.32E+09	0.262
345.676	15161	2	304449	3	-0.86	7.69E + 09	0.121
855.235	248694	4	365620	4	-0.92	1.10E + 09	0.514
875.549	201884 231742	5 6	316098	4	-0.71	1.70E+09 1.67E+09	0.418
947.498	226765	4	332306	4	-0.95	8.39E+08	0.136
947.627	205958	4	311485	3	-0.47	2.54E + 09	0.506
950.444	211178	2	316392	1	-0.9	9.31E + 08	0.602
955.029	237470	2	342179	3	-0.99	7.50E + 08 7.12E + 08	0.082
968.715	233903	5	337133	4	-0.53	2.12E+0.09	0.184
968.96	238975	4	342179	3	-0.91	8.76E + 08	0.38
969.848	211178	2	314287	1	-0.96	7.78E + 08	0.447
971.561	209226	3	312153	2	-0.74	1.30E + 09 7.46E + 08	0.36
974.366	228284	1	330915	1	-0.85	9.83E+08	0.304
974.427	221971	1	324596	2	-0.95	7.96E + 08	0.16
977.91	209226	3	311485	3	-0.81	1.09E + 09	0.444
979.023	234616	3	336758	3	-0.89	9.02E + 08 8.20E + 08	0.657
979.593	237470	2	339553	1	-0.84	9.99E+08	0.272
981.587	219074	3	320950	3	-0.43	2.58E + 09	0.568
983.043	272271	3	373995	3	0.15	9.80E + 09	0.686
984.931	248694	4	350224	3	-0.82	1.04E + 09	0.529
987.519	219006	2	320270	3	-0.85	9.13E+08	0.431
989.361	240990	5	342065	4	-0.93	8.04E + 08	0.437
993.417	220287	3	320950	3	-0.44	2.44E + 09	0.699
995.294	269705	1	370178	1	-0.49	2.17E + 09 1.44E + 00	0.718
998.64	230497	3	330633	3	-0.91	$1.44E \pm 0.09$ $8.32E \pm 0.08$	0.472
999.56	269705	1	369749	2	-0.38	2.77E + 09	0.802
1002.791	211178	2	310899	3	-0.82	1.01E + 09	0.376
1004.447	234616	3	334173	2	-0.93	7.80E + 08	0.176
1004.775	230497 238975	3 4	338400	5	-0.92	2.36E+0.9	0.395
1008.689	233168	4	332306	4	-0.03	6.09E + 09	0.737
1010.52	209226	3	308185	4	-0.44	2.40E + 09	0.352
1010.858	234616	3	333541	3	-0.88	8.61E+08	0.381
1010.803	233207	2	331952	2	-0.87	$8.93E \pm 08$	0.195
1015.599	212337	1	310801	1	-0.61	1.60E + 0.09	0.762
1016.034	237470	2	335892	2	-0.78	1.08E + 09	0.138
1016.226	233903	5	332306	4	-0.4	2.59E + 09	0.633
1018.342	205958	4	304157 337133	5 4	-0.21	4.00E+09	0.372
1018.813	231742	6	329895	6	-0.47	2.20E + 0.09	0.812
1019.775	226765	4	324826	3	-0.94	7.42E + 08	0.308
1020.245	237876	1	335892	2	-0.62	1.53E+09 1.20E+00	0.511
1020.907	201884 245366	2	343272	4	-0.69	1.30E+09 1.72E+09	0.164 0.364
1021.656	219006	2	316886	3	0.08	7.66E + 09	0.709
1022.541	246405	3	344201	4	-0.38	2.69E + 09	0.342
1022.675	238975	4	336758	3	-0.28	3.36E + 09 8.17E + 08	0.707
1022.885	245509	6	329406	6	-0.89	1.64E+10	0.649
1024.293	226765	4	324394	5	-0.43	2.37E + 09	0.164
1025.733	246405	3	343897	2	-0.31	3.11E + 09	0.381
1025.955	228807	2	326277	3	-0.88	8.44E + 08 1.62E + 10	0.301
1026.843	219006	2	316392	1	-0.75	$1.03E \pm 10$ $1.12E \pm 09$	0.724 0.297
1027.826	245979	2	343272	1	-0.52	1.90E + 09	0.483
1028.231	211178	2	308432	3	-0.44	2.32E + 09	0.731
1028.773	219074	3	316277 311485	2	-0.72	1.21E+09 8 30E+08	0.286
1030.672	219074	3	316098	4	0.03	6.74E+09	0.581
1031.11	221971	1	318954	2	-0.54	1.80E + 09	0.367
1032.578	253379	3	350224	3	0.2	1.00E+10	0.778
1032.8	225122 233207	5 2	321947 330022	52	-0.24 -0.67	3.59E+09 1.33E±09	0.476
1032.923	245366	2	342179	3	-0.61	1.54E + 0.09	0.26
1033.088	226765	4	323562	4	-0.26	3.47E + 09	0.312
1034.094	237470	2	334173	2	-0.66	1.38E+09	0.278
1035.929	212337 211178	1 2	308868 307655	2	-0.5 -0.53	1.96E+09 1.86E±09	0.542
1036.571	233903	5	330375	5	0.41	1.61E + 10	0.735
1036.767	226765	4	323219	3	-0.65	1.37E + 09	0.181
1038.068	234582	1	330915	1	-0.79	1.01E + 09	0.351
1038.250	∠19006 228284	2	313321 324596	2	-0.62 -0.52	1.49E+09 1.88E+09	0.326
1039.43	214364	4	310571	4	-0.61	1.51E + 09	0.198
1039.505	245979	2	342179	3	-0.15	4.35E + 09	0.686
1040.923	222582	2	318651	3	-0.7	1.23E+09	0.322
1041.459	233903	$\frac{2}{5}$	329895	3 6	-0.30	2.70E+09 8.20E+08	0.04
1042.471	269705	1	365631	1	-0.35	2.74E + 0.09	0.761
1043.319	245366	2	341214	3	-0.15	4.32E + 09	0.759
1043.721	220287	3	316098	4	0.05	6.86E+09	0.795
1044.06	230497 220287	э 3	315986	а 3	-0.85	$1.30E \pm 0.09$ 8.71E \pm 0.8	0.470
1045.065	245366	2	341054	2	-0.67	1.32E + 09	0.244
1045.373	246405	3	342065	4	0.16	8.92E+09	0.822
1047.028	201884	5 1	297392	6 4	0.57	2.26E+10 7.51E→ 00	0.91
1047.058	230738	0	326244	1	-0.81	9.48E+08	0.252
1047.083	233903	5	329406	6	-0.05	5.44E + 09	0.883
1047.729	248694	4	344138	5	0.43	1.64E + 10	0.846
1047.778	201884	5	297246	$\frac{2}{5}$	-0.11	4.72E+09	0.259

Table A21: Continued

Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA 6.04E+08	CF 0.126
1050.034	245979 209226	2	341214 304449	3	-1	1.51E+09	$0.126 \\ 0.498$
1050.625	226765	4	321947	5	-0.6	1.52E + 09	0.103
1051.803	245979	2	341054	2	-0.29	3.10E+09	0.62
1054.754	246405 228807	3	341214 323559	3	-0.06	5.18E+09 6.47E+08	$0.462 \\ 0.134$
1056.54	246405	3	341054	2	-0.81	9.32E + 08	0.178
1057.109	245509	1	340107	0	-0.76	1.03E + 09	0.752
1058.586	225122	5	319588	5	0.16	8.57E + 09	0.693
1060.122	230497 221971	3	324826 316277	3 2	-0.53 -0.45	1.75E+09 2.12E+09	$0.595 \\ 0.767$
1061.065	228284	1	322529	1	-0.91	7.28E + 08	0.166
1061.719	245366	2	339553	1	-0.68	1.23E + 09	0.443
1062.662	237470	2	331573	1	-0.4	2.38E+09	0.66
1062.969	245509	1	339553	1	-0.75	2.38E+09	0.253 0.767
1065.211	205958	4	299836	4	-0.2	3.69E + 09	0.336
1065.274	238975	4	332848	4	0.23	9.87E + 09	0.75
1065.397	230497	3	324359	2	-0.18	3.89E + 09 5.24E + 00	0.774 0.765
1065.864	214364	4	308185	4	-0.78	9.70E+08	$0.705 \\ 0.515$
1066.986	228807	2	322529	1	-0.98	6.15E + 08	0.261
1068.504	225122	5	318711	4	-0.3	2.92E + 09	0.324
1069.688	248694	4	342179	3	-0.25	3.23E+09 1 32E+10	0.718
1071.238	272271	3	365620	4	0.35 0.37	1.36E+10 1.36E+10	0.853
1071.238	221971	1	315321	2	-0.97	6.19E + 08	0.1
1073.381	237470	2	330633	3	-0.39	2.38E + 09	0.772
1074.462	233207	2	326277	3	-0.84	$8.36E \pm 08$	0.28
1074.510	230497	3	323559	2	-0.1	2.11E+09	0.807
1076.869	228284	1	321146	1	-0.97	6.14E + 08	0.225
1077.322	226765	4	319588	5	-0.31	2.81E + 09	0.429
1078.496	230497	3 5	323219	3	-0.23	$3.42E \pm 09$ 1 56E \pm 10	0.664
1079.718	228807	$\frac{3}{2}$	321424	2	-0.46	1.97E+09	0.35
1080.254	234582	1	327153	2	-0.73	1.07E + 09	0.369
1080.646	234616	3	327153	2	-1	5.74E + 08	0.226
1081.327	219006	2	311485 331573	3	-0.96	6.20E + 08 1.06E + 09	0.146
1082.073	219074	3	311485	3	-0.25	3.23E+09	0.702
1082.968	228807	2	321146	1	-0.66	1.25E + 09	0.374
1083.244	221971	1	314287	1	-0.65	1.27E + 09	0.5
1085.271	228807	2	320950	3	-0.3	2.84E+09 6 10E+09	0.461
1087.335	226765	4	318651	3	-0.17	3.86E+09	0.786
1088.313	209226	3	301111	3	-0.63	1.32E + 09	0.157
1088.926	228284	1	320118	1	-0.68	1.17E + 09	0.364
1089.023	219074 230738	3	310899	3	-0.69	1.15E+09 6.45E+08	0.639
1089.837	239158	0	330915	1	-0.96	6.19E + 08	0.641
1090.459	222582	2	314287	1	-0.96	6.14E + 08	0.437
1091.011	238975	4	330633	3	-0.26	3.11E + 09	0.703
1091.48	233207 219074	2	310571	4	-0.14	$4.01E \pm 0.09$ $6.17E \pm 0.08$	0.651
1094.097	238975	4	330375	5	-0.65	1.26E + 0.09	0.814
1094.231	233207	2	324596	2	-0.77	9.46E + 08	0.149
1095.09	240990	5	332306	4	-0.03	5.20E + 09 0.51E + 00	0.634
1095.434	233168	4	324394	5	0.23	1.27E+10	0.858
1096.812	231742	6	322915	7	0.63	2.34E + 10	0.933
1097.618	269705	1	360811	0	-0.57	1.48E + 09	0.877
1098.55	245366 253370	2	336395	1	-0.64	1.26E+09 3.41E+09	0.688
1101.46	234582	1	325371	1	-0.59	1.41E+09	0.325
1101.576	245979	2	336758	3	-0.38	2.28E + 09	0.457
1102.897	228284	1	318954	2	-0.47	1.84E + 09	0.355
1103.629	209226 245366	3	299836 335892	4	-0.11	4.25E+09 3.17E+09	0.839
1104.751	253379	3	343897	2	-0.23	3.23E+09	0.806
1105.998	245979	2	336395	1	-0.59	1.41E + 09	0.531
1106.102	230738	0	321146	1	-0.85	7.70E + 08	0.334
1106.20	246405	4 3	336758	4 3	-0.19	1.41E+09	0.555
1107.618	220287	3	310571	4	-0.82	8.19E + 08	0.695
1108.518	234616	3	324826	3	-0.96	6.02E+08	0.119
11109.296	228807 214364	2	318954 304449	2	-0.63 0.13	1.28E+09 7.30E±09	0.3
1110.479	233168	4	323219	3	-0.52	1.63E + 09	0.431
1110.948	225122	5	315136	6	-0.09	4.41E + 09	0.458
1110.968	233207	2	323219	3	-0.98	5.69E+08	0.54
1111.933	211178 219006	2	308868	3 2	-0.81	0.00E+09 8.32E+08	0.881
1113.679	214364	4	304157	5	0.28	1.04E + 10	0.891
1113.871	234582	1	324359	2	-0.46	1.87E + 09	0.757
1113.927	230497	3	320270	3	-0.94	6.21E + 08	0.386
1110.434	222382	∠ 3	308432	∡ 3	-0.51	2.04E+09 1.50E+09	0.35
1120.113	237876	1	327153	2	-0.33	2.45E+09	0.692
1120.817	226765	4	315986	3	-0.4	2.10E + 09	0.355
1122.197	219074	3	308185	4	-0.07	4.49E+09 1.77E+00	0.838
1123.883	234382 240990	1 5	329895	⊿ 6	-0.48	$1.62E \pm 10$	0.320
1124.825	222582	$\tilde{2}$	311485	3 3	-0.92	6.40E + 08	0.24
1126.034	237470	2	326277	3	-0.38	2.19E + 09	0.692
1126.124	253379 214364	3 4	342179 303053	3 4	-1 0.07	5.27E + 08 $6.12E \pm 09$	0.345
1127.569	253379	3	342065	4	-0.13	3.88E+09	0.378
1127.855	245509	1	334173	2	-0.23	3.06E + 09	0.782
1128.906	219074	3	307655	2	-0.6	1.31E + 09	0.538
1128.909	220287 212337	3 1	308868 300851	2	-0.87 -0.87	7.11E+08 $7.13E\pm08$	0.526
1130.093	211178	2	299666	2	-0.95	5.83E+08	0.16
1130.723	248694	4	337133	4	-0.21	3.24E + 09	0.635
1131.007	240990	5	329406	6	-0.88	6.90E+08	0.551
1131.634	237876	1	326244	1	-0.8	8.30E+08	0.344

Table A21: Continued

Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA 6.42E⊥00	CF 0.761
1132.942	205958	4	294224	4	0.14	7.10E+09	0.701 0.714
1133.549	222582	2	310801	1	-0.48	1.71E+09	0.772
1133.576	233207 245366	2	321424 333541	2	-0.93	2.35E+09	$0.126 \\ 0.372$
1134.22	212337	1	300503	1	-0.48	1.74E + 09	0.777
1134.494	220287 228807	3	308432 316886	3	-0.07	4.42E+09 1.34E+09	$0.76 \\ 0.185$
1135.53	248694	4	336758	3	-0.67	1.10E+09	0.442
1135.801	233903	5	321947	5	-1	5.19E + 08	0.093
1136.45	228284 220287	1 3	316277 308185	2	-0.94	$5.98E \pm 08$ $4.21E \pm 09$	$0.215 \\ 0.601$
1139.37	211178	2	298946	2	-0.49	1.67E + 09	0.732
1139.586	219006	2	306757	1	-0.65	1.17E + 09 2.17E + 00	0.508
1140.571	253379	3	341054	2	-0.67	1.12E+09	0.353
1141.629	233903	5	321497	4	0.14	7.01E + 09	0.77
1141.751 1142.067	228807 211178	2	316392 298738	1 2	-0.84 -0.75	7.51E+08 9.04E+08	$0.434 \\ 0.445$
1142.929	237876	1	325371	1	-0.64	1.16E + 0.09	0.527
1144.103	209226	3	296631	3	-0.02	4.85E+09	0.748
1144.581	237470	2	324826	3	-0.39	2.09E+09 7.92E+08	0.703 0.162
1145.088	212337	1	299666	2	-0.32	2.47E + 09	0.874
1145.452	238975 246405	4	326277 333541	3	-0.36 -0.4	2.22E+09 2.01E+09	$0.855 \\ 0.407$
1147.764	237470	2	324596	2	-0.32	2.44E+09	0.494
1148.079	233168	4	320270	3	-0.96	5.50E + 08	0.358
1148.096	239158	3 0	326244	3 1	-0.46 -0.51	1.74E+09 1.57E+09	0.73 0.485
1148.933	228284	1	315321	2	-0.98	5.23E + 08	0.129
1150.613	233207 234616	2	320118	1	-0.75	8.95E+08 1.90E+09	0.299 0.647
1153.028	226765	4	313493	4	-0.84	7.31E+08	0.181
1154.614	212337	1	298946	2	-0.8	8.01E+08	0.287
1155.794	269705 228807	1 2	356226 315321	2	-0.09 -0.55	4.03E+09 1.39E+09	$0.75 \\ 0.615$
1156.829	245509	1	331952	2	-0.61	1.23E + 09	0.468
1156.837	246405	3	332848	4	-0.81	7.66E + 08	0.266
1157.144	201884	5	288304	5	0.33	1.06E+10	0.908
1157.385	212337	1	298738	2	-0.57	1.35E+09	0.522
1158.935	222582 228284	2	$308868 \\ 314566$	2	-0.44 -0.83	1.79E+09 7.44E+08	$0.546 \\ 0.864$
1161.585	237470	2	323559	2	-0.9	6.21E + 08	0.306
1163.156	245979	2	331952	2	-0.4	1.97E+09	0.564
1165.884	203938	4 3	291912 294998	2	-0.08	4.05E+09	0.79
1166.223	233207	2	318954	2	-0.79	8.02E + 08	0.211
1167.065	233903 234616	5	319588 320270	5	-0.81	7.67E+08 5.17E+09	0.311
1168.104	211178	2	296787	1	-0.35	2.18E+09	0.792
1168.951	246405	3	331952	2	-0.98	5.12E+08	0.466
1169.747	233168 230497	4 3	318711 315986	4 3	-0.71	9.51E+08 1.93E+09	0.128 0.367
1169.823	233168	4	318651	3	-0.47	1.65E + 09	0.339
1169.977	214364 211178	4	299836 296631	4	-0.4	1.94E+09 1.54E+09	0.241
1170.296	225122	$\frac{2}{5}$	310571	4	0.06	5.53E+09	0.232
1170.711	238975	4	324394	5	-0.64	1.12E + 09	0.232
1176.5	209226 248694	3 4	294224 333541	4 3	-0.41 -0.57	1.87E+09 1.28E+09	$0.203 \\ 0.548$
1179.131	233903	5	318711	4	-0.73	8.96E + 08	0.178
1180.051	201884 245366	5	286626	4	0.25	8.58E+09 1 32E+09	0.875 0.464
1181.255	245979	2	330633	3	-0.53	1.32E+0.9 1.41E+0.9	$0.404 \\ 0.598$
1181.296	237876	1	322529	1	-0.97	5.07E+08	0.174
1183.249	245509 212337	1	330022 296787	2	-0.78	7.86E+08 7.76E+08	$0.367 \\ 0.238$
1188.292	248694	4	332848	4	-0.73	8.69E + 08	0.796
1189.092	225122	5	309220	5	-0.08	3.92E+09 7 39E+08	0.8 0.254
1192.003	233903	5	317795	6	-0.17	3.19E+09	0.234
1193.033	211178	2	294998	2	-0.6	1.17E + 09	0.206
1193.236	220705 253379	4 3	310371 337133	4 4	-0.37	1.99E+09 2.85E+09	$0.324 \\ 0.592$
1198.107	231742	6	315207	5	0.39	1.13E + 10	0.893
1199.13 1199.816	$231742 \\ 228807$	6 2	$315136 \\ 312153$	6 2	-0.21 -0.75	2.85E+09 8.27E+08	0.842
1201.728	272271	3	355484	2	0.08	5.57E + 0.09	0.88
1202.148	233207	2	316392	1	-0.73	8.58E+08	0.664
1203.805	233207 225122	2 5	308185	4	-1 -0.81	4.07E+08 7.21E+08	0.141 0.707
1204.874	230497	3	313493	4	0.13	6.18E+09	0.689
1205.236	238975 214364	4 4	321947 297246	5	0.24	8.00E+09 2.41E±09	0.741
1203.355	233168	4	315986	3	-0.29	2.32E+09 2.32E+09	0.505
1207.731	237470	2	320270	3	-0.77	7.77E+08	0.177
1209.392	209226	3 2	291912 311485	3 3	-0.66 -0.56	9.97E+08 1.26E+09	0.133
1211.053	240990	5	323562	4	-0.48	1.48E + 09	0.697
1212.783	226765	4	309220	5	0.24	7.90E+09 1 34E - 00	0.643
1214.392	234616	3	316886	3	-0.53	7.40E+09	0.358
1217.821	233207	2	315321	2	-0.97	4.78E + 08	0.287
1220.407 1224.269	$248694 \\ 248694$	4 4	$330633 \\ 330375$	3 5	-0.55 -0.92	1.28E+09 5.38E+08	$0.662 \\ 0.735$
1224.564	234616	3	316277	2	-0.62	1.07E + 09	0.664
1227.039	219006	2	300503	1	-0.85	6.29E+08	0.553
1231.033	233903 237470	2	318651	3	-0.62	1.06E+09	0.619
1235.224	240990	5	321947	5	-0.74	7.97E + 08	0.249
1237.255	220287 253379	3 २	301111 334173	3	-0.62	1.04E+09 9.57E ± 08	0.356
1238.205	219074	3	299836	4	-0.54	1.24E+09	0.645
1238.43	246405	3	327153	2	-0.46	$1.49E{+}09$	0.678
			214				

		TODIO 7	121.001	unuo	u		
Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA	CF
1239.647	205958	4	286626	4	-0.57	1.17E + 09	0.162
1239.769	219006	2	299666	2	-0.59	1.12E + 09	0.501
1240.499	238975	4	319588	5	-0.5	1.36E + 09	0.233
1240.818	219074	3	299666	2	-0.84	6.26E + 08	0.488
1242.12	240990	5	321497	4	-0.29	2.20E + 09	0.884
1244.932	233168	4	313493	4	-0.29	2.20E + 09	0.687
1245.361	245979	2	326277	3	-0.95	4.82E + 08	0.151
1249.024	230738	0	310801	1	-0.98	4.48E + 08	0.524
1250.943	219006	2	298946	2	-0.46	1.49E + 09	0.572
1252.011	219074	3	298946	2	-0.93	5.00E + 08	0.264
1252.199	214364	4	294224	4	-0.72	8.16E + 08	0.327
1254.631	234582	1	314287	1	-0.83	6.23E + 08	0.318
1255.269	219074	3	298738	2	-0.44	1.54E + 09	0.822
1258.346	253379	3	332848	4	-0.63	9.91E + 08	0.654
1259.487	248694	4	328091	4	-0.88	5.50E + 08	0.657
1259.9	228284	1	307655	2	-0.7	8.37E + 08	0.711
1266.981	253379	3	332306	4	-0.95	4.74E + 08	0.475
1267.755	221971	1	300851	0	-0.94	4.81E + 08	0.662
1271.32	220287	3	298946	2	-0.73	7.76E + 08	0.481
1273.374	221971	1	300503	1	-0.68	8.54E + 08	0.47
1273.626	237470	2	315986	3	-0.95	4.63E + 08	0.351
1274.322	228284	1	306757	1	-0.94	4.77E + 08	0.281
1274.679	220287	3	298738	2	-0.81	6.45E + 08	0.404
1282.872	228807	2	306757	1	-0.67	8.82E + 08	0.363
1283.19	225122	5	303053	4	-0.64	9.36E + 08	0.769
1286.644	240990	5	318711	4	-0.51	1.23E + 09	0.301
1287.089	221971	1	299666	2	-0.82	6.10E + 08	0.31
1288.248	219006	2	296631	3	-0.91	4.99E + 08	0.479
1288.932	248694	4	326277	3	-0.86	5.49E + 08	0.537
1289.381	219074	3	296631	3	-0.77	6.87E + 08	0.441
1289.527	214364	4	291912	3	-0.96	4.36E + 08	0.353
1301.853	246405	3	323219	3	-0.83	5.80E + 08	0.374
1301.985	240990	5	317795	6	-0.82	5.92E + 08	0.081
1302.645	221971	1	298738	2	-1	3.93E + 08	0.204
1309.528	222582	2	298946	2	-0.95	4.41E + 08	0.607
1331.703	246405	3	321497	4	-0.67	8.04E + 08	0.536
1338.443	225122	5	299836	4	-0.86	5.18E + 08	0.546
1348.69	240990	5	315136	6	-0.79	5.94E + 08	0.08
1352.459	214364	4	288304	5	-0.43	1.36E + 09	0.33
1352.508	220287	3	294224	4	-0.58	9.66E + 08	0.441
1364.543	245366	2	318651	3	-0.74	6.48E + 08	0.326
1372.908	219074	3	291912	3	-0.99	3.60E + 08	0.603
1383.857	214364	4	286626	4	-0.98	3.66E + 08	0.167
1503.459	248694	4	315207	5	-0.82	$4.44E \pm 08$	0.581

Table A21: Continued

a: Exprimental values taken from [37, 36]

In VII

Energy Levels

Table A22: Comparison between available experimental data and calculated even energy levels (in cm^{-1}) in In VII

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E^a_{exp}	E^{b}_{calc}	ΔE	J	Leading components (in %) in LS coupling c
0	30	-30	4.5	94.1 4d ⁷ (⁴ F) ⁴ F + 5.6 4d ⁷ (² G) ² G
5736	5757	-21	3.5	$98.3 \ 4d^7 \ (^4F) \ ^4F$
10382	10412	-30	1.5	$87.9 4d^7 (^4\text{F}) ^4\text{F} + 7.5 4d^7 (^2\text{D}) ^2\text{D}$
16903	17056	-153	1.5	$60.4 4d^7 (^4\text{P}) ^4\text{P} + 34.2 4d^7 (^2\text{P}) ^2\text{P}$
18509	18288	221	2.5	94.6 $4d^7 (^4P) ^4P$
20666	20638	28	4.5	$75.8 4d^7 (^2\text{G}) ^2\text{G} + 18.7 4d^7 (^2\text{H}) ^2\text{H} + 5.3 4d^7 (^4\text{F}) ^4\text{F}$
21571	21571	0	0.5	$82.2 \text{ 4d}^7 (^4\text{P}) ^4\text{P} + 17.6 \text{ 4d}^7 (^2\text{P}) ^2\text{P}$
26023	25982	41	3.5	$95.5 \text{ 4d}^7 (^2\text{G}) ^2\text{G}$
27420	27556	-136	1.5	$34.2 \text{ 4d}^7 (^2\text{P}) ^2\text{P} + 33.9 \text{ 4d}^7 (^4\text{P}) ^4\text{P} + 22.9 \text{ 4d}^7 (^2\text{D}) ^2\text{D}$
27662	27679	-17	5.5	$99.8 \text{ 4d}^7 (^2 \text{H}) ^2 \text{H}$
30441	30289	152	2.5	$71.2 \text{ 4d}^7 (^2\text{D}) ^2\text{D} + 19.4 \text{ 4d}^7 (^2\text{D}) ^2\text{D}$
33744	33753	-9	4.5	$81 \ 4d^7 \ (^2H) \ ^2H + 18.4 \ 4d^7 \ (^2G) \ ^2G$
39221	39235	-14	1.5	$58.1 \text{ 4d}^7 (^2\text{D}) \ ^2\text{D} + 29.2 \text{ 4d}^7 (^2\text{P}) \ ^2\text{P} + 5 \text{ 4d}^7 (^4\text{P}) \ ^4\text{P}$
41865	41850	15	2.5	$95.5 \text{ 4d}^7 (^2 \text{F}) ^2 \text{F}$
45079	45093	-14	3.5	$96.4 \ 4d^7 \ (^2F) \ ^2F$
66339	66371	-32	1.5	$89.8 \text{ 4d}^7 (^2\text{D}) \ ^2\text{D} + 9.3 \text{ 4d}^7 (^2\text{D}) \ ^2\text{D}$
				a: From Ryabtsev [38]

a: From Ryabtsev [38] b: This work c: Only the component ≥ 5% are given

Table A23: Comparison between available experimental data and calculated odd energy levels (in $\rm cm^{-1}$) in In VII

E^a_{exp}	E^b_{calc}	ΔE	J	Leading components (in $\%$) in LS coupling ^{c}
347961	347613	348	3.5	44.9 $4d^{6}5p$ (⁵ D) ${}^{6}F$ + 21.2 $4d^{6}5p$ (⁵ D) ${}^{4}D$ + 16.2 $4d^{6}5p$ (⁵ D) ${}^{6}P$
348264	348164	100	2.5	56.1 $4d^{6}5p$ (⁵ D) ${}^{6}F$ + 18.7 $4d^{6}5p$ (⁵ D) ${}^{4}D$ + 5.7 $4d^{6}5p$ (⁵ D) ${}^{4}F$
351191	350831	360	4.5	$0.1 \ 4d_{0}^{6}5p \ ({}^{1}G) \ {}^{2}H + 40.4 \ 4d_{0}^{6}5p \ ({}^{5}D) \ {}^{6}F + 27.5 \ 4d_{0}^{6}5p \ ({}^{5}D) \ {}^{4}F$
353170	354663	-1493	3.5	$1.6 \ 4d^{0}5p \ ({}^{3}F) \ {}^{4}D + 31.2 \ 4d^{0}5p \ ({}^{5}D) \ {}^{6}D + 29.4 \ 4d^{6}5p \ ({}^{5}D) \ {}^{6}P$
357547	357404	143	3.5	$34.8 \ 4d^{0}5p \ (^{3}D) \ ^{6}P + 44.3 \ 4d^{0}5p \ (^{3}D) \ ^{4}D + 5.3 \ 4d^{0}5p \ (^{3}D) \ ^{4}F$
358516	358205	311	2.5	$19.8 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}D + 30.5 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}P + 17.6 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}D$
358496	358361	135	4.5	$50 \ 4d^{\circ} \text{5p} (^{\circ} \text{D})^{\circ} \text{F} + 42.8 \ 4d^{\circ} \text{5p} (^{\circ} \text{D})^{\circ} \text{F}$ 24.2 $4d^{\circ} \text{5p} (^{\circ} \text{D})^{\circ} \text{6p} + 20.8 \ 4d^{\circ} \text{5p} (^{\circ} \text{D})^{\circ} 4\text{D} + 14.7 \ 4d^{\circ} \text{5p} (^{\circ} \text{D})^{\circ} 4\text{D}$
361026	361061	35	2.5	$54.5 4d^{6}5p^{(5)} + 16.1 4d^{6}5p^{(5)} $
361620	361647	-27	0.5	$61.6 4d^{6}5p ({}^{5}D) {}^{4}D + 15.2 4d^{6}5p ({}^{5}D) {}^{6}F + 7.1 4d^{6}5p ({}^{3}F) {}^{4}D$
362040	362073	-33	3.5	$64.5 \ 4d^{6}5p \ (^{5}D) \ ^{4}F + 18.5 \ 4d^{6}5p \ (^{5}D) \ ^{6}F + 4.6 \ 4d^{6}5p \ (^{3}G) \ ^{4}F$
363519	363584	-65	2.5	$46.5 \ 4d^{6}5p \ (^{5}D) \ ^{4}P + 20.2 \ 4d^{6}5p \ (^{5}D) \ ^{4}F + 16.3 \ 4d^{6}5p \ (^{5}D) \ ^{6}P$
363801	363757	44	3.5	$13.9 \ 4d^{6}5p \ (^{5}D) \ ^{4}D + 13.8 \ 4d^{6}5p \ (^{3}H) \ ^{4}H + 12.4 \ 4d^{6}5p \ (^{3}H) \ ^{2}G$
363857	363941	-84	2.5	$47.1 \ 4d^{6}5p(^{5}D) \ ^{4}F + 18 \ 4d^{6}5p(^{5}D) \ ^{4}P + 10.5 \ 4d^{6}5p(^{5}D) \ ^{6}F$
365647	365754	-107	1.5	76.7 $4d^{6}5p$ (⁵ D) ${}^{4}F$ + 4 $4d^{6}5p$ (³ G) ${}^{4}F$
367434	367200	234	5.5	$51.5 \ 4d^{6}5p \ (^{3}H) \ ^{4}G + 13.7 \ 4d^{6}5p \ (^{3}G) \ ^{4}G + 9.9 \ 4d^{6}5p \ (^{3}H) \ ^{4}I$
367647	367427	220	1.5	71.6 $4d^{6}5p ({}^{5}D) {}^{4}P + 8.4 4d^{6}5p ({}^{3}P) {}^{4}P + 5.1 4d^{6}5p ({}^{3}P) {}^{4}S$
367590	367513	77	4.5	26.6 $4d^{6}5p (^{3}H) {}^{4}G + 15 4d^{6}5p (^{3}H) {}^{2}G + 13.8 4d^{6}5p (^{3}G) {}^{4}F$
367570	367664	-94	0.5	83.8 $4d^{6}5p$ (⁵ D) ${}^{4}P$ + 5.7 $4d^{6}5p$ (⁵ D) ${}^{6}D$
367959	368218	-259	2.5	14.9 4d ⁶ 5p (³ P) ${}^{4}D$ + 9.4 4d ⁶ 5p (⁵ D) ${}^{4}D$ + 9 4d ⁶ 5p (⁵ D) ${}^{4}F$
368796	368873	-77	3.5	$31.2 \ 4d^{6}5p \ ({}^{3}F) \ {}^{4}G + 12.5 \ 4d^{6}5p \ ({}^{3}G) \ {}^{4}H + 11 \ 4d^{6}5p \ ({}^{3}H) \ {}^{4}G$
368956	369089	-133	2.5	$37.4 \ 4d^{0}5p \ (^{3}F) \ ^{4}G + 8.3 \ 4d^{0}5p \ (^{3}F) \ ^{4}F + 7.2 \ 4d^{0}5p \ (^{3}H) \ ^{4}G$
371041	370999	42	4.5	$42.7 \ 4d^{\circ}5p \ (^{\circ}H)^{-4}I + 10.5 \ 4d^{\circ}5p \ (^{\circ}G)^{-4}G + 10.1 \ 4d^{\circ}5p \ (^{\circ}F)^{-4}F$
371496	371628	-132	1.5	$39.6 \ 4d^{\circ}5p \ (^{\circ}F) \ ^{\circ}F + 22.2 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}F + 11 \ 4d^{\circ}5p \ (^{\circ}F) \ ^{\circ}D$
371734	371749	-15	3.5	$26.5 \ 4d^{\circ} \text{5p} (^{\circ} \text{H})^{-1} \text{H} + 20.5 \ 4d^{\circ} \text{5p} (^{\circ} \text{F})^{-1} \text{D} + 9.1 \ 4d^{\circ} \text{5p} (^{\circ} \text{G})^{-1} \text{H}$
374317	374228	89	3.5	$14.8 \text{ 4d}^{\circ}\text{5p}(^{\circ}\text{D})^{\circ}\text{F} + 25.6 \text{ 4d}^{\circ}\text{5p}(^{\circ}\text{H})^{\circ}\text{G} + 9.4 \text{ 4d}^{\circ}\text{5p}(^{\circ}\text{G})^{\circ}\text{F}$
274050	274047	-20	4.0	$(12.14d^{5}p^{(1)})$
374950	376071	122	4.5	42.140 5p (11) 1 ± 20.840 5p (3) $4 \pm 18.4d^{6}$ 5p (3) $4C \pm 13.04d^{6}$ 5p (3C) $4E$
376235	376181	54	3.5	$^{23.9} 4d^{6}5p (^{3}G) ^{4}H + 22.6 4d^{6}5p (^{3}F) ^{4}D + 12.6 4d^{6}5p (^{3}D) ^{4}D$
376198	376272	-74	2.5	$14.8 4d^{6}5p (^{3}P) ^{4}P + 9.7 4d^{6}5p (^{3}P) ^{4}P + 9.4d^{6}5p (^{3}D) ^{4}P$
376936	376680	256	4.5	$26.1 \ 4d^{6}5p \ (^{3}G) \ ^{4}F + 12.5 \ 4d^{6}5p \ (^{3}F) \ ^{4}F + 8.7 \ 4d^{6}5p \ (^{3}F) \ ^{4}F$
377141	377057	84	2.5	$25.4 4d^{6}5p (^{3}\text{F}) ^{4}\text{D} + 18.5 4d^{6}5p (^{3}\text{D}) ^{4}\text{D} + 12.7 4d^{6}5p (^{3}\text{D}) ^{4}\text{F}$
377145	377224	-79	5.5	19.6 $4d^{6}5p({}^{3}F) {}^{4}G + 26.1 4d^{6}5p({}^{3}H) {}^{2}I + 18.5 4d^{6}5p({}^{3}G) {}^{2}H$
377189	377287	-98	6.5	$36.9 \ 4d^{6}5p \ (^{3}H) \ ^{2}I + 27.8 \ 4d^{6}5p \ (^{3}G) \ ^{4}H + 25.9 \ 4d^{6}5p \ (^{3}H) \ ^{4}H$
377873	377913	-40	3.5	$36.2 \ 4d^{6}5p \ (^{3}G) \ ^{4}G + 15.6 \ 4d^{6}5p \ (^{3}F) \ ^{4}G + 9.2 \ 4d^{6}5p \ (^{3}H) \ ^{2}G$
378221	378251	-30	3.5	$38.9 \ 4d^{6}5p \ (^{3}P) \ ^{4}D + 17.6 \ 4d^{6}5p \ (^{3}P) \ ^{4}D + 11.5 \ 4d^{6}5p \ (^{3}F) \ ^{4}F$
378650	378627	23	4.5	$16.2 \ 4d^{6}5p \ (^{3}G) \ ^{4}G + 18.2 \ 4d^{6}5p \ (^{3}F) \ ^{4}G + 9.4 \ 4d^{6}5p \ (^{3}H) \ ^{2}G$
378630	378663	-33	2.5	$32.7 \ 4d^{6}5p \ (^{3}G) \ ^{4}G + 10.4 \ 4d^{6}5p \ (^{3}F) \ ^{4}D + 7.6 \ 4d^{6}5p \ (^{3}P) \ ^{4}P$
378726	378735	-9	1.5	7.3 4d ⁶ 5p (³ P) ⁴ D + 14 4d ⁶ 5p (³ F) ⁴ D + 13.8 4d ⁶ 5p (³ D) ⁴ D
378995	379131	-136	5.5	$40.4 \ 4d^{0}5p \ ({}^{3}H) \ {}^{4}H + 19.9 \ 4d^{0}5p \ ({}^{3}G) \ {}^{2}H + 13.6 \ 4d^{0}5p \ ({}^{1}I) \ {}^{2}H$
380519	380331	188	3.5	$28.9 \text{ 4d}^{\circ}5p (^{3}\text{G}) ^{4}\text{F} + 11.1 \text{ 4d}^{\circ}5p (^{3}\text{P}) ^{4}\text{D} + 10.2 \text{ 4d}^{\circ}5p (^{3}\text{F}) ^{4}\text{G}$
380707	380770	-63	0.5	$5.6 \text{ 4d}^{\circ}5p (^{\circ}S) ^{2}P + 20 \text{ 4d}^{\circ}5p (^{\circ}F) ^{4}D + 14.3 \text{ 4d}^{\circ}5p (^{\circ}P) ^{4}D$
381246	381010	236	2.5	$21.7 \ 4d^{\circ}5p({}^{\circ}G) \ F + 21.7 \ 4d^{\circ}5p({}^{\circ}H) \ G + 11.5 \ 4d^{\circ}5p({}^{\circ}F) \ F$
382193	382187	0	0.0 1 E	$9.3 4d^{\circ} 5p(^{-1}) = H + 14.2 4d^{\circ} 5p(^{\circ} H) = H + 13.5 4d^{\circ} 5p(^{\circ} F) = G$
282262	282226	-200	1.5	14.5 4d 5p ($^{\circ}$ F) 5 + 10.6 4d 5p ($^{\circ}$ F) F + 10.1 4d 5p ($^{\circ}$ F) D 10.8 4d 65p (3 C) 2 H + 15.2 4d 65p (3 F) 4C + 8.2 4d 65p (3 C) 2 C
382111	382521	-410	4.5	$40.94d^{6}5p(^{3}P)^{2}S + 14.94d^{6}5p(^{3}D)^{2}P + 13.14d^{6}5p(^{3}P)^{4}P$
383254	383192	-410	2.5	$22.8 \ 4d^{6}5p \ (^{3}H) \ ^{4}G \ + \ 17.2 \ 4d^{6}5p \ (^{3}D) \ ^{4}F \ + \ 14.5 \ 4d^{6}5p \ (^{3}D) \ ^{4}P$
383076	383296	-220	6.5	$74 4d^{6}5p (^{1}I) ^{2}K + 11 4d^{6}5p (^{1}I) ^{2}I + 8.8 4d^{6}5p (^{3}H) ^{2}I$
383934	383858	76	2.5	$15.9 \ 4d^{6}5p \ (^{3}D) \ ^{4}P + 11.4 \ 4d^{6}5p \ (^{3}G) \ ^{4}F + 9.9 \ 4d^{6}5p \ (^{3}P) \ ^{4}P$
384525	384626	-101	4.5	$27.9 \ 4d^{6}5p \ (^{3}G) \ ^{4}H + 26.9 \ 4d^{6}5p \ (^{3}H) \ ^{4}H + 20.5 \ 4d^{6}5p \ (^{3}H) \ ^{2}G$
384701	384766	-65	2.5	$7.1 \ 4d^{6}5p \ (^{1}D) \ ^{2}F + 13.4 \ 4d^{6}5p \ (^{3}D) \ ^{4}P + 9.2 \ 4d^{6}5p \ (^{3}F) \ ^{2}F$
384721	384811	-90	5.5	23 4d ⁶ 5p (³ H) ² I + 17.3 4d ⁶ 5p (¹ I) ² H + 15.6 4d ⁶ 5p (³ G) ⁴ H
384926	384879	47	3.5	$30.6 \ 4d^{6}5p \ (^{3}H) \ ^{4}G + 13 \ 4d^{6}5p \ (^{3}D) \ ^{4}F + 8.5 \ 4d^{6}5p \ (^{3}H) \ ^{4}H$
385231	385587	-356	3.5	29.5 $4d^{6}5p ({}^{3}F) {}^{2}G + 15 4d^{6}5p ({}^{3}H) {}^{2}G + 9.7 4d^{6}5p ({}^{3}F) {}^{2}G$
385902	385698	204	5.5	23.6 $4d^{6}5p({}^{3}G){}^{4}G + 13.6 4d^{6}5p({}^{3}G){}^{4}H + 12.8 4d^{6}5p({}^{3}H){}^{2}I$
385876	385731	145	1.5	25.3 4d ⁶ 5p (3 F) 4 D + 14.7 4d ⁶ 5p (3 D) 2 P + 9.9 4d ⁶ 5p (3 D) 4 P
385749	385753	-4	0.5	$29.5 \text{ 4d}^{6}\text{5p} (^{3}\text{D}) ^{4}\text{P} + 24.4 \text{ 4d}^{6}\text{5p} (^{3}\text{P}) ^{4}\text{D} + 14.6 \text{ 4d}^{6}\text{5p} (^{3}\text{P}) ^{2}\text{S}$
385969	385869	100	4.5	19.3 4d ⁶ 5p (³ H) ² H + 8.6 4d ⁶ 5p (³ F) ⁴ F + 7.6 4d ⁶ 5p (³ G) ⁴ G
386607	386674	-67	2.5	$12.7 \ 4d^{\circ} \text{5p} (^{\circ} \text{F}) = \text{F} + 13.3 \ 4d^{\circ} \text{5p} (^{\circ} \text{G}) = \text{G} + 12.5 \ 4d^{\circ} \text{5p} (^{\circ} \text{G}) = \text{F}$
380773 287246	287011	-00	3.0	19.1 4d 5p (H) G + 13.5 4d 5p (G) G + 12.1 4d 5p (F) F 18.7 $4d^{6}5p$ (${}^{3}F$) ${}^{2}D$ + 12.8 $4d^{6}5p$ (${}^{3}F$) ${}^{4}F$ + 0.7 $4d^{6}5p$ (${}^{3}P$) ${}^{4}P$
387340 387444	387232	212	4.5	$15.7 4d^{6}5p^{(3}F) 4G^{+} 16.9 4d^{6}5p^{(3}G) 4G^{+} 14.6 4d^{6}5p^{(3}H) 4G^{+}$
387772	387685	87	3.5	$9.4 \ 4d^65p \ (^3F) \ ^4F + 20.3 \ 4d^65p \ (^3D) \ ^2F + 15.9 \ 4d^65p \ (^3F) \ ^2G$
388005	388100	-95	2.5	27.1 $4d^{6}5p(^{3}F)^{2}D + 10.5 4d^{6}5p(^{3}F)^{4}F + 8 4d^{6}5p(^{3}G)^{4}F$
388322	388304	18	4.5	$27.2 \ 4d^{6}5p \ (^{3}F) \ ^{2}G + 24.1 \ 4d^{6}5p \ (^{1}G) \ ^{2}H + 19 \ 4d^{6}5p \ (^{1}I) \ ^{2}H$
389002	389085	-83	2.5	$8.9 \ 4d^{6}5p \ (^{3}P) \ ^{2}D + 16.3 \ 4d^{6}5p \ (^{3}F) \ ^{2}D + 14.3 \ 4d^{6}5p \ (^{3}P) \ ^{4}D$
389679	389733	-54	5.5	$43.6 \ 4d^{6}5p \ (^{3}H) \ ^{2}H + 24.6 \ 4d^{6}5p \ (^{1}I) \ ^{2}H + 9.9 \ 4d^{6}5p \ (^{3}G) \ ^{4}H$
390689	390618	71	3.5	24.4 $4d^{6}5p(^{3}G)^{2}G + 14 4d^{6}5p(^{1}G)^{2}F + 11 4d^{6}5p(^{3}G)^{4}H$
391658	391687	-29	1.5	$10.2 \ 4d^{6}5p \ ({}^{3}P) \ {}^{2}D + 12.7 \ 4d^{6}5p \ ({}^{3}G) \ {}^{4}F + 9.8 \ 4d^{6}5p \ ({}^{3}D) \ {}^{4}D$
391912	391947	-35	5.5	$30.7 \ 4d^{0}5p \ (^{3}G) \ ^{2}H + 19.5 \ 4d^{0}5p \ (^{3}H) \ ^{2}H + 14.1 \ 4d^{0}5p \ (^{3}G) \ ^{4}H$
392432	392337	95	2.5	$24.6 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}D + 12.2 \ 4d^{\circ}5p \ (^{\circ}F) \ ^{\circ}D + 11.5 \ 4d^{\circ}5p \ (^{\circ}F) \ ^{\circ}D$
392332	392475	-143	1.5	$8.7 4d^{\circ} 5p (^{\circ}D)^{-}P + 14.4 4d^{\circ} 5p (^{\circ}D)^{-}D + 8.9 4d^{\circ} 5p (^{\circ}F)^{-}D$
392012	392371	41	3.5	15.240° Sp (G) G + 18.240° Sp (G) F + 11.540° Sp (G) F 26.44655 (3C) 2C + 26.2.44655 (3C) 2H + 11.6.44655 (3C) 4H
393202	393170	32	3.5	$27.2 4d^{6}5p (^{1}F) ^{2}G + 12.4 4d^{6}5p (^{1}G) ^{2}F \pm 11.4 4d^{6}5p (^{3}F) ^{2}F$
393373	393526	-153	2.5	$7.3 \ 4d^{6}5p \ (^{3}D) \ ^{4}F + 18.1 \ 4d^{6}5p \ (^{3}G) \ ^{4}F + 13.7 \ 4d^{6}5n \ (^{3}F) \ ^{4}D$
393595	393688	-93	1.5	$26.7 \ 4d^{6}5p \ (^{3}D) \ ^{2}P + 17.5 \ 4d^{6}5p \ (^{3}G) \ ^{4}F + 7.7 \ 4d^{6}5p \ (^{3}P) \ ^{2}D$
394009	393815	194	3.5	19.2 $4d^{6}5p$ (³ D) ⁴ D + 25.7 $4d^{6}5p$ (³ D) ⁴ F + 5.4 $4d^{6}5p$ (³ G) ⁴ F
394078	393917	161	4.5	$0.4 \ 4d^{6}5p \ (^{5}D) \ ^{6}F + 31.5 \ 4d^{6}5p \ (^{3}D) \ ^{4}F + 14 \ 4d^{6}5p \ (^{3}G) \ ^{2}G$
394267	394151	116	2.5	11.5 $4d^{6}5p$ (³ D) ² F + 16.3 $4d^{6}5p$ (³ G) ⁴ F + 15.9 $4d^{6}5p$ (³ D) ⁴ F
394901	395136	-235	0.5	$4.6 \ 4d^{6}5p \ (^{3}D) \ ^{4}D + 24.6 \ 4d^{6}5p \ (^{3}D) \ ^{4}P + 16.1 \ 4d^{6}5p \ (^{3}P) \ ^{2}S$
395387	395477	-90	2.5	$2.7 \ 4d^{6}5p \ (^{1}F) \ ^{2}D + 25.4 \ 4d^{6}5p \ (^{3}D) \ ^{2}D + 20.4 \ 4d^{6}5p \ (^{3}D) \ ^{2}F$
396039	395870	169	4.5	$31.3 \ 4d^{0}5p \ ({}^{3}D) \ {}^{4}F + 16.3 \ 4d^{0}5p \ ({}^{3}H) \ {}^{2}H + 12.9 \ 4d^{6}5p \ ({}^{3}G) \ {}^{2}G$
396255	396329	-74	1.5	$10.1 \ 4d^{\circ}5p \ (^{\circ}P) \ ^{2}P + 22.8 \ 4d^{\circ}5p \ (^{1}D) \ ^{2}D + 12.4 \ 4d^{\circ}5p \ (^{1}D) \ ^{2}P$
396772	396758	14	3.5	$0.6 \ 4d^{\circ}5p \ (^{\circ}P)^{-2}D + 20.9 \ 4d^{\circ}5p \ (^{\circ}G)^{-2}G + 11.8 \ 4d^{\circ}5p \ (^{\circ}D)^{-2}F$
397464	397152	312	3.5 9 F	$30.3 4d^{\circ} p (^{\circ}D) = F + 19.6 4d^{\circ} b (^{\circ}D) = D + 12 4d^{\circ} b (^{\circ}F) = D$
397213	397303 307799	-32	⊿.ə ⊿ ≍	27 4u op (°G) F + 24.5 4u op (°F) F + 11.2 4u op (°D) F $47.8 4d^{6}5_{\rm D}$ (¹ I) ² H $\pm 17.6 4d^{6}5_{\rm D}$ (³ C) ² H $\pm 9.1 4d^{6}5_{\rm D}$ (³ F) ² C
397012	397080	-111	4.0 5.5	41.0 + 41.0 + 11.0 +
308110	308173	63	6.5	$83.4.46^{6}$ 5p (¹) ² I + 11.5.46^{6}5p (¹ I) ² K + 3.9.46 ⁶ 5p (³ H) ⁴ H

Table A23: Continued

E^a_{exp}	E^{b}_{calc}	ΔE	J	Leading components (in $\%$) in LS coupling ^{c}
398952	398896	56	2.5	$36.9 \ 4d^{6}5p \ (^{3}D) \ ^{2}D + 9 \ 4d^{6}5p \ (^{1}D) \ ^{2}F + 8.9 \ 4d^{6}5p \ (^{1}F) \ ^{2}D$
399514	399439	75	1.5	$15.9 \ 4d^{6}5p \ (^{3}P) \ ^{4}D + 13.5 \ 4d^{6}5p \ (^{1}S) \ ^{2}P + 12.7 \ 4d^{6}5p \ (^{3}D) \ ^{2}D$
400183	400010	173	4.5	$34.3 \ 4d^{6}5p \ (^{1}G) \ ^{2}G + 23.2 \ 4d^{6}5p \ (^{3}H) \ ^{2}H + 8.6 \ 4d^{6}5p \ (^{1}G) \ ^{2}H$
400538.4	400349	189.4	5.5	$47.6 \ 4d^{6}5p \ (^{1}G) \ ^{2}H + 24 \ 4d^{6}5p \ (^{1}G) \ ^{2}H + 8.4 \ 4d^{6}5p \ (^{3}F) \ ^{4}G$
400870	400764	106	3.5	$5.8 \ 4d^{6}5p \ (^{1}G) \ ^{2}F + 24.2 \ 4d^{6}5p \ (^{3}G) \ ^{2}G + 14.2 \ 4d^{6}5p \ (^{1}F) \ ^{2}G$
401788	401778	10	3.5	$43.6 \ 4d^{6}5p \ (^{3}F) \ ^{4}D + 13.7 \ 4d^{6}5p \ (^{3}P) \ ^{4}D + 10.8 \ 4d^{6}5p \ (^{3}G) \ ^{2}F$
404002	403760	242	2.5	$24.9 \ 4d^{6}5p \ (^{1}G) \ ^{2}F + 15.2 \ 4d^{6}5p \ (^{3}D) \ ^{2}F + 11.3 \ 4d^{6}5p \ (^{1}G) \ ^{2}F$
404466	404396	70	4.5	$53.9 \ 4d^{6}5p \ (^{1}F) \ ^{2}G + 17.5 \ 4d^{6}5p \ (^{3}F) \ ^{4}G + 3.5 \ 4d^{6}5p \ (^{3}F) \ ^{4}G$
404853	404799	54	1.5	$22.5 \ 4d^{6}5p \ (^{1}D) \ ^{2}D + 17.6 \ 4d^{6}5p \ (^{3}P) \ ^{4}D + 10.4 \ 4d^{6}5p \ (^{1}D) \ ^{2}P$
405249	405005	244	1.5	$19.7 4d^{6}5p (^{1}S) ^{2}P + 13.6 4d^{6}5p (^{3}P) ^{2}D + 13.3 4d^{6}5p (^{3}P) ^{4}S$
406806	407182	-376	3.5	$30.4 \ 4d^{6}5p \ (^{1}D) \ ^{2}F + 12 \ 4d^{6}5p \ (^{1}G) \ ^{2}F + 10.4 \ 4d^{6}5p \ (^{3}F) \ ^{4}D$
407640	407442	198	2.5	$46.3 \ 4d^{6}5p \ (^{3}F) \ ^{4}G + 13.2 \ 4d^{6}5p \ (^{1}F) \ ^{2}F + 7.2 \ 4d^{6}5p \ (^{1}F) \ ^{2}D$
408551	408601	-50	3.5	41 $4d^{6}5p$ (¹ F) ² F + 13.7 $4d^{6}5p$ (¹ D) ² F + 11.7 $4d^{6}5p$ (¹ G) ² F
408655	408914	-259	1.5	$40.1 \ 4d^{6}5p \ (^{1}F) \ ^{2}D + 7.3 \ 4d^{6}5p \ (^{3}F) \ ^{4}F + 5.8 \ 4d^{6}5p \ (^{3}P) \ ^{4}D$
409420	409438	-18	4.5	$34.1 \ 4d^{6}5p \ (^{3}F) \ ^{2}G + 20.1 \ 4d^{6}5p \ (^{1}F) \ ^{2}G + 13.4 \ 4d^{6}5p \ (^{3}F) \ ^{4}G$
410057	410015	42	2.5	$38.9 \ 4d^{6}5p \ (^{1}F) \ ^{2}F + 14.4 \ 4d^{6}5p \ (^{3}F) \ ^{4}G + 9 \ 4d^{6}5p \ (^{1}F) \ ^{2}D$
411076	411035	41	3.5	$50.5 \ 4d^{6}5p \ (^{3}F) \ ^{4}G + 8.6 \ 4d^{6}5p \ (^{1}F) \ ^{2}G + 6.5 \ 4d^{6}5p \ (^{3}F) \ ^{4}G$
413681	413798	-117	1.5	26 4d ⁶ 5p (³ P) ⁴ S + 24.3 4d ⁶ 5p (³ F) ² D + 9 4d ⁶ 5p (¹ D) ² D
416462	416141	321	1.5	$32.3 \ 4d^{6}5p \ (^{3}P) \ ^{4}P + 18.7 \ 4d^{6}5p \ (^{3}P) \ ^{4}S + 11.4 \ 4d^{6}5p \ (^{1}S) \ ^{2}P$
416206	416271	-65	2.5	19.6 $4d^{6}5p(^{3}F) {}^{4}F + 17.2 4d^{6}5p(^{3}P) {}^{4}D + 9.7 4d^{6}5p(^{3}F) {}^{4}D$
417097	416997	100	0.5	$49.4 \ 4d^{6}5p \ (^{3}F) \ ^{4}D + 15.8 \ 4d^{6}5p \ (^{3}P) \ ^{2}S + 7.6 \ 4d^{6}5p \ (^{3}P) \ ^{4}P$
417531	417640	-109	3.5	$33.9 \ 4d^65p \ (^3F) \ ^4F + 12.2 \ 4d^65p \ (^1G) \ ^2F + 11.1 \ 4d^65p \ (^1G) \ ^2G$
417677	417926	-249	2.5	9.2 $4d^{6}5p$ (³ P) ⁴ P + 30.4 $4d^{6}5p$ (³ P) ² D + 14.5 $4d^{6}5p$ (³ P) ² D
418393	418439	-46	1.5	21.8 4d ⁶ 5p (³ P) ² D + 17.1 4d ⁶ 5p (³ F) ⁴ F + 14.2 4d ⁶ 5p (³ F) ⁴ D
419771	419942	-171	3.5	43.9 $4d^{6}5p ({}^{3}F) {}^{2}G + 17.9 4d^{6}5p ({}^{1}G) {}^{2}F + 5.9 4d^{6}5p ({}^{1}F) {}^{2}F$
420288	420263	25	4.5	$26.2 4d^{6}5p ({}^{1}G) {}^{2}H + 19 4d^{6}5p ({}^{3}F) {}^{4}F + 13.2 4d^{6}5p ({}^{1}G) {}^{2}H$
420923	420518	405	1.5	25 4d ⁶ 5p (³ F) ⁴ D + 21 4d ⁶ 5p (³ P) ² D + 10.6 4d ⁶ 5p (³ F) ² D
421363	421296	67	2.5	$45.2 \ 4d^{6}5p \ (^{3}F) \ ^{2}D + 14.1 \ 4d^{6}5p \ (^{3}F) \ ^{4}F + 10.9 \ 4d^{6}5p \ (^{3}P) \ ^{4}P$
421229	421329	-100	3.5	$2.8 \ 4d^{6}5p \ (^{1}G) \ ^{2}F + 22.6 \ 4d^{6}5p \ (^{3}F) \ ^{2}G + 20.2 \ 4d^{6}5p \ (^{3}P) \ ^{4}D$
422052	422076	-24	2.5	22.7 4d ⁶ 5p (³ F) ⁴ D + 21.4 4d ⁶ 5p (³ F) ⁴ F + 7.7 4d ⁶ 5p (³ P) ⁴ D
423109	423090	19	4.5	$37.9 \ 4d^{6}5p \ (^{3}F) \ ^{4}F + 30 \ 4d^{6}5p \ (^{3}F) \ ^{2}G + 13.3 \ 4d^{6}5p \ (^{3}F) \ ^{4}F$
424983	425071	-88	3.5	$26 \ 4d^{6}5p \ (^{3}F) \ ^{2}F + 19.5 \ 4d^{6}5p \ (^{1}G) \ ^{2}G + 11.7 \ 4d^{6}5p \ (^{3}P) \ ^{4}D$
426759	426604	155	2.5	$14.2 \ 4d^{6}5p \ (^{3}P) \ ^{2}D + 14.5 \ 4d^{6}5p \ (^{1}G) \ ^{2}F + 13 \ 4d^{6}5p \ (^{3}P) \ ^{4}P$
427084	427113	-29	2.5	$46.7 \ 4d^{6}5p \ (^{3}F) \ ^{2}F + 12.6 \ 4d^{6}5p \ (^{3}F) \ ^{2}F + 7 \ 4d^{6}5p \ (^{3}P) \ ^{2}D$
427155	427549	-394	5.5	$60.9 \ 4d^{6}5p \ (^{1}G) \ ^{2}H + 28.9 \ 4d^{6}5p \ (^{1}G) \ ^{2}H$
430363	430560	-197	4.5	55.9 4d ⁶ 5p (¹ G) ² G + 15.6 4d ⁶ 5p (¹ G) ² G + 8.5 4d ⁶ 5p (¹ G) ² H
432957	432999	-42	3.5	9.6 $4d^{6}5p ({}^{3}F) {}^{2}F + 19.7 4d^{6}5p ({}^{3}F) {}^{2}F + 18.5 4d^{6}5p ({}^{1}G) {}^{2}G$
436247	436217	30	1.5	$66.6 \ 4d^{0}5p \ (^{1}D) \ ^{2}D + 9.8 \ 4d^{0}5p \ (^{1}D) \ ^{2}P + 6.8 \ 4d^{6}5p \ (^{1}D) \ ^{2}D$
447561	447476	85	2.5	$46.7 \ 4d^{6}5p \ (^{1}D) \ ^{2}F + 24.1 \ 4d^{6}5p \ (^{1}D) \ ^{2}D + 12.5 \ 4d^{6}5p \ (^{1}D) \ ^{2}F$

a: From Ryabtsev [38] b: This work c: Only the component $\geq 5\%$ are given

10010 112	ii compa		101 501			10101011	probab	an	, 111 111 1
	Wavelength	Lower Level ^a	J_{Low}	Upper level ^a	J_{Up}	log gf	gA	CF	l I
	Ă	$\rm cm^{-1}$		$\rm cm^{-1}$			s^{-1}		Í
	248.323	27662	5.5	430363	4.5	-0.54	3.14E + 10	0.241	Í
	248.458	45079	3.5	447561	2.5	-0.94	1.24E + 10	0.275	Í
	250.493	33744	4.5	432957	3.5	-0.52	3.25E + 10	0.185	Í
	251.286	18509	2.5	416462	1.5	-0.87	1.43E + 10	0.2	Í
	252.878	27662	5.5	423109	4.5	-0.4	4.15E + 10	0.275	Í
	253.561	41865	2.5	436247	1.5	-0.64	2.38E + 10	0.406	Í
	255.598	33744	4.5	424983	3.5	-0.58	2.68E + 10	0.24	Í .
	257.502	16903	1.5	405249	1.5	-0.97	1.07E + 10	0.179	Í
	258 075	33744	4.5	421229	3.5	-0.56	2.78E + 10	0 174	Í
	258 572	18509	2.5	405249	1.5	-0.73	1.86E + 10	0.512	l I
	259.049	33744	4.5	419771	3.5	-0.42	$3.79E \pm 10$	0.219	l I
	250.540	45079	3.5	430363	4.5	0.37	$4.92E \pm 10$	0.682	1
	250.020	40015	4.5	384721	5.5	0.78	$1.63E \pm 10$	0.002	Í
	260.666	8600	4.5	202222	1.5	-0.75	1.00E + 10	0.233	1
	260.000	18500	2.5	401788	2.5	-0.95	$1.09E \pm 10$	0.17	1
	200.907	10009	2.5	200000	0.0	-0.39	$4.03E \pm 10$ $2.12E \pm 10$	0.381	l I
	260.915	5730	3.5	389002	2.5	-0.67	2.12E + 10	0.408	1
	260.951	10382	1.5	393595	1.5	-0.87	1.33E + 10 1.74E + 10	0.149	Í
	201.032	0	4.5	382362	4.5	-0.75	1.74E + 10	0.23	1
	261.946	27662	5.5	409420	4.5	0.04	1.06E + 11	0.621	1
	261.98	5736	3.5	387444	4.5	-0.7	1.94E + 10	0.15	Í
	261.984	39221	1.5	420923	1.5	-0.51	3.00E + 10	0.326	1
	262.277	10382	1.5	391658	1.5	-0.89	1.24E + 10	0.132	l I
	262.305	27420	1.5	408655	1.5	-0.87	1.31E + 10	0.118	1
	262.948	8699	2.5	389002	2.5	-0.74	1.77E + 10	0.311	l I
	263.017	20666	4.5	400870	3.5	-0.98	1.01E+10	0.036	Í
	263.028	41865	2.5	422052	2.5	-0.93	1.12E + 10	0.239	Í
	263.224	45079	3.5	424983	3.5	-0.58	2.53E+10	0.356	Í
	263.493	20666	4.5	400183	4.5	-0.71	1.88E + 10	0.064	Í
	263.812	41865	2.5	420923	1.5	-0.73	1.79E + 10	0.315	Í
	263.856	0	4.5	378995	5.5	-0.9	1.20E + 10	0.546	Í
	263.884	18509	2.5	397464	3.5	-0.39	3.92E + 10	0.582	Í
	264.366	18509	2.5	396772	3.5	-0.98	$9.90E \pm 09$	0.394	Í .
	264.396	0	4.5	378221	3.5	-0.07	8.22E + 10	0.701	Í
	264 412	5736	3.5	383934	2.5	-0.88	1.27E + 10	0.319	Í
	264.473	30441	2.5	408551	3.5	-0.51	$2.96E \pm 10$	0.296	1
	264.520	45070	3.5	400001	4.5	0.85	$1.35E \pm 10$	0.502	Í
	264.525	96092	2.5	423103	9.5	-0.35	1.55 ± 10 4.76 ± 10	0.332	1
	264.505	41865	0.5	404002	2.5	-0.5	$4.70E \pm 10$ 1.20E ± 10	0.374	l I
	204.010	22744	2.5	419771	0.0 0 F	-0.80	$1.30E \pm 10$	0.324	1
	205.019	33744	4.0	207052	3.0 E E	-0.51	$2.92E \pm 10$ 1.02E ± 10	0.403	1
	205.05	20000	4.5	391933	1.5	-0.97	$1.02E \pm 10$ $1.01E \pm 10$	0.008	Í
	205.128	8699	2.5	383870	1.5	-0.97	1.01E + 10	0.197	
	265.15	0	4.5	377145	5.5	-0.56	2.64E + 10	0.715	l l
	265.277	10382	1.5	387346	1.5	-0.95	1.07E + 10	0.243	l I
	265.297	0	4.5	376936	4.5	-0.08	7.96E+10	0.44	1
	265.39	27662	5.5	404466	4.5	-0.04	8.66E + 10	0.579	Í
	265.394	20666	4.5	397464	3.5	-0.63	2.21E+10	0.135	l I
	265.546	27420	1.5	404002	2.5	-0.74	1.71E + 10	0.183	1
	265.584	41865	2.5	418393	1.5	-0.86	1.32E + 10	0.168	1
	265.791	0	4.5	376235	3.5	-0.77	1.61E + 10	0.253	l I
	265.797	8699	2.5	384926	3.5	-0.28	4.98E + 10	0.415	Í
	265.798	10382	1.5	386607	2.5	-0.91	1.17E + 10	0.176	Í
	265.82	0	4.5	376194	4.5	-0.59	2.44E + 10	0.22	Í
	265.882	20666	4.5	396772	3.5	-0.72	1.78E + 10	0.097	Í
	266.291	16903	1.5	392432	2.5	-0.83	1.38E + 10	0.125	Í
	266.304	5736	3.5	381246	2.5	-0.76	1.63E + 10	0.556	Í
	266.362	16903	1.5	392332	1.5	-0.86	1.31E + 10	0.15	Í
	266.5	8699	2.5	383934	2.5	-0.85	1.32E + 10	0.144	Í
	266.702	0	4.5	374950	5.5	-0.94	1.07E + 10	0.319	Í .
	266.821	5736	3.5	380519	3.5	0.15	1.33E + 11	0.799	Í
	266 886	45079	3.5	419771	3.5	-0.79	1.52E + 10	0 143	Í
	267.051	0	4.5	374461	4.5	-0.81	1.45E+10	0.187	Í
	267 153	õ	4.5	374317	3.5	-0.97	$9.92E \pm 0.0$	0.176	l I
	267.265	26023	3.5	400183	4.5	-0.81	$1.46E \pm 10$	0.161	l l
	267.435	18500	2.5	302/32	2.5	0.42	$3.55E \pm 10$	0.496	Í
	201.433	10202	1.5	282024	2.0	-0.42	1.21E + 10	0.430	1
	207.7	20666	1.5	204079	4.5	-0.85	$1.51E \pm 10$ $1.74E \pm 10$	0.214	Í
	207.801	20000	4.5	204000	4.0	-0.73	1.74E+10 6 51E+10	0.074	1
	201.00	20000	4.5	394009	3.0	-0.10	$0.51E \pm 10$	0.000	1
	201.013	0099	2.5	382010	1.0	-0.93	1.11E + 10 1.50E + 10	0.237	Í
	268.052	33744	4.5	406806	3.5	-0.79	1.52E + 10	0.161	1
	208.148	20023	3.5	398952	2.5	-1	$9.35E \pm 10$	0.154	l I
	268.158	5736	3.5	378650	4.5	-0.9	1.16E + 10	0.231	1
	268.189	10382	1.5	383254	2.5	-0.38	3.88E + 10	0.556	1
	268.386	45079	3.5	417677	2.5	0.02	9.72E + 10	0.651	Í
	268.423	8699	2.5	381246	2.5	-0.18	6.12E + 10	0.564	l I
	268.43	20666	4.5	393202	3.5	-0.21	5.73E + 10	0.306	l I
	268.447	20666	4.5	393179	4.5	-0.51	2.87E + 10	0.121	1
	268.491	45079	3.5	417531	3.5	-0.61	2.30E+10	0.282	l I
	268.746	16903	1.5	389002	2.5	-0.92	1.10E + 10	0.099	Í
	268.856	20666	4.5	392612	3.5	-0.89	1.20E + 10	0.086	Í
	268.95	41865	2.5	413681	1.5	-0.37	3.90E + 10	0.625	Í
	269.01	0	4.5	371734	3.5	-0.27	4.99E + 10	0.481	Í.
	269.115	26023	3.5	397612	4.5	-0.57	2.46E + 10	0.15	Í.
	269.222	26023	3.5	397464	3.5	-0.51	2.82E + 10	0.33	Í.
	269.248	5736	3.5	377141	2.5	-0.15	6.57E + 10	0.587	Í.
	269.36	26023	3.5	397273	2.5	-0.02	$8.88E \pm 10$	0.325	Í.
	269.363	20666	4.5	391912	5.5	-0,66	2.03E + 10	0.197	Í.
	269 397	5736	3.5	376936	4.5	-0.24	$5.28E \pm 10$	0.747	Í.
	269.45	45079	3.5	416206	2.5	-0.71	$1.81E \pm 10$	0.385	Í.
	269 468	16003	1.5	388005	2.5	-0.95	$1.02E \pm 10$	0.156	Í.
	269 661	30221	1.5	410057	2.5	-0.8	$1.47E \pm 10$	0 176	Í.
	260 011	18500	2.5	380002	2.5	-0.3	$1.81E \pm 10$	0.277	Í
	203.311	10009 5796	2.J 9 E	376104	2.0 1 5	0.25	5 2012 + 10	0.479	Í.
	209.930	0100	0.0 5 5	300194	4.0 6 5	-0.20 0.0F	9.20E+10 8.15E / 10	0.472	Í
	209.940	10282	0.0 1 K	390110	0.5	0.00	4 47E + 10	0.710	Í
	270.033	10382	1.0	300/07	0.0	-0.31	4.4/E+10 7.06E/10	0.774	Í.
	270.251	8699	2.5	3/8726	1.5	-0.06	(.90E+10	0.774	Í
	410.403	20000	4.0	090009	0.0	-0.79	1.4/12+10	0.08	(

Table A24: Computed oscillator strengths and transition probabilities in In VII.

Table .	A24:	Continue	ł
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Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA	CF
270.337	66339 8600	1.5	436247	1.5	-0.18	6.00E+10	0.665
270.684	39221	1.5	408655	1.5	-0.52	2.75E+10	0.330 0.229
270.736	26023	3.5	395387	2.5	-0.18	6.09E + 10	0.528
270.81	18509	2.5	387772	3.5	-0.86	1.26E + 10	0.547
270.875	8699 30441	2.5	377873 399514	3.5 1.5	-0.24	5.20E+10 4 40E+10	0.746
271.023	16903	1.5	385876	1.5	-1	9.04E+09	0.104
271.116	16903	1.5	385749	0.5	-0.85	1.28E + 10	0.3
271.124	27420	1.5	396255	1.5	-0.84	1.31E + 10	0.106
271.153	0 5736	4.5	308790	3.5 4.5	-0.91	1.11E+10 3.98E+10	0.39
271.311	5736	3.5	374317	3.5	-0.6	2.26E + 10	0.233
271.362	30441	2.5	398952	2.5	0.06	1.04E + 11	0.607
271.413	8699	2.5	377141	2.5	-0.62	2.16E + 10	0.315
271.401	27002	5.5 1.5	396039	4.5 2.5	-0.45	3.23E+10 3.38E+10	0.441 0.503
271.559	26023	3.5	394267	2.5	-0.51	2.80E + 10	0.369
271.597	41865	2.5	410057	2.5	-0.16	6.30E + 10	0.55
271.707	33744	4.5	401788	3.5	-0.3	4.56E + 10	0.502
271.888	16903	1.5	384701	2.5	-0.93	$1.78E \pm 10$	0.243 0.258
271.993	20666	4.5	388322	4.5	0.03	9.59E + 10	0.503
272.042	0	4.5	367590	4.5	0.08	1.07E + 11	0.762
272.082	8699 27420	2.5	376235 394901	3.5	-0.85	1.28E+10 1.78E+10	0.404 0.242
272.158	0	4.5	367434	5.5	0.27	1.69E + 11	0.803
272.364	26023	3.5	393179	4.5	-0.84	1.31E + 10	0.179
272.386	33744	4.5	400870	3.5	0.11	1.16E + 11	0.468
272.401	20666	4.5	387772	3.5	-0.35	4.00E+10 2.02E+10	0.271 0.254
272.593	27420	1.5	394267	2.5	-0.98	9.36E+09	0.121
272.636	41865	2.5	408655	1.5	-0.93	1.06E + 10	0.149
272.785	26023	3.5	392612	3.5	-0.05	7.94E+10	0.584
272.897	33744 18509	4.5 2.5	400183 384926	4.5 3.5	-0.06 -0.75	$1.60E \pm 10$	0.297 0.548
272.914	27662	5.5	394078	4.5	-0.19	5.83E + 10	0.442
272.977	30441	2.5	396772	3.5	-0.74	1.62E + 10	0.179
273.081	18509	2.5	384701	2.5	-0.92	1.07E + 10 5.04E + 10	0.166
273.226	45079	4.5	411076	3.5	-0.18	$3.36E \pm 10$	0.309
273.226	5736	3.5	371734	3.5	-0.89	1.16E + 10	0.209
273.259	27420	1.5	393373	2.5	-0.62	2.16E + 10	0.237
273.361	10382	1.5	376198	2.5	-0.83	1.34E+10 1.52E+10	0.291
273.499	39221	2.5	404853	1.5	-0.44	3.27E+10	0.109 0.285
273.51	8699	2.5	374317	3.5	-0.58	2.32E + 10	0.239
273.585	27662	5.5	393179	4.5	-0.14	6.49E + 10	0.502
273.654	18509 5736	2.5	383934 371041	2.5	-0.48	2.92E+10 1.86E+10	0.345
273.745	20666	4.5	385969	4.5	-0.8	1.40E+10	0.238 0.076
273.817	16903	1.5	382111	0.5	-0.64	2.05E + 10	0.335
274.137	39221	1.5	404002	2.5	-0.63	2.10E+10	0.206
274.164	18509	2.5	383254 390689	2.5	-0.53	2.60E+10 6.19E+10	0.498 0.344
274.3	20666	4.5	385231	3.5	-0.64	2.02E + 10	0.086
274.495	21571	0.5	385876	1.5	-0.43	3.32E + 10	0.49
274.529	20666	4.5	384926	3.5	-0.69	1.83E+10 1.20E+10	0.294
274.546	27662	1.5	391658	1.5	-0.67	1.20E + 10 1.89E + 10	0.057 0.157
274.568	33744	4.5	397953	5.5	0.13	1.19E + 11	0.735
274.591	21571	0.5	385749	0.5	-0.85	1.24E + 10	0.761
274.684	20666	4.5 4.5	384721 397612	5.5 4.5	-0.01	$8.62E \pm 10$ 2 59E \pm 11	0.861 0.766
274.876	0	4.5	363801	3.5	-0.17	5.98E+10	0.514
275.124	45079	3.5	408551	3.5	-0.61	2.14E + 10	0.181
275.191	41865	2.5	405249	1.5	-0.96	9.60E + 09	0.147
275.437	5736	2.5 3.5	393595 368796	1.5 3.5	-0.51	1.49E+10	0.343 0.254
275.461	33744	4.5	396772	3.5	-0.93	1.03E + 10	0.092
275.664	30441	2.5	393202	3.5	-0.79	1.42E + 10	0.173
276.015	26023	3.5 4 ¤	388322	4.5 1 ¤	-0.19	5.68E+10 3.10EJ 10	0.707
276.073	5736	3.5	367959	2.5	-0.28	4.59E+10	0.437
276.113	30441	2.5	392612	3.5	-0.65	1.98E + 10	0.325
276.139	41865	2.5	404002	2.5	-0.56	2.38E+10 1.34E-10	0.199
276.23	27662	4.0 5.5	389679	5.5	0.63	3.76E+11	0.200
276.326	30441	2.5	392332	1.5	-0.57	2.34E + 10	0.226
276.355	5736	3.5	367590	4.5	-0.96	9.48E+09	0.092
276.452 276.452	45079 16903	3.5 1.5	406806 378630	$\frac{3.5}{2.5}$	0.07	1.04E+11 1.55E+10	0.57 0.244
276.475	20666	4.5	382362	4.5	-0.13	6.54E + 10	0.365
276.562	27420	1.5	389002	2.5	-0.53	2.60E + 10	0.198
276.605	20666	4.5	382193 301659	5.5 1 F	-0.43	3.25E+10	0.325
276.921	10382	$^{2.0}_{1.5}$	371496	1.5 1.5	-0.8	1.39E+10 8.83E+09	$0.145 \\ 0.148$
277.199	26023	3.5	386775	3.5	-0.41	3.39E + 10	0.354
277.269	27662	5.5	388322	4.5	-0.66	1.90E+10	0.183
277.454	66339 8600	1.5 2.5	426759 368956	2.5	-0.34 -0.86	3.93E+10 1.21E±10	0.478 0.170
278.197	33744	4.5	393202	3.5	-0.82	1.32E+10	0.097
278.407	27420	1.5	386607	2.5	-0.72	1.63E + 10	0.204
278.548	41865	2.5	400870	3.5	-0.38	3.55E+10	0.307
278.802	45079 26023	3.5 3.5	404002 384701	2.5 2.5	-0.99	o.(1E+09 9.40E+09	0.141 0.084
278.837	18509	2.5	377141	2.5	-0.89	1.10E + 10	0.192
278.938	26023	3.5	384525	4.5	-0.69	1.73E+10	0.561
278.943	U 20666	4.5 4.5	358496 378005	$\frac{4.5}{5.5}$	-0.46 -0.82	2.98E+10 1 30E+10	0.322 0.177
279.142	27662	4.5 5.5	385902	5.5	-0.24	4.93E+10	0.709
279.342	20666	4.5	378650	4.5	-0.06	7.52E + 10	0.499
279.544	18509	2.5	376235	3.5	-0.93	1.01E+10	0.133
279.684 279.853	0 30441	$\frac{4.5}{2.5}$	357547 387772	3.5 3.5	-0.13 -0.55	0.27E+10 2.42E+10	0.349 0.331
279.892	27420	1.5	384701	2.5	-0.88	1.12E + 10	0.121
			220				

	г.	Fable .	A24: Con	tinue	d		
Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA	CF
280.044	41865	2.5	398952	$2.\hat{5}$	-0.89	1.10E + 10	0.13
280.066	27662	5.5	384721	5.5	-0.93	1.00E + 10	0.127
280.22	27662	5.5	384525	4.5	-0.69	1.73E + 10	0.177
280.341	45079	3.5	401788	3.5	-0.48	2.79E + 10	0.434
280.632	26023	3.5	382362	4.5	-1	8.49E + 09	0.108
280.636	30441	2.5	386775	3.5	-0.56	2.32E + 10	0.426
280.659	5736	3.5	362040	3.5	-0.71	1.67E + 10	0.151
281.362	27662	5.5	383076	6.5	-0.48	2.81E + 10	0.915
281.367	41865	2.5	397273	2.5	-0.31	4.16E + 10	0.205
281.48	10382	1.5	365647	1.5	-0.94	9.68E + 09	0.157
281.555	0	4.5	355170	3.5	-0.93	9.92E + 09	0.25
281.565	8699	2.5	363857	2.5	-0.88	1.10E + 10	0.179
281.671	66339	1.5	421363	2.5	-0.69	1.71E + 10	0.477
281.764	41865	2.5	396772	3.5	-0.74	1.53E + 10	0.186
281.936	27420	1.5	382111	0.5	-0.58	2.20E + 10	0.302
282.021	66339	1.5	420923	1.5	-0.74	1.52E + 10	0.258
282.099	30441	2.5	384926	3.5	-0.93	9.78E + 09	0.2
282.208	5736	3.5	360085	2.5	-0.52	2.55E + 10	0.293
282.259	20666	4.5	374950	5.5	-0.85	1.19E + 10	0.331
282.365	39221	1.5	393373	2.5	-0.96	9.14E + 09	0.136
282.587	45079	3.5	398952	2.5	-0.91	1.03E + 10	0.095
283.106	18509	2.5	371734	3.5	-0.74	1.52E + 10	0.183
283.463	5736	3.5	358516	2.5	-0.7	1.64E + 10	0.311
283.661	45079	3.5	397612	4.5	-1	8.39E + 09	0.178
283.827	8699	2.5	361026	1.5	-0.37	3.52E + 10	0.328
283.909	33744	4.5	385969	4.5	-0.81	1.28E + 10	0.061
284.244	5736	3.5	357547	3.5	-0.81	1.28E + 10	0.236
284.707	10382	1.5	361620	0.5	-0.57	2.21E + 10	0.332
284.745	0	4.5	351191	4.5	-0.67	1.74E + 10	0.352
284.933	45079	3.5	396039	4.5	-0.54	2.37E + 10	0.557
285.171	16903	1.5	367570	0.5	-0.51	2.55E + 10	0.572
285.19	10382	1.5	361026	1.5	-0.89	1.06E + 10	0.263
285.883	41865	2.5	391658	1.5	-0.96	9.06E + 09	0.163
286.101	27662	5.5	377189	6.5	-0.65	1.84E + 10	0.901
286.534	45079	3.5	394078	4.5	-0.48	2.70E + 10	0.359
286.71	39221	1.5	388005	2.5	-0.79	1.32E + 10	0.171
286.715	27420	1.5	376198	2.5	-0.97	8.69E + 09	0.109
286.854	18509	2.5	367119	1.5	-0.43	3.00E + 10	0.364
287.274	45079	3.5	393179	4.5	-0.41	3.11E + 10	0.401
287.389	0	4.5	347961	3.5	-0.4	3.22E + 10	0.349
287.742	45079	3.5	392612	3.5	-0.98	8.37E + 09	0.097
287.826	30441	2.5	377873	3.5	-0.96	8.81E + 09	0.187
287.901	66339	1.5	413681	1.5	-0.31	3.98E + 10	0.571
288.248	20666	4.5	367590	4.5	-0.83	1.18E + 10	0.108
289.395	21571	0.5	367119	1.5	-0.73	1.50E + 10	0.226
289.563	18509	2.5	363857	2.5	-0.94	9.25E + 09	0.199
289.61	18509	2.5	363801	3.5	-0.9	9.92E + 09	0.246
289.847	18509	2.5	363519	2.5	-0.32	3.83E + 10	0.364
291.234	41865	2.5	385231	3.5	-0.26	4.32E + 10	0.43
291.391	16903	1.5	360085	2.5	-0.76	1.35E + 10	0.263
291.947	5736	3.5	348264	2.5	-0.77	1.32E + 10	0.2
294.598	45079	3.5	384525	4.5	-0.7	1.52E + 10	0.368
294.952	18509	2.5	357547	3.5	-0.79	1.23E + 10	0.336

a: Experimental values from [38]

Cs IV-VII

$\mathbf{Cs}\ \mathbf{IV}$

Energy Levels

Table A25: Comparison between available experimental data and calculated energy levels (in $\rm cm^{-1})$ in Cs IV

) 0.0	- •			
E^a_{exp}	E^b_{calc}	ΔE	J	Leading components (in %) in LS coupling c
Even Parity	96	96	2	82.8 $5e^{2}5p^{4}$ (³ P) ³ P \pm 13.1 $5e^{2}5p^{4}$ (¹ D) ¹ D
9749.4	9857	107.6	0	$72.65^{2}5^{2}5^{4}$ (³ P) ³ P + $73.25^{2}5^{2}5^{4}$ (¹ S) ¹ S
12902	12910	-107.0	1	$(1)^{12.0} (35^{2}5p^{4})^{17} + 25.2^{10} (35^{10})^{17} + 25.2^{10} $
20754	20769	-15	2	$82.5s^{2}5p^{4}$ (¹ D) ¹ D + 13.1.5s ² 5p ⁴ (³ P) ³ P
43279.4	43245	34.4	0	$71.85s^25p^4$ (¹ S) ¹ S + 23.15s ² 5p ⁴ (³ P) ³ P
Odd Parity	40240	01.1	0	11.0 05 0p (5) 5 20.1 05 0p (1) 1
114307.7	114559	-251.3	2	76 $5s5p^5$ (² S) ³ P + 14.8 $5s^25p^35d$ (² D) ³ P + 6.2 $5s^25p^35d$ (² P) ³ P
121242.5	121377	-134.5	1	$65.3 \ ss5p^{5}$ (² S) ³ P + 14.4 $5s^{2}5p^{3}sd$ (² D) ³ P + 5.9 $5s^{2}5p^{3}sd$ (² P) ³ P
128086.3	127893	193.3	0	$70.2 \ 5s5p^5$ (² S) ³ P + 16.7 $5s^25p^35d$ (² D) ³ P + 5.9 $5s^25p^35d$ (² P) ³ P
136143.1	136175	-31.9	2	$69.8 \ 5s^2 5p^3 5d \ (^4S) \ ^5D + 7.1 \ 5s^2 5p^3 5d \ (^2P) \ ^3D + 5.7 \ 5s^2 5p^3 5d \ (^4S) \ ^3D$
135979.9	136185	-205.1	3	$73 5s^25p^35d$ (⁴ S) ⁵ D + $6.8 5s^25p^35d$ (² P) ³ F + $6.5 5s^25p^35d$ (² P) ³ D
136625.7	136529	96.7	0	$80.3 \ 5s^2 5p^3 5d \ (^4S) \ ^5D + 6.8 \ 5s^2 5p^3 5d \ (^2P) \ ^3P$
136868.6	136871	-2.4	1	$82.8 \ 5s^2 5p^3 5d \ (^4S)^5 D$
141402.9	141043	359.9	1	$41.3 \ 5s^2 5p^3 5d \ (^2D) \ ^1P + 35.2 \ 5s5p^5 \ (^2S) \ ^1P + 6.5 \ 5s5p^5 \ (^2S) \ ^3P$
142167	142307	-140	2	$22.8 5s^{2}5p^{3}5d ({}^{4}S) {}^{3}D + 19.1 5s^{2}5p^{3}5d ({}^{2}D) {}^{3}D + 18.9 5s^{2}5p^{3}5d ({}^{4}S) {}^{5}D$
147695.5	147934	-238.5	3	$33.1 5s^2 5p^3 5d$ (⁴ S) ³ D + 27.7 $5s^2 5p^3 5d$ (² D) ³ D + 17.5 $5s^2 5p^3 5d$ (⁴ S) ⁵ D
148640	148616	24	1	$49.5 \ 5s^2 5p^3 5d \ (^4S) \ ^3D + 36.4 \ 5s^2 5p^3 5d \ (^2D) \ ^3D$
150982.7	151200	-217.3	2	$50.7 5s^2 5p^3 5d$ (² D) ³ F + 20.5 $5s^2 5p^3 5d$ (² D) ³ D + 12.9 $5s^2 5p^3 5d$ (⁴ S) ³ D
152832.1	151413	1419.1	0	$81.2 5s^{2}5p^{3}5d (^{2}D) ^{1}S + 7.1 5s^{2}5p^{3}5d (^{2}P) ^{3}P + 5.6 5s^{2}5p^{3}5d (^{4}S) ^{5}D$
152776.7	153154	-377.3	3	$63.8 5s^{2}5p^{3}5d (^{2}D) {}^{3}F + 8.9 5s^{2}5p^{3}5d (^{2}D) {}^{3}D + 7.8 5s^{2}5p^{3}5d (^{2}P) {}^{3}F$
155045.5	155818	-772.5	3	$62.5 \ 5s^{2}5p^{3}5d \ (^{2}D) \ ^{3}G + 13.8 \ 5s^{2}5p^{3}5d \ (^{2}D) \ ^{3}F + 7.1 \ 5s^{2}5p^{3}5d \ (^{2}P) \ ^{1}F$
162425.9	162117	308.9	1	$40.8 5s^{2}5p^{3}5d ({}^{2}D)_{5}^{3}D + 34.1 5s^{2}5p^{3}5d ({}^{2}P)_{5}^{3}D + 8.9 5s^{2}5p^{3}5d ({}^{4}S)^{3}D$
164609.5	164599	10.5	2	$74.2 5s^{2}5p^{3}6s ({}^{4}S) {}^{5}S + 14.3 5s^{2}5p^{3}6s ({}^{2}P) {}^{3}P$
166472.1	166537	-64.9	2	$29 5s^{2}5p^{3}5d (^{2}P) {}^{1}D + 17.4 5s^{2}5p^{3}5d (^{2}D) {}^{1}D + 16.7 5s^{2}5p^{3}5d (^{2}P) {}^{3}F$
167553.8	167863	-309.2	1	$46.2 \ 5s^{2} 5p^{3} 6s \ (^{4}S) \ ^{3}S + 13.5 \ 5s^{2} 5p^{3} 5d \ (^{2}P) \ ^{3}P + 10.3 \ 5s^{2} 5p^{3} 5d \ (^{2}D) \ ^{3}S$
169843.8	169324	519.8	0	$43.6 5s^2 5p^3 5d (^2P) ^3P + 31.8 5s^2 5p^3 5d (^2D) ^3P + 12 5s^2 5p^3 5d (^2D) ^1S$
170401.9	170004	397.9	2	$30.1 5s^{2}5p^{3}5d$ (² P) ³ D + 17.9 $5s^{2}5p^{3}5d$ (⁴ S) ³ D + 17.1 $5s^{2}5p^{3}5d$ (² D) ³ D
171449.5	170569	880.5	1	$34.5 5s^{2}5p^{3}5d$ (² P) ³ P + 25.1 $5s^{2}5p^{3}6s$ (⁴ S) ³ S + 13.5 $5s^{2}5p^{3}5d$ (² D) ³ P
173942.4	173752	190.4	3	$41.9 5s^{2}5p^{3}5d (^{2}D) ^{3}D + 20.7 5s^{2}5p^{3}5d (^{4}S) ^{3}D + 12.1 5s^{2}5p^{3}5d (^{2}P) ^{4}F$
174718.7	175394	-675.3	2	$56 5s^2 5p^3 5d ({}^{2}P) {}^{3}F + 17.7 5s^2 5p^3 5d ({}^{2}D) {}^{3}F + 12 5s^2 5p^3 5d ({}^{2}P) {}^{3}P$
174789.4	175490	-700.6	3	$61.2 5s^{2}5p^{5}5d ({}^{2}P) {}^{3}F + 21.7 5s^{2}5p^{5}5d ({}^{2}P) {}^{3}D + 8.3 5s^{2}5p^{5}5d ({}^{2}D) {}^{3}G$
179159.8	178997	162.8	2	$32 5s^{-}5p^{-}5d (^{-}D) ^{+}P + 23.2 5s^{-}5p^{-}5d (^{-}P) ^{+}P + 13.7 5s5p^{-} (^{-}S) ^{+}P$
179477.8	179928	-450.2	1	$19.6 \text{ss}^{-5}\text{p}^{\circ}\text{5d} (^{-}\text{D}) ^{\circ}\text{P} + 33 \text{ss}^{-5}\text{p}^{\circ}\text{5d} (^{-}\text{D}) ^{\circ}\text{S} + 21.6 \text{ss}^{-5}\text{p}^{\circ}\text{6s} (^{-}\text{D}) ^{\circ}\text{D}$
180538.2	180199	339.2	3	$31.4 \text{5}^{-5}\text{5}^{-5}\text{5}\text{6}(^{-}\text{D}) = F + 26.1 \text{5}^{-5}\text{5}^{-5}\text{5}\text{6}(^{-}\text{P}) = D + 20 \text{5}^{-5}\text{5}^{-5}\text{5}\text{6}(^{-}\text{S}) = D$
181944.8	182111	-166.2	2	$50.2 \text{5s}^{-5} \text{5s}^{-1} $
102011	182390	121	2	$35.5 \ 5s \ 5p^{-}5d(-p)^{-}r + 25.0 \ 5s \ 5p^{-}5d(-D)^{-}r + 7.7 \ 5s \ 5p^{-}5d(-S)^{-}D$
102070.0	182973	-401.7	2	48 55 50 05 (D) $^{+}$ D + 14.5 55 50 05 (S) $^{+}$ S + 12.0 55 50 50 (D) $^{+}$ F 72 2 5 2 5 3 5 2 6 2 (2D) 3 D + 10 1 5 2 5 3 5 3 5 4 (2 D) 1 F + 0.2 5 2 5 3 5 4 (2 D) 1 F
100/10.0	185018	750.1	1	(3.2 ss sp os (D) D + 10.1 ss sp sd (P) F + 9.2 ss sp sd (D) F
185915.9	187087	-759.1	2	51.855 5p 5d (D) 5 ± 19.055 p (S) 1 ± 10.55 p 5d (D) $1 = 10.55$ f 36.25
180217.8	188884	220.4	2	51.55 5p 5d (D) D + 19.4 5s 5p 5d (P) D + 10.2 5s 5p 6s (D) D $50.65e^{2}5p^{3}6e^{-2}D)^{-1}D + 17.5e^{2}5p^{3}6e^{-2}D)^{-3}D + 11.35e^{2}5p^{3}5d^{-2}P)^{-3}D$
180301 7	180104	107.7	1	$31.5e^{2}5p^{3}5d$ (² P) ³ D + 14.8 $5e^{2}5p^{3}5d$ (² P) ¹ P + 13.3 $5e^{2}5p^{3}5d$ (⁴ S) ³ D
190309.8	190123	186.8	3	$27.65s^25p^{3}5d(^{2}P)^{3}D + 21.45s^25p^{3}6s(^{2}D)^{3}D + 21.25s^25p^{3}5d(^{2}P)^{1}F$
192952	192246	706	0	$33.2.5s^{2}5p^{3}5d({}^{2}D) {}^{3}P + 32.2.5s^{2}5p^{3}5d({}^{2}P) {}^{3}P + 16.2.5s5p^{5}({}^{2}S) {}^{3}P$
194685.9	194638	47.9	1	$18.3.5s^{2}5p^{3}5d(^{2}D)$ $^{1}P + 18.2.5s5p^{5}(^{2}S)$ ^{1}P
198135.3	198085	50.3	0	$86.8.5s^25p^36s(^2P)^{3}P + 7.5.5s^25p^35d(^2D)^{3}P$
197380.8	198310	-929.2	2	$45.4 5s^25p^35d$ (² D) ¹ D + 18.5 $5s^25p^35d$ (² P) ¹ D + 15.9 $5s^25p^35d$ (² P) ³ D
198514.1	198580	-65.9	1	$63.5s^25p^36s$ (² P) ³ P + 21.7 $5s^25p^36s$ (² P) ¹ P
199392.1	199058	334.1	3	$40.9 5s^{2}5p^{3}5d$ (² P) ¹ F + 34.9 $5s^{2}5p^{3}5d$ (² D) ¹ F + 6.7 $5s^{2}5p^{3}5d$ (⁴ S) ³ D
207937.6	207733	204.6	2	$67.7 5s^{2}5p^{3}6s$ (² P) ³ P + 12.9 $5s^{2}5p^{3}6s$ (² D) ³ D + 11.3 $5s^{2}5p^{3}6s$ (² D) ¹ D
208500	208754	-254	1	$48.9 5s^{2}5p^{3}6s(^{2}P)^{1}P + 18.9 5s^{2}5p^{3}6s(^{2}D)^{3}D + 17.7 5s^{2}5p^{3}6s(^{2}P)^{3}P$
246061	245994	67	2	$70.5 \ 5s^2 5p^3 6d \ (^4S) \ ^5D + 9 \ 5s^2 5p^3 6d \ (^2P) \ ^3D + 6.8 \ 5s^2 5p^3 6d \ (^4S) \ ^3D$
246089.4	246060	29.4	3	$72.2 \ 5s^2 5p^3 6d \ (^4S) \ ^5D + 7.6 \ 5s^2 5p^3 6d \ (^2P) \ ^3D + 7.2 \ 5s^2 5p^3 6d \ (^2P) \ ^3F$
246233	246183	50	1	$80.3 \ 5s^2 5p^3 6d \ (^4S) \ ^5D + 9.5 \ 5s^2 5p^3 6d \ (^2P) \ ^3P$
248688	248744	-56	2	$56.7 \ 5s^2 5p^3 6d \ (^4S) \ ^3D + 11.1 \ 5s^2 5p^3 6d \ (^2P) \ ^1D + 10.1 \ 5s^2 5p^3 6d \ (^4S) \ ^5D$
250634.2	250479	155.2	1	$77.5 \ 5s^2 5p^3 6d \ (^4S) \ ^3D + 7.6 \ 5s^2 5p^3 6d \ (^2P) \ ^1P + 5.6 \ 5s^2 5p^3 6d \ (^2P) \ ^3D$
250415.4	250690	-274.6	3	$68.1 \ 5s^2 5p^3 6d \ (^4S) \ ^3D + 10.4 \ 5s^2 5p^3 6d \ (^2P) \ ^1F + 7.9 \ 5s^2 5p^3 6d \ (^4S) \ ^5D$
251551.7	251582	-30.3	2	$70.2 \ 5s^2 5p^3 7s \ (^4S) \ ^5S + 20.5 \ 5s^2 5p^3 7s \ (^2P) \ ^3P + 5.5 \ 5s^2 5p^3 7s \ (^2D) \ ^3D$
253194.4	253181	13.4	1	$64.8 \ 5s^2 5p^3 7s \ (^4S) \ ^3S + 14.6 \ 5s^2 5p^3 7s \ (^2P) \ ^1P + 11.8 \ 5s^2 5p^3 7s \ (^2D) \ ^3D$
261177.8	261224	-46.2	2	$58.5 \ 5s^2 5p^3 6d \ (^2D) \ ^3F + 11.6 \ 5s^2 5p^3 6d \ (^4S) \ ^3D + 7 \ 5s^2 5p^3 6d \ (^4S) \ ^5D$
261868.3	261761	107.3	1	$53.1 \ 5s^2 5p^3 6d \ (^2D) \ ^3D + 17.6 \ 5s^2 5p^3 6d \ (^2D) \ ^1P + 8 \ 5s^2 5p^3 6d \ (^4S) \ ^5D$
261644.7	261763	-118.3	3	$46.6 5s^{2}5p^{3}6d {\binom{2}{D}}{}^{3}F + 16.2 5s^{2}5p^{3}6d {\binom{2}{D}}{}^{3}D + 8.8 5s^{2}5p^{3}6d {\binom{2}{P}}{}^{3}D$
262150.2	262160	-9.8	3	$59.2 \ 5s^{2}5p^{3}6d \ (^{2}D) \ ^{3}G + 12.4 \ 5s^{2}5p^{3}6d \ (^{4}S) \ ^{3}D + 7.8 \ 5s^{2}5p^{3}6d \ (^{2}P) \ ^{3}F$
262537	262218	319	0	$54.4 \ 5s^{2} 5p^{3} 6d \ (^{2}D) \ ^{1}S + 20.5 \ 5s^{2} 5p^{3} 6d \ (^{2}D) \ ^{3}P + 13.1 \ 5s^{2} 5p^{3} 6d \ (^{2}P) \ ^{3}P$
264175.5	264280	-104.5	2	$24.4 5s^{2}5p^{3}6d (^{2}D) {}^{3}P + 31.8 5s^{2}5p^{3}6d (^{2}D) {}^{3}D + 14 5s^{2}5p^{3}6d (^{4}S) {}^{3}D$
265107.3	265152	-44.7	1	$29.8 5s^{2}5p^{3}6d (^{2}D) {}^{3}P + 25.4 5s^{2}5p^{3}6d (^{2}D) {}^{3}S + 15.1 5s^{2}5p^{3}6d (^{2}D) {}^{1}P$
267056.1	266938	118.1	2	$43.5 5\text{s}^{2}5\text{p}^{3}7\text{s}$ (² D) ³ D + 21 $5\text{s}^{2}5\text{p}^{3}7\text{s}$ (⁴ S) ³ S + 19.9 $5\text{s}^{2}5\text{p}^{3}7\text{s}$ (² D) ¹ D
267199.4	267145	54.4	3	$63.7 5s^{2}5p^{3}6d (^{2}D) ^{3}D + 27.6 5s^{2}5p^{3}6d (^{2}D) ^{3}F$
267211	267258	-47	1	$62.9 5s^{-}5p^{-}7s (^{2}D) + 25.8 5s^{-}5p^{-}7s (^{4}S) + 5 5s^{-}5p^{-}7s (^{2}P) + P$
268007.3	268056	-48.7	2	$43.7 5s^{-}5p^{-}6d (^{-}D) ^{-}D + 32.6 5s^{-}5p^{-}6d (^{-}D) ^{-}P + 10.7 5s^{-}5p^{-}6d (^{-}D) ^{-}D$
268328	268130	198	0	p_{z} as a p p_{z} p_{z} $(T_{z}) = P + 33.9$ as a p p_{z} p_{z} $(T_{z}) = S$

Table A25. Continued

				Table A25. Commuted
E^a_{exp}	E^{b}_{calc}	ΔE	J	Leading components (in $\%$) in LS coupling ^c
268521.1	268496	25.1	1	$35.4 \ 5s^2 5p^3 6d \ (^2D) \ ^1P + 32.9 \ 5s^2 5p^3 6d \ (^2D) \ ^3P + 24.6 \ 5s^2 5p^3 6d \ (^2D) \ ^3D$
269477.7	269838	-360.3	1	$59.6 \ 5s^2 5p^3 6d \ (^2D) \ ^3S + 21.1 \ 5s^2 5p^3 6d \ (^2D) \ ^3P + 16.4 \ 5s^2 5p^3 6d \ (^2D) \ ^1P$
270015.6	270145	-129.4	2	$58.4 \ 5s^2 5p^3 6d \ (^2D) \ ^1D + 26.8 \ 5s^2 5p^3 6d \ (^2D) \ ^3P + 6.6 \ 5s^2 5p^3 6d \ (^2D) \ ^3F$
270688.4	270491	197.4	3	$72.9 \ 5s^2 5p^3 6d \ (^2D) \ ^1F + 11.6 \ 5s^2 5p^3 6d \ (^2D) \ ^3D + 5.3 \ 5s^2 5p^3 6d \ (^2D) \ ^3G$
272133.7	272152	-18.3	3	$98.8 \ 5s^2 5p^3 7s \ (^2D) \ ^3D$
272805.3	272831	-25.7	2	$64.9 \ 5s^2 5p^3 7s \ (^2D) \ ^1D + 33.6 \ 5s^2 5p^3 7s \ (^2D) \ ^3D$
278199.8	278247	-47.2	2	$71.4 \ 5s^2 5p^3 6d \ (^2P) \ ^3F + 17.9 \ 5s^2 5p^3 6d \ (^2P) \ ^1D$
279262.5	279238	24.5	2	$39.3 \ 5s^2 5p^3 6d \ (^2P) \ ^3P + 38.5 \ 5s^2 5p^3 6d \ (^2P) \ ^3D + 17.7 \ 5s^2 5p^3 6d \ (^2P) \ ^1D$
279539.7	279471	68.7	3	$52.2 \ 5s^2 5p^3 6d \ (^2P) \ ^3F + 22.9 \ 5s^2 5p^3 6d \ (^2P) \ ^3D + 20.7 \ 5s^2 5p^3 6d \ (^2P) \ ^1F$
280241.9	280361	-119.1	1	$56.9 \ 5s^2 5p^3 6d \ (^2P) \ ^3D + 21.5 \ 5s^2 5p^3 6d \ (^2P) \ ^1P + 15.5 \ 5s^2 5p^3 6d \ (^2P) \ ^3P$
283542	283545	-3	0	$98.4 \ 5s^2 5p^3 7s \ (^2P)^{-3}P$
283908	283915	-7	1	$67.7 \ 5s^2 5p^3 7s \ (^2P) \ ^3P + 31 \ 5s^2 5p^3 7s \ (^2P) \ ^1P$
288142	287995	147	1	$55 5s^2 5p^3 6d (^2P) {}^3P + 10.7 5s^2 5p^3 6d (^2P) {}^3D + 8.9 5s^2 5p^3 6d (^2D) {}^1P$
289119	289209	-90	3	$58.6 \ 5s^2 5p^3 6d \ (^2P) \ ^1F + 15.6 \ 5s^2 5p^3 6d \ (^2D) \ ^3G + 10.6 \ 5s^2 5p^3 6d \ (^2P) \ ^3F$
289400.1	289563	-162.9	3	$45.6 \ 5s^2 5p^3 6d \ (^2P) \ ^3D + 16.9 \ 5s^2 5p^3 6d \ (^2P) \ ^3F + 11.1 \ 5s^2 5p^3 6d \ (^2D) \ ^1F$
289626	289807	-181	0	$64.2 \ 5s^2 5p^3 7d \ (^4S) \ ^5D + 20.7 \ 5s5p^4 4f \ (^3P) \ ^5D + 7.7 \ 5s^2 5p^3 7d \ (^2P) \ ^3P$
289723	290023	-300	2	$21.6 \ 5s^2 5p^3 6d \ (^2P) \ ^3D + 23.8 \ 5s^2 5p^3 6d \ (^2P) \ ^1D + 13.6 \ 5s^2 5p^3 6d \ (^2D) \ ^3F$
290157	290433	-276	3	$73.7 \ 5s^2 5p^3 7d \ (^4S) \ ^5D + 5.6 \ 5s^2 5p^3 7d \ (^2P) \ ^3D$
293926.5	291738	2188.5	2	$80.3 \ 5s^2 5p^3 5g \ (^4S) \ ^5G + 10 \ 5s^2 5p^3 5g \ (^2P) \ ^3F + 5.7 \ 5s5p^4 4f \ (^3P) \ ^5G$
292768.2	292384	384.2	1	$41.5s^{2}5p^{3}6d$ (² P) ¹ P + $33.6.5s^{2}5p^{3}7d$ (⁴ S) ³ D
294402.4	293916	486.4	1	$46.9 \ 5s^2 5p^3 7d \ (^4S) \ ^3D + 15.7 \ 5s^2 5p^3 6d \ (^2P) \ ^1P + 10.9 \ 5s^2 5p^3 6d \ (^2P) \ ^3D$

46.9 5s⁻5p⁻/a (⁻S) ⁻D + 15.7 5s⁻0p⁻/b
a: Energy Levels from Sansonetti [39]
b: This work
c: Only the components ≥ 5% are given

<u>\</u>	ra La	L		T	log of	σA	CF
^Ritz	Llow	J_{low}	L_{up}	J_{up}	log gi		C1
A	cm 1	-	cm -			s -	
367.466	0	2	272134	3	-0.73	9.12E + 09	0.403
372.627	20754	2	289119	3	-0.89	6.18E + 09	-0.182
373.124	0	2	268007	2	-0.92	5.72E + 09	0.127
374.252	0	2	267199	3	-0.88	6.34E + 09	0.201
374.453	0	2	267056	2	-0.81	7.35E + 09	0.451
393 222	12902	1	267211	1	-0.75	$7.64E \pm 0.09$	0.495
204.052	12002	2	252104	1	0.56	1.17E + 10	0.55
206 745	20754	2	200104	2	-0.30	1.17 ± 10 1.74 ± 10	-0.00
396.745	20754	2	272805	2	-0.39	1.74E + 10	-0.533
397.973	12902	1	264176	2	-0.88	5.59E+09	0.138
399.336	0	2	250415	3	-0.61	1.04E + 10	-0.208
400.105	20754	2	270688	3	-0.61	1.03E + 10	-0.158
400.82	43279	0	292768	1	-0.92	5.00E + 09	0.176
401.185	20754	2	270016	2	-0.92	5.05E + 09	0.114
512.727	12902	1	207938	2	-0.63	5.98E + 09	0.202
528.492	0	2	189218	2	-0.5	7.46E + 09	-0.051
529.76	9749	0	198514	1	-0.59	6.06E + 09	0.119
532.635	20754	2	208500	1	-0.56	$6.45E \pm 0.09$	-0.164
534 235	20754	2	207938	2	-0.28	$1.22E \pm 10$	0.337
538 448	20104	2	185710	2	0.15	1.22E + 10 $1.64E \pm 10$	0.152
542.068	12002	1	107281	2	-0.15	1.04D + 10 2.62E + 10	0.102
542.008	12902	1	197301	2	0.00	$2.03E \pm 10$ $2.75E \pm 10$	-0.402
547.725	0	2	102575	1	0.23	3.73E+10	-0.341
547.912	0	2	182511	2	-0.44	8.12E + 09	-0.034
549.617	0	2	181945	2	-0.67	4.79E + 09	0.066
550.104	12902	1	194686	1	0.25	3.94E + 10	0.504
553.899	0	2	180538	3	0.9	1.71E + 11	-0.549
555.401	12902	1	192952	0	0.2	3.37E + 10	-0.504
556.662	9749	0	189392	1	0.55	7.54E + 10	-0.485
557.172	0	2	179478	1	0.35	4.88E + 10	0.327
558,161	0	2	179160	2	0.85	1.50E + 11	-0.508
559 791	20754	2	199392	3	1.02	$2.23E \pm 11$	-0.532
566 165	20754	2	107381	2	0.66	$9.54E \pm 10$	0.462
567 164	12002	1	197301	2	0.00	$3.54E \pm 10$ 1 55E ± 10	0.402
507.104	12902	1	109210	4	-0.13	1.55E+10	-0.178
567.651	9749	0	185914	1	-0.42	8.01E+09	0.103
572.117	0	2	1/4/89	3	-0.27	1.11E + 10	-0.25
573.511	12902	1	187267	2	0.68	9.69E + 10	-0.556
574.903	0	2	173942	3	0.36	4.63E + 10	0.154
574.938	20754	2	194686	1	0.4	5.11E + 10	-0.401
577.995	12902	1	185914	1	0.32	4.22E + 10	-0.477
578.624	9749	0	182573	1	-0.7	3.96E + 09	0.072
583.262	0	2	171450	1	-0.09	1.59E + 10	0.153
589.375	12902	1	182573	1	-0.54	5.51E + 09	0.076
591.566	12902	1	181945	2	-0.36	8.42E + 09	0.167
592 987	20754	2	189392	1	-0.54	5.52E + 0.9	-0.153
593 599	20754	2	189218	2	0.43	$5.11E \pm 10$	-0.100
506 822	20704	2	167554	1	0.45	$4.04E \pm 00$	0.041
000.823	10000	2	170479	1	-0.07	4.04E+09	-0.041
600.327	12902	1	179478	1	-0.53	5.46E + 09	0.054
600.701	0	2	100472	2	-0.92	2.21E+09	-0.028
605.474	20754	2	185914	1	0.19	2.82E + 10	-0.238
606.19	20754	2	185719	3	-0.48	6.05E+09	-0.06
607.498	0	2	164610	2	-0.63	4.24E + 09	-0.199
617.973	20754	2	182573	1	-0.97	1.90E + 09	0.062
617.983	12902	1	174719	2	-0.38	7.35E + 09	-0.33
618.429	9749	0	171450	1	-0.59	4.39E + 09	0.072
625.844	20754	2	180538	3	-0.49	5.52E + 09	-0.033
630.726	12902	1	171450	1	-0.49	$5.31E \pm 0.9$	-0.087
631 20	20754	2	179160	2	-0.78	$2.78E \pm 0.0$	0.049
624 021	12002	4	170402	2	-0.76	4.78E+09	0.042
034.921	12902	1	160044	4	-0.34	4.70E+09	0.032
037.179	12902	1	169844	0	-0.99	1.66E+09	-0.058
644.972	0	2	155046	3	-0.66	3.57E + 09	0.108
649 201	20754	2	174789	3	-0.7	3.17E + 09	0.225
010.201	00554	0	174710	2	-0.94	1.82E + 09	0.083
649.5	20754	2	1/4/19	-	0.01		
649.5 652.791	$20754 \\ 20754$	$\frac{2}{2}$	174719 173942	3	-0.48	5.21E + 09	-0.042

Table A26: Computed oscillator strengths and transition probabilities Cs IV.

a: Energy Levels from [39]

Cs V

Energy Levels

Table A27: Comparison between available experimental data and calculated energy levels (in $\rm cm^{-1})$ in Cs V

)	•			
E^a_{exp}	E_{calc}^{b}	ΔE	J	Leading components (in %) in LS coupling c
Odd Parity				
0	-297	297	1.5	76.5 $5s^{2}5p^{3}$ (⁴ S) ⁴ S + 15.4 $5s^{2}5p^{3}$ (² P) ² P + 5.4 $5s^{2}5p^{3}$ (² D) ² D
15077.4	15294	-216.6	1.5	$68.3 \ 5s^{2}5p^{3} \ (^{2}D) \ ^{2}D + 14.9 \ 5s^{2}5p^{3} \ (^{4}S) \ ^{4}S + 13.3 \ 5s^{2}5p^{3} \ (^{2}P) \ ^{2}P$
20373.5	20797	-423.5	2.5	$96.3 5s^2 5p^3 (^2D) ^2D$
31951.1	31750	201.1	0.5	$96 5s^2 5p^3 (^2P) ^2P$
42273.7	42133	140.7	1.5	$67.2 \ 5s^2 5p^3 \ (^2P) \ ^2P + 22.6 \ 5s^2 5p^3 \ (^2D) \ ^2D + 6 \ 5s^2 5p^3 \ (^4S) \ ^4S$
Even Parity				
113901.7	113715	186.7	2.5	84 $5s5p^4$ (³ P) ⁴ P + 8.3 $5s^25p^25d$ (³ P) ⁴ P + 5 $5s5p^4$ (¹ D) ² D
123192.4	123104	88.4	1.5	$82.7 5s5p^4 (^{3}P) ^{4}P + 9.2 5s^25p^25d (^{3}P) ^{4}P$
125858.3	125954	-95.7	0.5	81 $5s5p^4$ (³ P) ⁴ P + 9.2 $5s^25p^25d$ (³ P) ⁴ P + 7.1 $5s5p^4$ (¹ S) ² S
139959.2	140458	-498.8	1.5	$55.7 \ 5s5p^4 \ (^{1}D) \ ^{2}D + 14.6 \ 5s^{2}5p^{2}5d \ (^{1}D) \ ^{2}D + 8.1 \ 5s5p^{4} \ (^{3}P) \ ^{2}P$
144333	144743	-410	2.5	$69.5 \ 5s5p^4 \ (^{1}D) \ ^{2}D + 18.9 \ 5s^{2}5p^{2}5d \ (^{1}D) \ ^{2}D + 5.7 \ 5s5p^{4} \ (^{3}P) \ ^{4}P$
154971.2	154583	388.2	1.5	$33.7 \ 5s^2 5p^2 5d \ (^{3}P) \ ^{2}P + 18.4 \ 5s5p^4 \ (^{3}P) \ ^{2}P + 16.7 \ 5s5p^4 \ (^{1}D) \ ^{2}D$
158248.8	157799	449.8	0.5	$30.9 \ 5s^2 5p^2 5d \ (^{3}P) \ ^{2}P + 31.2 \ 5s5p^4 \ (^{3}P) \ ^{2}P + 20.8 \ 5s5p^4 \ (^{1}S) \ ^{2}S$
157903	158258	-355	1.5	$66.4 \ 5s^2 5p^2 5d \ (^{3}P) \ ^{4}F + 11.7 \ 5s 5p^4 \ (^{3}P) \ ^{2}P + 8.7 \ 5s^2 5p^2 5d \ (^{3}P) \ ^{2}P$
160327.9	160329	-1.1	2.5	$54 5s^2 5p^2 5d (^3P) {}^4F + 25.7 5s^2 5p^2 5d (^3P) {}^4D + 6.2 5s^2 5p^2 5d (^1S) {}^2D$
166800.2	166980	-179.8	2.5	$39.8 5s^2 5p^2 5d (^1D) ^2F + 27 5s^2 5p^2 5d (^3P) ^2F + 24.1 5s^2 5p^2 5d (^3P) ^4F$
167231.1	167718	-486.9	3.5	$71.9 5s^2 5p^2 5d ({}^{3}P) {}^{4}F + 22 5s^2 5p^2 5d ({}^{3}P) {}^{4}D$
169557.9	169711	-153.1	0.5	$63.3 5s^2 5p^2 5d ({}^{3}P) {}^{4}D + 19.4 5s 5p^4 ({}^{1}S) {}^{2}S + 5.9 5s^2 5p^2 5d ({}^{1}D) {}^{2}S$
170736.7	170595	141.7	3.5	$36.4 \ 5s^2 5p^2 5d \ (^1D) \ ^2F + 27.3 \ 5s^2 5p^2 5d \ (^3P) \ ^4D + 14.8 \ 5s^2 5p^2 5d \ (^3P) \ ^2F$
171936.7	172220	-283.3	1.5	$74.9 5s^2 5p^2 5d (^3P) ^4D + 11.4 5s^2 5p^2 5d (^3P) ^4F$
175576.8	175111	465.8	0.5	$27.7 5s5p^4$ (¹ S) ² S + 25.7 $5s^25p^25d$ (³ P) ⁴ D + 19.5 $5s^25p^25d$ (³ P) ² P
175405	175415	-10	2.5	$47.7 5s^25p^25d$ (³ P) ⁴ D + 14.9 $5s^25p^25d$ (³ P) ⁴ F + 11.8 $5s^25p^25d$ (³ P) ² F
184244 5	184647	-402.5	3.5	$33.85s^25p^25d$ (³ P) ⁴ D + 31.15s^25p^25d (¹ D) ² G + 17.5s^25p^25d (³ P) ² F
187619.8	187180	439.8	2.5	$662.5s^25p^25d$ (³ P) ⁴ P + 11.9.5s^25p^25d (³ P) ⁴ D + 6.8.5s^25p^25d (¹ D) ² D
188245.8	187859	386.8	1.5	$382555p^4$ (³ P) ² P + 2815s ² 5p ² 5d (¹ D) ² P + 1285s ² 5p ² 5d (³ P) ² P
189415.9	189230	185.9	3.5	$50.1.5s^25p^25d$ (¹ D) ² G + 30.1. $5s^25p^25d$ (¹ D) ² F + 14. $5s^25p^25d$ (³ P) ⁴ D
189992.1	189967	25.1	1.5	$49.65s^25p^25d$ (³ P) ⁴ P + 8.25s^25p^25d (³ P) ² D + 6.65s^25p^25d (¹ S) ² D
191236 7	190783	453.7	0.5	$58.9.5s^25p^25d$ (³ P) ⁴ P + 14.9.5s^25p^25d (¹ D) ² P + 10.5s^25p^25d (¹ D) ² S
105328 /	195100	228.4	1.5	$40.45s^25p^25d$ (³ P) ² D + 18.95s ² 5p ² 5d (¹ S) ² D + 12.75s ² 5p ² 5d (³ P) ⁴ P
100/03 5	108863	540.5	2.5	$40.4 \text{ bs of bd} (1)^{-1} D + 10.3 \text{ bs of bd} (2)^{-1} D + 12.7 \text{ bs of bd} (1)^{-1}$ $44.5 5s^25p^25d (^{3}P)^{-2}D + 10.3 5s^25p^25d (^{3}P)^{-2}F + 13.9 5s^25p^25d (^{1}D)^{-2}D$
200123.6	199740	383.6	0.5	44.5 55 5p 5d (1) $D + 15.5$ 55 5p 5d (1) $P + 15.5$ 55 5p 5d (D) D 40.8 $5e^{2}5p^{2}6e^{-3}P + 20.5e^{2}5p^{2}5d^{-1}D + 15.5e^{2}5p^{2}6e^{-3}P + 2P$
200123.0	201077	64.6	0.5	$40.855506(1)$ 1 $\pm 29550950(1)$ 1 $\pm 1655250^{2}5d(3P)$ 4P $\pm 14.852^{2}50^{2}5d(1D)$ 2P
201141.0	201011	76.0	1.5	$24.2 535p$ (1) 1 \pm 10.5 55 5p 5d (1) 1 \pm 14.6 55 5p 5d (D) 1 55 2 5c ² 5p ² 5d (1D) 2D \pm 12 2 5c5p ⁴ (1D) 2D \pm 0.8 5c ² 5p ² 5d (1D) 2D
200373.9	206522	1210.9	0.5	25.3 55 5p 5d (D) = 15.3 5s5p (D) = 9.6 5s 5p 5d (D) = 1
205205.2	200523	-1319.0	0.5	$25.4 55 5p 5d (D) 1 + 24.2 55 5p 6s (1) 1 + 15 55 5p 5d (D) 5 26 \pm 22 \pm$
200712	200334	1071 4	2.5	20.55 Sp $5d(D)$ $D + 21.5$ SS $5p$ $5d(D)$ $F + 10.2$ SS $5p$ $5d(T)$ F
211084.4	210013	1071.4	2.0	41.6 3s 3p 3d (S) $D + 20.9$ 3s 3p 3d (D) $D + 17.7$ 3s 3p 3d (P) D
210475.5	210247	220.3	3.0	$50.4 \text{ 5s } \text{5p } 5d(\mathbf{F}) + 25.4 \text{ 5s } \text{5p } 5d(\mathbf{D}) + 75 \text{ 5p } 5d(\mathbf{D}) + 25.4 \text{ 5s } \text{5p } 5d(\mathbf{D}) + 10.7 \text{ 5s } \text{5p } 5d(\mathbf{D}) + 10.7 \text{ 5s } \text{5p } 5d(\mathbf{D}) + 10.7 \text{ 5s } \text{5p } \text{5d}(\mathbf{D}) + 10.7 \text{ 5s } \text{5d}(\mathbf{D}) + 10.7 \text{ 5s } \text{5d}(\mathbf{D}) + 10.7 \text{5s } \text{5d}(D$
211470.1	211137	1207.0	1.0	$(1.758 \text{ Sp OS}(-\Gamma)) = + 10.758 \text{ Sp OS}(-\Gamma) = - 17.45.25 25.(3D) 2D$
214163.1	215561	-1397.9	1.5	$24.8 \text{ ss}^{-}\text{sp}^{-}\text{sd} (^{-}\text{D})^{-}\text{P} + 15.0 \text{ ss}^{-}\text{sp}^{-}\text{sd} (^{-}\text{P})^{-}\text{P} + 15.4 \text{ ss}^{-}\text{sp}^{-}\text{ss} (^{-}\text{P})^{-}\text{P}$
210035.5	215996	639.5	0.5	57.5 as ap os (P) P + 18.5 as ap od (D) S + 9 as ap os (P) P
21/(54.6	217690	04.0	2.5	$01.1 \text{ os } \text{op } \text{os } (^{-}\text{P}) = P + 21.0 \text{ os } \text{op } \text{os } (^{-}\text{D}) = D + 5.8 \text{ os } \text{op } \text{os } (^{+}\text{S}) = D$
220013.2	220236	-222.8	0.5	$27.4 \text{ bs}^{-}\text{5p}^{-}\text{5d} (^{-}\text{D})^{-}\text{S} + 15 \text{ 5s}^{-}\text{5p}^{-}\text{5d} (^{+}\text{P})^{-}\text{P} + 12.5 \text{ 5s}^{-}\text{5p}^{-} (^{+}\text{P})^{-}\text{P}$
221933.8	222642	-708.2	1.5	$32.3 \text{ ss } \text{ sp } \text{ os } (^{-}P)^{-}P + 34.1 \text{ ss } \text{ sp } \text{ os } (^{-}D)^{-}D + 9.8 \text{ ss } \text{ sp } \text{ 5d } (^{-}D)^{-}P$
224000.6	223990	10.6	2.5	14.0 $\text{ps}^{-2}\text{p}^{-2}\text{d}({}^{\circ}\text{P}) = \text{F} + 30.4 \text{ ps}^{-2}\text{p}^{-2}\text{d}({}^{\circ}\text{S}) = D + 28.9 \text{ ps}^{-2}\text{p}^{-2}\text{d}({}^{\circ}\text{P}) = D$
223839.4	224621	-781.6	1.5	$48.4 \text{ss}^{-5} \text{p}^{-5} $
235192.8	235205	-12.2	2.5	$69.9 \text{s}^{-} \text{s}^{-} \text{o}^{-} \text{(}^{-} \text{D}) \stackrel{\text{a}}{\rightarrow} \text{D} + 26.4 \text{s}^{-} \text{s}^{-} \text{f}^{-} \text{s}^{-} \text{(}^{-} \text{P}) \stackrel{\text{a}}{\rightarrow} \text{P}$
237340	237087	253	1.5	$53.3 5s^{-}5p^{-}6s (^{-}D) + 37.7 5s^{-}5p^{-}6s (^{-}P) + P$
252603.3	252564	39.3	0.5	$86.2 \ 5s^2 5p^2 6s \ (^{\circ}S) \ ^{\circ}S + 6.5 \ 5s^2 5p^2 6s \ (^{\circ}P) \ ^{\circ}P$

a: Energy Levels from Sansonetti [39] b: This work c: Only the components ≥ 5% are given

λ_{Ritz}	E^a_{low}	J_{low}	Eup	Jup	log gf	gA	CF
Å	cm^{-1}	1 5	cm^{-1}	1 5	0.00	s ⁻¹	0.020
449.918	21051	1.5	237340	1.5	-0.99	3.38E+09	-0.032
454 307	15077	1.5	235193	2.5	-0.32	1.54E+10	0.382
459.233	0	1.5	217755	2.5	-0.11	2.46E + 10	0.319
460.901	20374	2.5	237340	1.5	-0.49	1.01E + 10	0.135
465.508	20374	2.5	235193	2.5	-0.05	2.74E + 10	-0.354
472.867	0	1.5	211476	1.5	-0.39	1.22E + 10	0.183
475.444	42274	1.5	252603	0.5	-0.73	5.56E + 09 7.74E + 00	0.169
485.427	15077	1.5	221934	1.5	-0.37	1.74E+09 1.59E+10	0.103
491.094	20374	2.5	224001	2.5	-0.96	3.02E+09	0.017
496.129	20374	2.5	221934	1.5	-0.24	1.57E + 10	-0.113
496.135	15077	1.5	216636	0.5	-0.42	1.02E + 10	0.14
499.691	0	1.5	200124	0.5	-0.43	9.99E+09	0.21
511 958	0	1.5	199404	2.5	-0.07	2.24E+10 2.23E+10	-0.264
512.646	42274	1.5	237340	1.5	0.3	5.07E+10	-0.599
516.024	20374	2.5	214163	1.5	-0.19	1.64E + 10	0.108
518.352	42274	1.5	235193	2.5	-0.29	1.27E + 10	-0.279
521.137	31951	0.5	223839	1.5	0.33	5.30E + 10	0.285
521.826	15077	1.5	206712	2.5	0.52	8.11E+10	0.255
522.745	15077	1.5	200370	1.5	0.34	$5.31E \pm 10$ $5.83E \pm 10$	0.591
523.279	20374	2.5	211476	1.5	-0.39	9.91E+09	-0.287
524.354	20374	2.5	211084	2.5	-0.25	1.34E + 10	0.09
525.968	15077	1.5	205203	0.5	-0.91	2.98E + 09	0.028
526.034	20374	2.5	210475	3.5	1.02	2.53E+11	0.62
526.338	0 31051	1.5	189992	1.5	0.62	1.00E+11 6.20E+10	0.497
531 739	31951	0.5	221934	0.5	-0.95	2.64E+09	-0.024
532.993	0	1.5	187620	2.5	0.77	1.38E + 11	0.597
536.658	20374	2.5	206712	2.5	0.65	1.02E + 11	0.553
537.449	15077	1.5	201142	0.5	0.17	3.38E + 10	0.269
537.627	20374	2.5	206376	1.5	-0.08	1.91E+10	0.4
541.404 542 517	15077	0.5	210030 199404	$\frac{0.5}{2.5}$	-0.01	2.20E+10 9.72E+10	0.402
548.811	31951	0.5	214163	1.5	-0.63	5.32E + 09	-0.06
550.276	42274	1.5	224001	2.5	0.87	1.64E + 11	0.511
550.765	42274	1.5	223839	1.5	0.22	3.65E + 10	0.335
556.607	42274	1.5	221934	1.5	-0.21	1.33E+10	0.077
562 621	20374 42274	2.5	199404	2.5	0.2	3.35E+10 4.17E+10	-0.179
570.109	42274	1.5	175405	2.5	-0.18	1.37E+10	0.253
571.576	20374	2.5	195328	1.5	-0.84	2.90E+09	-0.09
573.313	31951	0.5	206376	1.5	-0.56	5.59E + 09	-0.101
573.52	42274	1.5	216636	0.5	-0.5	6.34E + 09	0.1
577.194	31951	0.5	205203	0.5	0.04	2.24E + 10 2.05E + 10	0.325
579.568	15077	1.5	187620	2.5	-0.49	$6.46E \pm 09$	0.239
581.609	0	1.5	171937	1.5	-0.75	3.51E+09	0.228
581.769	42274	1.5	214163	1.5	0.02	2.11E + 10	0.108
591.008	42274	1.5	211476	1.5	-0.96	2.07E + 09	-0.044
591.05	31951	0.5	201142	0.5	-0.85	2.72E+09	0.057
592.38	42274	2.0 1.5	211084	$\frac{3.3}{2.5}$	-0.24	3.74E+09	-0.131
595.691	20374	2.5	188246	1.5	0.34	4.09E+10	-0.34
597.921	20374	2.5	187620	2.5	-0.23	1.09E + 10	-0.43
608.131	42274	1.5	206712	2.5	-1	1.81E + 09	-0.01
610.236	20374	2.5	184245	3.5	-0.37	7.60E+09	0.129
623 722	0 31921	0.5	195328	1.5	-0.37	7.00E+09 5.38E±00	-0.071
623.723	15077	1.5	175405	2.5	-0.31	2.34E+09	0.033
629.454	42274	1.5	201142	0.5	-0.83	2.51E + 09	0.035
645.03	20374	2.5	175405	2.5	-0.79	2.57E + 09	0.194
659.791	20374	2.5	171937	1.5	-0.82	2.30E + 09	0.381
698.464	15077	1.5	158249	0.5	-0.76	2.34E+09	-0.057
742 055	20374 20374	2.5 2.5	154071	1.5	-1	$1.20E \pm 09$ 1.96E ± 00	-0.048
750.17	42274	1.5	175577	0.5	-0.75	1.17E+09	-0.034
800.757	15077	1.5	139959	1.5	-0.65	2.34E + 09	-0.039
806.715	20374	2.5	144333	2.5	-0.65	2.30E + 09	-0.037
811.738	0	1.5	123192	1.5	-0.81	1.59E + 09	0.047
877.95	0	1.5	113902	2.5	-0.74	1.57E+09	0.045
		a:	Energy Lev	veis iroi	n [39]		

Table A28: Computed oscillator strengths and transition probabilities Cs V.

Cs VI

Energy Levels

Table A29: Comparison between available experimental data and calculated energy levels (in cm⁻¹) in Cs VI

) 0.0 .				
E^a_{exp}	E^{b}_{calc}	ΔE	J	Leading components (in %) in LS coupling c
Even Parity				
0	45	-45	0	$86.3 5s^2 5p^2 (^{3}P) ^{3}P + 11.1 5s^2 5p^2 (^{1}S) ^{1}S$
12176	12006	170	1	$97.4 \ 5s^2 5p^2 \ (^{3}P) \ ^{3}P$
17628.2	17723	-94.8	2	$63.5 \ 5s^2 5p^2 \ (^{3}P) \ ^{3}P + 33.7 \ 5s^2 5p^2 \ (^{1}D) \ ^{1}D$
35061.4	35134	-72.6	2	$62.8 \ 5s^2 5p^2 \ (^1D) \ ^1D + 33.8 \ 5s^2 5p^2 \ (^3P) \ ^3P$
52410.3	52368	42.3	0	$84.7 \ 5s^2 5p^2 \ (^1S) \ ^1S + 11.2 \ 5s^2 5p^2 \ (^3P) \ ^3P$
Odd Parity				
106878.6	106911	-32.4	2	90.9 $5s5p^3$ (⁴ S) ⁵ S + 7.3 $5s5p^3$ (² P) ³ P
131766.8	131977	-210.2	1	73 $5s5p^3$ (² D) ³ D + 12.3 $5s5p^3$ (² P) ³ P + 7.2 $5s^25p5d$ (² P) ³ D
133089.4	133160	-70.6	2	71 $5s5p^3$ (² D) ³ D + 14 $5s5p^3$ (² P) ³ P + 6.6 $5s^25p5d$ (² P) ³ D
138042.8	138025	17.8	3	$89.8 5s5p^3 (^2D) \ ^3D + 7.8 \ 5s^25p5d \ (^2P) \ ^3D$
152634.7	152692	-57.3	0	$91.3 5s5p^3 (^2P) {}^3P + 6.9 5s^25p5d (^2P) {}^3P$
154198.2	154083	115.2	1	$73.7 \ 5s5p^3 \ (^2P) \ ^3P + 12.1 \ 5s5p^3 \ (^2D) \ ^3D + 5.8 \ 5s^25p5d \ (^2P) \ ^3P$
154775.8	154559	216.8	2	$39.8 5s5p^3$ (² P) ³ P + $23.2 5s5p^3$ (² D) ¹ D + $14.3 5s5p^3$ (² D) ³ D
168730.2	168396	334.2	2	$32 5s5p^3 (^2D) {}^1D + 28.1 5s5p^3 (^2P) {}^3P + 26.4 5s^25p5d (^2P) {}^1D$
175645.3	175441	204.3	1	$64.3 5s5p^3$ (⁴ S) ³ S + 25.7 $5s5p^3$ (² P) ¹ P
181755.2	181684	71.2	2	$85.5 \ 5s^2 5p5d \ (^2P) \ ^3F + 8.1 \ 5s5p^3 \ (^2D) \ ^1D$
187270	187505	-235	3	$88.1 \ 5s^2 5p5d \ (^2P) \ ^3F$
194461	194979	-518	1	$50.5 \ 5s5p^3 \ (^2P) \ ^1P + 22.9 \ 5s5p^3 \ (^4S) \ ^3S + 13.3 \ 5s^25p5d \ (^2P) \ ^1P$
197579.4	197530	49.4	2	$21.6 \ 5s^2 5p5d \ (^2P) \ ^3D + 44 \ 5s^2 5p5d \ (^2P) \ ^3P + 14.6 \ 5s^2 5p5d \ (^2P) \ ^1D$
199798.6	199665	133.6	1	$59.7 \ 5s^2 5p5d \ (^2P) \ ^3D + 15.8 \ 5s^2 5p5d \ (^2P) \ ^3P + 7 \ 5s5p^3 \ (^2P) \ ^1P$
209795.3	209937	-141.7	2	$34.1 \ 5s^2 5p5d \ (^2P) \ ^1D + 37.1 \ 5s^2 5p5d \ (^2P) \ ^3D + 14.9 \ 5s5p^3 \ (^2D) \ ^1D$
212146.6	212162	-15.4	3	$75.2 \ 5s^2 5p5d \ (^2P) \ ^3D + 7.3 \ 5s^2 5p5d \ (^2P) \ ^3F + 6.7 \ 5s^2 5p5d \ (^2P) \ ^1F$
212928.1	212908	20.1	0	$89.1 \ 5s^2 5p5d \ (^2P) \ ^3P + 6.6 \ 5s5p^3 \ (^2P) \ ^3P$
214185.9	214144	41.9	1	$64.9 \ 5s^2 5p5d \ (^2P) \ ^3P + 20.2 \ 5s^2 5p5d \ (^2P) \ ^3D + 6.1 \ 5s5p^3 \ (^2P) \ ^3P$
216002.8	215978	24.8	2	$43.4 5s^{2}5p5d$ (² P) ³ P + 26.2 $5s^{2}5p5d$ (² P) ³ D + 11.5 $5s^{2}5p5d$ (² P) ¹ D
226523.4	226643	-119.6	3	$85.2 \ 5s^{2}5p5d \ (^{2}P) \ ^{1}F + 8.3 \ 5s^{2}5p5d \ (^{2}P) \ ^{3}D + 1.1 \ 5p^{3}5d \ (^{2}P) \ ^{1}F$
232014.9	231831	183.9	1	$72.7 \ 5s^{2}5p5d \ (^{2}P) \ ^{1}P + 8.5 \ 5s5p^{3} \ (^{2}P) \ ^{1}P + 5.8 \ 5s^{2}5p5d \ (^{2}P) \ ^{3}D$
242213.3	242174	39.3	0	$96.5 \ 5s^2 5p6s \ (^2P)^{-3}P$
243719.2	243768	-48.8	1	$72.6 5s^{2}5p6s$ (² P) ³ P + 20.5 $5s^{2}5p6s$ (² P) ¹ P
260952	260958	-6	2	$96.2 \ 5s^2 5p6s \ (^2P) \ ^3P$
264226.7	264221	5.7	1	$72.2 \ 5s^25p6s \ (^2P)^{-1}P + 22.6 \ 5s^25p6s \ (^2P)^{-3}P$

a: Energy Levels from Sansonetti [39] b: This work c: Only the components ≥ 5% are given

λ_{Ritz}	E^a_{low}	Jlow	Eup	Jup	log gf	gA	CF
Å	$\rm cm^{-1}$		cm^{-1}			s^{-1}	
401.968	12176	1	260952	2	-0.33	1.92E + 10	-0.758
405.517	17628	2	264227	1	-0.68	8.46E + 09	-0.154
410.308	0	0	243719	1	-0.41	1.54E + 10	-0.476
410.975	17628	$\tilde{2}$	260952	2	-0.06	$3.44E \pm 10$	0.749
431 885	12176	1	243719	1	-0.7	$7.08E \pm 09$	0.557
434 712	12176	1	242213	0	-0.5	1.12E + 10	0.677
436 366	35061	2	264227	1	0.11	4.50E + 10	0.704
442.3	17628	2	243719	1	-0.19	$2.19E \pm 10$	0.528
442 692	35061	2	260952	2	-0.37	$1.44E \pm 10$	0.73
442.092	52410	0	260352	1	-0.37	$1.78E \pm 10$	0.75
478 700	17628	2	204227	3	-0.23	$2.74E \pm 10$	0.114
410.103	12176	1	2160020	2	-0.05	5.75E+00	-0.114
490.013	12170	1	210003	1	-0.08	3.75E+09	-0.030
495.025	12170	1	214160	1	0.15	3.80E + 10	-0.474
498.127	12170	1	212928	1	-0.11	2.09E + 10	-0.000
500.504	17600	0	199799	1	0.36	0.10E + 10	0.487
504.097	17628	2	216003	2	-0.02	2.51E+10	-0.13
506.023	12176	1	209795	2	0.32	5.42E + 10	0.669
508.756	17628	2	214186	1	-0.17	1.75E + 10	-0.403
514.09	17628	2	212147	3	0.81	1.64E + 11	0.674
514.242	0	0	194461	1	-0.45	8.92E + 09	-0.148
520.38	17628	2	209795	2	0.32	5.17E + 10	0.449
522.297	35061	2	226523	3	0.85	1.75E+11	0.676
522.715	52410	0	243719	1	-0.81	3.82E + 09	-0.23
532.985	12176	1	199799	1	-0.16	1.63E + 10	0.203
539.364	12176	1	197579	2	0.43	6.17E + 10	0.647
548.591	12176	1	194461	1	-0.67	4.74E + 09	0.139
552.665	35061	2	216003	2	0.52	7.26E + 10	-0.593
555.706	17628	2	197579	2	0.1	2.72E + 10	-0.185
556.779	52410	0	232015	1	0.37	5.04E + 10	0.527
558.271	35061	2	214186	1	-0.28	1.12E + 10	-0.528
564.7	35061	2	212147	3	-0.12	1.59E + 10	0.121
569.329	0	0	175645	1	-0.49	6.64E + 09	0.178
572.299	35061	2	209795	2	-0.1	1.63E + 10	-0.154
589.477	17628	2	187270	3	-0.2	1.22E + 10	0.657
589.695	12176	1	181755	2	-0.95	2.17E + 09	0.556
607.027	35061	2	199799	1	-0.65	4.07E + 09	-0.158
609.284	17628	2	181755	2	-0.69	3.63E + 09	0.351
611.736	12176	1	175645	1	-0.18	1.18E + 10	-0.29
615.316	35061	2	197579	2	-0.4	7.08E + 09	0.07
627.354	35061	2	194461	1	0.08	2.04E + 10	-0.312
632.843	17628	2	175645	1	0.23	2.84E + 10	0.429
681.692	35061	2	181755	2	-0.78	2.36E + 09	-0.244
703.974	52410	0	194461	1	-0.69	2.79E + 09	0.071
704.115	12176	1	154198	1	-0.52	4.07E + 0.09	0.155
711.953	12176	1	152635	0	-0.95	$1.47E \pm 0.09$	0.141
729.141	17628	2	154776	2	-0.29	$6.40E \pm 0.09$	0.101
748.118	35061	2	168730	2	-0.36	5.20E + 09	0.08
758 917	0	õ	131767	1	-0.7	$2.31E\pm0.0$	0.007
827 038	12176	1	133089	2	-0.58	2.60E + 09	0.079
830.464	17628	2	138043	3	-0.55	2.00 ± 0.09 2.05 ± 0.09	0.079
071 040	35061	2	138043	3	-0.07	2.05E+09 8.05E+09	0.004
911.049	33001	4	100040	0	-0.9	0.995-700	0.079

Table A30: Computed oscillator strengths and transition probabilities Cs VI.

Cs VII

Energy Levels

E ^a _{exp}	E^{b}_{calc}	ΔE	J	Leading components (in %) in LS coupling c
Odd Parity	cure			
0	-2	2	0.5	$97.9 5s^2 5p (^1S) ^2P$
19379.3	19383	-3.7	1.5	$97.7 5s^2 5p (^1S) ^2P$
166536.9	166537	-0.1	2.5	$99.6 \ 5s^2 4f \ (^1S) \ ^2F$
167296.5	167296	0.5	3.5	$99.6 5s^{2}4f(^{1}S)^{2}F$
260637.9	260489	148.9	1.5	$29.2 5p^{3} (^{2}D) ^{2}D + 35.9 5p^{3} (^{4}S) ^{4}S + 21.5 5p^{3} (^{2}P) ^{2}P$
270870.2	271020	-149.8	1.5	52.4 5p° (^{-S}) ^{-S} + 32.9 5p° (^{-D}) ^{-D} + 12.9 5s5p5d (^o P) ^{-D}
272400.9	272341	59.9	2.5	71.8 5p° (-D) -D + 25.7 5s5p5d (-P) -D
293283.2	293298	-14.8	1.5	91.5 555p5d ($^{\circ}P$) $^{\circ}F$
293209.4	293379	-109.0	0.5	$85 \text{ Sp}^{-1}(\mathbf{r}) \mathbf{r} + 10.5 \text{ SSSp3d}(\mathbf{r}) \mathbf{r}$
297070.8	297338	-201.2	2.5	50.4 550501 (F) F $54 55^3 (^2P) ^2P + 12.6 555554 (^3P) ^2P + 10.55^3 (^4g) ^4g$
302322.8	302270	202.8	3.5	34 5p (1) 1 + 12.0 55555d (1) 1 + 10 5p (5) 5 80 5c555d (³ P) ⁴ F + 7.8 5c555d (³ P) ⁴ D
310602.0	310460	-817.0	2.5	59 550 50 (1) 1° $+$ 7.8 550 50 (1) D 51.2 5650 50 (^{3}P) $^{4}P + 26.0$ 5650 50 (^{3}P) $^{4}D + 8.8$ 5650 50 (^{1}P)
312206 3	311930	276.3	1.5	$51.2 55555d (^{3}P) ^{4}D + 273 55555d (^{3}P) ^{4}P + 33 55555d (^{1}P) ^{4}D$
312626.8	312342	284.8	0.5	85.8555504 (³ P) ⁴ D + 7.65555054 (³ P) ⁴ P
320848.6	320846	2.6	0.5	$93.6.5s^{2}6p$ (¹ S) ² P
322850.6	322908	-57.4	2.5	25.65555505d (³ P) ² F + 21.1555555d (³ P) ⁴ D + 17.555555d (¹
324129.9	323877	252.9	1.5	$36.7 5s5p5d$ (³ P) ² D + $16 5s^{2}6p$ (¹ S) ² P + $11 5s5p5d$ (¹ P) ² I
324722.6	324859	-136.4	3.5	87.9 5s5p5d (³ P) ⁴ D + 9.2 5s5p5d (³ P) ⁴ F
326029.5	325976	53.5	2.5	43.7 5s5p5d (³ P) ⁴ D + 22.2 5s5p5d (³ P) ⁴ P + 21.2 5s5p5d (³
326357.4	326556	-198.6	0.5	90.5 5s5p5d (^{3}P) ^{4}P + 8.3 5s5p5d (^{3}P) ^{4}D
326711.9	326660	51.9	1.5	49.7 5s5p5d (³ P) ${}^{4}P$ + 23.7 5s ² 6p (¹ S) ${}^{2}P$ + 21.6 5s5p5d (³ P)
328057.7	328165	-107.3	1.5	$50.9 5s^2 6p (^{1}S) ^{2}P + 16.6 5s5p5d (^{3}P) ^{4}P + 14.3 5s5p5d (^{3}P)$
332409.5	331502	907.5	2.5	27.6 5s5p5d (³ P) ² D + 25 5s5p5d (³ P) ⁴ P + 17.4 5s5p5d (¹ P)
342601.4	342153	448.4	3.5	$57.3 5s5p5d (^{3}P) ^{2}F + 40 5s5p5d (^{1}P) ^{2}F$
348210.7	348178	32.7	1.5	$50.8 5s5p5d (^{3}P) ^{2}P + 28.3 5s5p5d (^{1}P) ^{2}D + 8.9 5p^{3} (^{2}P) ^{2}$
356097.4	356127	-29.6	3.5	46.1 5s5p5d (¹ P) ${}^{2}F$ + 38.2 5s5p5d (³ P) ${}^{2}F$ + 8.3 5s ${}^{2}5f$ (¹ S)
356019.7	356421	-401.3	0.5	$63.6 5s5p5d (^{3}P) ^{2}P + 21.8 5s5p5d (^{1}P) ^{2}P$
357398.5	357204	194.5	2.5	$52.8 5s5p5d$ (¹ P) ² F + 26.3 $5s5p5d$ (³ P) ² F + 9.8 $5s^{2}5f$ (¹ S) ³
365025	364524	501	1.5	48.2 5s5p5d (¹ P) ² P + 22.5 5s5p5d (¹ P) ² D + 15.5 5s5p5d (³)
364989.8	364956	33.8	0.5	$65.9 \ 5s5p5d \ (^{1}P) \ ^{2}P + 18.9 \ 5s5p5d \ (^{3}P) \ ^{2}P + 9.3 \ 5p^{3} \ (^{2}P) \ ^{2}$
366610.1	367646	-1035.9	2.5	$60.7 5s5p5d (^{1}P) ^{2}D + 16.7 5s5p5d (^{3}P) ^{2}D + 10.5 5p^{3} (^{2}D)$
368265.1	368590	-324.9	1.5	21.9 5s5p5d (^{1}P) ^{2}D + 37.6 5s5p5d (^{1}P) ^{2}P + 11.7 5s5p5d (^{3}P)
379095	379026	69	0.5	93.7 sp6s $({}^{3}P)$ ${}^{4}P$
383877.1	383868	9.1	1.5	$87.1 \text{ sp6s} (^{3}\text{P}) {}^{4}\text{P} + 6.5 \text{ sp6s} (^{3}\text{P}) {}^{2}\text{P}$
384897	384908	-11	2.5	88 $5s^25f$ (¹ S) ² F + 8.4 $5s5p5d$ (¹ P) ² F
385051.8	385054	-2.2	3.5	$89.8 \ 5s^2 5f \ (^1S) \ ^2F + 7.7 \ 5s5p5d \ (^1P) \ ^2F$
390998.4	391082	-83.6	0.5	89.4 sp6s (³ P) ² P
398620.2	398699	-78.8	2.5	98.7 sp6s (^{3}P) ^{4}P
406417.6	406333	84.6	1.5	86.6 sp6s $\binom{3}{4}$ P $\stackrel{2}{}$ P + 8.6 sp6s $\binom{3}{4}$ P
434063.6	434150	-86.4	0.5	$88.4 \text{ sp6s} (^{1}\text{P}) ^{2}\text{P}$
435440	435353	87	1.5	$88.3 \text{ sp6s} (^{1}\text{P}) ^{2}\text{P}$
Even Parity				22 2 7 7 2 (3D) 4D · 2 7 7 2 (10) 20
104226.2	104221	5.2	0.5	$92.6 5s5p^2 (^{3}P) ^{4}P + 6 5s5p^2 (^{4}S) ^{2}S$
114254.9	114308	-53.1	1.5	98 psop^- ("P) "P 94.6 r.r.^2 (3p) 4p + 19.6 r.r. 2 (1p) 2p
122261.3	122240	21.3	2.5	84.0 ssp^- ("P) "P + 13.9 ssp^- ("D) "D $82.7 \text{ f}_{-}\text{f}_{-}^2$ (1D) 2D + 0 f $\text{f}_{-}^2\text{f}_{-}^1$ (1C) 2D + f 1 f (f - 2) (3D) 2D
141108.5	141335	-100.5	1.5	-62.7 osop (D) D + 9.5 os od (-S) -D + 5.1 osop ² (°P) -P 74.4 $\text{E}_{\text{r}}\text{E}_{\text{r}}^{2}$ (1D) 2D + 14.8 $\text{E}_{\text{r}}\text{E}_{\text{r}}^{2}$ (3D) 4D + 6.1 $\text{E}_{\text{r}}^{2}\text{E}_{\text{r}}$ (1C) 20
14/182.2	147001	181.2	2.5	(4.4 bsop (D) D + 14.8 bsop (P) P + 9.1 bs 2 5d (S) 2 .
128100.0	178940	105.3	0.5	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
170220 4	170240	-49.1	0.5	$(3.3 \text{ use}) (5) 5 + 32.3 \text{ use}^{-} (^{-}\text{P})^{-}\text{P}$
205004.2	205079	-41.0 00.0	1.5	83 $5e^{2}5d$ (¹ S) ² D \pm 10 2 $5e^{5}p^{2}$ (¹ D) ² D
203394.2	203972	-171	1.0 2.5	$85 3 5s^{2} 5d (^{1}S) ^{2}D + 88 5s 5r^{2} (^{1}D) ^{2}D$
263007 7	263214	-206.3	2.5	$67.85_{55} p 4 f ({}^{3}F) 4 G \pm 20.5_{55} p 4 f ({}^{3}F) 4 F \pm 5.65_{55} p 4 f ({}^{3}F) 2$
265224 4	264989	235.4	3.5	$44.8555p4f({}^{3}F) {}^{4}G + 43.655p4f({}^{3}F) {}^{4}F \pm 0.1565p4f({}^{3}F)$
268166.6	268286	-119.4	1.5	$875s5p4f(^{3}F)^{4}F + 7.35s5p4f(^{3}F)^{4}D$
268650	268773	-123	2.5	$49.3 585p4f ({}^{3}F) {}^{4}F + 18.5 585p4f ({}^{3}F) {}^{4}D + 11.9 585p4f ({}^{3}F)$
268882.9	268843	39.9	4.5	$49.3 585p4f({}^{3}F) {}^{4}F + 43.6 585p4f({}^{3}F) {}^{4}G + 6.5 585p4f({}^{3}F)$
269022.7	268854	168 7	3.5	$26.9 555p4f({}^{3}F) {}^{4}D + 23.1 555p4f({}^{3}F) {}^{2}F + 21.4 555p4f({}^{3}F)$
273351.5	273351	0.5	0.5	$97.5s^26s$ (¹ S) ² S
274950.7	275180	-229.3	2.5	$49.5 555p4f(^{1}F)^{2}F + 19.1 555p4f(^{3}F)^{4}G + 15.3 555p4f(^{1}F)^{4}F$
276972.2	276854	118.2	3.5	$28.5 555p4f (^{1}F) ^{2}F + 31.8 555p4f (^{1}F) ^{2}G + 14.4 555p4f (^{3}F)$
284435.5	284391	44.5	3.5	38.9 5s5p4f (³ F) ⁴ F + 36 5s5p4f (³ F) ⁴ D + 14.9 5s5p4f (³ F) ⁴
286808.3	286764	44.3	2.5	$67.8 5s5p4f ({}^{3}F) {}^{4}D + 24.5 5s5p4f ({}^{3}F) {}^{4}F$
289470.5	289848	-377.5	3.5	$43.8 555p4f(^{1}F)^{2}G + 16.4 555p4f(^{3}F)^{2}F + 15.1 555p4f(^{3}F)$
295868.7	295303	565.7	2.5	$58.2 5s5p4f (^{1}F) ^{2}D + 17.1 5s5p4f (^{3}F) ^{2}F + 9.1 5s5p4f (^{3}F)$
302199	302337	-138	1.5	$68.3 5s5p4f (^{1}F) ^{2}D + 25 5s5p4f (^{3}F) ^{2}D$
313168.4	312989	179.4	2.5	$56.6 5s5p4f ({}^{3}F) {}^{2}F + 31.7 5s5p4f ({}^{1}F) {}^{2}F + 7.6 5s5p4f ({}^{1}F)$
313848.9	313861	-12.1	3.5	$54.7 5s5p4f ({}^{3}F) {}^{2}F + 36.7 5s5p4f ({}^{1}F) {}^{2}F$
317249.8	317257	-7.2	4.5	$68 5s5p4f ({}^{3}F) {}^{2}G + 27.3 5s5p4f ({}^{1}F) {}^{2}G$
317726.7	317650	76.7	3.5	88.3 5s5p4f (³ F) ² G + 7.3 5s5p4f (¹ F) ² G
202022 7	323956	-22.3	1.5	$65.1 5s5p4f ({}^{3}F) {}^{2}D + 29.7 5s5p4f ({}^{1}F) {}^{2}D$
323933.7				

Table A31: Comparison between available experimental data and calculated energy levels (in $\rm cm^{-1})$ in Cs VII

as as solution for the second state of the second st

			~				
λ_{Ritz}	E^{a}_{low}	J_{low}	E_{up}	J_{up}	log gf	gA	CF
Å	$\rm cm^{-1}$		$\rm cm^{-1}$			s^{-1}	
365.829	0	0.5	273352	0.5	-0.4	1.99E + 10	-0.895
393.744	19379	1.5	273352	0.5	-0.13	3.19E + 10	0.898
485.451	0	0.5	205994	1.5	0.42	7.36E + 10	0.617
527.962	19379	1.5	208787	2.5	0.67	1.12E + 11	0.746
535.863	19379	1.5	205994	1.5	-0.1	1.85E + 10	0.71
546.998	114255	1.5	297071	2.5	-0.83	3.28E + 09	-0.582
557.602	0	0.5	179339	1.5	-0.2	1.37E + 10	-0.314
572.051	122261	2.5	297071	2.5	-0.84	2.98E + 09	0.692
600.082	104226	0.5	270870	1.5	-0.57	5.04E + 09	-0.442
625.156	19379	1.5	179339	1.5	0.4	4.26E + 10	0.497
629.677	19379	1.5	178191	0.5	-0.04	1.52E + 10	-0.553
632.546	0	0.5	158091	0.5	0.08	2.01E+10	0.607
638.507	114255	1.5	270870	1.5	-0.18	1.08E + 10	-0.581
639.338	104226	0.5	260638	1.5	-0.53	4.80E + 09	-0.414
657.718	141169	1.5	293209	0.5	-0.27	8.32E + 09	0.28
672.907	122261	2.5	270870	1.5	-0.21	9.02E + 09	-0.454
683.139	114255	1.5	260638	1.5	-0.45	5.08E + 09	-0.399
708.373	0	0.5	141169	1.5	-0.41	5.24E + 09	-0.146
722.666	122261	2.5	260638	1.5	-0.09	1.04E + 10	-0.556
773.205	166537	2.5	295869	2.5	-0.66	2.41E + 09	-0.179
782.455	19379	1.5	147182	2.5	-0.53	3.23E + 09	-0.095
798.603	147182	2.5	272401	2.5	-0.25	5.91E + 09	0.169
808.486	147182	2.5	270870	1.5	-0.67	2.21E + 09	-0.376
818.505	167297	3.5	289471	3.5	-0.82	1.52E + 09	-0.083
837.034	141169	1.5	260638	1.5	-0.85	1.33E + 09	-0.062
869.425	178191	0.5	293209	0.5	-0.61	2.16E + 09	0.124
975.166	158091	0.5	260638	1.5	-0.84	1.03E+09	-0.067
975.745	166537	2.5	269023	3.5	-0.98	7.26E + 08	-0.402
983.031	167297	3.5	269023	3.5	-0.93	8.04E + 08	0.074
984.384	167297	3.5	268883	4.5	-0.87	9.25E + 08	-0.42
1074.558	179339	1.5	272401	2.5	-0.62	1.40E + 09	0.066
2409.463	167297	3.5	208787	2.5	-0.69	2.35E + 08	0.246
2533.624	166537	2.5	205994	1.5	-0.9	1.31E + 08	0.234
3139.163	265224	3.5	297071	2.5	-0.64	1.60E + 08	-0.813
3302.05	263008	2.5	293283	1.5	-0.71	1.17E + 08	-0.797
		_					

Table A32: Computed oscillator strengths and transition probabilities Cs VII.

a: Energy Levels from [40]

Ag IV-VII

Ag IV

Energy Levels

Table A	433:	Con	iparison	between	ava	ailable	e experime	ental o	data	and	calculated	even	energy
levels (in c	$m^{-1})$	in Ag IV	V									
		D <i>Q</i>	- ph	4 15	-	r 11		01) I T 0	1 01 11	C			

-)	0			
\mathbf{E}^{a}	E^{b} .	ΔΕ	T	Leading components (in %) in LS Coupling ^c
Lexp	L'calc		3	Leading components (in 70) in Lo Coupling
0	-15	15	4	98.4 4d° (°F) °F
4172.5	4177	-4.5	3	$99.4 \ 4d^8 \ (^{3}F) \ ^{3}F$
5920.6	5929	9.1	ő	(3F) $(3F)$ $(3F)$ (152) (152) (15) (15) (15)
5829.0	0000	-0.4	2	$62.1 4 d^{-} (-F)^{-}F + 15.3 4 d^{-} (-D)^{-}D$
11871.5	11887	-15.5	2	$58.8 \text{ 4d}^{\circ} (^{\circ}\text{P}) ^{\circ}\text{P} + 28.1 \text{ 4d}^{\circ} (^{1}\text{D}) ^{1}\text{D} + 12.1 \text{ 4d}^{\circ} (^{\circ}\text{F}) ^{\circ}\text{F}$
15899.8	15889	10.8	1	99 4d ⁸ (³ P) ³ P
16002.4	16006	2.6	0	$06 = 448 (^{3}\text{D}) ^{3}\text{D}$
10092.4	10090	-3.0	0	90.5 4u (T) T
17397.7	17388	9.7	2	55.8 4d° (1D) 1D + 38.2 4d° (3P) 3P + 5.1 4d° (3F) 3F
20570	20572	-2	4	$98.2 \text{ dd}^8 (^{1}\text{G}) ^{1}\text{G}$
47138.6	47140	1.4	0	9654d8(15)15
47138.0	47140	-1.4	0	
96396.69	96411	-14.31	5	96.7 4d'5d (*F) ^o F
99147.15	99148	-0.85	4	$95.1 \ 4d^75d \ (^4F) \ ^5F$
101960 51	101960	8 40	2	06.9 44754 (4E) 5E
101200.51	101209	-0.49	э	90.8 4d 3d (F) F
102632.67	102643	-10.33	2	96.1 4d' 5d (4 F) 5 F
103471 58	103482	-10.42	1	95.2 4 d^{7} 5d $({}^{4}$ F) 5 F
107022.2	106002	20.2	4	00.2 44754 (4F) 3F
10/022.5	100995	29.5	4	90.2 4d 5d (F) F
110376.64	110333	43.64	3	$47.2 4d' 5d (^{4}\text{F}) ^{3}\text{F} + 46.3 4d' 5d (^{4}\text{P}) ^{3}\text{P}$
110778.97	110773	5.97	2	78.7 $4d^{7}5d$ (⁴ P) ⁵ P + 17.1 $4d^{7}5d$ (² P) ³ P
111004.7	110045	50.7	-	$(4 - 1)^{7} = (4 - 1)^{5} = (4 - 2)^{7} = $
111004.7	110945	59.7	3	51 4d 5d (F) F + 40.3 4d 5d (F) F
112611.74	112591	20.74	1	$86.3 \text{ 4d}' \text{ 5d} (^{4}\text{P}) {}^{3}\text{P} + 11.1 \text{ 4d}' \text{ 5d} (^{2}\text{P}) {}^{3}\text{P}$
112688 86	112724	-35 14	2	89.4 d^{7} 5d (4 F) 3 F
115550.00	115500	00.111	-	$244771(20)^{3}$
115550.39	115522	28.39	э	84 4a 5a (G) G + 10.4 4a 5a (H) H
116806	116732	74	4	$70.7 \text{ 4d}' \text{ 5d} (^2\text{G}) ^3\text{G} + 16.1 \text{ 4d}' \text{ 5d} (^2\text{H}) ^3\text{H} + 7.2 \text{ 4d}' \text{ 5d} (^2\text{G}) ^1\text{G}$
118603.01	118602	1.01	2	$35.2 \text{ 4d}^7 \text{5d} (^2\text{P}) ^3\text{P} + 34.5 \text{ 4d}^7 \text{5d} (^4\text{P}) ^3\text{P} + 14.4 \text{d}^7 \text{5d} (^2\text{D}) ^3\text{D}$
110010.01	110705	111.00	-	$12 4 417 \pm 1(27) 37 \pm 900 417 \pm 1(47) 37 \pm 97 6 417 \pm 1(27) 17$
118613.78	118725	-111.22	1	$13.4 \text{ 4d}^{\circ} \text{ 5d} (^{-}\text{D})^{\circ} \text{D} + 29.2 \text{ 4d}^{\circ} \text{ 5d} (^{-}\text{P})^{\circ} \text{P} + 27.6 \text{ 4d}^{\circ} \text{ 5d} (^{-}\text{P})^{\circ} \text{P}$
119119.24	119036	83.24	3	$95.8 \text{ 4d}^{\prime} \text{5d} (^2 \text{G}) {}^3 \text{G}$
120216 19	120504	-287.81	0	$60.8 4d^{7} 5d (^{2}P)^{3}P + 38.3 4d^{7} 5d (^{4}P)^{3}P$
120210.15	120004	-201.01	0	
120871.27	120938	-66.73	6	99.5 4d ⁻ 5d (⁻ H) ⁻ H
121766.62	121780	-13.38	4	$49.9 \text{4d}^{\prime} \text{5d} (^{2}\text{G}) {}^{1}\text{G} + 24.4 \text{4d}^{\prime} \text{5d} (^{2}\text{H}) {}^{3}\text{H} + 22.1 \text{4d}^{\prime} \text{5d} (^{2}\text{G}) {}^{3}\text{G}$
121832.93	121771	61.93	2	59.7 4d ⁷ 5d (⁴ P) ³ P + 21.1 4d ⁷ 5d (² P) ³ P + 5.5 4d ⁷ 5d (⁴ P) ⁵ P
121002.00	121111	01.50	2	
122456.21	122460	-3.79	ъ	$80.5 \text{ 4d}^{\circ} \text{5d} (-H)^{\circ} H + 12.6 \text{ 4d}^{\circ} \text{5d} (-H)^{\circ} H + 6.3 \text{ 4d}^{\circ} \text{5d} (-G)^{\circ} G$
122676.15	122661	15.15	1	$45.1 \text{ 4d}' \text{ 5d} (^{4}\text{P}) {}^{3}\text{P} + 32.9 \text{ 4d}' \text{ 5d} (^{2}\text{P}) {}^{3}\text{P} + 12.8 \text{ 4d}' \text{ 5d} (^{2}\text{D}) {}^{3}\text{D}$
122820.45	122674	146 45	3	73.9.4 $d^{7}5d^{(2}D)^{3}D + 19.6.4d^{7}5d^{(2}D)^{3}D$
105050.00	105000	140.40	1	(D, T) = (
125076.99	125239	-162.01	1	$34.6 \ 4d^{\circ} \ 5d^{\circ} (-P) \ P + 28.8 \ 4d^{\circ} \ 5d^{\circ} (-D) \ D + 18.8 \ 4d^{\circ} \ 5d^{\circ} (-P) \ P$
125077.14	124942	135.14	2	46.7
125735 19	125754	-18.81	4	58.7 4 d^{7} 5d (² H) ³ H + 36.8 4 d^{7} 5d (² G) ¹ G
105057.0	105000	10.01		$c_0 = 4.7 \epsilon_1 (4p) 3p + 20.4 4.7 \epsilon_1 (2p) 3p$
125857.9	125808	49.9	0	$60.74d^{\circ} 5d^{\circ} (P)^{\circ} P + 38.44d^{\circ} 5d^{\circ} (P)^{\circ} P$
127929.34	128045	-115.66	5	$84.4 \text{ 4d}' \text{ 5d} (^{2}\text{H}) ^{1}\text{H} + 8.6 \text{ 4d}' \text{ 5d} (^{2}\text{H}) ^{3}\text{H} + 6.3 \text{ 4d}' \text{ 5d} (^{2}\text{G}) ^{3}\text{G}$
130570.62	130656	-85 38	1	49.7 4d ⁷ 5d $\binom{2}{2}$ $\stackrel{1}{P}$ + 29.8 4d ⁷ 5d $\binom{2}{2}$ $\stackrel{3}{D}$ + 14.7 4d ⁷ 5d $\binom{4}{2}$ $\stackrel{3}{P}$
101005 50	100000	00.00	-	
131005.72	130922	83.72	2	$52.7 \text{ 4d} 5d (^{-}\text{D}) ^{-}\text{D} + 14.7 \text{ 4d} 5d (^{-}\text{D}) ^{-}\text{D} + 14.2 \text{ 4d} 5d (^{-}\text{P}) ^{-}\text{P}$
132758.38	132711	47.38	2	$94.6 \ 4d^{7} \ 5d^{(2F)} \ ^{3} F +$
133265 26	133263	2.26	3	93.2 4d ⁷ 5d (² F) ³ F +
1945 77.00	194690	50.11	4	
134577.89	134630	-52.11	4	96.2 4d 5d (F) F +
138852.05	138696	156.05	3	$93.4 \text{ 4d}' \text{ 5d} (^2 \text{F}) ^1 \text{F} +$
152454 1	152526	-71.9	1	87.8 $4d^{7}5d$ (² D) ³ D + 10.9 $4d^{7}5d$ (² D) ³ D
152005.0	152020	20.1	0	(1) (1) (2) (2) (2) (2) (1) (2) (2) (2) (2) (2) (2) (2) (2) (2) (2
153025.9	153064	-38.1	2	$81.9 \text{ 4d}^{\circ} \text{5d} (^{-}\text{D}) \stackrel{\circ}{}_{\text{o}}^{\text{D}} + 13.5 \text{ 4d}^{\circ} \text{5d} (^{-}\text{D}) \stackrel{\circ}{}_{\text{o}}^{\text{D}}$
154125.9	154104	21.9	3	$75.6 \text{ 4d}^{7} \text{5d} (^{2}\text{D}) \ ^{3}\text{D} + 20.2 \text{ 4d}^{7} \text{5d} (^{2}\text{D}) \ ^{3}\text{D}$
158398	158358	40	2	78.6 4d ⁷ 5d (² D) ¹ D + 16.5 4d ⁷ 5d (² D) ¹ D
100050	100000	10	2	(D) = (D) + (D) = (D) + (D) + (D) = (D) + (D)
246679.7	246668	11.7	ъ	$75.1 \text{ 4d}^{\circ} \text{5d} (-F)^{\circ} F + 15.8 \text{ 4d}^{\circ} \text{5d} (-F)^{\circ} G$
247262	247243	19	4	$55.7 \text{ 4d}^{7} \text{5d} (^{4}\text{F}) ^{5}\text{F} + 25 \text{ 4d}^{7} \text{5d} (^{4}\text{F}) ^{5}\text{D} + 8.4 \text{ 4d}^{7} \text{5d} (^{4}\text{F}) ^{5}\text{G}$
247618	247689	-71	6	85.4 4d ⁷ 5d (4 F) 5 G \pm 10.5 4d ⁷ 5d (4 F) 5 H
241010	241000	100.0	0	$a_1 = a_1 = a_1 = a_2 = a_2 = a_1 = a_2 = a_2 = a_2 = a_1 = a_2 = a_2 = a_2 = a_1 = a_2 $
250366.9	250240	126.9	2	$38.2 \text{ 4d}^{\circ} \text{ 5d} (-F)^{\circ} F + 24.7 \text{ 4d}^{\circ} \text{ 5d} (-F)^{\circ} D + 14.3 \text{ 4d}^{\circ} \text{ 5d} (-F)^{\circ} P$
250505.6	250438	67.6	4	46 4d' 5d (4 F) 5 D + 30.2 4d' 5d (4 F) 5 G + 10.9 4d' 5d (4 F) 3 G
251310.2	251342	-31.8	3	$53.5 \ 4d^{7}5d \ (^{4}F) \ ^{3}D + 24.3 \ 4d^{7}5d \ (^{4}F) \ ^{5}F + 12.8 \ 4d^{7}5d \ (^{4}F) \ ^{5}C$
2520000	050005	000.0	Ļ	$r_{1} = r_{1} (4\pi) 5 (1 + 98.0 + 37 + 10.4 + 17 + 10.4 + 17 + 14.5 + 10.4 + 17 + 14.5 + 14.$
252092.8	202320	-232.2	Э	20.2 4u ou (F) G + 20.0 4u ou (F) H + 18.4 4u ou (F) H
253120.5	252903	217.5	4	27 4d' 5d (${}^{*}F$) ${}^{\circ}G$ + 29.8 4d' 5d (${}^{4}F$) ${}^{\circ}G$ + 10.6 4d' 5d (${}^{4}F$) ${}^{3}F$
261776.2	261795	-18.8	3	$80.1 \ 4d^{7}6s \ (^{4}F) \ ^{5}F + 17.9 \ 4d^{7}6s \ (^{4}F) \ ^{3}F$
262002.0	262055	221.0	Ē	04 2 4d75d (4P) 5F + 16 4d75d (4F) 5F
202023.0	203033	-201.2	0	$34.0 40 00 (\Gamma) \Gamma = 1.0 40 00 (\Gamma) \Gamma$
263413.8	263104	309.8	2	$54.9 4 \text{d}^{\circ}_{2} \text{d}^{(\text{*}P)} \text{°F} + 10 4 \text{d}^{\circ}_{2} \text{d}^{(\text{*}P)} \text{°D} + 8 4 \text{d}^{\circ}_{2} \text{d}^{(\text{*}P)} \text{°D}$
265006.2	265053	-46.8	7	$78.2 \ 4d^75d \ (^2G) \ ^3I + 10.5 \ 4d^75d \ (^2H) \ ^3K + 7.1 \ 4d^75d \ (^2H) \ ^1K$
265332 4	265481	-148.6	1	$76.4d^{7}5d(^{4}P)^{5}D \pm 9.6.4d^{7}5d(^{2}P)^{3}F \pm 6.8.4d^{7}5d(^{4}P)^{3}F$
200002.4	200401	-140.0		$r_{1} = r_{2} = r_{1} = r_{2} = r_{2} = r_{1} = r_{2} = r_{1} = r_{2} = r_{1} = r_{1} = r_{2} = r_{1} = r_{1} = r_{2} = r_{1} = r_{1$
265345.3	265411	-65.7	5	$42.4 \ 4d' \ 5d'("G) \ "G + 25.8 \ 4d' \ 5d'("G) \ "H + 8 \ 4d' \ 5d'("G) \ "H$
266079.3	266089	-9.7	5	$24 \text{ 4d}^{\prime} \text{5d} (^{2}\text{G})^{-1}\text{H} + 36.8 \text{ 4d}^{\prime} \text{5d} (^{2}\text{G})^{-3}\text{G} + 11.3 \text{ 4d}^{7} \text{5d} (^{2}\text{G})^{-3}\text{H}$
267820 7	267885	-64 3	Δ	$3714d^{7}5d(^{2}G)^{3}F + 3174d^{7}5d(^{2}H)^{3}G + 1614d^{7}5d(^{2}H)^{3}F$
000045 0	201000	-04.0	-1	$37.2 \times 177.1 \times 200$ $311 \times 2007 \times 177.1 \times 200$ $117 \times 201 \times 177.1 \times 200$
269345.3	269557	-211.7	5	$37.3 4a_{Da} (G) H + 30.5 4d' 5d (G) H + 21 4d' 5d (H) G$
269391.3	269281	110.3	6	$44.1 \ 4d' \ 5d' (^2G)^{-1}I + 39.2 \ 4d' \ 5d' (^2G)^{-3}I + 11.7 \ 4d^7 \ 5d' (^2G)^{-3}H$
269452 5	269619	-166.5	7	$50.7.4d^{7}5d(^{2}H)^{3}K + 48.1.4d^{7}5d(^{2}H)^{1}K$
070000 5	203013	-100.0	-	$\pi_1 \circ 417 \epsilon_1 (2\pi) 3 \circ 1 = 11 4 417 \epsilon_1 (2 \circ) 1\pi_1 = 10 \circ 417 \epsilon_1 (2 \circ) 3\pi_1$
270208.7	270284	-75.3	ъ	$(1.5 40.50 (H)^{-1}G + 11.4 40.50 (-G)^{-1}H + 10.8 40.50 (-G)^{-1}H$
272280.4	272071	209.4	7	96.9 4d'5d (² H) ³ I
272423 91	272266	157 91	6	$36.3 \ 4d^{7}5d \ (^{2}H) \ ^{3}I + 50.4 \ 4d^{7}5d \ (^{2}H) \ ^{3}H + 7.9 \ 4d^{7}5d \ (^{2}H) \ ^{1}I$
979105 0	072001	104.0	~	$40.4 \ 437 \ est{211} \ 311 \ 000 \ 437 \ est{211} \ 211 \ 311 \ 000 \ 437 \ est{211} \ 211 \ 1$
273195.6	273001	194.6	6	$40.4 40^{2} a (H)^{2} H + 22.2 4 a^{2} b a (H)^{2} H + 16.2 4 a^{2} b a (H)^{1}$
273420.8	273459	-38.2	6	$64.4 \text{ 4d} \cdot 5 \text{d} (^2\text{H}) \ ^3\text{K} + 9.3 \ 4 \text{d} \cdot 5 \text{d} (^2\text{G}) \ ^1\text{I} + 8.2 \ 4 \text{d} \cdot 5 \text{d} (^2\text{H}) \ ^1\text{I}$
274634 3	274715	-80.7	5	$81.3 4d^{7}6s ({}^{2}G) {}^{3}G + 8.9 4d^{7}6s ({}^{2}H) {}^{3}H + 5.1 4d^{7}6s ({}^{2}H) {}^{1}H$
0700150	070145	70.0		$(2\alpha)^{3\alpha}$
278215.8	278145	70.8	3	90.3 40 0S (-G) G
280700.6	280693	7.6	5	$56.8 \text{ 4d}' \text{ 6s} (^2\text{H})^{-3}\text{H} + 42 \text{ 4d}' \text{ 6s} (^2\text{H})^{-1}\text{H}$

 $\begin{array}{c} 5 & 50.6 \ \text{4d} \ 08 \ (\text{ H}) & \text{H} + 42 \ \text{4d} \ 08 \ (\\ & \text{a: From Ankita} \ [41] \\ & \text{b: This work} \\ \text{c: Only the component} \geq 5\% \ \text{are given} \end{array}$

Table A34: Comparison between available experimental data and calculated odd energy levels (in cm^{-1}) in Ag IV

\mathbf{E}^{a}_{exp}	E^b_{calc}	ΔE	J	Leading components (in $\%$) in LS Coupling ^{c}
159220.05	159200	20.05	4	$50.7 \ 4d^7 5p \ (^4F) \ ^5D + 29.8 \ 4d^7 5p \ (^4F) \ ^5F + 6.7 \ 4d^7 5p \ (^4F) \ ^3F$
160255.4	160177	78.4	5	$64.4 \ 4d^{7}5p \ (^{4}F) \ ^{5}F + 18.1 \ 4d^{7}5p \ (^{4}F) \ ^{5}G + 13.9 \ 4d^{7}5p \ (^{4}F) \ ^{3}G$
162487.2	162516	-28.8	3	$37.7 \ 4d^{7}5p \ (^{4}F) \ ^{5}D + 46.6 \ 4d^{7}5p \ (^{4}F) \ ^{5}F + 5.7 \ 4d^{7}5p \ (^{4}P) \ ^{5}D$
164107.86	164046	61.86	4	$30.7 \ 4d^75p \ ({}^4F) \ {}^5F + 32.4 \ 4d^75p \ ({}^4F) \ {}^5G + 21.6 \ 4d^75p \ ({}^4F) \ {}^5D$
164677.68	164724	-46.32	2	$60.3 \ 4d^75p \ (^4F) \ ^5F + 22.7 \ 4d^75p \ (^4F) \ ^5D$
165602.1	165581	21.1	6	95.6 $4d^{7}5p ({}^{4}F) {}^{5}G$
165602.4	165490	112.4	5	$38.8 \ 4d^{7}5p \ (^{4}F) \ ^{3}G + 32.2 \ 4d^{7}5p \ (^{4}F) \ ^{5}F + 24.2 \ 4d^{7}5p \ (^{4}F) \ ^{5}G$
166005.9	165993	12.9	3	$37 4d^{7}5p ({}^{4}F) {}^{5}G + 22.4 4d^{7}5p ({}^{4}F) {}^{5}D + 16.2 4d^{7}5p ({}^{4}F) {}^{5}F$
166077.8	166105	-27.2	1	$69.4 \ 4d^{7}5p \ (^{4}F) \ ^{5}F + 12.6 \ 4d^{7}5p \ (^{4}F) \ ^{5}D + 5.1 \ 4d^{7}5p \ (^{4}F) \ ^{3}D$
167533.2	167561	-27.8	2	$29.8 4d^75p ({}^{4}\text{F}) {}^{5}\text{D} + 36.8 4d^75p ({}^{4}\text{F}) {}^{5}\text{G} + 15.1 4d^75p ({}^{4}\text{P}) {}^{5}\text{D}$
167566.07	167471	95.07	4	$28.6 \ 4d^75p \ (^4F) \ ^5G + 23.5 \ 4d^75p \ (^4F) \ ^3F + 18.5 \ 4d^75p \ (^4F) \ ^5F$
168370 19	168417	-46.81	2	$2424d^{7}5p(^{4}F)^{5}G + 3214d^{7}5p(^{4}P)^{5}S + 1244d^{7}5p(^{4}F)^{5}F$
168493 34	168531	-37.66	2	$56.7 \ 4d^75p \ (^4P) \ ^5S + 17.2 \ 4d^75p \ (^4F) \ ^5G + 5.2 \ 4d^75p \ (^4F) \ ^5D$
168595.64	168516	79.64	3	$23.4 4d^{7}5p ({}^{4}F) {}^{5}F + 36.7 4d^{7}5p ({}^{4}F) {}^{5}G + 12.6 4d^{7}5p ({}^{4}F) {}^{5}D$
168599 51	168622	-22.49	1	$4544d^{7}5p(^{4}F)^{5}D + 2944d^{7}5p(^{4}F)^{5}D + 1484d^{7}5p(^{4}F)^{5}F$
168748 31	168813	-64 69	0	$57.8 4d^7 5p (^4F) ^5D + 34.5 4d^7 5p (^4P) ^5D$
160725.47	160708	-04.03	4	$48.2 4d^{7} \text{ fm} (^{4} \text{ F}) ^{3} \text{ Fm} + 10.1 4d^{7} \text{ fm} (^{4} \text{ Fm}) ^{5} \text{ Fm} + 11.2 4d^{7} \text{ fm} (^{4} \text{ Fm}) ^{3} \text{ C}$
170002 42	170084	21.41	-4 E	46.2 4 d 5 p(F) F + 19.1 4 d 5 p(F) F + 11.2 4 d 5 p(F) G
1710092.43	171004	8.43	3	35.740 Sp (F) $G = 40.940$ Sp (F) G
171201.77	171200	-60.25	3	43.4 4 d 5 p (F) D + 20 4 d 5 p (F) F + 0.0 4 d 5 p (G) F
173009.03	173074	-4.95	4	$26.447 \text{ sp}(-\mathbf{F}) = 6 + 20.447 \text{ sp}(-\mathbf{F}) = 6.000 \text{ sp}(-$
173500.58	173634	-73.42	2	$30 40^{\circ} \text{ p} (-F)^{\circ} \text{D} + 28.8 40^{\circ} \text{p} (-F)^{\circ} \text{F} + 6.8 40^{\circ} \text{p} (-G)^{\circ} \text{F}$
173713.49	173729	-15.51	3	$37.1 \ 4d^{2} \text{ 5p} (^{2} \text{F}) \ ^{3} \text{F} + 27.4 \ 4d^{2} \text{ 5p} (^{2} \text{F}) \ ^{3} \text{D} + 12.1 \ 4d^{2} \text{5p} (^{2} \text{F}) \ ^{3} \text{G}$
174638.9	174641	-2.1	2	$32.1 \ 4d^{2} \ 5p({}^{2} \ F) \ 0F + 11.7 \ 4d^{2} \ 5p({}^{2} \ F) \ 0D + 10.8 \ 4d^{2} \ 5p({}^{2} \ F) \ 0F$
175020.93	175135	-114.07	1	19.3 4d' 5p (^{2}P) ^{3}P + 24.1 4d' 5p (^{4}F) ^{3}D + 10.7 4d' 5p (^{4}P) ^{3}S
175057.11	175042	15.11	3	70.4 4d' 5p (4 F) 3 G + 11.2 4d' 5p (4 F) 3 G
176497.56	176581	-83.44	1	$31.1 \text{ 4d}' \text{ 5p} ({}^{4}\text{F}) {}^{3}\text{D} + 12.9 \text{ 4d}' \text{ 5p} ({}^{4}\text{F}) {}^{3}\text{D} + 10.3 \text{ 4d}' \text{ 5p} ({}^{2}\text{P}) {}^{3}\text{D}$
177602.49	177533	69.49	5	$42.6 \ 4d^{7}5p \ (^{2}G) \ ^{3}H + 19.6 \ 4d^{7}5p \ (^{2}G) \ ^{1}H + 16.1 \ 4d^{7}5p \ (^{2}H) \ ^{3}I$
177872.52	177837	35.52	2	$1.1 \ 4d^75p \ (^2D) \ ^3F + 20.6 \ 4d^75p \ (^4P) \ ^5D + 16.7 \ 4d^75p \ (^4F) \ ^5D$
178004.8	177876	128.8	3	$38.4 4d^75p (^4P) {}^5D + 20.3 4d^75p (^4P) {}^3D + 15.3 4d^75p (^4F) {}^5D$
178319.66	178276	43.66	4	$34.2 4d^75p (^2\text{G}) ^3\text{F} + 16.3 4d^75p (^4\text{F}) ^3\text{F} + 12.6 4d^75p (^2\text{G}) ^3\text{G}$
179820.39	179909	-88.61	0	$37.7 \ 4d^75p \ (^4P) \ ^5D + 34.2 \ 4d^75p \ (^4F) \ ^5D + 20.5 \ 4d^75p \ (^2P) \ ^3P$
179913.67	179774	139.67	1	$31 \ 4d^7 5p \ (^4P) \ ^5D + 15.8 \ 4d^7 5p \ (^4F) \ ^5D + 13.4 \ 4d^7 5p \ (^4P) \ ^3S$
180280.87	180202	78.87	4	$43.1 \ 4d^{7}5p \ (^{4}P) \ ^{5}D + 35.3 \ 4d^{7}5p \ (^{2}G) \ ^{3}H$
180529.11	180390	139.11	4	$33.7 \ 4d^{7}5p^{(2}G)^{3}H + 40.2 \ 4d^{7}5p^{(4}P)^{5}D + 8.8 \ 4d^{7}5p^{(2}G)^{1}G$
180542.7	181002	-459.3	0	$47.6 4d^{7}5n (^{2}P) {}^{3}P + 18.3 4d^{7}5n (^{2}D) {}^{3}P + 11.1 4d^{7}5n (^{4}P) {}^{3}P$
181163 79	181061	102 79	ž	$265 4d^{7}5p (^{4}P) ^{5}P + 166 4d^{7}5p (^{4}P) ^{5}D + 128 4d^{7}5p (^{2}P) ^{1}D$
181404 63	181630	225 37	2	20.5 4d 5p(1) 1 + 10.0 4d 5p(1) D + 12.0 4d 5p(1) D $32.7 \text{ 4d}^7 \text{5p}(^2\text{P})$ $^3\text{P} + 17.5 \text{ 4d}^7 \text{5p}(^4\text{F})$ $^3\text{D} + 13.4 \text{ 4d}^7 \text{5p}(^4\text{P})$ ^3D
191552.02	181466	-225.51	6	52.740 5p (1) 1 \pm 17.540 5p (1) D \pm 15.440 5p (1) D 61 4d ⁷ 5p (² C) ³ H \pm 22.2 4d ⁷ 5p (² H) ³ I
101002.90	101400	00.93	1	5140 Sp(G) = 1 + 52.5 40 Sp(G) = 1 $29.7 447 \epsilon_{-} (4p) \text{ Sp}(G) = 1 \epsilon_{-} (4p) \text{ Sp}(G) = 19.9 447 \epsilon_{-} (2p) \text{ Sp}(G)$
101040.00	101002	-0.10	1	$32.7 4d^{2} \text{ 5p} (-\mathbf{F})^{-1} \mathbf{F} + 15.5 4d^{2} \text{ 5p} (-\mathbf{F})^{-1} \mathbf{D} + 12.8 4d^{-5} \text{ 5p} (-\mathbf{F})^{-1} \mathbf{F}$
181942.22	181883	59.22	3	$38.6 4d^{\circ} \text{ sp} (^{-}\text{P})^{\circ}\text{P} + 26.6 4d^{\circ} \text{ sp} (^{-}\text{P})^{\circ}\text{D} + 12.3 4d^{\circ} \text{ sp} (^{-}\text{P})^{\circ}\text{D}$
182242.73	182198	44.73	3	$29.5 \text{ 4d}^{\circ} \text{ 5p} (^{-}\text{G})^{\circ}\text{G} + 29.6 \text{ 4d}^{\circ} \text{5p} (^{-}\text{G})^{\circ}\text{F} + 6.7 \text{ 4d}^{\circ} \text{5p} (^{-}\text{G})^{\circ}\text{F}$
182317.58	182377	-59.42	5	$80.5 \text{ 4d}^{\circ}\text{5p} (^{2}\text{H})^{\circ}\text{G} + 7.7 \text{ 4d}^{\circ}\text{5p} (^{2}\text{F})^{\circ}\text{G}$
182910.1	182948	-37.9	6	$48.9 \ 4d^{2} \ 5p(^{2} \ H)^{-1} \ + \ 27.1 \ 4d^{2} \ 5p(^{2} \ H)^{-1} \ + \ 18.4 \ 4d^{-5} \ 5p(^{2} \ G)^{-1} \ H$
183023.82	182897	126.82	4	$30.6 \text{ 4d}' \text{ 5p} (^2\text{G}) ^1\text{G} + 29.6 \text{ 4d}' \text{ 5p} (^2\text{G}) ^3\text{F} + 12.5 \text{ 4d}' \text{ 5p} (^2\text{H}) ^1\text{G}$
183234.89	183147	87.89	2	$13.3 \text{ 4d}' \text{ 5p} (\text{^{4}P}) \text{^{5}D} + 25.1 \text{ 4d}' \text{ 5p} (\text{^{4}P}) \text{^{5}P} + 15.2 \text{ 4d}' \text{ 5p} (\text{^{4}P}) \text{^{5}P}$
183395.67	183414	-18.33	3	$0 d6^{\circ}S6p ({}^{3}P) {}^{5}P + 17.2 dd' 5p ({}^{4}P) {}^{3}D + 15.8 dd' 5p ({}^{2}G) {}^{1}F$
183927.65	183930	-2.35	1	$25.5 \text{ 4d}' \text{ 5p} (^{4}\text{P}) ^{3}\text{S} + 21.7 \text{ 4d}' \text{ 5p} (^{4}\text{P}) ^{3}\text{D} + 20.5 \text{ 4d}' \text{ 5p} (^{2}\text{P}) ^{3}\text{P}$
183962.99	183915	47.99	5	$65 \text{ 4d}' \text{ 5p} (^2\text{G}) ^{3}\text{G} + 14.7 \text{ 4d}' \text{ 5p} (^2\text{H}) ^{3}\text{I} + 11.5 \text{ 4d}' \text{ 5p} (^2\text{G}) ^{1}\text{H}$
184078.3	184501	-422.7	0	$45.1 \ 4d^{7}5p \ (^{2}P) \ ^{1}S + 21.6 \ 4d^{7}5p \ (^{4}P) \ ^{3}P + 15.3 \ 4d^{7}5p \ (^{4}P) \ ^{5}D$
184379.86	184250	129.86	3	$34.6 4d^75p (^4P) ^3D + 22.7 4d^75p (^2G) ^1F + 13.4 4d^75p (^4P) ^5P$
184576.17	184455	121.17	1	7.7 $4d^{7}5p$ (² P) ³ D + 29.9 $4d^{7}5p$ (⁴ P) ⁵ P + 25.3 $4d^{7}5p$ (⁴ P) ³ S
185280.63	185270	10.63	2	$34.8 \ 4d^{7}5p \ (^{4}P) \ ^{3}P + 17.3 \ 4d^{7}5p \ (^{2}D) \ ^{3}P + 11.5 \ 4d^{7}5p \ (^{4}P) \ ^{3}D$
185599.89	185443	156.89	3	$33.8 4d^75p (^2D) ^3D + 12.5 4d^75p (^2G) ^3G + 11.4 4d^75p (^2D) ^3F$
185894.25	185928	-33.75	4	$33.6 \ 4d^75p \ (^2H) \ ^3G + 18.4 \ 4d^75p \ (^2G) \ ^3G + 16 \ 4d^75p \ (^2G) \ ^3H$
186269.64	186363	-93.36	5	$42.5 \ 4d^75p \ (^2H) \ ^3I + 42.6 \ 4d^75p \ (^2G) \ ^3H + 8.7 \ 4d^75p \ (^2G) \ ^3G$
186411.3	186451	-39.7	7	99.6 $4d^{7}5p (^{2}H)^{-3}I$
186418.2	186561	-142.8	1	$46.1 \ 4d^75p \ (^4P) \ ^3P + 17.3 \ 4d^75p \ (^2P) \ ^1P + 14.9 \ 4d^75p \ (^2P) \ ^3D$
186593.36	186491	102.36	3	$34.9 \ 4d^75p \ (^2G) \ ^3F + 23.3 \ 4d^75p \ (^2G) \ ^3G + 6 \ 4d^75p \ (^2F) \ ^3G$
186616.09	186498	118.09	2	$43.7 \ 4d^75p \ (^2G) \ ^3F + 15.5 \ 4d^75p \ (^2D) \ ^3F + 9.5 \ 4d^75p \ (^4P) \ ^3P$
186710.07	186709	1.07	4	$47 \ 4d^7 5p \ (^2G) \ ^3G + 29.4 \ 4d^7 5p \ (^2H) \ ^3G + 6.5 \ 4d^7 5p \ (^2H) \ ^1G$
186740.29	186711	29.29	5	$59.2 \ 4d^{7}5p \ (^{2}G)^{-1}H + 20.2 \ 4d^{7}5p \ (^{2}H)^{-3}I + 11 \ 4d^{7}5p \ (^{2}G)^{-3}H$
187354.94	187352	2.94	3	$29.3 \ 4d^{7}5p \ (^{2}P) \ ^{3}D + 19.7 \ 4d^{7}5p \ (^{2}D) \ ^{3}F + 10.3 \ 4d^{7}5p \ (^{2}D) \ ^{3}D$
187417.14	187426	-8.86	2	$21.8 \ 4d^{7}5p^{(4}P)^{3}D + 32 \ 4d^{7}5p^{(2}G)^{3}F + 10.6 \ 4d^{7}5p^{(4}P)^{3}P$
187875.22	187794	81.22	1	$36 \ 4d^7 5p^{(2)} D^{3} D + 17.1 \ 4d^7 5p^{(4P)} D^{3} D + 8.1 \ 4d^7 5p^{(4F)} D^{3} D$
187965.5	187818	147.5	2	$18.1 \ 4d^{7}5p^{(2)}D^{3}D + 17.2 \ 4d^{7}5p^{(2)}P^{3}P + 13.2 \ 4d^{7}5p^{(4)}P^{5}P$
188922.26	188825	97.26	3	$30.1 \ 4d^{7}5p(^{2}H)^{3}G + 16.2 \ 4d^{7}5p(^{2}D)^{1}F + 13.3 \ 4d^{7}5p(^{2}G)^{3}G$
189103.2	189199	-95.8	1	$14.4 \ 4d^{7}5p^{(4}P)^{3}D + 26.6 \ 4d^{7}5p^{(4}P)^{3}P + 23.2 \ 4d^{7}5p^{(2}P)^{3}D$
189963.65	190034	-70.35	2	$39.8 \ 4d^{7}5p \ (^{2}P) \ ^{3}D + 11.3 \ 4d^{7}5p \ (^{2}P) \ ^{1}D + 10.4 \ 4d^{7}5p \ (^{2}D) \ ^{3}P$
190120.3	189961	159.3	4	$73.8 \ 4d^{7}5p \ (^{2}D) \ ^{3}F + 14.3 \ 4d^{7}5p \ (^{2}D) \ ^{3}F$
190754	190921	-167	6	$39.4 \ 4d^{7}5p \ (^{2}H) \ ^{3}I + 41.6 \ 4d^{7}5p \ (^{2}H) \ ^{1}I + 14.3 \ 4d^{7}5p \ (^{2}G) \ ^{3}H$
191361 65	191500	-138.35	6	$87.7 4d^{7}5p (^{2}H)^{3}H + 8.9 4d^{7}5p (^{2}H)^{1}I$
191677.8	192067	-389.2	ő	$60.9 \ 4d^75n \ (^4P) \ ^3P + 34.8 \ 4d^75n \ (^2P) \ ^1S$
192003 49	191969	34 49	3	$30.3 4d^{7}5p ({}^{2}C) {}^{1}F + 15.3 4d^{7}5p ({}^{2}D) {}^{3}F + 15.4d^{7}5p ({}^{2}P) {}^{3}D$
102182 72	102251	68.28	5	$73.7 4d^{7}5p (^{2}H) ^{3}H + 14.6 4d^{7}5p (^{2}H) ^{1}H$
1022102.72	102240	107.12	1	43.7 40.5 p(11) 11 + 14.0 40.5 p(11) 11 $48.6 4d^{7} 5 p(^{2} p) ^{3} S + 18.1 4d^{7} 5 p(^{2} p) ^{3} p + 11.7 4d^{7} 5 p(^{2} p) ^{1} p$
192212.07	192340	-127.13	2	$24.0 \ 4d^{7}{}_{5p} (^{2}{}_{p}) \ ^{3}{}_{p} + 17 \ 4d^{7}{}_{5p} (^{2}{}_{p}) \ ^{1}{}_{p} + 14.7 \ 4d^{7}{}_{5p} (^{2}{}_{p}) \ ^{3}{}_{p}$
1020200	100720	000	∠ 1	$15.3 4d^{7}5 (2)$ $1 \pm 10 4d^{7}6 (2)$ $3 \pm 17.9 43^{7}6 (2)$ 10^{-1}
102010.00	102140	30.9 61.99	1 1	$21.3 4d^{7}\text{5p} (^{2}\text{P}) ^{1}\text{D} \pm 16 4d^{7}\text{5p} (^{2}\text{D}) ^{3}\text{F} \pm 10.9 4d^{7}\text{E} (^{2}\text{D}) ^{3}\text{F}$
102641 40	102704	01.63 150 51	4	51.5 + 0.5 + 0.5 + 10.40 p (D) r + 10.3 + 0.5 + 0.
104600.00	104655	-102.01	4	$26.0 \text{ Ad}^{7} 5_{\text{D}} (^{2}\text{H}) \frac{1}{2} + 20.0 \text{ Ad}^{7} 5_{\text{L}} (^{2}\text{C}) \frac{1}{2} + 20.0 \text{ Ad}^{7} 5_{\text{L}} (^{2}\text{C}) \frac{1}{2} + 10.4 \text{ Ad}^{7} 5_{\text{L}} (^{2}\text{T}) \frac{3}{3} \text{T}$
194622.62	194055	-32.38	4	50.940 op (H) G + 39.840 op (G) G + 13.440 op (H) H 22.2447z (2D) 1D + $10.0447z$ (2D) 1D + $10.0447z$ (2D) 3D
195399.42	195405	-5.58	2	$23.3 40^{\circ} \text{ pp} (^{-}\text{D})^{-}\text{D} + 16.2 40^{\circ} \text{ pp} (^{-}\text{F})^{-}\text{D} + 13.8 40^{\circ} \text{ pp} (^{2}\text{D})^{-}\text{P}$
195561.29	195414	147.29	3	$30.9 \ 40^{\circ} \text{ op } (^{-}\text{D})^{-}\text{F} + 13.4 \ 40^{\circ} \text{ op } (^{-}\text{F})^{\circ}\text{F} + 9.2 \ 40^{\circ} \text{ op } (^{2}\text{D})^{\circ}\text{F}$
190892.5	196894	-1.5	2	$20.1 40^{\circ} \text{p} (^{-}\text{F})^{-}\text{D} + 30.9 40^{\circ} \text{p} (^{-}\text{F})^{\circ}\text{F} + 7.5 40^{\circ} \text{p} (^{-}\text{D})^{-1}\text{D}$
197185.75	197105	80.75	1	52.4 4d 5p (``D) ``P + 15.3 4d '5p (``P) ``S + 13.5 4d '5p (`'P) ``P
197847.4	197902	-54.6	5	78.5 4d 5p ($^{-}$ H) $^{-}$ H + 10.7 4d 5p ($^{-}$ H) $^{-}$ H
198486.52	198395	91.52	3	40.7 4d' 5p (² F) ${}^{3}G + 22.3$ 4d' 5p (² H) ${}^{3}G + 8.1$ 4d' 5p (² D) ${}^{1}F$
198660.9	198641	19.9	1	$40.6 \ 4d' \ 5p \ (^2D) \ ^3P + 18.6 \ 4d' \ 5p \ (^2P) \ ^1P + 7.6 \ 4d' \ 5p \ (^2P) \ ^3S$
198990.4	199026	-35.6	4	$32.7 \ 4d' \ 5p \ (^2F) \ ^3G + 22.9 \ 4d' \ 5p \ (^2F) \ ^1G + 22.4 \ 4d' \ 5p \ (^2F) \ ^3F$
199028	198887	141	0	70.9 $4d_{7}^{7}5p_{2}(^{2}D)_{2}^{3}P + 13.6 4d_{7}^{7}5p_{2}(^{2}P)_{3}^{3}P + 8.1 4d_{7}^{7}5p_{2}(^{2}P)_{1}^{1}S$
201269.41	201193	76.41	3	$62.4 4d^75p (^2F) {}^3F + 10.5 4d^75p (^2F) {}^3G + 6.1 4d^75p (^2D) {}^3F$
201341.9	201422	-80.1	2	$40.3 \ 4d^75p \ (^2F) \ ^3F + 27.6 \ 4d^75p \ (^2F) \ ^1D + 12.5 \ 4d^75p \ (^2F) \ ^3D$

Table A34. Continued

			1	
E ^a _{exp}	E^{b}_{calc}	ΔE	J	Leading components (in %) in LS Coupling ^{c}
201957.65	201885	72.65	3	$52.8 4d^75p (^2F) ^3D + 8.2 4d^75p (^2P) ^3D + 6.8 4d^75p (^2D) ^3D$
201962	202036	-74	4	53 $4d^{7}5p$ (² F) ¹ G + 32.7 $4d^{7}5p$ (² F) ³ G + 5 $4d^{7}5p$ (² H) ³ G
203084.6	203019	65.6	1	76.1 $4d^{7}5p(^{2}F)^{3}D + 7.4 4d^{7}5p(^{2}D)^{3}D + 7.3 4d^{7}5p(^{2}D)^{3}D$
203154.5	203085	69.5	5	86.7 $4d^{7}5p (^{2}F) {}^{3}G + 8.2 4d^{7}5p (^{2}H) {}^{3}G$
203236.5	203222	14.5	4	$62.8 \ 4d^75p \ (^2F) \ ^3F + 14.9 \ 4d^75p \ (^2F) \ ^1G + 10.8 \ 4d^75p \ (^2F) \ ^3G$
203284.2	203222	62.2	2	$61 \ 4d^75p \ (^2F) \ ^3D + 16.3 \ 4d^75p \ (^2F) \ ^1D + 5.9 \ 4d^75p \ (^2D) \ ^3D$
208471.3	208530	-58.7	3	$85.3 \ 4d^75p \ (^2F) \ ^1F + 7.1 \ 4d^75p \ (^2F) \ ^3D$
215234.5	215218	16.5	2	$72.7 \ 4d^75p \ (^2D) \ ^3P + 16.6 \ 4d^75p \ (^2D) \ ^3P$
215899	216010	-111	2	75.2 $4d^{7}5p$ (² D) ³ F + 8.9 $4d^{7}5p$ (² D) ³ F + 5.9 $4d^{7}5p$ (² F) ³ F
216295	216283	12	1	$75.4 4d^75p (^2D) \ ^3P + 7.4 \ ^4d^75p (^2D) \ ^3P + 7 \ ^4d^75p (^2D) \ ^1P$
217731.7	217711	20.7	0	88.8 $4d^{7}5p$ (² D) ³ P + 6.2 $4d^{7}5p$ (² D) ³ P
217970.8	217899	71.8	3	$65.1 \ 4d^75p \ (^2D) \ ^3F + 12.7 \ 4d^75p \ (^2D) \ ^3F + 7.2 \ 4d^75p \ (^2D) \ ^1F$
221125	221099	26	4	$72.5 \ 4d^75p \ (^2D) \ ^3F + 18.5 \ 4d^75p \ (^2D) \ ^3F$
222038.4	222260	-221.6	1	41.1 $4d^{7}5p$ (² D) ¹ P + 30.1 $4d^{7}5p$ (² D) ³ D + 9.5 $4d^{7}5p$ (² D) ³ P
222519.6	222446	73.6	3	$66 \ 4d^75p \ (^2D) \ ^1F + 11.8 \ 4d^75p \ (^2D) \ ^3F + 11.5 \ 4d^75p \ (^2D) \ ^1F$
224873	225200	-327	1	44.3 $4d^{7}5p$ (² D) ³ D + 39.1 $4d^{7}5p$ (² D) ¹ P + 8.9 $4d^{7}5p$ (² D) ³ D
224987.6	225025	-37.4	2	$60.7 \ 4d^75p \ (^2D) \ ^3D + 14.9 \ 4d^75p \ (^2D) \ ^1D + 13.5 \ 4d^75p \ (^2D) \ ^3D$
226882.1	226511	371.1	2	$51.7 4d^75p (^2D) \ ^1D + 17.8 \ 4d^75p (^2D) \ ^1D + 12 \ 4d^75p (^2D) \ ^3D$
227643.2	227547	96.2	3	$63.2 4d^75p (^2D) ^3D + 21.1 4d^75p (^2D) ^3D + 6.6 4d^75p (^2D) ^1F$

 Wavelength	Lower Level ^a	J	Upper level ^a	J	log of	on proce	CF	5118
Å	cm ⁻¹	^o Low	cm ⁻¹	Up	105 51	1	01	
491.732	11872	2	215235	2	-0.93	3.26E + 09	0.186	
495.153	0	4	201958	3	-0.92	3.25E + 09	0.121	
495.173	20570	4	222520	3	-0.22	1.62E + 10	0.563	
499.494	16092	0	216295	1	-0.99	2.74E + 09	-0.419	
501.669	15900	1	215235	2	-0.74	4.78E + 09	-0.548	
502.231	4173	3	203284	2	-0.9	3.32E + 09	0.251	
505.467	17398	2	215235	2	-0.81	4.05E+09	-0.316	
506.584	20570	4	217971	3	-0.97	2.81E + 09	0.556	
523 359	17398	2	203085	3	-0.89	3.32E+09 3.48E+09	-0.25	
525.983	0	4	190120	4	-0.88	3.15E+09	-0.269	
526.077	11872	2	201958	3	-0.65	5.42E + 09	0.157	
531.349	4173	3	192373	2	-0.99	2.41E + 09	-0.199	
532.194	20570	4	208471	3	0.05	2.66E + 10	-0.785	
533.662	15900	1	203284	2	-0.56	6.41E + 09	0.417	
533.746	0	4	187355	3	-0.4	9.42E + 09	-0.441	
534.231	15900	1	203085	1	-0.94	2.71E+09	0.388	
524.750	5830 16002	2	192831	1	-0.95	2.59E + 09 2.72E + 00	0.152	
535 863	11872	2	198487	3	-0.65	5.72E+09 5.26E+09	-0.402	
537.94	0	4	185894	4	-1	2.29E+09	0.144	
537.963	17398	2	203284	2	-0.69	4.71E + 09	-0.344	
538.239	4173	3	189964	2	-0.79	3.78E + 09	-0.403	
538.793	0	4	185600	3	-0.3	1.14E + 10	-0.391	
539.624	11872	2	197186	1	-0.94	2.64E + 09	-0.11	
541.829	17398	2	201958	3	-0.42	8.55E+09	-0.324	
543.083	5830	2	189964	2	-0.55	6.45E+09	0.598	
544.00	4173	4	187066	9 9	-0.30	9.00E+09 9.32E±00	-0.029	
544,396	11872	2	195561	3	-0.65	4.99E+09	-0.24	
545.269	0	4	183396	3	-1	2.24E+09	0.111	
545.632	5830	2	189103	1	-0.67	4.83E + 09	0.356	
545.719	4173	3	187417	2	-0.29	1.15E + 10	-0.626	
546.066	15900	1	199028	0	-0.98	2.34E + 09	0.551	
546.172	5830	2	188922	3	-0.35	1.00E + 10	-0.388	
546.377	0	4	183024	4	-0.42	8.47E + 09	-0.493	
547.162	15900	1	198661	1	-0.81	3.45E + 09 2.18E + 10	0.384	
548 183	4173	3	186593	3	-0.01	$1.28E \pm 10$	-0.446	
548.493	0	4	182318	5	0.11	2.86E+10	-0.677	
549.041	5830	2	187966	2	-0.97	2.38E + 09	0.284	
549.625	0	4	181942	3	-0.69	4.51E + 09	-0.332	
550.292	4173	3	185894	4	-0.53	6.53E + 09	-0.205	
550.699	5830	2	187417	2	-0.57	5.94E + 09	-0.222	
551.305	20570	4	201958	3	-0.71	4.31E+09	0.519	
551.684	17398	2	198661	1	-0.6	5.51E + 09	-0.365	
553 139	5830	2	186616	2	-0.87	$2.98E \pm 09$ 8 18E \pm 09	-0.393	
553.745	5830	2	186418	1	-0.72	4.16E + 09	-0.589	
554.013	11872	2	192373	2	-0.2	1.37E + 10	0.505	
554.504	11872	2	192213	1	-0.72	4.16E + 09	0.265	
554.916	4173	3	184380	3	-0.78	3.59E + 09	-0.525	
556.21	17398	2	197186	1	-0.3	1.09E + 10	-0.407	
557.104	15900	1	195399	2	-0.98	2.23E+09	-0.347	
550 194	4173	3	183390	3	-0.03	5.08E+09	0.319	
560.066	5830	2	184380	3	-0.52	$2.38E \pm 0.9$ 6 39E \pm 0.9	-0.23	
560.791	0	4	178320	4	0.06	2.42E+10	-0.55	
561.576	4173	3	182243	3	-0.52	6.36E + 09	-0.292	
561.792	17398	2	195399	2	-0.09	1.70E + 10	-0.492	
562.637	47139	0	224873	1	-0.48	7.06E + 09	0.674	
563.171	5830	2	183396	3	-0.83	3.15E+09	0.152	
563.981	15900	1	193211	2	-1	2.11E + 09	-0.401	
564 233	20370	4 2	197847	1	-0.02	2.02E+10 $2.40E\pm00$	0.500	
564.81	11872	2	188922	3	-0.67	4.48E+09	-0.331	
571.457	20570	4	195561	3	-0.62	4.84E + 09	0.283	
571.756	47139	0	222038	1	-0.47	6.91E + 09	-0.622	
572.719	17398	2	192003	3	-0.22	1.22E + 10	0.542	
574.539	20570	4	194623	4	0.37	4.78E+10	-0.572	
575.661	0	4	173713	3	-0.28	1.06E + 10	-0.45	
577 796	20570	3	193641	2 4	-0.99	$2.08E \pm 10$ 1.03E \pm 10	-0.10	
581.173	15900	1	187966	2	-0.86	2.74E+09	0.323	
581.206	11872	2	183928	1	-0.98	2.08E + 09	0.117	
582.13	16092	0	187875	1	-0.94	2.27E + 09	0.286	
582.393	17398	2	189103	1	-1	1.95E + 09	-0.123	
582.707	20570	4	192183	5	-0.64	4.46E + 09	0.67	
583.317	20570	4	192003	3	-0.83	2.87E + 09	-0.37	
585.022	0	4	171202	3	-0.63	4.01E+09	-0.138	
586 626	4173	4	174630	2	-0.74	3.54E+09 $3.77E\pm09$	-0.263	
589.152	0	4	169735	4	-0.35	8.63E+09	-0.244	
589.828	4173	3	173713	3	-0.92	2.32E + 0.09	-0.084	
589.855	11872	2	181405	2	-0.84	2.75E + 09	0.216	
590.36	4173	3	173561	2	-0.97	2.04E+09	-0.081	
592.384	5830	2	174639	2	-0.99	1.96E + 09	-0.088	
592.851	15900	1	184576	1	-0.93	2.22E+09	0.264	
595.139	15900	1	183928	1	-0.77	3.17E+09	-0.275	
596.193 596.78	0830 N	2	167566	2	-0.69	3.81E+09 5.19E⊥09	0.171	
598.697	4173	3	171202	3	-0.57	$5.00E \pm 09$	0.196	
601.792	20570	4	186740	5	-0.59	4.75E + 0.09	-0.594	
602.417	17398	2	183396	3	-0.97	1.96E + 09	-0.118	
617.887	11872	2	173713	3	-0.74	3.20E + 09	0.322	
627.627	11872	2	171202	3	-0.89	2.18E + 09	0.142	J

Table A35: Computed oscillator strengths and transition probabilities Ag IV.

Table A35: Continued

Wavelength 953-299	Lower Level 169735	J _{Low}	Upper level 274634	JUP	log gf -0.92	gA 8 90E+08	CF -0.404
965.216	159220	4	262824	5	-0.74	1.32E + 09	-0.171
1007.161 1008.597	162487 181553	3 6	261776 280701	3 5	-0.77 -0.55	1.13E+09 1.84E+09	-0.122 0.32
1021.086	180281	4	278216	3	-0.31	3.15E + 09 1.07E + 10	-0.555
1022.534	180529	4	278216	3	-0.3	3.23E+09	0.668
1023.785 1023.873	$183024 \\ 164108$	4	280701 261776	5	-0.7 -0.65	1.28E+09 1.42E+09	0.287 0.145
1027.369	166078	1	263414	2	-0.77	1.06E+09	0.269
$1029.882 \\ 1030.59$	$164678 \\ 177602$	2 5	$261776 \\ 274634$	3 5	-0.31 -0.23	3.05E+09 3.75E+09	-0.524 0.773
1038.264	178320	4	274634	5	0.01	6.30E+09	0.808
1041.959 1042.964	167533	2	263414	2	-0.62 -0.47	1.46E+09 2.07E+09	-0.325
1044.165	166006 169735	3	261776 265345	3	-0.18	4.03E+09 8.69E+08	0.513 0.137
1049.784	167566	4	262824	5	-0.94	7.05E+08	-0.164
1053.514 1054.65	168493 168596	2 3	263414 263414	2 2	-0.66 -0.73	1.29E+09 1.13E+09	-0.248 -0.328
1054.693	168600	1	263414	2	-0.49	1.94E+09	-0.188
1054.782 1061.457	$185894 \\ 167566$	4	280701 261776	5	-0.29 0.03	3.08E+09 6.34E+09	$0.639 \\ 0.792$
1063.937	186710	4	280701	5	-0.97	6.32E+08	0.128
1073.185	181553	5 6	274634	5 5	0.25	1.03E+10	0.735
1079.728	185600	3	278216 278216	3	-0.67	1.23E+09 2.24E+09	-0.541
1086.476	169735	4	261776	3	-0.47	1.92E+09	-0.419
1090.225 1091.436	182910 186593	6 3	$274634 \\ 278216$	5	-0.36 -0.29	2.44E+09 2.87E+09	-0.291 -0.658
1091.578	183024	4	274634	5	-0.55	1.58E + 09	0.248
1091.707 1092.828	$186616 \\ 186710$	2 4	$278216 \\ 278216$	3 3	-0.4 -0.77	2.21E+09 9.56E+08	$0.61 \\ 0.556$
1100.376	182318	5	273196	6	-0.6	1.37E + 09	0.088
1100.461	181555	2	278216	3	-0.23	1.61E+09	0.563
1102.885	183963 162487	5	274634 253121	5	0.11	7.13E+09 1.26E+09	-0.79
1104.064	171202	3	261776	3	-0.9	6.87E+08	0.275
1104.842 1107.598	182910 182910	6 6	273421 273196	6 6	-0.86 -0.09	7.62E+08 4.40E+09	$0.103 \\ 0.257$
1108.424	177602	5	267821	4	-0.51	1.68E+09	-0.368
1109.8 1117.146	182318 182910	5 6	$272424 \\ 272424$	6 6	$0.21 \\ 0.25$	8.73E+09 9.41E+09	-0.591
1117.305	178320	4	267821	4	-0.33	2.49E+09	0.16
1117.845	191362	6	280701	5	-0.47	1.65E+09	0.129 0.725
1119.902 1123.436	188922 164108	3	278216 253121	3	-0.96 -0.56	5.78E + 08 1.47E + 09	-0.287 -0.145
1125.835	162487	3	251310	3	0.02	5.50E+09	0.492
1127.958 1129.715	$181553 \\ 192183$	6 5	270209 280701	5 5	-0.74 0.27	9.59E+08 9.76E+09	-0.362 -0.864
1130.24	177602	5	266079	5	-0.35	2.35E+09	0.12
1131.674 1135.822	186270 159220	5 4	$274634 \\ 247262$	5 4	-0.9 0.51	0.58E+08 1.65E+10	-0.207 -0.577
1136.126	162487	3	250506	4	0.07	6.08E+09 7.60E+08	-0.402
1137.662	181553	6	269453	7	0.15	7.35E+09	0.583
1137.771 1137.919	182318 162487	5	270209 250367	5	0.33 0.31	1.10E+10 1.04E+10	0.516
1139.476	178320	4	266079	5	-0.84	7.44E + 08	-0.042
1139.695 1143.384	$177602 \\ 159220$	5 4	$265345 \\ 246680$	5 5	$0.41 \\ 0.06$	1.32E+10 5.87E+09	-0.657 0.286
1144.655	160255	5	247618	6	0.57	1.91E + 10	0.598
1145.494 1146.758	182910 164108	6 4	270209 251310	5 3	-0.94 -0.37	5.79E+08 2.19E+09	-0.276 0.419
1147.432 1147.913	186270 166006	5	273421	6	0.56	1.85E+10	-0.623
1147.515	182318	5	269391	6	-0.63	1.18E+09	-0.444
1148.645 1149.059	$193641 \\ 182318$	4 5	280701 269345	5 5	-0.61 0.05	1.24E+09 5.70E+09	-0.504 0.619
1149.087	178320	4	265345	5	0.27	9.53E + 09	0.562
1149.338 1150.404	$160255 \\ 186270$	5 5	$247262 \\ 273196$	4 6	-0.22	8.36E+09 2.89E+09	-0.741 0.234
1150.533	176498	$\frac{1}{7}$	263414	2	-0.46	1.74E + 09	-0.302
1152.282 1153.662	186411 186740	5	273196 273421	6	-0.61 0.34	1.24E+09 1.10E+10	-0.406
1154.301	164678 182010	2	251310 269453	3	-0.96	5.48E + 08 3.83E + 10	-0.061
1156.667	186740	5	273196	6	-0.05	4.40E+09	0.327
1157.082 1157.438	160255 164108	5 4	246680 250506	5 4	$0.51 \\ 0.43$	1.60E+10 1.34E+10	0.648 -0.619
1159.478	183963	5	270209	5	-0.93	5.80E + 08	0.094
1160.709 1161.737	$186270 \\ 194623$	5 4	$272424 \\280701$	6 5	-0.63 -0.61	1.15E+09 1.22E+09	-0.182 -0.396
1162.62	186411	7	272424	6	-0.11	3.81E+09	0.677
1164.563 1165.522	180411 180281	4	266079	5	0.53 -0.53	1.45E+09	0.751 0.16
1167.008	164678	2	250367	2	-0.59	1.27E+09	0.091
1168.904	180529	4	266079	5	-0.4	8.07E+08	-0.101
$1169.026 \\ 1169.548$	$177873 \\ 182318$	2 5	$263414 \\ 267821$	$^{2}_{4}$	-0.18 0.2	3.17E+09 7.67E+09	-0.46 -0.72
1170.837	178005	3	263414	2	-0.89	6.19E+08	0.295
$1172.274 \\ 1175.579$	$166006 \\ 180281$	$\frac{3}{4}$	$251310 \\ 265345$	3 5	-0.44 -0.85	1.79E+09 6.89E+08	-0.171 -0.081
1175.758	180281	4	265332	4	-0.24	2.81E+09	0.602
$1177.812 \\ 1179.2$	$165602 \\ 180529$	5 4	250506 265332	$\frac{4}{4}$	-0.29 -0.32	2.45E+09 2.32E+09	$0.424 \\ 0.539$
1179.289	183024	4	267821	4	0.14	6.72E+09	0.519
1183.058	167566	3 4	247202 252093	4 5	0.33	4.09E+08 1.03E+10	0.444
1183.063 1183.236	181553 190120	6 4	266079 274634	5	-0.87	6.46E + 08 $5.42E \pm 08$	0.214
1183.374	178320	4	262824	5	-0.97	5.18E+08	0.516

Table A35: Continued

Wavelength	Lower Level	JLow	Upper level	J_{Up}	log gf	gA	CF
1184.483 1186.036	$183396 \\ 185894$	3 4	$267821 \\ 270209$	4 5	-0.67 -0.49	1.01E+09 1.54E+09	-0.323 0.318
1191.34	186270	5	270209	5	-0.54	1.37E+09	-0.365
1191.843	177873	2	261776	3	-0.86	6.52E + 08	0.318
1192.496	183963	5	267821	4	-0.29	2.41E+0.09	0.332
1193.426	181553	6	265345	5	-0.36	2.04E + 09	0.583
1193.645 1194.114	167533	2	251310 251310	3	-0.87 -0.65	6.30E+08 1.05E+09	-0.132 0.14
1197.603	179914	1	263414	2	-0.7	9.36E + 08	0.113
1197.624	186710	4	270209	5	-0.63	1.11E + 09	-0.181
1198.038	181553	6	265006	7	0.88	3.54E+10	0.303 0.877
1198.307	185894	4	269345	5	-0.03	4.34E + 09	-0.479
1199.182 1199.256	181942 169735	3 4	265332 253121	4	0.32	9.83E+09 2.81E+09	0.454
1203.056	186270	5	269391	6	0.48	1.38E+10	-0.851
1203.722	186270	5	269345	5	-0.33	2.17E + 09 1.07E + 10	0.324
1204.014	186411	47	269453	7	-0.71	8.98E+08	-0.851
1204.412	170092	5	253121	4	-0.67	9.90E + 08	0.479
1205.698 1206.954	197847	4 5	250506 280701	4 5	-0.66 -0.57	1.02E+09 1.23E+09	0.059 -0.149
1208.977	168596	3	251310	3	-0.93	5.43E + 08	0.053
1209.907 1210 138	186740 186710	5	269391 269345	6	0.65 0.17	2.03E+10 6.76E+00	0.717 0.565
1210.138	186740	5	269345	5	-0.06	3.96E+09	-0.395
1211.067	164108	4	246680	5	-0.51	1.42E + 09	-0.095
1211.491 1212.98	180281 190754	4 6	262824 273196	5 6	0.5	1.43E+10 1.33E+09	0.862
1213.074	182910	6	265345	$\tilde{5}$	-0.92	5.42E + 08	-0.227
1214.221	169735	4	252093	5	0.42	1.20E+10 1.21E+10	-0.675
1215.314	120871	6	202824 203155	5	-0.7	8.95E+08	-0.342
1217.785	183963	5	266079	5	0.32	9.40E+09	0.59
1218.085 1218.633	182910 191362	6 6	265006 273421	7 6	0.19	6.97E+09 8.30E+08	-0.269 0.274
1219.276	165602	6	247618	6	0.51	1.44E+10	0.875
1219.28	165602	5	247618	6	-0.06	3.91E + 09	0.219
1220.454	183396	3	265332	4	-0.1	3.60E+09	0.435
1220.722	171202	3	253121	4	-0.33	2.06E + 09	-0.23
1221.987 1225.87	191362 169735	6 4	273196 251310	6	0.28	8.38E+09 2.06E+09	$0.441 \\ 0.311$
1226.226	186270	5	267821	$\tilde{4}$	-0.83	6.51E + 08	0.381
1228.768	183963	5	265345	5	0.07	5.19E+09	0.331
1230.95	192183	5	273421	6	0.2	6.96E+09	0.849
1233.386	165602	6	246680	5	-0.18	2.92E + 09	0.745
1233.391 1233.62	165602 191362	5 6	246680 272424	5 6	-0.05 0.3	3.91E+09 8.76E+09	0.297 0.41
1234.372	192183	5	273196	6	0.36	9.95E+09	0.577
1235.292	184380	3	265332	4	0.01	4.47E + 09	0.487
1235.808	169735	4	250506	4	-0.89	5.62E+08	$0.944 \\ 0.061$
1246.243	192183	5	272424	6	-0.09	3.46E + 09	-0.197
1248.308 1249.197	171202 173069	3 4	251310 253121	3	-0.18	2.84E+09 3.90E+09	$0.3 \\ 0.454$
1252.981	186270	5	266079	5	-0.56	1.18E + 09	0.117
1259.335	173713	3	253121	4	-0.66	9.09E+08	0.08
1264.005	167566	4	246680	5	-0.82	6.37E+08	0.181
1264.612	186270	5	265345	5	-0.98	4.42E + 08	0.037
1268.278	191362	4 6	270209	э 5	0.24	$9.90E \pm 0.08$ $7.15E \pm 0.09$	-0.395 0.75
1280.56	191362	6	269453	7	-0.4	1.61E + 09	0.376
1281.624	192183	5	270209 269345	5 5	-0.96	4.43E+08 2 19E+09	0.092 0.663
1288.714	173713	3	251310	3	-0.57	1.07E+09	0.12
1293.979	102633	2	179914	1	-0.92	4.75E+08	-0.492
1301.482	101261	4 3	178005	4 3	-0.98	4.08E+08	0.108
1305.278	101261	3	177873	2	-0.7	7.87E+08	-0.456
1319.065	122456 115550	э 5	198990	4 6	-0.67	3.83E+08 3.83E+08	-0.346 -0.246
1320.937	193641	4	269345	5	-0.84	5.55E + 08	-0.422
1322.087 1322.005	192183	5	267821	4 5	-0.82	5.73E + 08 6.69E + 08	0.101
1327.172	197847	5	273196	6	-0.52	1.13E+09	0.11
1338.282	194623	4	269345	5	-0.15	2.66E+09	-0.691
1340.172 1351.293	153026 110377	2	227643 184380	3	-0.76	3.91E+08	-0.405
1352.247	125077	1	199028	0	-0.95	4.05E + 08	0.34
1353.982 1355.111	153026 121767	2	226882 195561	2	-0.76 -0.84	6.28E+08 $5.22E\pm08$	$0.244 \\ 0.358$
1358.712	118614	1	192213	1	-0.86	5.01E + 08	0.34
1358.996	125077	2	198661	1	-0.73	6.72E+08	-0.265
1360.224 1362.859	154126 111005	3	227643 184380	3	-0.62	5.03E+09 8.69E+08	0.612 0.518
1364.156	178005	3	251310	3	-0.92	4.29E + 08	0.16
$1365.091 \\ 1369.376$	$125735 \\ 103472$	4	198990 176498	4	-0.8 -0.93	5.71E + 08 4.23E + 08	$0.542 \\ -0.651$
1369.506	110377	3	183396	3	-0.73	6.62E + 08	-0.255
1372.571	121767	4	194623	4	-0.69	7.25E+08	0.12
1376.105	112612	4 1	196487 185281	3 2	-0.43 -0.88	4.70E+09	-0.342
1377.81	122820	3	195399	2	-0.68	7.46E + 08	-0.417
1378.673 1380.495	152454 193641	1 4	224988 266079	2 5	-0.46 -0.71	1.21E+09 6.73E+08	-0.705 0.188
1380.749	102633	2	175057	3	-0.76	6.09E + 08	0.403
1380.855	152454	1	224873	1	-0.48	1.16E + 09	0.64
1381.939	178005	э 3	250367	3 2	-0.94	4.02E+08 6.02E+08	$0.105 \\ 0.241$
1385.686	122456	5	194623	4	-0.94	3.98E + 08	0.249
1386.728	125735	4	197847	5	-0.68	7.30E + 08	0.577

Table A35: Continued

Wavelength	Lower Level	JLow	Upper level	J_{Un}	log gf	gA	CF
1389.575	112612	1	184576	1	-0.9	4.31E + 08	-0.286
1389.628	153026	2	224988	2	-0.13	2.54E+09	0.482
1391.307	121767	4	193641	4	-0.13	2.58E+09 7.21E+08	0.656
1392.592	101261	3	173069	4	-0.37	1.46E+09	0.385
1399.449	194623	4	266079	5	-0.54	9.74E + 08	0.203
1402.576	107022	4	178320	4	-0.74	6.24E + 08	0.189
1403.745	111005	3	182243	3	-0.94	3.89E + 08	0.314
1404.785	122456	5	193641	4	-0.89	4.40E + 08	0.227
1405.099	96397	5	167566	4	-0.97	3.60E+08	-0.108
1405.139	110779	2	181942	3	-0.59	$4.06E \pm 09$	-0.696
1406.849	102633	2	173713	3	-0.81	5.18E + 08	0.58
1407.573	110779	2	181823	1	-0.69	6.88E + 08	0.279
1407.896	110377	3	181405	2	-0.8	5.39E + 08	-0.243
1409.405	131006	2	201958	3	-0.79	5.47E + 08	-0.332
1409.537	99147	4	170092	5	0.06	3.84E + 09	-0.438
1409.691	102633	3	181942	3	-0.82	$5.12E \pm 08$ $4.07E \pm 08$	0.151
1412.686	110377	3	181164	2	-0.92	3.43E+08	-0.181
1414.042	115550	5	186270	5	-0.71	6.52E + 08	0.19
1415.966	112612	1	183235	2	-0.4	1.34E + 09	-0.464
1417.638	121833	2	192373	2	-0.62	8.03E + 08	0.313
1418.633	120871	6	191362	6	0.46	9.47E + 09	0.684
1420.761	110779	2	181164	2	-0.64	$7.62E \pm 08$	0.299
1420.839	132758	2	203085	1	-0.85	$2.06E \pm 0.09$	-0.212
1422.024	125077	2	195399	2	-0.76	5.73E+08	0.193
1423.21	131006	2	201269	3	-0.47	1.12E + 0.09	0.658
1425.467	110377	3	180529	4	-0.36	1.44E + 09	0.474
1428.185	133265	3	203284	2	-0.18	2.18E + 09	-0.469
1429.159	133265	3	203237	4	-0.36	1.41E + 09	-0.363
1429.771	101261	3	171202	3	-0.96	3.57E + 08	-0.4
1429.914	116806	4	186740	5	-0.7	6.56E+08	0.102
1430.246	127929	3	197847	Э 4	0.42	$8.48E \pm 09$ $1.63E \pm 09$	0.675
1430.523	116806	4	186710	4	-0.33	1.54E+09	0.427
1432.603	119119	3	188922	3	-0.73	$6.10E \pm 0.08$	0.364
1432.924	116806	4	186593	3	-0.74	5.94E + 08	-0.126
1434.175	122456	5	192183	5	0.4	8.14E + 09	0.663
1434.79	122676	1	192373	2	-0.89	4.17E + 08	0.193
1436.384	138852	3	208471	3	0.22	5.35E + 09	0.717
1437.106	152454	1	222038	1	-0.42	1.22E + 09	0.675
1437.766	122820	3	192373	2	-0.9	4.06E + 08	-0.158
1438.344	153026	2	222520	4	-0.23	$1.88E \pm 09$ $1.76E \pm 09$	-0.027
1439.602	116806	4	186270	5	-0.46	1.13E+09	-0.117
1441.925	118614	1	187966	2	-0.79	5.15E + 08	0.227
1443.498	111005	3	180281	4	-0.24	1.84E + 09	-0.491
1444.143	158398	2	227643	3	-0.64	7.30E + 08	-0.745
1444.967	96397	5	165602	5	-0.34	1.46E + 09	0.252
1444.974	96397	5	165602	6	0.55	1.13E + 10	-0.832
1445.102	132758	2	201958	3	-0.58	8.36E + 08	-0.641
1447.424	110800	4	185894	4	-0.62	7.71E + 08	-0.172
1451.204	122450	4	191502	4	-0.51	$9.84E \pm 0.00$ $3.52E \pm 0.00$	-0.499
1453.639	112612	1	181405	2	-0.68	6.61E + 08	-0.48
1454.505	118603	2	187355	3	-0.04	2.91E + 09	-0.686
1455.673	133265	3	201962	4	0.1	3.96E + 09	0.744
1455.765	133265	3	201958	3	-0.6	7.87E + 08	0.337
1456.482	134578	4	203237	4	0.07	3.67E + 09	0.491
1458.076	132758	2	201342	2	-0.14	2.30E + 09	0.704
1458.225	112612	4	203155	2	-0.87	$4.21E \pm 08$	-0.701
1459.619	132758	2	201269	3	-0.38	1.30E+09	-0.471
1460.193	158398	2	226882	2	0.02	3.26E + 09	0.699
1460.388	101261	3	169735	4	-0.3	1.55E + 09	0.631
1460.763	130571	1	199028	0	-0.87	4.22E + 08	0.589
1461.584	99147	4	167566	4	-0.55	8.83E+08	0.143
1461.719	11000	2	183903	2	0.27	$5.79E \pm 09$ 1.42E ± 00	0.696
1464.176	122456	5	190754	6	-0.13	2.31E+09	0.206
1467.767	121833	2	189964	2	-0.99	3.19E + 0.08	-0.245
1468.638	130571	1	198661	1	-0.39	1.26E + 09	-0.682
1470.498	133265	3	201269	3	-0.2	1.94E + 09	0.322
1472.617	125735	4	193641	4	-0.06	2.70E+09	0.516
1475.933	125077	2 5	192831	1	-0.37	1.32E+09	-0.639
1478.674	110377	3	178005	3	-0.27	$1.63E \pm 0.09$	0.651
1479.491	119119	3	186710	4	-0.53	9.11E + 08	-0.662
1479.862	116806	4	184380	3	-0.83	4.47E + 08	-0.383
1481.551	119119	3	186616	2	-0.19	1.95E + 09	-0.753
1482.05	119119	3	186593	3	-0.15	2.17E + 09	0.636
1482.065	115550	5	183024	4	-0.26	1.68E + 09	-0.347
1484.125	134578	4	201958	3	-0.08	2.49E+09 1.30E+00	-0.527
1485 100	101961	о 2	162910	0 3	-0.34	1.39E+09 4.57E+08	0.220
1485.841	112612	1	179914	1	-0.48	$9.94E \pm 0.8$	-0.573
1485.887	122820	3	190120	4	0.35	6.71E + 0.09	-0.804
1486.16	122676	1	189964	2	-0.75	5.41E + 08	0.243
1487.523	110779	2	178005	3	-0.65	6.73E + 08	-0.195
1487.904	112612	1	179820	0	-0.9	3.85E + 08	-0.601
1489.048	116806	4	183963	5	-0.33	1.42E+09	-0.721
1489.078	121767	4	188922	3	-0.77	5.09E+08	-0.251 0.507
1489 516	122020	1	192213	1	-0.77	$3.11E \pm 0.08$	0.229
1490.456	110779	2	177873	2	-0.57	8.00E+08	-0.335
1491.331	203155	5	270209	5	-0.99	3.12E + 08	0.131
1492.535	111005	3	178005	3	-0.69	6.10E + 08	-0.246
1492.557	154126	3	221125	4	0.35	6.68E+09	-0.77
1494.18	125077	2	192003	3	-0.19	1.93E+09	0.712
1495.488	11005	3	195904	2	-0.78	4.91E+08	-0.273
1497.300	127020	3 5	104622	4	-0.27	1.00E+09 2.32E±00	0.605
1499.441	134578	4	201269	3	-0.72	$5.66E \pm 0.08$	0.518
1499.448	107022	4	173713	3	-0.83	4.37E + 08	-0.11

Table A35: Continued

Wavelength 1499.754	Lower Level 118603	J _{Low}	Upper level 185281	J _{Up} 2	log gf -0.61	gA 7.27E+08	CF -0.236
1501.734	116806	4	183396	3	-0.37	1.26E + 09	0.658
1501.736 1504.197	158398 119119	2 3	224988 185600	2	-0.89 -0.61	3.84E+08 7.31E+08	-0.251 0.5
1504.325	158398	2	224873	1	-0.41	1.17E + 09	0.729
1504.772 1504.947	99147 125735	4	165602 192183	5 5	-0.23	4.95E+09 6.63E+08	-0.829 -0.68
1507.046	125858	0	192213	1	-0.81	4.58E + 08	0.534
1509.017	101261 125735	3 4	192003	4 3	-0.23	3.78E+09 1.73E+09	-0.804 0.675
1510.168	116806	4	183024	4	-0.06	2.53E + 09	0.749
1510.528	120216 131006	$^{0}_{2}$	$186418 \\ 197186$	1	-0.75 -0.25	5.13E+08 1.64E+09	-0.406 -0.697
1515.093	115550	5	181553	6	0.46	8.43E+09	-0.797
1515.768 1516.002	118603 102633	$\frac{2}{2}$	$184576 \\ 168596$	1 3	-0.8 0.11	4.63E+08 3.74E+09	-0.292 -0.817
1517.755	131006	2	196893	2	-0.64	6.64E+08	-0.33
1520.292	$118603 \\ 132758$	2	184380 198487	3	-0.87 -0.23	3.90E+08 1.71E+09	-0.425
1521.488	133265	3	198990	4	-0.57	7.84E+08	-0.146
1525.785	127929 120871	6	186411	47	-0.38	1.19E+09 1.15E+10	-0.859
1526.205	121833	2	187355	3	-0.29	1.49E + 09 1.08E + 00	-0.719
1528.194 1531.068	118614	4	182243 183928	1	-0.10	1.98E+09 5.58E+08	0.325
1531.919	152454	1	217732	0	-0.59	7.33E+08	-0.797
1531.939	119119	3	184380	3	-0.78	4.72E+08 3.13E+08	0.555
1533.242	133265	3	198487	3	-0.33	1.33E+09	-0.678
1534.127	112689	2	177873	2	-0.67	6.07E+08	0.437
1535.44	103472	1	168600	1	-0.39	1.16E + 09 0.17E + 08	0.773
1537.947 1539.085	121767	4	186740	5	-0.49	2.23E+09	-0.245
1539.392	99147 152026	4	164108	4	0.23	4.80E+09	-0.765
1539.801	121767	4	186710	4	-0.4	1.12E+09	-0.329
1540.819	102633	2	167533	2	-0.12	2.15E + 09 1.60E + 00	-0.754
1541.149	125077	1	189964	2	-0.23	1.60E+09 1.60E+09	-0.587
1542.524	130571	1	195399	2	-0.69	5.65E + 08	0.555
1542.375	118603	2	183396	3	-0.77	4.73E+08	0.41 0.251
1544.512	101261	3	166006 187417	3	0.08	3.38E+09 1.64E+09	-0.744
1546.403	203155	5	267821	$\frac{2}{4}$	-0.94	3.22E+08	-0.245
1547.224	118603 118614	2	183235	2	-0.79	4.49E+08 7.44E+08	-0.217
1549.053	131006	2	195561	3	-0.04	2.54E+0.09	-0.625
1550.315	121767 138852	4	186270 203284	5	0.13	3.73E+09 1.11E+09	0.735
1552.493	134578	4	198990	4	-0.08	2.29E+09	-0.698
1552.947	$131006 \\ 138852$	2	195399 203237	2	-0.57 -0.24	7.40E+08 1.59E+09	0.288
1555.595	122456	5	186740	5	-1	2.77E + 08	0.241
1556.327 1556.615	122456 110779	5	186710 175021	4	-0.24 -0.73	1.59E+09 5 15E+08	-0.421 -0.618
1558.131	107022	4	171202	3	0.11	3.57E + 09	-0.753
1559.232	132758 121767	2 4	196893 185894	2 4	-0.56 -0.77	7.53E+08 4 68E+08	$0.414 \\ 0.217$
1559.537	158398	2	222520	3	0.09	3.36E+09	-0.63
1560.997	103472 125077	1	167533 189103	2	-0.88 -0.67	3.65E+08 5.90E+08	-0.146 0.364
1563.968	122676	1	186616	2	-0.54	7.77E + 08	-0.578
1565.927 1565.957	110779 96397	2 5	$174639 \\ 160255$	2 5	-0.99 0.37	2.81E+08 6.34E+09	$0.56 \\ 0.833$
1566.29	125077	2	188922	3	-0.32	1.30E + 09	0.663
1566.296 1567.184	$154126 \\ 112689$	3 2	217971 176498	3 1	-0.52 -0.54	8.30E + 08 7.82E + 08	-0.703 -0.673
1568.064	122820	3	186593	3	-0.8	4.28E+08	-0.468
1569.576	122676 120216	1 0	186418 183928	1	-0.71	5.28E+08 4.46E+08	$0.378 \\ 0.332$
1571.329	158398	2	222038	1	-0.46	9.42E + 08	-0.6
1575.427	116806	4	180281	4	-0.92	4.89E+08	$0.34 \\ 0.321$
1576.101	121833	2	185281	2	-0.52	8.14E+08	0.279 0.752
1576.171	152454	1	215899	2	-0.07	2.28E+09	-0.69
1576.341	122456	5	185894	4	0.01	2.76E+09 5.19E+08	-0.679
1576.86	101261	3	164678	2	-0.05	2.42E+09	0.744
1577.953	102633	2	166006	3	-0.82	4.08E+08	-0.106
1578.801	118603	2	181942	3	-0.64	6.15E+08	-0.163
1578.86	110377 153026	3	173713	3	-0.29	1.37E+09 1.82E+09	0.553 0.781
1581.145	125858	0	189103	1	-0.38	1.12E+0.9 1.12E+0.9	-0.615
1581.773 1582.602	118603 125735	2 4	181823 188922	1	-0.73 -0.26	4.93E+08 1 47E+09	-0.436 -0.769
1582.681	110377	3	173561	2	-0.42	1.01E+09	-0.522
1584.196 1584.536	$119119 \\ 138852$	3	$182243 \\ 201962$	3 4	-0.5 -0.05	8.47E + 08 $2.39E \pm 09$	-0.277 -0.442
1585.537	107022	4	170092	5	0.22	4.42E + 09	0.807
1590.119 1590.505	125077 153026	$\frac{2}{2}$	$187966 \\ 215899$	2 2	-0.13 -0.62	1.97E+09 6.33E+08	0.596 -0.608
1591.157	101261	3	164108	4	-0.76	4.61E + 08	-0.095
1591.732 1591.765	127929 96397	5 5	$190754 \\ 159220$	$\frac{6}{4}$	$0.42 \\ 0.25$	6.93E+09 4.69E+09	-0.848 -0.793
1592.316	118603	2	181405	2	-0.56	7.33E+08	0.297
1592.402 1592.589	125077 118614	1	$187875 \\181405$	$\frac{1}{2}$	-0.56 -0.84	7.13E+08 3.82E+08	-0.429 -0.244
1592.878	122820	3	185600	3	0.01	2.67E + 09	0.752
1593.136	115550 121833	5 2	178320 184576	4 1	0.11 -0.75	3.41E+09 4.70E+08	-0.784 0.289
1594.561	107022	4	169735 172712	4	0.18	3.93E + 09 1.77E + 00	0.67
1094.073	111009	3	113113	3	-0.17	1.110+09	0.732

Wavelength Lower Level J _{FW} log J_FW log J_FW <thlog j_fw<="" th=""></thlog>			Table	<u>A35: Con</u>	tinue	ed		
1566.19 130571 1 133211 2 -0.09 2.14E+09 -0.746 1597.106 121767 4 14840 3 -0.74 4.99E+08 0.242 1598.471 111005 11715 1 -0.75 4.99E+08 0.242 1598.791 118614 1 1181164 2 -0.44 8.46E+08 0.421 1598.799 118832 2 14342 2 -0.42 8.46E+08 0.474 1601.02 123825 3 155573 1 0.77 4.93E+08 -0.434 1606.16 1330571 1 122831 1 -0.77 4.45E+08 0.434 1607.545 131006 2 13314 2 -0.474 1.9558 0.722 1611.549 112055 5 17702 5 -0.12 1.94E+09 -0.674 1611.491 120853 1.48210 6 -0.58 6.77E+08 -0.724 1611.491 120850 1.7762 5 -0.12 1.94E+09 -0.674 1611.491 <td>Wavelength 1595.089</td> <td>Lower Level 110377</td> <td>J_{Low} 3</td> <td>Upper level 173069</td> <td>J_{Up} 4</td> <td>log gf -0.01</td> <td>$_{2.58E+09}^{gA}$</td> <td>CF -0.81</td>	Wavelength 1595.089	Lower Level 110377	J_{Low} 3	Upper level 173069	J_{Up} 4	log gf -0.01	$_{2.58E+09}^{gA}$	CF -0.81
19.97.008 1.21767 4 1.84380 3 -0.41 1.0112+08 -0.349 1598.466 1.18603 2 18164 2 -0.34 1.21E+09 -0.71 1598.721 1.18614 1.81614 2 -0.34 1.21E+09 -0.71 1598.721 1.18614 1.81614 2 -0.34 0.428 9.81E+08 -0.361 1598.721 1.18614 2 0.752 1.38248 -0.72 0.352 8.352+08 -0.401 1603.38 112689 2 175057 3 -0.15 3.635+09 -0.72 1604.31 112689 2 175057 3 -0.472 1.582+08 -0.404 1610.433 1.12687 4 1.83953 5 -0.39 1.04E+09 -0.472 1611.449 1.12687 4 1.83963 5 -0.72 1.45E+08 -0.321 1611.451 1.12687 4 -0.58 -0.686+08 -0.268 16	1596.419	130571	1	193211	2	-0.09	2.14E + 09	-0.746
1598.446 118003 2 181164 2 -0.51 8.00E+08 -0.54 1598.771 118614 1 181164 2 -0.64 5.64E+08 -0.243 1598.771 11863 2 1483 2 -0.65 5.64E+08 -0.243 1601.02 122820 3 155281 2 -0.5 8.32E+08 0.511 1604.311 112689 2 175021 1 -0.75 4.35E+08 0.494 1607.431 112689 2 175021 1 -0.77 4.15E+08 0.332 1601.431 121767 4 183928 1 -0.89 1.46E+09 -0.468 1611.431 110050 1 71002 5 -0.12 1.44E+09 -0.272 1614.744 118504 2 174039 2 -0.28 1.45E+09 0.631 1611.441 120871 6 122076 1 148396 3 -0.58 6.77E+08 -0.722 1614.744 1280871 2 123393 2 -0.3	1597.106 1597.285	121767 103472	4	184380 166078	3	-0.41 -0.72	1.01E+09 4.99E+08	-0.526 0.242
1988.771 11005 3 173661 2 -0.34 1.21E+09 -0.71 1900.26 138852 3 201342 2 -0.49 8.46E+08 -0.474 1601.62 122820 3 155521 2 -0.49 8.46E+08 -0.792 1603.38 112869 2 175057 3 0.15 3.63E+08 -0.992 1604.311 112869 2 175057 3 0.67 4.54E+08 -0.491 1607.55 131006 2 19321 2 -0.87 3.54E+08 -0.408 1610.433 110553 173660 4 -0.127 1.48E+09 -0.617 1611.431 111055 3 173669 4 -0.127 1.44E+09 -0.621 1614.241 121877 4 183963 3 -0.58 6.77E+08 -0.722 1614.341 121877 183043 0 -0.88 6.75E+08 -0.561 1614.454 121885 0 -0.671 1.54E+09 -0.611 1614.454 12	1598.446	118603	2	181164	2	-0.51	8.00E + 08	-0.54
1508.799 121833 2 144380 3 -0.42 0.81E+08 -0.474 1601.02 122820 3 155281 2 -0.5 8.32E+08 0.53 1604.311 112689 2 175021 1 -0.72 4.36E+08 0.33 1604.311 1122687 2 193211 1 -0.77 3.55E+08 0.33 1607.811 121677 4 183963 -0.33 1.64E+08 -0.368 1607.811 1121677 4 183963 -0.437 1.56E+08 0.327 1611.231 1131005 3 174693 -0.421 1.44E+09 -0.37 1611.431 1120871 6 1.6210 -0.586 6.77E+08 -0.326 1624.543 121839 2 134390 2 -0.44 1.48E+09 -0.679 1624.541 1218767 1 184078 0 -0.88 2.68E+08 -0.544 1624.5401 122867 1	1598.571 1598 721	111005 118614	3	173561 181164	2	-0.34 -0.66	1.21E+09 5.64E+08	-0.71 -0.243
1600.26 138852 3 201342 2 -0.48 8.46E+08 0.551 1601.02 122520 3 13581 2 -0.5 8.22E+08 0.551 1605.239 133205 3 15561 3 0.17 3.63E+08 0.334 1605.61 130571 1 122831 1 -0.79 4.16E+08 0.332 1607.685 131006 2 133225 -0.83 1.04E+09 -0.228 1611.433 1218530 5 177602 4 -0.48 5.33E+08 0.261 1611.733 1126850 5 177602 4 -0.48 5.33E+08 0.763 1614.204 1126867 6 -0.85 6.77E+08 -0.764 1.644734 1.0847 0.066 1.641751 1.18467 1.06473 0.075 0.664 1.78320 4 -0.4 9.97E+08 0.765 1628.407 122676 1 183024 4 0.71 1.68E+08	1598.799	121833	2	184380	3	-0.42	9.81E + 08	-0.369
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1600.26 1601.02	138852 122820	3	201342 185281	2	-0.49	8.46E+08 $8.32E\pm08$	$0.474 \\ 0.551$
1604.311 112889 2 175021 1 -0.72 4.93E+08 -0.84 1605.239 133265 3 15561 3 -0.77 5.4E+08 0.348 1607.811 121767 4 158063 5 -0.39 3.36E+08 0.348 1611.431 121833 2 183028 5 -0.12 1.94E+09 -0.637 1611.549 112550 5 177062 5 -0.12 1.94E+09 -0.637 1614.204 120871 6 162910 6 -0.58 6.77E+08 -0.74 1.84E+08 0.601 1624.339 121833 2 183366 3 -0.56 6.50E+08 -0.344 1624.361 1218767 1 183366 3 -0.56 6.50E+09 -0.82 1628.667 122676 1 183024 4 -0.17 1.68E+08 0.374 1633.275 101261 3 1624873 -0.77 1.68E+08 0.	1603.38	112689	2	175057	3	0.15	3.63E+09	-0.792
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1604.311	112689	2	175021	1	-0.72	4.93E+08	-0.494
1607.815 131066 2 103211 2 -0.87 3.53E+08 0.23E 1610.443 121863 2 183923 1 -0.89 3.36E+08 -0.37E 1611.231 111005 5 173662 4 -0.12 144E+09 -0.637 1611.831 120833 2 164678 2 -0.67 5.48E+08 0.616 1614.754 120871 6 152910 6 -0.58 6.77E+08 0.722 1614.4204 112869 2 174633 0.64 7.34E+08 0.324 1624.359 121833 2 183966 -0.68 6.67E+08 -0.548 1625.461 121867 1 184078 0 -0.33 1.17E+09 -0.456 1628.463 1212676 1 184024 0.76 6.88E+09 0.617 1632.461 1212676 1 183924 1 0.72 2.98E+08 0.171 1632.461 1212676	1606.16	130571	1	192831	1	-0.79	4.16E + 08	0.304 0.293
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1607.585	131006	2	193211	2	-0.87	3.53E+08	0.232
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1610.443	121707	4 2	183928	1	-0.39	3.36E+08	-0.408
1011.2439 117.602 3 -0.12 1.345+199 -0.122 1011.204 112280 2 -0.64 6.77E-68 0.722 1011.204 112815 2 174339 2 -0.24 1.48E+109 0.061 1014.754 113814 1 180543 0 -0.68 5.39B+00 0.331 1624.359 121833 2 183396 3 -0.56 -0.756 1624.369 122876 1 184078 0 -0.48 -0.82 1628.607 1228767 1 183024 -0.071 1.68E+09 -0.661 1633.261 122767 1 183024 -0.57 4.555 -0.071 1633.261 121767 1 183024 -0.57 4.556+00 0.131 1634.41 9147 1602457 -0.71 1.68E+00 0.121 1635.012 119119 3 180241 -0.171 1.88924 -0.071 1.8882+00 0.131 <tr< td=""><td>1611.231</td><td>111005</td><td>3</td><td>173069</td><td>4</td><td>-0.12</td><td>1.94E + 09</td><td>-0.637</td></tr<>	1611.231	111005	3	173069	4	-0.12	1.94E + 09	-0.637
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$1611.549 \\ 1611.733$	$115550 \\ 102633$	$\frac{5}{2}$	$177602 \\ 164678$	5	-0.12 -0.67	1.94E+09 5.48E+08	-0.722 0.163
1614.704 112659 2 174639 2 -0.24 1.48E-09 0.661 1622.611 121767 4 183396 3 -0.54 7.34E+08 0.375 1622.611 121767 4 183396 3 -0.54 7.34E+08 0.375 1627.437 120871 6 178320 4 0.175 5.6E+09 -0.679 1628.607 122876 1 184078 0 -0.98 2.68E+08 -0.679 1628.613 122876 1 184078 0 -0.98 2.68E+08 -0.679 1633.275 101261 3 102487 -0.071 1.68E+09 0.84 1633.275 101261 3 102487 -0.071 1.88D24 -0.171 1.68E+09 0.84 1634.649 130571 1 197635 0 0.98 2.35E+08 -0.074 1639.207 125735 4 186740 0.08 3.75E+09 0.575 1639.404 131006 2 192003 -1 2.46E+08 -0.074	1611.894	120871	6	182910	6	-0.58	6.77E + 08	-0.722
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1614.204 1614.754	112689 118614	2	174639 180543	2	-0.24 -0.68	1.48E+09 5.39E+08	$0.661 \\ 0.756$
$\begin{array}{llllllllllllllllllllllllllllllllllll$	1622.611	121767	4	183396	3	-0.54	7.34E + 08	0.332
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1624.359	121833	2	183396	3	-0.56	6.90E+08	-0.344
$\begin{array}{llllllllllllllllllllllllllllllllllll$	1627.437	120871	4 6	182318	5	0.37	5.96E+09	-0.82
$\begin{array}{l c c c c c c c c c c c c c c c c c c c$	1628.403	119119	3	180529	4	-0.17	1.68E + 09	-0.679
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1628.607 1628.613	122676 121833	1 2	184078 183235	0	-0.98 -0.63	2.68E+08 5.93E+08	-0.564 0.297
$\begin{array}{llllllllllllllllllllllllllllllllllll$	1629.539	131006	2	192373	2	-0.33	1.17E + 09	-0.456
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1632.461 1632.613	121767 122676	4	183024	4	-0.57	6.75E + 08 2 00E + 08	0.171 0.193
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1633.275	101261	3	162487	3	-0.71	4.88E+08	0.133
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1635.012	119119	3	180281	4	-0.17	1.68E + 09	0.58
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1636.431 1636.44	154126 99147	3 4	215235 160255	2 5	-0.9	2.88E+09 3.13E+08	-0.794 0.074
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	1636.469	130571	1	191678	õ	-0.98	2.65E + 08	-0.492
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1639.207 1639.404	125735 131006	4	186740 192003	5	0.18	3.75E+09 2.46E+08	0.578
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1639.791	134578	4	195561	3	-0.63	5.72E + 08	0.496
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1642.799	112689	2	173561	2	-0.92	3.00E+08	-0.137
$\begin{array}{llllllllllllllllllllllllllllllllllll$	1647.944	120871	4 6	181553	6	-0.62	$4.19E \pm 0.09$ $5.81E \pm 0.08$	-0.664
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1651.047	122456	5	183024	4	-0.93	2.87E + 08	-0.125
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1651.501 1651.698	$121767 \\ 107022$	4	182318 167566	5 4	-0.9 -0.55	3.11E+08 6.89E+08	$0.515 \\ 0.216$
$\begin{array}{llllllllllllllllllllllllllllllllllll$	1651.952	125735	4	186270	5	-0.11	1.91E + 09	0.524
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1652.271 1653.546	125077 121767	2 4	185600 182243	3	-0.86	3.37E+08 6.09E+08	0.142 0.263
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1654.153	122456	5	182910	6	0.31	4.93E+09	-0.732
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1662.832	138852	3	198990	4	-0.2	1.55E+09 5.46E+08	-0.598
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1666.936	121833	2	181823	1	-0.82	3.65E+08	-0.13
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1678.618	158398	2	217971	3	-0.5	7.48E+08	-0.712
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1683.451 1686.263	118603 125077	2	178005 184380	3	-0.75 -0.91	4.13E+08 2.86E+08	-0.209
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1687.208	118603	2	177873	$\tilde{2}$	-0.93	2.77E + 08	-0.151
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1692.141 1700.364	122456 127929	5	181553 186740	6 5	-0.6	5.90E + 08 2.93E + 08	-0.125 -0.471
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1701.238	127929	5	186710	4	-0.29	1.17E + 09	0.796
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1701.766 1706.945	121767 122820	4	180529 181405	4	-0.59 -0.64	5.83E+08 5.35E+08	0.656 0.61
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1707.064	107022	4	165602	5	-0.16	1.60E + 09	-0.379
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1708.985	121767	4	180281	4	-0.83	3.35E+08	-0.386
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1720.676	110377	3	168493	2	-0.44	8.15E+08	0.233 0.592
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1722.936	138852	3	196893	2	-0.55	6.31E+08	-0.534
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1736.384	1110779	3	168596	3	-0.4	3.28E+08	0.093 0.312
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1739.474	111005	3	168493	2	-0.59	5.71E + 08	-0.407
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1741.384 1743.208	134578 111005	4	192003 168370	3	-0.81 -0.97	3.42E+08 2.34E+08	0.558
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1748.575	110377	3	167566	4	-0.56	5.99E + 08	-0.508
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1761.983 1763.719	110779 133265	2	167533 189964	2	-1	2.16E+08 2.59E+08	-0.505 0.56
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1768.429	138852	3	195399	2	-0.75	3.84E + 08	-0.473
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1769.675	125735	4	182243	3	-0.98	2.25E+08	-0.219
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1772.480 1780.251	121833	2	178005	3	-0.78	3.63E+08	-0.295
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1780.504	132758	2	188922	3	-0.81	3.27E + 08	0.423
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1784.914 1786.104	$118614 \\ 112612$	1	174639 168600	2	-0.83 -0.8	3.09E+08 3.31E+08	$0.466 \\ 0.536$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1788.692	112689	2	168596	3	-1	2.08E + 08	-0.366
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1789.498 1790.963	$112612 \\ 121767$	$\frac{1}{4}$	168493 177602	2 5	-0.79	3.42E + 08 2.63E ± 08	-0.298
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1793.06	138852	3	194623	4	-0.86	2.88E + 08	-0.59
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1797.615	110377	3	166006	3	-0.95	2.30E+08	0.335
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1815.064	127929	∠ 5	183024	3 4	-0.95 -0.51	2.20E+08 6.21E+08	-0.352
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1818.818	127929	5	182910	6	-0.33	9.36E+08	-0.16
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1845.526 1878.53	$115550 \\ 107022$	5 4	169735 160255	4 5	-0.77 -0.54	3.30E+08 5.48E+08	$0.645 \\ 0.386$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1883.127	111005	3	164108	4	-0.65	4.25E + 08	-0.482
	1900.093 2094.028	$133265 \\ 134578$	$\frac{3}{4}$	$185894 \\ 182318$	$\frac{4}{5}$	-0.72 -0.76	3.56E+08 2.65E+08	$0.455 \\ 0.517$

a: Energy Levels from [41]

Ag V

Energy Levels

- /				
E_{exp}^{a}	E_{calc}°	ΔE	J	Leading components (in %) in LS Coupling
0	52	-52	4.5	$95.8 \text{ 4d}^7 (^4\text{F}) ^4\text{F}$
3690.5	3720	-29.5	3.5	$98.6 4d^7 (^4\text{F}) ^4\text{F}$
5815.6	5839	-23.4	2.5	96.4 4d ⁷ $({}^{4}F)$ ${}^{4}F$
7097.3	7119	-21.7	1.5	$93.5.4d^7$ (⁴ F) ⁴ F
14204 4	14256	51.6	1.5	$67.7 4d^7 (^4\text{P}) ^4\text{P} \pm 20.1 4d^7 (^2\text{P}) ^2\text{P}$
14204.4	14230	-51.0	1.5	07.740(1)1 + 29.140(1)1
14899.4	14/42	157.4	2.5	90.140° (P) P 10.140° (P) P
16874.7	16822	52.7	4.5	$81.2 \text{ 4d}^{\circ} (^{2}\text{G}) ^{2}\text{G} + 14.8 \text{ 4d}^{\circ} (^{2}\text{H}) ^{2}\text{H}$
17067.2	17013	54.2	0.5	$86.5 \text{ 4d}'_{7}$ (*P) *P + 13 4d' (*P) *P
20442.1	20350	92.1	3.5	96.9 4d' $(^{2}G)^{2}G$
21570.7	21644	-73.3	1.5	$41.9 4d^7 (^2\text{P}) \ ^2\text{P} + 27.7 \ 4d^7 (^4\text{P}) \ ^4\text{P} + 23.1 \ 4d^7 (^2\text{D}) \ ^2\text{D}$
22531.9	22597	-65.1	5.5	99.6 4d ⁷ (² H) ² H
24361.2	24142	219.2	2.5	$74.2 \text{ 4d}^7 (^2\text{D}) ^2\text{D} + 19.5 \text{ 4d}^7 (^2\text{D}) ^2\text{D}$
24599.1	24932	-332.9	0.5	86.6 4d ⁷ (² P) ² P + 13.4d ⁷ (⁴ P) ⁴ P
26267 7	26202	24.2	4.5	$84.7 4d^7 (^{2}\text{H}) ^{2}\text{H} + 14.6 4d^7 (^{2}\text{C}) ^{2}\text{C}$
20301.1	20092	-24.3	4.0	(34.740 (11) 11 + 14.040 (3) 3
30134.4	29990	144.4	1.0	58.940 (D) D + 27.940 (F) F + 0.540 (D) D
34634.7	34635	-0.3	2.5	96.7 4d' (°F) °F
36593.8	36589	4.8	3.5	$97.4 \ 4d' \ (^2F) \ ^2F$
55041.2	55152	-110.8	1.5	$87.7 \text{ 4d}' (^2\text{D}) ^2\text{D} + 11.3 \text{ 4d}' (^2\text{D}) ^2\text{D}$
56771.9	56712	59.9	2.5	$76.2 \text{ 4d}^7 (^2\text{D}) \ ^2\text{D} + 20.5 \text{ 4d}^7 (^2\text{D}) \ ^2\text{D}$
132745	132725	20	4.5	$96.9 \ 4d^6 5s \ (^5D) \ ^6D$
135036.4	135044	-76	3.5	$97.5.4d^{6}5s(^{5}D)^{6}D$
136401	136423	-22	2.5	$96.3 4d^{6}5s$ (⁵ D) ⁶ D
127240.7	127294	24.2	1 5	06 410 E (5D) 6D
107049.7	107064	-34.3	1.5	90 4d 35 (D) D
137913.8	137955	-41.2	0.5	$96 4d^{\circ}5s (^{\circ}D) ^{\circ}D$
146216.3	146173	43.3	3.5	93.8 4d 5s (°D) ⁴ D
148667.4	148684	-16.6	2.5	$92.5 \text{ 4d}^{\circ}5s (^{\circ}D) ^{4}D$
150005.7	150069	-63.3	1.5	92.2 $4d^{\circ}5s$ $(^{\circ}D)$ ^{4}D
150869.3	150959	-89.7	0.5	$93.3 \ 4d^65s \ (^5D) \ ^4D$
156155	156054	101	4.5	$36.5 \ 4d^{6}5s \ (^{3}H)^{4}H + 26.2 \ 4d^{6}5s \ (^{3}G)^{4}G + 20.3 \ 4d^{6}5s \ (^{3}F)^{4}F$
156445 1	156503	-57.9	2.5	56 4d ⁶ 5s (³ P) ⁴ P + 30 8 4d ⁶ 5s (³ P) ⁴ P
156645	156747	102	65	$06 4d^{6} 5a (^{3} \mu) 4\mu$
150045	150747	-102	0.5	5040.55(11)11
156797.8	156827	-29.2	5.5	$75.4 \ 4d^{\circ}5s (^{\circ}H) \ ^{\circ}H + 23.5 \ 4d^{\circ}5s (^{\circ}G) \ ^{\circ}G$
156901.5	156789	112.5	3.5	$51.2 \ 4d^{\circ}5s \ (^{\circ}H) \ ^{\bullet}H + 19.8 \ 4d^{\circ}5s \ (^{\circ}G) \ ^{\bullet}G + 11.4 \ 4d^{\circ}5s \ (^{\circ}F) \ ^{\bullet}F$
159226.1	159228	-1.9	4.5	$32.5 \ 4d^{0}5s \ (^{3}F) \ ^{4}F + 47.5 \ 4d^{0}5s \ (^{3}H) \ ^{4}H + 9.8 \ 4d^{0}5s \ (^{3}F) \ ^{4}F$
159922.5	159873	49.5	2.5	$62.5 \ 4d^{6}5s \ (^{3}F) \ ^{4}F + 19.9 \ 4d^{6}5s \ (^{3}G) \ ^{4}G + 13 \ 4d^{6}5s \ (^{3}F) \ ^{4}F$
160022.6	160022	0.6	3.5	$46.3 \ 4d^{6}5s \ (^{3}F) \ ^{4}F + 30.8 \ 4d^{6}5s \ (^{3}H) \ ^{4}H + 11.9 \ 4d^{6}5s \ (^{3}F) \ ^{4}F$
160124.6	160298	-173.4	1.5	$42.6 \ 4d^{6}5s \ (^{3}F) \ ^{4}F + 19.6 \ 4d^{6}5s \ (^{3}P) \ ^{4}P + 9.4 \ 4d^{6}5s \ (^{3}P) \ ^{4}P$
160703.6	160726	-22.4	1.5	23.8 4d ⁶ 5s (³ P) ⁴ P + 39.8 4d ⁶ 5s (³ F) ⁴ F + 10.4 4d ⁶ 5s (³ P) ⁴ P
161490 5	161478	12.5	5.5	$61.24d^{6}5s(^{3}G)^{4}G + 18.24d^{6}5s(^{3}H)^{2}H + 17.34d^{6}5s(^{3}H)^{4}H$
163052 4	163006	46.4	0.5	$51.0 \ 4d^{6}5e^{-3}(3P) \ 4P \ \pm \ 23.2 \ 4d^{6}5e^{-3}(3P) \ 4P \ \pm \ 0.8 \ 4d^{6}5e^{-1}(1S) \ 2S$
164021.7	164007	94.7	0.5	$51.9 + 41.58 + 17 \pm 25.2 + 41.58 + 17 \pm 5.6 + 41.58 + 5.6 + 41.58 + 5.6 + 41.58 + 5.6 + $
164031.7	164007	24.7	2.5	65.740° S (°G) $^{\circ}$ G + 17.540 $^{\circ}$ S (°F) $^{\circ}$ F + 9.440 $^{\circ}$ S (°F) $^{\circ}$ F
164077.6	164049	28.6	4.5	$71 \text{ 4d}^{\circ}\text{5s} (^{\circ}\text{G}) ^{\circ}\text{G} + 12.6 \text{ 4d}^{\circ}\text{5s} (^{\circ}\text{H}) ^{\circ}\text{H} + 8.5 \text{ 4d}^{\circ}\text{5s} (^{\circ}\text{F}) ^{\circ}\text{F}$
164685.3	164678	7.3	3.5	$60.6 \ 4d^{0}5s \ (^{3}G) \ ^{4}G + 18.4 \ 4d^{0}5s \ (^{3}F) \ ^{4}F + 8.8 \ 4d^{0}5s \ (^{3}H) \ ^{4}H$
165333.7	165403	-69.3	4.5	$67.4 \ 4d^{0}5s \ (^{3}H) \ ^{2}H + 15.3 \ 4d^{0}5s \ (^{3}G) \ ^{2}G + 9.7 \ 4d^{0}5s \ (^{3}F) \ ^{4}F$
165594.7	165717	-122.3	5.5	$69.2 \ 4d^{6}5s \ (^{3}H) \ ^{2}H + 14.8 \ 4d^{6}5s \ (^{3}G) \ ^{4}G + 9.2 \ 4d^{6}5s \ (^{1}I) \ ^{2}I$
166466.5	166347	119.5	3.5	$38.4 \ 4d^{6}5s \ (^{3}F) \ ^{2}F + 12 \ 4d^{6}5s \ (^{3}F) \ ^{2}F + 10.8 \ 4d^{6}5s \ (^{3}G) \ ^{2}G$
167020.6	167206	-185.4	1.5	$37.8 \ 4d^{6}5s \ (^{3}P) \ ^{2}P + 21.2 \ 4d^{6}5s \ (^{3}P) \ ^{4}P + 18 \ 4d^{6}5s \ (^{3}P) \ ^{2}P$
167526.5	167353	173.5	2.5	$82.6 \ 4d^{6}5s \ (^{3}D) \ ^{4}D$
167078.2	167781	107.2	1.5	83.8 $4d^{6}5e^{(3}D) + 5.3 4d^{6}5e^{(3}P) + 2P$
169201.9	169124	197.2	2.5	(35.041.05(D) + 0.041.05(1))
100321.0	108134	101.0	3.5	84.840 ss(D) D + 0.140 ss(F) F
169166.4	169171	-4.6	2.5	$66 4d^{\circ}5s (^{\circ}F) = F + 11 4d^{\circ}5s (^{\circ}F) = F + 9.7 4d^{\circ}5s (^{\circ}G) = G$
170864.7	170877	-12.3	4.5	$75.4 \ 4d^{\circ}5s \ (^{\circ}G) \ ^{2}G + 13.6 \ 4d^{\circ}5s \ (^{\circ}H) \ ^{2}H + 4.4 \ 4d^{\circ}5s \ (^{\circ}G) \ ^{2}G$
171530.2	171632	-101.8	6.5	95.9 4d ⁰ 5s (¹ I) ² I
171713.4	171610	103.4	0.5	$39.5 \ 4d^65s \ (^{3}P) \ ^{2}P + 21.9 \ 4d^65s \ (^{3}P) \ ^{2}P + 15.8 \ 4d^65s \ (^{1}S) \ ^{2}S$
172070.3	172101	-30.7	5.5	$86.7 \ 4d^{6}5s \ (^{1}I) \ ^{2}I + 12.2 \ 4d^{6}5s \ (^{3}H) \ ^{2}H$
172346.3	172296	50.3	3.5	$75.1 \ 4d^{6}5s \ (^{3}G) \ ^{2}G + 8 \ 4d^{6}5s \ (^{1}G) \ ^{2}G + 6.6 \ 4d^{6}5s \ (^{1}G) \ ^{2}G$
175085.4	174729	356.4	4.5	$57.4 \ 4d^{6}5s \ (^{1}G) \ ^{2}G + 17.7 \ 4d^{6}5s \ (^{1}G) \ ^{2}G + 14.8 \ 4d^{6}5s \ (^{3}H) \ ^{2}H$
175241.7	175169	72.7	1.5	$75.8 \ 4d^65s \ (^3D) \ ^2D + 7.5 \ 4d^65s \ (^1D) \ ^2D$
175532.8	175180	352.8	3.5	$50.3 \ 4d^{6}5s \ (^{1}G) \ ^{2}G + 215 \ 4d^{6}5s \ (^{3}F) \ ^{2}F + 14 \ 4d^{6}5s \ (^{1}G) \ ^{2}G$
175691 9	175363	258.8	25	$84.7 \ 4d^{6}5s \ (^{3}D) \ ^{2}D + 5 \ 4d^{6}5s \ (^{1}D) \ ^{2}D$
170040.0	170475	200.0 F00.0	2.0	$61.9.465_{10}(1)(2) + 10.0.46t_{10}(1)(2) + 0.0.46t_{10}(3)(2)$
178940.2	170200	-028.8	∠.0 1 ⁻	01.2 40 38 (D) D + 12.0 40 38 (D) D + 0.8 40 38 (D) D
179242	179623	-381	1.5	$03.4 40^{\circ}$ S (D) D + 13.9 4d $^{\circ}$ S (D) $^{\circ}$ D + 12.9 4d $^{\circ}$ S (D) 2 D
181638.7	181737	-98.3	3.5	$77 4d^{-}$ bs $(^{+}F) = F + 16 4d^{-}$ 5s $(^{+}F) = F$
181871.6	181975	-103.4	2.5	77.3 4d°5s (4 F) 4 F + 13.7 4d°5s (3 F) 4 F
185621.8	185331	290.8	0.5	$65.7 \ 4d^{0}5s \ (^{3}P) \ ^{4}P + 15 \ 4d^{6}5s \ (^{1}S) \ ^{2}S + 13.6 \ 4d^{6}5s \ (^{3}P) \ ^{4}P$
186287.9	186349	-61.1	1.5	$64.3 \ 4d^{6}5s \ (^{3}P) \ ^{4}P + 30.2 \ 4d^{6}5s \ (^{3}P) \ ^{4}P$
188223.5	188196	27.5	4.5	76.9 $4d^{6}5s$ (³ F) ⁴ F + 18.5 $4d^{6}5s$ (³ F) ⁴ F
188493.6	188504	-10.4	1.5	$82.7 \ 4d^{6}5s \ ({}^{3}F) \ {}^{4}F + 13.3 \ 4d^{6}5s \ ({}^{3}F) \ {}^{4}F$
189621-1	189679	-57 9	2.5	$68.2 \ 4d^{6}5s \ ({}^{3}F) \ {}^{4}F + 12.8 \ 4d^{6}5s \ ({}^{1}F) \ {}^{2}F + 11.7 \ 4d^{6}5s \ ({}^{3}F) \ {}^{4}F$
1800/3 0	180050	_15 1	35	$63.3 \ 4d^{6}5s \ (^{3}F) \ ^{4}F \ \pm \ 16.1 \ 4d^{6}5s \ (^{1}F) \ ^{2}F \ \pm \ 12.8 \ 4d^{6}5s \ (^{3}F) \ ^{4}F$
100604 4	100000	1070	0.0 0 =	$58.4 \ 465_{\text{E}} \ (3\text{P}) \ 4\text{P} \pm 39.8 \ 4.65_{\text{E}} \ (3\text{P}) \ 4\text{P}$
190094.4	100082	-101.0	2.0	$30.3 \pm 0.05 (T)$ T $\pm 32.0 \pm 0.07 (T)$ T FOR A16F, (3D) 2D $\pm 1.07 (A16F)$ (1C) 2C $\pm 1.10 (A16F)$ (3D) 2D
196026.9	196024	2.9	3.5	$59.5 \ 4d^{\circ} ss ({}^{\circ} F) = F + 10.7 \ 4d^{\circ} ss ({}^{\circ} G) = G + 11.3 \ 4d^{\circ} ss ({}^{\circ} F) = F$
197022.4	196962	60.4	2.5	78.5 4d $^{\circ}$ 5s ($^{\circ}$ F) $^{\circ}$ F + 13.5 4d $^{\circ}$ 5s ($^{\circ}$ F) $^{\circ}$ F
198032.6	198047	-14.4	1.5	$60.1 \text{ 4d}^{\circ}5s (^{\circ}P) ^{2}P + 33.5 \text{ 4d}^{\circ}5s (^{\circ}P) ^{2}P$
198329.2	198502	-172.8	4.5	$67.8 \ 4d^{6}5s \ (^{1}G) \ ^{2}G + 27.9 \ 4d^{6}5s \ (^{1}G) \ ^{2}G$
199047.5	199081	-33.5	3.5	$52.1 \ 4d^{6}5s \ (^{1}G) \ ^{2}G + 22.4 \ 4d^{6}5s \ (^{1}G) \ ^{2}G + 16.8 \ 4d^{6}5s \ (^{3}F) \ ^{2}F$
215969.7	215921	48.7	2.5	$79.2 \ 4d^{6}5s \ (^{1}D) \ ^{2}D + 19.1 \ 4d^{6}5s \ (^{1}D) \ ^{2}D$
216022 7	215923	99.7	1.5	79.1 4d ⁶ 5s (¹ D) ² D + 19.2 4d ⁶ 5s (¹ D) ² D
210022.1	210020	55.1	a. E.c.	a Van Kleef [30] and Kildivarova [49]
			a: From	h van Kieer [50] and Kindiyarova [42]
				5.1 ms work
			C: U1	ny one component 2 570 are given

Table A36: Comparison between available experimental data and calculated even energy levels (in $\rm cm^{-1})$ in Ag V

Table A37: Comparison between available experimental data and calculated even energy levels (in $\rm cm^{-1})$ in Ag V

exp	-calc		0	Leading components (in 70) in Lo Coupling
203717.6	203736	-18.4	3.5	73.4 4d ⁶ 5p (5 D) 6 D + 10.8 4d ⁶ 5p (5 D) 6 P + 6.3 4d ⁶ 5p (5 D) 6 F
203754.6	203717	37.6	4.5	79.8 $4d^{6}5p$ (^{5}D) $^{6}D + 10.3$ $4d^{6}5p$ (^{5}D) $^{6}F + 6.5$ $4d^{6}5p$ (^{5}D) ^{4}F
205222	205319	-97	2.5	82.4 4d 6 5p (5 D) 6 D + 6 4d 6 5p (5 D) 6 F + 5.6 4d 6 5p (5 D) 6 P
206213	206334	-121	1.5	86.6 $4d^{0}5p (^{5}D) ^{0}D$
206960	207101	-141	0.5	91.6 $4d^{6}5p$ (⁵ D) ⁶ D
211036.8	210841	195.8	3.5	$49.7 \ 4d^{0}5p \ (^{9}D) \ ^{0}F + 19 \ 4d^{0}5p \ (^{9}D) \ ^{4}D + 16.7 \ 4d^{0}5p \ (^{9}D) \ ^{6}P$
211406.6	211285	121.6	2.5	$64.9 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}F + 15.8 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{4}D + 5.4 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{4}F$
211707.2	211631	76.2	1.5	75.3 $4d^{6}5p$ (⁵ D) ${}^{6}F$ + 12.6 $4d^{6}5p$ (⁵ D) ${}^{4}D$
211735.3	211683	52.3	0.5	81.2 $4d^{6}5p$ (⁵ D) ${}^{6}F$ + 11.2 $4d^{6}5p$ (⁵ D) ${}^{4}D$
212362	212197	165	4.5	$52.7 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}F + 25.1 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{4}F + 17.6 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}D$
212913.5	212758	155.5	5.5	96.1 $4d^{0}5p(^{\circ}D)^{\circ}F$
214916	214736	180	3.5	$37.6 \ 4d^{6}5p \ (^{5}D) \ ^{6}P + 24.2 \ 4d^{6}5p \ (^{5}D) \ ^{6}D + 22.3 \ 4d^{6}5p \ (^{5}D) \ ^{6}F$
217207.5	217163	44.5	3.5	$52.8 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{4}D + 30.8 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}P + 6.2 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{4}F$
217509.8	217489	20.8	4.5	$59.7 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{4}F + 34.7 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}F$
217602.8	217494	108.8	2.5	$24.9 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{4}D + 37.8 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{6}P + 13.1 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{6}D$
218960	218934	26	2.5	41.4 $4d^{0}5p(^{\circ}D) P + 37.2 4d^{0}5p(^{\circ}D) ^{4}D + 7.2 4d^{0}5p(^{\circ}D) ^{4}P$
219501	219562	-61	1.5	$60 \ 4d^{6}5p \ (^{5}D) \ ^{4}D + 12.5 \ 4d^{6}5p \ (^{5}D) \ ^{6}F + 10.6 \ 4d^{6}5p \ (^{5}D) \ ^{6}P$
220038.1	220157	-118.9	0.5	$69.5 \ 4d^{6}5p \ (^{5}D) \ ^{4}D + 13.3 \ 4d^{6}5p \ (^{5}D) \ ^{6}F + 5.6 \ 4d^{6}5p \ (^{3}F) \ ^{4}D$
220181	220211	-30	3.5	70.6 $4d^{6}5p (^{5}D) ^{4}F + 17.9 4d^{6}5p (^{5}D) ^{6}F$
220259.6	220050	209.6	1.5	$69.6 \ 4d^{6}5p \ (^{5}D) \ ^{6}P + 9.5 \ 4d^{6}5p \ (^{5}D) \ ^{4}D + 5.8 \ 4d^{6}5p \ (^{3}P) \ ^{4}S$
221491.8	221543	-51.2	2.5	75.7 $4d^{6}5p$ (⁵ D) ${}^{4}F$ + 8.3 $4d^{6}5p$ (⁵ D) ${}^{6}F$
221974.2	222260	-285.8	2.5	$75.7 \ 4d^{6}5p \ (^{5}D) \ ^{4}P + 8.6 \ 4d^{6}5p \ (^{5}D) \ ^{6}P$
222687.9	222713	-25.1	1.5	$83.4 \ 4d^{6}5p \ (^{5}D) \ ^{4}F$
223839.7	223850	-10.3	1.5	58.5 $4d^{6}5p$ (⁵ D) ⁴ P + 11.2 $4d^{6}5p$ (⁵ D) ⁶ P + 5.2 $4d^{6}5p$ (³ P) ⁴ P
224933.7	225169	-235.3	0.5	$87.9 \ 4d^{6}5p \ (^{5}D) \ ^{4}P$
225565.2	225491	74.2	3.5	2.8 4d ⁶ 5p (3 F) 2 F + 15.6 4d ⁶ 5p (3 H) 4 H + 14.2 4d ⁶ 5p (3 H) 2 G
226047.1	225903	144.1	4.5	$3.1 \ 4d^{6}5p \ (^{3}F) \ ^{2}G + 21.7 \ 4d^{6}5p \ (^{3}H) \ ^{4}I + 16.3 \ 4d^{6}5p \ (^{3}G) \ ^{4}H$
226128.1	226457	-328.9	1.5	19.4 $4d^{6}5p$ (³ P) ⁴ P + 24.7 $4d^{6}5p$ (⁵ D) ⁴ P + 21.4 $4d^{6}5p$ (³ P) ⁴ S
226921.4	226990	-68.6	5.5	$2.1 \ 4d^{6}5p \ (^{1}I) \ ^{2}H + 30.4 \ 4d^{6}5p \ (^{3}H) \ ^{4}I + 27.4 \ 4d^{6}5p \ (^{3}H) \ ^{4}H$
227669.1	227709	-39.9	6.5	28 $4d^{6}5p(^{3}H)$ $^{4}H + 38.3 4d^{6}5p(^{3}H)$ $^{4}I + 24.7 4d^{6}5p(^{3}H)$ ^{2}I
227841.1	227850	-8.9	5.5	58 $4d^{6}5p(^{3}H)$ $^{4}G + 11.6 4d^{6}5p(^{3}G)$ $^{4}G + 9.8 4d^{6}5p(^{3}F)$ ^{4}G
228205.9	228325	-119.1	4.5	$14.5 \ 4d^{6}5p \ (^{3}H) \ ^{4}H + 30.6 \ 4d^{6}5p \ (^{3}H) \ ^{4}G + 14.9 \ 4d^{6}5p \ (^{3}H) \ ^{2}G$
228296.2	228331	-34.8	2.5	$16.8 \ 4d^{6}5p \ (^{3}P) \ ^{4}D + 13.3 \ 4d^{6}5p \ (^{3}P) \ ^{2}D + 8.2 \ 4d^{6}5p \ (^{3}P) \ ^{4}P$
228811.9	228864	-52.1	3.5	$35 \ 4d^{6}5p \ (^{3}F) \ ^{4}G + 15.5 \ 4d^{6}5p \ (^{3}H) \ ^{4}G + 9.1 \ 4d^{6}5p \ (^{3}G) \ ^{4}H$
228957 4	229010	-52.6	2.5	$43.1 \ 4d^{6}5p \ (^{3}F) \ ^{4}G + 11.5 \ 4d^{6}5p \ (^{3}H) \ ^{4}G + 8 \ 4d^{6}5p \ (^{3}F) \ ^{4}F$
230133.6	230107	26.6	4.5	$44 \ 1 \ 4d^{6}5p \ (^{3}H) \ ^{4}I + 99 \ 4d^{6}5p \ (^{3}G) \ ^{4}G + 97 \ 4d^{6}5p \ (^{3}F) \ ^{4}F$
230157.0	230147	10.9	2.5	21 4 4d ⁶ 5p (³ F) ${}^{4}F \pm 10.2$ 4d ⁶ 5p (³ D) ${}^{4}F \pm 7.8$ 4d ⁶ 5p (³ F) ${}^{4}D$
220847.0	220147	17.1	2.5	21.4 4d 5p (1) $r + 10.2$ 4d 5p (1) $r + 1.5$ 4d 5p (1) D
220050 4	230803	-17.1	1.5	27.640 5p (11) 11 + 19.440 5p (1) D + 9.840 5p (3) 11 $42.24d^{65}$ (3) 4 E + 22.04d^{65} (3) 4 E + 11.54d^{65} (3) 4 E
230950.4	231012	150.0	1.5	$43.5 4d^{-}5p(^{-}F) = F + 23.9 4d^{-}5p(^{-}D) = F + 11.5 4d^{-}5p(^{-}F) = 18.6 4d^{6}E_{-}(^{3}D) 4D + 17.7 4d^{6}E_{-}(^{3}D) 4D$
232339.2	232310	-150.8	0.5	$18.0 40^{\circ} \text{p} (^{\circ} \text{r}) + 17.7 40^{\circ} \text{p} (^{\circ} \text{r}) + 17.3 40^{\circ} \text{p} (^{\circ} \text{r}) D$
232379.3	232427	-47.7	3.5	$12.2 4 \text{d}^{-5} \text{p} (^{-1} \text{D}) = \text{F} + 25.4 4 \text{d}^{-5} \text{p} (^{-1} \text{H}) = \text{G} + 7.7 4 \text{d}^{-5} \text{p} (^{-3} \text{G}) = \text{F}$
232641.2	232768	-126.8	1.5	19.8 4d $^{\circ}$ 5p ($^{\circ}$ P) $^{\circ}$ S + 17.4 4d $^{\circ}$ 5p ($^{\circ}$ P) $^{\circ}$ D + 13.3 4d $^{\circ}$ 5p ($^{\circ}$ F) $^{\circ}$ D
232648.2	232763	-114.8	4.5	$19.4 \ 4d^{\circ}5p \ (^{\circ}H) \ ^{\circ}G + 19.8 \ 4d^{\circ}5p \ (^{\circ}H) \ ^{\circ}G + 13.2 \ 4d^{\circ}5p \ (^{\circ}H) \ ^{\circ}I$
232966.3	232962	4.3	5.5	$43 4d^{\circ}5p (^{\circ}H) + 1 + 23 4d^{\circ}5p (^{\circ}G) + 9.9 4d^{\circ}5p (^{\circ}H) + H$
233297.3	233320	-22.7	7.5	$94.5 \ 4d^{6}5p \ (^{3}H) \ ^{4}I + 5.3 \ 4d^{6}5p \ (^{1}I) \ ^{2}K + 0.1 \ 4d^{5}5s5f \ (^{4}G) \ ^{4}I$
233624.6	233574	50.6	2.5	$21.2 \text{ 4d}^{\circ}5p (^{\circ}P) ^{4}P + 18 \text{ 4d}^{\circ}5p (^{\circ}P) ^{4}P + 16.7 \text{ 4d}^{\circ}5p (^{\circ}P) ^{2}D$
233689.1	233662	27.1	4.5	12.1 $4d^{0}5p({}^{3}F) {}^{4}F + 19.7 4d^{0}5p({}^{3}H) {}^{4}H + 14.4 4d^{0}5p({}^{3}G) {}^{4}F$
233938.4	233992	-53.6	3.5	$26.6 \ 4d^{0}5p \ ({}^{3}F) \ {}^{4}D + 20.9 \ 4d^{0}5p \ ({}^{3}G) \ {}^{4}H + 12.3 \ 4d^{0}5p \ ({}^{3}D) \ {}^{4}D$
233966.1	234005	-38.9	6.5	$40.6 \ 4d^{6}5p \ (^{3}H) \ ^{2}I + 29.3 \ 4d^{6}5p \ (^{3}H) \ ^{4}H + 24.4 \ 4d^{6}5p \ (^{3}G) \ ^{4}H$
234222.4	234076	146.4	0.5	19.3 $4d^{6}5p(^{1}S)^{2}P + 14 4d^{6}5p(^{3}P)^{4}D + 10.3 4d^{6}5p(^{3}P)^{4}P$
234472.1	234426	46.1	5.5	7.1 $4d^{6}5p$ (³ G) ⁴ G + 27 $4d^{6}5p$ (³ H) ² I + 20 $4d^{6}5p$ (³ G) ² H
234862.8	234952	-89.2	3.5	$45.5 \ 4d^{6}5p \ (^{3}P) \ ^{4}D + 22.7 \ 4d^{6}5p \ (^{3}P) \ ^{4}D + 7.4 \ 4d^{6}5p \ (^{3}F) \ ^{4}F$
234924.5	234878	46.5	2.5	$28.5 \ 4d^{6}5p \ (^{3}F) \ ^{4}D + 14.8 \ 4d^{6}5p \ (^{3}D) \ ^{4}D + 11.1 \ 4d^{6}5p \ (^{3}D) \ ^{4}F$
234990.5	234934	56.5	4.5	29 4d ⁶ 5p (³ G) 4 F + 16.5 4d ⁶ 5p (³ F) 4 F + 11.4 4d ⁶ 5p (³ F) 4 F
235354.3	235474		0 5	50 4d ⁶ 5p (³ H) ⁴ I + 31.6 4d ⁶ 5p (³ H) ⁴ H + 11.5 4d ⁶ 5p (³ H) ² I
235669.8		-119.7	6.5	
235732.5	235662	-119.7 7.8	$\frac{6.5}{2.5}$	$33.3 \ 4d^{\circ}5p \ (^{\circ}G) \ ^{*}G + 14.4 \ 4d^{\circ}5p \ (^{\circ}F) \ ^{*}D + 8 \ 4d^{\circ}5p \ (^{\circ}G) \ ^{2}F$
235881.0	$235662 \\ 235674$	-119.7 7.8 58.5	$\frac{6.5}{2.5}$ 4.5	33.3 4d ⁶ 5p (³ G) ⁴ G + 14.4 4d ⁶ 5p (³ F) ⁴ D + 8 4d ⁶ 5p (³ G) ² F 29.6 4d ⁶ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G
200001.0	$235662 \\ 235674 \\ 235905$	-119.7 7.8 58.5 -23.1		$\begin{array}{l} 33.3 \ 4d^55p \ (^3G) \ ^4G + 14.4 \ 4d^55p \ (^3F) \ ^4D + 8 \ 4d^5p \ (^3G) \ ^4G \\ 29.6 \ 4d^65p \ (^3G) \ ^4G + 15.6 \ 4d^65p \ (^3F) \ ^4G + 11.1 \ 4d^65p \ (^3F) \ ^2G \\ 36.3 \ 4d^65p \ (^3G) \ ^4G + 14.9 \ 4d^65p \ (^3F) \ ^4G + 8.6 \ 4d^65p \ (^3H) \ ^2G \end{array}$
235915	235662 235674 235905 236132	-119.7 7.8 58.5 -23.1 -217	$ \begin{array}{r} 6.5 \\ 2.5 \\ 4.5 \\ 3.5 \\ 5.5 \\ \end{array} $	$\begin{array}{l} 33.3 \ 4d^{6}5p \ (^{3}\mathrm{G}) \ ^{4}\mathrm{G} + 14.4 \ 4d^{6}5p \ (^{3}\mathrm{F}) \ ^{4}\mathrm{D} + 8 \ 4d^{6}5p \ (^{3}\mathrm{G}) \ ^{4}\mathrm{F} \\ 29.6 \ 4d^{6}5p \ (^{3}\mathrm{G}) \ ^{4}\mathrm{G} + 15.6 \ 4d^{6}5p \ (^{3}\mathrm{F}) \ ^{4}\mathrm{G} + 11.1 \ 4d^{6}5p \ (^{3}\mathrm{F}) \ ^{2}\mathrm{G} \\ 36.3 \ 4d^{6}5p \ (^{3}\mathrm{G}) \ ^{4}\mathrm{G} + 14.9 \ 4d^{6}5p \ (^{3}\mathrm{F}) \ ^{4}\mathrm{G} + 8.6 \ 4d^{6}5p \ (^{3}\mathrm{H}) \ ^{2}\mathrm{G} \\ 36.6 \ 4d^{6}5p \ (^{3}\mathrm{H}) \ ^{4}\mathrm{H} + 25.2 \ 4d^{6}5p \ (^{3}\mathrm{G}) \ ^{2}\mathrm{H} + 11.9 \ 4d^{6}5p \ (^{1}\mathrm{I}) \ ^{2}\mathrm{H} \end{array}$
235915 236095.4	$\begin{array}{c} 235662 \\ 235674 \\ 235905 \\ 236132 \\ 236068 \end{array}$	-119.7 7.8 58.5 -23.1 -217 27.4	$ \begin{array}{r} 6.5 \\ 2.5 \\ 4.5 \\ 3.5 \\ 5.5 \\ 1.5 \\ \end{array} $	33.3 4d ^o 5p (³ G) ⁴ G + 14.4 4d ^o 5p (³ F) ⁴ D + 8 4d ^o 5p (³ G) ⁴ F 29.6 4d ⁶ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁶ 5p (³ G) ⁴ G + 14.9 4d ⁶ 5p (³ F) ⁴ G + 8.6 4d ⁶ 5p (³ H) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ G) ² H + 11.9 4d ⁶ 5p (¹) ² H 25.8 4d ⁶ 5p (³ F) ⁴ D + 14.2 4d ⁶ 5p (³ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D
$\begin{array}{c} 235081.3 \\ 235915 \\ 236095.4 \\ 237217.6 \end{array}$	$\begin{array}{c} 235662 \\ 235674 \\ 235905 \\ 236132 \\ 236068 \\ 237183 \end{array}$	-119.7 7.8 58.5 -23.1 -217 27.4 34.6	$ \begin{array}{r} 6.5 \\ 2.5 \\ 4.5 \\ 3.5 \\ 5.5 \\ 1.5 \\ 0.5 \\ \end{array} $	33.3 $4d^{\circ}5p$ (°G) ⁴ G + 14.4 $4d^{\circ}5p$ (°F) ⁴ D + 8 $4d^{\circ}5p$ (°G) ⁴ F 29.6 $4d^{6}5p$ (°G) ⁴ G + 15.6 $4d^{6}5p$ (°F) ⁴ G + 11.1 $4d^{6}5p$ (°F) ² G 36.3 $4d^{6}5p$ (°G) ⁴ G + 14.9 $4d^{6}5p$ (°F) ⁴ G + 8.6 $4d^{6}5p$ (°F) ² G 36.6 $4d^{6}5p$ (°F) ⁴ D + 14.2 $4d^{6}5p$ (°G) ² H + 11.9 $4d^{6}5p$ (°F) ² H 25.8 $4d^{6}5p$ (°F) ⁴ D + 14.2 $4d^{6}5p$ (°D) ⁴ D + 7.5 $4d^{6}5p$ (°F) ⁴ D 25.7 $4d^{6}5p$ (°F) ⁴ D + 13.6 $4d^{6}5p$ (°D) ⁴ D + 11.6 $4d^{6}5p$ (°F) ⁴ D
235081.3 235915 236095.4 237217.6 237351.1	235662 235674 235905 236132 236068 237183 237243	-119.7 7.8 58.5 -23.1 -217 27.4 34.6 108.1	$ \begin{array}{r} 6.5 \\ 2.5 \\ 4.5 \\ 3.5 \\ 5.5 \\ 1.5 \\ 0.5 \\ 3.5 \\ 3.5 \\ \end{array} $	$\begin{array}{l} 33.3 \ 4d^6{}^5p\ (^3{\rm G})\ ^4{\rm G} + 14.4 \ 4d^6{}^5p\ (^3{\rm F})\ ^4{\rm D} + 8\ 4d^6{}^5p\ (^3{\rm G})\ ^4{\rm F} \\ 29.6 \ 4d^6{}^5p\ (^3{\rm G})\ ^4{\rm G} + 15.6 \ 4d^6{}^5p\ (^3{\rm F})\ ^4{\rm G} + 11.1\ 4d^6{}^5p\ (^3{\rm F})\ ^4{\rm G} \\ 36.3 \ 4d^6{}^5p\ (^3{\rm G})\ ^4{\rm G} + 14.9\ 4d^6{}^5p\ (^3{\rm F})\ ^4{\rm G} + 8.6\ 4d^6{}^5p\ (^3{\rm H})\ ^2{\rm G} \\ 36.6 \ 4d^6{}^5p\ (^3{\rm H})\ ^4{\rm H} + 25.2\ 4d^6{}^5p\ (^3{\rm G})\ ^2{\rm H} + 11.9\ 4d^6{}^5p\ (^1{\rm I})\ ^2{\rm H} \\ 25.8\ 4d^6{}^5p\ (^3{\rm F})\ ^4{\rm D} + 14.2\ 4d^6{}^5p\ (^5{\rm D})\ ^4{\rm D} + 7.5\ 4d^6{}^5p\ (^3{\rm P})\ ^4{\rm P} \\ 25.7\ 4d^6{}^5p\ (^3{\rm F})\ ^4{\rm D} + 13.6\ 4d^6{}^5p\ (^5{\rm D})\ ^4{\rm D} + 11.6\ 4d^6{}^5p\ (^3{\rm P})\ ^4{\rm P} \\ 34.6\ 4d^6{}^6p\ (^3{\rm G})\ ^4{\rm F} + 14.4\ 4d^6{}^5p\ (^3{\rm F})\ ^4{\rm F} + 8.4\ 4d^6{}^5p\ (^3{\rm P})\ ^4{\rm P} \end{array}$
$\begin{array}{c} 235361.9\\ 235915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\end{array}$	235662 235674 235905 236132 236068 237183 237243 237745	-119.7 7.8 58.5 -23.1 -217 27.4 34.6 108.1 -79.8	$ \begin{array}{r} 6.5 \\ 2.5 \\ 4.5 \\ 3.5 \\ 5.5 \\ 1.5 \\ 0.5 \\ 3.5 \\ 1.5 \\ 1$	$\begin{array}{l} 33.3 \ 4d^6{}^5p\ (^3{\rm G})\ ^4{\rm G} + 14.4 \ 4d^6{}^5p\ (^3{\rm F})\ ^4{\rm D} + 8\ 4d^9{}^5p\ (^3{\rm G})\ ^4{\rm F} \\ 29.6 \ 4d^6{}^5p\ (^3{\rm G})\ ^4{\rm G} + 15.6 \ 4d^6{}^5p\ (^3{\rm F})\ ^4{\rm G} + 11.1 \ 4d^6{}^5p\ (^3{\rm F})\ ^2{\rm G} \\ 36.3 \ 4d^6{}^5p\ (^3{\rm G})\ ^4{\rm G} + 14.9 \ 4d^6{}^5p\ (^3{\rm F})\ ^4{\rm G} + 8.6 \ 4d^6{}^5p\ (^3{\rm H})\ ^2{\rm G} \\ 36.6 \ 4d^6{}^5p\ (^3{\rm H})\ ^4{\rm H} + 25.2 \ 4d^6{}^5p\ (^3{\rm G})\ ^2{\rm H} + 11.9 \ 4d^6{}^5p\ (^3{\rm F})\ ^4{\rm D} \\ 25.8 \ 4d^6{}^5p\ (^3{\rm F})\ ^4{\rm D} + 14.2 \ 4d^6{}^5p\ (^3{\rm D})\ ^4{\rm D} + 7.5 \ 4d^6{}^5p\ (^3{\rm P})\ ^4{\rm D} \\ 25.7 \ 4d^6{}^5p\ (^3{\rm F})\ ^4{\rm D} + 13.6 \ 4d^6{}^5p\ (^5{\rm D})\ ^4{\rm D} + 11.6 \ 4d^6{}^5p\ (^3{\rm P})\ ^4{\rm D} \\ 34.6 \ 4d^6{}^5p\ (^3{\rm G})\ ^4{\rm F} + 14.4 \ 4d^6{}^5p\ (^3{\rm F})\ ^4{\rm F} + 8.4 \ 4d^6{}^5p\ (^3{\rm F})\ ^4{\rm F} \\ 16.6 \ 4d^6{}^6p\ (^3{\rm D})\ ^4{\rm F} + 23.3 \ 4d^6{}^5p\ (^3{\rm F})\ ^2{\rm D} + 14.7 \ 4d^6{}^5n\ (^3{\rm P})\ ^4{\rm D} \end{array}$
$\begin{array}{c} 235361.9\\ 235915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\end{array}$	235662 235674 235905 236132 236068 237183 237243 237745 237823	-119.7 7.8 58.5 -23.1 -217 27.4 34.6 108.1 -79.8 -65.5	6.5 2.5 4.5 3.5 5.5 1.5 0.5 3.5 1.5 5.5 5.5	$\begin{array}{l} 33.3 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm G}) \ ^{4}{\rm G} + 14.4 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm F}) \ ^{4}{\rm D} + 8 \ 4d^{9}{}^{5}{\rm p} \ (^{3}{\rm G}) \ ^{4}{\rm G} \\ 29.6 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm G}) \ ^{4}{\rm G} + 15.6 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm F}) \ ^{4}{\rm G} + 11.1 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm F}) \ ^{2}{\rm G} \\ 36.3 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm G}) \ ^{4}{\rm G} + 14.9 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm F}) \ ^{4}{\rm G} + 8.6 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm H}) \ ^{2}{\rm G} \\ 36.6 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm H}) \ ^{4}{\rm H} + 25.2 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm G}) \ ^{2}{\rm H} + 11.9 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm H}) \ ^{2}{\rm H} \\ 25.8 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm F}) \ ^{4}{\rm D} + 14.2 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm D}) \ ^{4}{\rm D} + 7.5 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm P}) \ ^{4}{\rm D} \\ 25.7 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm F}) \ ^{4}{\rm D} + 13.6 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm D}) \ ^{4}{\rm D} + 11.6 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm P}) \ ^{4}{\rm D} \\ 34.6 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm G}) \ ^{4}{\rm F} + 14.4 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm F}) \ ^{4}{\rm F} + 8.4 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm P}) \ ^{4}{\rm D} \\ 34.6 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm D}) \ ^{4}{\rm F} + 23.3 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm F}) \ ^{2}{\rm D} + 14.7 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm P}) \ ^{4}{\rm D} \\ 21.5 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm P}) \ ^{4}{\rm G} + 21.8 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm H}) \ ^{2}{\rm I} + 19.9 \ 4d^{6}{}^{5}{\rm p} \ (^{3}{\rm G}) \ ^{4}{\rm G} \\ \end{array}$
$\begin{array}{r} 235361.9\\ 235915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\end{array}$	235662 235674 235905 236132 236068 237183 237243 237745 237823 237715	-119.7 7.8 58.5 -23.1 -217 27.4 34.6 108.1 -79.8 -65.5 149	6.5 2.5 4.5 3.5 5.5 1.5 0.5 3.5 1.5 5.5 2.5	33.3 4d ⁶ 5p (³ G) ⁴ G + 14.4 4d ⁶ 5p (³ F) ⁴ D + 8 4d ⁶ 5p (³ G) ⁴ F 29.6 4d ⁶ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁶ 5p (³ G) ⁴ G + 14.9 4d ⁶ 5p (³ F) ⁴ G + 8.6 4d ⁶ 5p (³ H) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ G) ² H + 11.9 4d ⁶ 5p (¹ I) ² H 25.8 4d ⁶ 5p (³ F) ⁴ D + 14.2 4d ⁶ 5p (³ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 25.7 4d ⁶ 5p (³ F) ⁴ D + 13.6 4d ⁶ 5p (⁵ D) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ D 34.6 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ² F + 8.4 4d ⁶ 5p (³ P) ⁴ F 16.6 4d ⁶ 5p (³ D) ⁴ F + 23.3 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ D 21.5 4d ⁶ 5p (³ F) ⁴ G + 21.8 4d ⁶ 5p (³ H) ² I + 19.9 4d ⁶ 5p (³ G) ⁴ G 24.7 4d ⁶ 5p (³ H) ⁴ G + 14.8 4d ⁶ 5p (³ G) ⁴ F + 12.8 4d ⁶ 5p (³ F) ⁴ F
$\begin{array}{c} 235363.5\\ 235915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\\ 237958.5\end{array}$	235662 235674 235905 236132 236068 237183 237243 237745 237823 237715 238087	-119.7 7.8 58.5 -23.1 -217 27.4 34.6 108.1 -79.8 -65.5 149 -128.5	$ \begin{array}{r} 6.5 \\ 2.5 \\ 4.5 \\ 3.5 \\ 5.5 \\ 1.5 \\ 0.5 \\ 3.5 \\ 1.5 \\ 5.5 \\ 2.5 \\ 4.5 \\ \end{array} $	33.3 4d ⁵ 5p (³ G) ⁴ G + 14.4 4d ⁵ 5p (³ F) ⁴ D + 8 4d ⁵ 5p (³ G) ⁴ F 29.6 4d ⁶ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁶ 5p (³ G) ⁴ G + 14.9 4d ⁶ 5p (³ F) ⁴ G + 8.6 4d ⁶ 5p (³ H) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ G) ² H + 11.9 4d ⁶ 5p (¹ I) ² H 25.8 4d ⁶ 5p (³ F) ⁴ D + 13.2 4d ⁶ 5p (⁵ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 25.7 4d ⁶ 5p (³ F) ⁴ D + 13.6 4d ⁶ 5p (⁵ D) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ F 16.6 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ F 16.6 4d ⁶ 5p (³ G) ⁴ F + 23.3 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ G) ⁴ G 24.7 4d ⁶ 5p (³ H) ⁴ G + 14.8 4d ⁶ 5p (³ G) ⁴ F + 12.8 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ³ G + 4 5.5 4d ⁶ 5p (³ H) ³ G + 4 5.5 4d ⁶ 5p (³ H) ³ G + 4 5.5 4d ⁶ 5p (³ H) ³ G + 4 5.5 4d ⁶ 5p (³ H) ³ G + 4 5.5 4d ⁶ 5p (³ H) ³ G + 4 5.5 4d ⁶ 5p (³ H) ³ G + 4 5.5 4d ⁶ 5p (³ H) ³ G + 5 5.5 4d ⁶ 5p (³ H) ³ G + 5 5.5 4d ⁶ 5p
$\begin{array}{c} 2353631.9\\ 235915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\\ 237958.5\\ 238116.8\end{array}$	235662 235674 235905 236132 236068 237183 237243 237745 237823 237715 238087 238112	$\begin{array}{r} -119.7 \\ 7.8 \\ 58.5 \\ -23.1 \\ -217 \\ 27.4 \\ 34.6 \\ 108.1 \\ -79.8 \\ -65.5 \\ 149 \\ -128.5 \\ 4.8 \end{array}$	b.5 2.5 4.5 3.5 5.5 1.5 0.5 3.5 1.5 2.5 4.5 1.5 2.5 4.5 1.5	$\begin{array}{l} 33.3 \ 4d^6{}{}{}{}{}{}{}{}{}{}{}{}{}{}{}{}{}{}{}$
$\begin{array}{r} 235915\\ 235915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237854\\ 237958.5\\ 238116.8\\ 238944.8 \end{array}$	235662 235674 235905 236132 236068 237183 237243 237745 237823 237715 238087 238112 238935	$\begin{array}{r} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\end{array}$		$\begin{array}{l} 33.3\ 4d^6{}{}{}{}{}{}{}{}{}{}{}{}{}{}{}{}{}{}{}$
$\begin{array}{r} 2353915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\\ 237958.5\\ 238116.8\\ 238944.8\\ 239288.9\end{array}$	235662 235674 235905 236132 236068 237183 237243 237745 237823 237715 238087 238112 238935 239651	$\begin{array}{c} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ -362.1 \end{array}$	b.5 2.5 4.5 3.5 1.5 0.5 3.5 1.5 2.5 4.5 1.5 2.5 4.5 1.5 0.5 3.5 0.5	33.3 4d ⁶ 5p (³ G) ⁴ G + 14.4 4d ⁶ 5p (³ F) ⁴ D + 8 4d ⁹ 5p (³ G) ⁴ F 29.6 4d ⁶ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁶ 5p (³ G) ⁴ G + 14.9 4d ⁶ 5p (³ F) ⁴ G + 8.6 4d ⁶ 5p (³ H) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ G) ² H + 11.9 4d ⁶ 5p (¹ H) ² H 25.7 4d ⁶ 5p (³ F) ⁴ D + 14.2 4d ⁶ 5p (³ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 25.7 4d ⁶ 5p (³ G) ⁴ G + 14.4 4d ⁶ 5p (³ D) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ D 34.6 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ F 16.6 4d ⁶ 5p (³ D) ⁴ F + 23.3 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ F) ⁴ G 21.5 4d ⁶ 5p (³ H) ⁴ G + 21.8 4d ⁶ 5p (³ G) ⁴ F + 12.8 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ⁴ G + 14.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ G 16.9 4d ⁶ 5p (³ G) ⁴ H + 23.4 4d ⁶ 5p (³ H) ² P + 10.9 4d ⁶ 5p (³ F) ⁴ S 21.7 4d ⁶ 5p (³ G) ⁴ H + 23.4 4d ⁶ 5p (³ H) ² P + 12.9 4d ⁶ 5p (³ F) ² F 36.9 4d ⁶ 5p (³ P) ² S + 13.4 4d ⁶ 5p (³ D) ² P + 12.9 4d ⁶ 5p (³ P) ⁴ D
235915 235915 236095.4 237217.6 237351.1 237665.2 237765.5 237864 237958.5 238944.8 239948.8 239948.9 239519.9	235662 235674 235905 236132 236068 237183 237243 237745 237823 237745 238087 238112 238935 239651 239419	$\begin{array}{r} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ -362.1\\ 100.2\end{array}$		33.3 4d ⁶ 5p (³ G) ⁴ G + 14.4 4d ⁶ 5p (³ F) ⁴ D + 8 4d ⁶ 5p (³ G) ⁴ F 29.6 4d ⁶ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁶ 5p (³ G) ⁴ G + 14.9 4d ⁶ 5p (³ F) ⁴ G + 8.6 4d ⁶ 5p (³ H) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ G) ² H + 11.9 4d ⁶ 5p (¹ I) ² H 25.8 4d ⁶ 5p (³ F) ⁴ D + 13.2 4d ⁶ 5p (⁵ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 25.7 4d ⁶ 5p (³ F) ⁴ D + 13.6 4d ⁶ 5p (⁵ D) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ D 34.6 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ D 21.5 4d ⁶ 5p (³ F) ⁴ G + 21.8 4d ⁶ 5p (³ G) ⁴ F + 12.8 4d ⁶ 5p (³ F) ⁴ G 24.7 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 16.9 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ F 16.9 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ D) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ F 32.17 4d ⁶ 5p (³ G) ⁴ H + 23.4 4d ⁶ 5p (³ H) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ F 36.9 4d ⁶ 5p (³ G) ² H + 13.7 4d ⁶ 5p (³ H) ² P + 11.7 4d ⁶ 5p (³ P) ⁴ F 36.9 4d ⁶ 5p (³ D) ⁴ F + 13.4 4d ⁶ 5p (³ G) ² P + 11.9 4d ⁶ 5p (³ P) ⁴ F 36.9 4d ⁶ 5p (³ D) ⁴ F + 13.4 4d ⁶ 5p (³ H) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ F 36.9 4d ⁶ 5p (³ D) ² F + 13.4 4d ⁶ 5p (³ H) ² P + 11.9 4d ⁶ 5p (³ P) ⁴ F 36.9 4d ⁶ 5p (³ D) ⁴ F + 13.4 4d ⁶ 5p (³ H) ² P + 11.9 4d ⁶ 5p (³ P) ⁴ F 36.9 4d ⁶ 5p (³ D) ⁴ F + 13.4 4d ⁶ 5p (³ H) ² P + 11.9 4d ⁶ 5p (³ P) ⁴ F 37.9 4d ⁶ 5p (³ D) ⁴ F + 18.5 4d ⁶ 5p (³ G) ² P + 11.7 4d ⁶ 5p (³ P) ⁴ F 37.9 4d ⁶ 5p (³ D) ⁴ F + 18.5 4d ⁶ 5p (³ G) ⁴ F + 11.7 4d ⁶ 5n (³ P) ⁴ H ⁴ G
235915 236915 236095.4 237217.6 237351.1 237665.2 237757.5 237864 237958.5 238116.8 238944.8 239288.9 239519.2 239754.7	235662 235674 235905 236132 236068 237183 237243 237745 237823 237745 238087 238112 238935 239651 239419 239770	-119.7 7.8 58.5 -23.1 -217 27.4 34.6 108.1 -79.8 -65.5 149 -128.5 4.8 9.8 -362.1 100.2 -15.3	6.5 2.5 4.5 5.5 1.5 0.5 3.5 1.5 2.5 4.5 1.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 3.5 2.5 3.5	33.3 4d ⁶ 5p (³ G) ⁴ G + 14.4 4d ⁶ 5p (³ F) ⁴ D + 8 4d ⁶ 5p (³ G) ⁴ F 29.6 4d ⁶ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁶ 5p (³ G) ⁴ G + 14.9 4d ⁶ 5p (³ F) ⁴ G + 8.6 4d ⁶ 5p (³ H) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 25.7 4d ⁶ 5p (³ F) ⁴ D + 13.2 4d ⁶ 5p (⁵ D) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ D 34.6 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ D 21.5 4d ⁶ 5p (³ G) ⁴ F + 23.3 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ D 21.5 4d ⁶ 5p (³ F) ⁴ G + 21.8 4d ⁶ 5p (³ H) ² I + 19.9 4d ⁶ 5p (³ G) ⁴ G 24.7 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ G) ⁴ H + 23.4 4d ⁶ 5p (³ G) ² H + 10.9 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ G) ⁴ H + 23.4 4d ⁶ 5p (³ H) ² P + 10.9 4d ⁶ 5p (³ F) ⁴ F 321.7 4d ⁶ 5p (³ G) ⁴ H + 23.4 4d ⁶ 5p (³ H) ⁴ H + 9 4d ⁶ 5p (³ F) ² F 36.9 4d ⁶ 5p (³ D) ⁴ F + 18.5 4d ⁶ 5p (³ D) ² P + 12.9 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ D) ⁴ F + 18.5 4d ⁶ 5p (³ H) ⁴ H + 11.7 4d ⁶ 5p (³ P) ⁴ D 23.3 4d ⁶ 5p (³ H) ² I + 18.9 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ P) ⁴ F)
235915 235915 236095.4 237217.6 237351.1 237665.2 237757.5 237864 237958.5 238116.8 238944.8 239288.9 239519.2 239754.7 239856.5	235662 235674 235905 236132 236068 237183 237243 237745 237823 237715 238087 238112 238935 239651 239419 2399770 240014	$\begin{array}{c} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ -362.1\\ 100.2\\ -15.3\\ -15.7\\ 5\end{array}$	6.5 2.5 4.5 3.5 5.5 1.5 0.5 3.5 1.5 2.5 4.5 1.5 0.5 3.5 5.5 2.5 4.5 3.5 5.5 2.5 4.5 3.5 5.5 3.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 5.5 1.5 3.5 1.5 3.5 1.5 3.5 1.5 3.5 1.5 3.5 1.5 3.5 1.5 3.5 1.5 3.5 1.5 3.5 1.5 3.5 1.5 3.5 1.5 3.5 1.5 3.5 1.5 3.5 1.5 3.5 1.5 3.5 5.5	33.3 4d ⁶ 5p (³ G) ⁴ G + 14.4 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 29.6 4d ⁶ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁶ 5p (³ G) ⁴ G + 14.9 4d ⁶ 5p (³ F) ⁴ G + 8.6 4d ⁶ 5p (³ H) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ G) ² H + 11.9 4d ⁶ 5p (¹ I) ² H 25.8 4d ⁶ 5p (³ F) ⁴ D + 14.2 4d ⁶ 5p (³ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 34.6 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ⁴ F + 8.4 4d ⁶ 5p (³ P) ⁴ D 34.6 4d ⁶ 5p (³ G) ⁴ F + 12.3 4d ⁶ 5p (³ F) ² D + 11.6 4d ⁶ 5p (³ P) ⁴ D 21.5 4d ⁶ 5p (³ G) ⁴ F + 23.3 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ D 21.5 4d ⁶ 5p (³ F) ⁴ G + 21.8 4d ⁶ 5p (³ G) ² H + 12.8 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ⁴ G + 14.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ D) ² P + 10.9 4d ⁶ 5p (³ F) ⁴ G 16.9 4d ⁶ 5p (³ B) ⁴ D + 13.7 4d ⁶ 5p (³ D) ² P + 10.9 4d ⁶ 5p (³ F) ² F 36.9 4d ⁶ 5p (³ D) ⁴ F + 18.5 4d ⁶ 5p (³ D) ² P + 12.9 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ D) ⁴ F + 18.5 4d ⁶ 5p (³ D) ² P + 12.9 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ D) ⁴ H + 21 4d ⁶ 5p (³ D) ⁴ H + 13.2 4d ⁶ 5p (³ F) ⁴ G 33 4d ⁶ 5p (³ H) ² I + 18.9 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ F) ⁴ G
235915 235915 236095.4 237217.6 237351.1 237665.2 237757.5 237864 237958.5 238116.8 238944.8 238944.8 239288.9 239519.2 239754.7 239956.5 239997.5	235662 235674 235905 236132 236068 237183 237243 237745 237823 237715 238087 238112 238935 239651 239419 239770 240014 240085	$\begin{array}{c} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ -362.1\\ 100.2\\ -15.3\\ -15.7\\ -87.5\end{array}$		33.3 4d ⁵ 5p (³ G) ⁴ G + 14.4 4d ⁵ 5p (³ F) ⁴ D + 8 4d ⁵ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁶ 5p (³ G) ⁴ G + 14.9 4d ⁶ 5p (³ F) ⁴ G + 8.6 4d ⁶ 5p (³ H) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ G) ² H + 11.9 4d ⁶ 5p (¹ I) ² H 25.7 4d ⁶ 5p (³ F) ⁴ D + 14.2 4d ⁶ 5p (³ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 34.6 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ⁴ F + 8.4 4d ⁶ 5p (³ F) ⁴ F 16.6 4d ⁶ 5p (³ G) ⁴ F + 12.3 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ F) ⁴ P 21.5 4d ⁶ 5p (³ H) ⁴ G + 21.8 4d ⁶ 5p (³ G) ⁴ F + 12.8 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ⁴ G + 14.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ⁴ G + 14.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ G 16.9 4d ⁶ 5p (³ D) ⁴ H + 13.7 4d ⁶ 5p (³ H) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ S 21.7 4d ⁶ 5p (³ D) ⁴ H + 23.4 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 36.9 4d ⁶ 5p (³ D) ⁴ F + 18.5 4d ⁶ 5p (³ G) ² F + 12.9 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ H) ² C + 18.4 4d ⁶ 5p (³ G) ⁴ F + 11.7 4d ⁶ 5p (³ F) ⁴ G 33 4d ⁶ 5p (³ H) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ F) ⁴ G 33 4d ⁶ 5p (³ G) ⁴ H + 21 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ F) ⁴ G 33 4d ⁶ 5p (³ G) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ F) ⁴ G 33 4d ⁶ 5p (³ G) ⁴ H + 21 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ F) ⁴ G 33 4d ⁶ 5p (³ G) ⁴ H + 21 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ F) ⁴ G 34 4d ⁶ 5p (¹ D) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 11.0 2 4d ⁶ 5p (³ F) ⁴ G 34 4d ⁶ 5p (¹ D) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 10 2 4d ⁶ 5p (³ F) ⁴ G 34 4d ⁶ 5p (¹ D) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 10 2 4d ⁶ 5p (³ F) ⁴ G 34 4d ⁶ 5p (¹ D) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 10 2 4d ⁶ 5p (³ F) ⁴ G 34 4d ⁶ 5p (³ G) ⁴ H + 21 4d ⁶ 5p (³ H) ⁴ G + 10 2 4d ⁶ 5p (³ F) ⁴ G 34 4d ⁶ 5p (³ G) ⁴ H + 21 4d ⁶ 5p (³ H) ⁴ G + 10 2 4d ⁶ 5p (³ F) ⁴ G 34 4d ⁶ 5p (³ G) ⁴ H + 21 4d ⁶ 5p (³ H) ⁴ G + 10 2 4d ⁶ 5p (³ F) ⁴ G 34 4d ⁶ 5p (³ G) ⁴ H + 21 4d ⁶
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$\begin{array}{r} 235915\\ 236915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\\ 237958.5\\ 238116.8\\ 239288.9\\ 239519.2\\ 239519.2\\ 239519.2\\ 239519.2\\ 23954.7\\ 239856.5\\ 239997.5\\ 240318.7\\ 240635.4\\ \end{array}$	235662 235674 235905 236132 236068 237183 237243 237745 237823 237715 238087 238112 238935 239651 239419 239770 240014 240085 240387 240387	$\begin{array}{c} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ 9.8\\ 9.362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.7.5\\ -61.3\\ 110.9\\ -87.5\\ -61.3\\ 110.9\\ -233.6\end{array}$		33.3 4d ⁶ 5p (³ G) ⁴ G + 14.4 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 29.6 4d ⁶ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁶ 5p (³ G) ⁴ G + 14.9 4d ⁶ 5p (³ F) ⁴ G + 8.6 4d ⁶ 5p (³ H) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 25.7 4d ⁶ 5p (³ F) ⁴ D + 14.2 4d ⁶ 5p (³ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 34.6 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ⁴ F + 8.4 4d ⁶ 5p (³ P) ⁴ D 24.7 4d ⁶ 5p (³ G) ⁴ F + 12.3 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ D 21.5 4d ⁶ 5p (³ G) ⁴ F + 23.3 4d ⁶ 5p (³ G) ² H + 12.8 4d ⁶ 5p (³ F) ⁴ F 15.6 4d ⁶ 5p (³ G) ⁴ F + 23.3 4d ⁶ 5p (³ G) ² H + 12.8 4d ⁶ 5p (³ F) ⁴ G 24.7 4d ⁶ 5p (³ H) ⁴ G + 21.8 4d ⁶ 5p (³ G) ² H + 12.8 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ G 21.7 4d ⁶ 5p (³ G) ⁴ H + 23.4 4d ⁶ 5p (³ D) ² P + 10.9 4d ⁶ 5p (³ F) ⁴ F 36.9 4d ⁶ 5p (³ D) ⁴ S + 18.5 4d ⁶ 5p (³ H) ² H + 9.4 4d ⁶ 5p (³ F) ⁴ G 23.3 4d ⁶ 5p (³ H) ² G + 18.4 4d ⁶ 5p (³ H) ⁴ G + 11.7 4d ⁶ 5p (³ H) ⁴ G 23.3 4d ⁶ 5p (³ H) ² H + 18.5 4d ⁶ 5p (³ H) ⁴ G + 11.7 4d ⁶ 5p (³ H) ⁴ G 23.3 4d ⁶ 5p (³ H) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 33.4d ⁶ 5p (¹ H) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 33.4d ⁶ 5p (¹ H) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ P) ⁴ D 7.8 4d ⁶ 5p (¹ H) ² F + 12.4 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 34.2 4d ⁶ 5p (³ H) ⁴ G + 12.2 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 34.2 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 34.2 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G
$\begin{array}{r} 235915\\ 236915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\\ 237958.5\\ 238116.8\\ 239288.9\\ 239519.2\\ 239754.7\\ 239856.5\\ 239975.5\\ 240318.7\\ 240427.9\\ 240625.4\\ 240655.4\\ \end{array}$	235662 235674 235905 236132 236068 237183 237243 237745 237823 237715 238087 238112 238935 239651 239419 2399770 240014 240085 240380 240337 240859	$\begin{array}{c} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -33.4\\ 8.3.4\end{array}$		33.3 4d ⁵ 5p (³ G) ⁴ G + 14.4 4d ⁵ 5p (³ F) ⁴ D + 8 4d ⁵ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁵ 5p (³ G) ⁴ G + 14.9 4d ⁵ 5p (³ F) ⁴ G + 8.6 4d ⁶ 5p (³ H) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ G) ² H + 11.9 4d ⁶ 5p (¹ I) ² H 25.7 4d ⁶ 5p (³ F) ⁴ D + 13.2 4d ⁶ 5p (⁵ D) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ F 16.6 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ⁴ F + 8.4 4d ⁶ 5p (³ P) ⁴ F 16.6 4d ⁶ 5p (³ G) ⁴ F + 14.3 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ F 16.6 4d ⁶ 5p (³ G) ⁴ F + 23.3 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ G) ⁴ G 24.7 4d ⁶ 5p (³ H) ⁴ G + 21.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ G 16.9 4d ⁶ 5p (³ P) ⁴ D + 13.7 4d ⁶ 5p (³ D) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ S 21.7 4d ⁶ 5p (³ H) ² C + 25.8 4d ⁶ 5p (³ D) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ S 21.7 4d ⁶ 5p (³ D) ⁴ H + 23.4 4d ⁶ 5p (³ D) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ S 21.7 4d ⁶ 5p (³ D) ² S + 13.4 4d ⁶ 5p (³ D) ² P + 11.7 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ D) ² S + 13.4 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ P) ⁴ G 23.3 4d ⁶ 5p (³ D) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ P) ⁴ G 23.4 4d ⁶ 5p (³ D) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ P) ⁴ G 33 4d ⁶ 5p (³ D) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ P) ⁴ G 33 4d ⁶ 5p (³ D) ⁴ F + 12.4 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ P) ⁴ G 33 4d ⁶ 5p (³ D) ⁴ H + 21 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ P) ⁴ G 33 4d ⁶ 5p (³ D) ⁴ H + 21 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ P) ⁴ G 33 4d ⁶ 5p (³ D) ⁴ H + 12.4 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ P) ⁴ G 33 4d ⁶ 5p (³ D) ⁴ H + 12.4 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ P) ⁴ G 34 4d ⁶ 5p (³ D) ⁴ G + 14.2 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ P) ⁴ G 38.5 4d ⁶ 5p (³ H) ⁴ G + 14.2 4d ⁶ 5p (³ D) ⁴ G + 9.5 4d ⁶ 5p (³ P) ⁴ G 38.5 4d ⁶ 5p (³ H) ⁴ G + 14.2 4d ⁶ 5p (³ D) ⁴ G + 9.5 4d ⁶ 5p (³ P) ⁴ G 38.5 4d ⁶ 5p (³
$\begin{array}{r} 235915\\ 236915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\\ 237958.5\\ 23816.8\\ 238944.8\\ 239928.9\\ 239519.2\\ 239754.7\\ 239856.5\\ 239997.5\\ 240318.7\\ 240425.4\\ 240625.4\\ 240655.4\\ 240657.4\\ \end{array}$	235662 235674 235905 236132 236068 237183 237243 237745 237823 237745 238087 238112 238935 239651 239419 239770 240014 240085 240380 240337 240859 240575	$\begin{array}{c} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ -362.1\\ 100.2\\ -15.3\\ -157.5\\ -87.5\\ -87.5\\ -61.3\\ 110.9\\ -233.6\\ 83.4\\ 98.9\end{array}$		33.3 4d ⁶ 5p (³ G) ⁴ G + 14.4 4d ⁶ 5p (³ F) ⁴ D + 8 4d ⁶ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁶ 5p (³ G) ⁴ G + 14.9 4d ⁶ 5p (³ F) ⁴ G + 8.6 4d ⁶ 5p (³ H) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ G) ² H + 11.9 4d ⁶ 5p (¹ I) ² H 25.7 4d ⁶ 5p (³ F) ⁴ D + 13.2 4d ⁶ 5p (⁵ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 25.7 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ D 34.6 4d ⁶ 5p (³ G) ⁴ F + 13.4 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ D 21.5 4d ⁶ 5p (³ F) ⁴ G + 21.8 4d ⁶ 5p (³ G) ² H + 13.9 4d ⁶ 5p (³ G) ⁴ G 24.7 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ G 16.9 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ² F 36.9 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ D) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ S 21.7 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ² F 36.9 4d ⁶ 5p (³ G) ⁴ H + 23.4 4d ⁶ 5p (³ G) ² P + 12.9 4d ⁶ 5p (³ P) ⁴ D 7.9 4d ⁶ 5p (³ H) ² G + 13.4 4d ⁶ 5p (³ G) ² P + 12.9 4d ⁶ 5p (³ F) ⁴ G 23.3 4d ⁶ 5p (³ H) ² I + 18.9 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ F) ⁴ G 33 4d ⁶ 5p (³ D) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ F) ⁴ G 33 4d ⁶ 5p (³ H) ² K + 12.4 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ P) ⁴ D 7.8 4d ⁶ 5p (³ H) ² K + 12.4 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ D 7.8 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ⁴ G + 14.2 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ D 7.8 4d ⁶ 5p (³ H) ⁴ G + 14.2 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ D 7.8 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ² G 19.6 4d ⁶ 5p (³ H) ⁴ G + 14.2 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ⁴ G + 14.2 4d ⁶ 5p (³ H) ² G + 9.5 4d ⁶ 5p (³ F) ² G 19.6 4d ⁶ 5p (³ H) ⁴ H + 16.7 4d ⁶ 5p (³ H) ² G + 16.7 4d ⁶ 5p (³ G) ⁴ F + 40.7 4d ⁶ 5p (³ G) ⁴ F < 40.7 4d ⁶ 5p (³ G) ⁴ G 19.6 4d ⁶ 5p (³ H) ⁴ H + 16.7
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235915 235915 236095.4 237217.6 237351.1 237665.2 237757.5 237864 237958.5 238116.8 238944.8 239288.9 239519.2 239754.7 239856.5 239997.5 240318.7 240427.9 240625.4 240655.4 240651.8	235662 235674 235905 236132 236068 237183 237243 237745 237823 237715 238087 238112 238935 239651 239419 239770 240014 240085 240037 2400572 240575 240653 240572	$\begin{array}{c} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -362.1\\ 100.2\\ -362.1\\ -362.1\\ 100.2\\ -362.1\\ $	6.5 2.5 4.5 3.5 5.5 1.5 0.5 3.5 1.55 2.5 4.5 1.55 2.5 4.5 2.5 4.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 3.5 2.5 4.5 3.5 3.5 2.5 4.5 3.5 3.5 3.5 4.5 3.5 3.5 3.5 3.5 4.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 5.5 3.5 4.5 3.5 5.5 3.5 4.5 5.5	33.3 4d ⁶ 5p (³ G) ⁴ G + 14.4 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 29.6 4d ⁶ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁶ 5p (³ G) ⁴ G + 14.9 4d ⁶ 5p (³ F) ⁴ G + 8.6 4d ⁶ 5p (³ H) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 25.7 4d ⁶ 5p (³ F) ⁴ D + 14.2 4d ⁶ 5p (³ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 25.7 4d ⁶ 5p (³ F) ⁴ D + 13.6 4d ⁶ 5p (⁵ D) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ D 34.6 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ D 21.5 4d ⁶ 5p (³ G) ⁴ F + 23.3 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ D 21.5 4d ⁶ 5p (³ H) ⁴ G + 21.8 4d ⁶ 5p (³ G) ² H + 12.8 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ⁴ G + 21.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ C) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ G) ⁴ H + 23.4 4d ⁶ 5p (³ D) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ S 21.7 4d ⁶ 5p (³ G) ⁴ H + 23.4 4d ⁶ 5p (³ D) ² P + 12.9 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ D) ² S + 13.4 4d ⁶ 5p (³ D) ² P + 12.9 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ D) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 11.7 4d ⁶ 5p (³ H) ⁴ G 23.3 4d ⁶ 5p (³ D) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ P) ⁴ D 17.8 4d ⁶ 5p (¹ D) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ P) ⁴ D 17.8 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ P) ⁴ D 17.8 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ P) ⁴ D 17.8 4d ⁶ 5p (³ H) ² H + 12.4 4d ⁶ 5p (³ G) ⁴ H + 5.7 4d ⁶ 5p (³ P) ⁴ D 17.4 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ G) ⁴ G + 8 4d ⁶ 5p (³ H) ⁴ G 19.6 4d ⁶ 5p (³ H) ² H + 12.3 4d ⁶ 5p (³ G) ⁴ G + 8 4d ⁶ 5p (³ H) ⁴ H 41.6 4d ⁶ 5p (³ H) ² H + 12.5 4d ⁶ 5p (³ G) ⁴ G + 12.1 4d ⁶ 5p (³ G) ⁴ G 11.7 4d ⁶ 5p (³ G) ⁴ H + 21.3 4d ⁶ 5p (³ G) ⁴ G + 12.1 4d ⁶ 5p (³ G) ⁴ G
$\begin{array}{r} 235915\\ 236915\\ 236915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\\ 237958.5\\ 238116.8\\ 239288.9\\ 239519.2\\ 239754.7\\ 239856.5\\ 239997.5\\ 240318.7\\ 240427.9\\ 240655.4\\ 240655.4\\ 240675.9\\ 240681.8\\ 240975.4\\ 24081.8\\ 240975.4\\ 24081.8$	235662 235662 235674 235905 236132 236068 237183 237243 237745 237823 237745 238087 238112 238935 239651 239651 239419 239770 240014 240085 240380 240337 240859 240575 240603 240575 240603 241069	$\begin{array}{c} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -33.6\\ 9.8\\ -362.1\\ 10.9\\ -233.6\\ 9.9\\ 78.8\\ -110.6\\ -1.4\\ 98.9\\ 78.8\\ -110.6\\ -1.4\\ -1$	$ \begin{array}{r} 6.5 \\ 2.5 \\ 4.5 \\ 3.5 \\ 5.5 \\ 1.5 \\ 0.5 \\ 3.5 \\ 1.5 \\ 2.5 \\ 4.5 \\ 1.5 \\ 2.5 \\ 4.5 \\ 2.5 \\ 4.5 \\ 2.5 \\ 4.5 \\ 3.5 \\ 2.5 \\ 4.5 \\ 3.5 \\ 2.5 \\ 4.5 \\ 3.5 \\ 2.5 \\ 4.5 \\ 3.5 \\ 2.5 \\ 4.5 \\ 3.5 \\ 2.5 \\ 4.5 \\ 3.5 \\ 2.5 \\ 3.5 \\ 4.5 \\ 3.5 \\ 3.5 \\ 4.5 \\ 3.5 \\ 3.5 \\ 4.5 \\ 3.5 \\ 4.5 \\ 3.5 \\ 4.5 \\ 3.5 \\ 3.5 \\ 4.5 \\ 3.5 \\ $	33.3 4d ⁵ 5p (³ G) ⁴ G + 14.4 4d ⁵ 5p (³ F) ⁴ D + 8 4d ⁵ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁶ 5p (³ G) ⁴ G + 14.9 4d ⁶ 5p (³ F) ⁴ G + 8.6 4d ⁶ 5p (³ H) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ D) ⁴ D + 7.5 4d ⁶ 5p (³ H) ⁴ D 25.7 4d ⁶ 5p (³ F) ⁴ D + 13.2 4d ⁶ 5p (⁵ D) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ D 25.7 4d ⁶ 5p (³ F) ⁴ D + 13.6 4d ⁶ 5p (³ D) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ P 16.6 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ D 21.5 4d ⁶ 5p (³ F) ⁴ G + 21.8 4d ⁶ 5p (³ G) ² H + 13.9 4d ⁶ 5p (³ G) ⁴ G 24.7 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² P + 10.9 4d ⁶ 5p (³ F) ⁴ G 16.9 4d ⁶ 5p (³ D) ² F + 13.4 4d ⁶ 5p (³ G) ² P + 11.7 4d ⁶ 5p (³ P) ⁴ D 21.7 4d ⁶ 5p (³ D) ² S + 13.4 4d ⁶ 5p (³ G) ² P + 11.7 4d ⁶ 5p (³ P) ⁴ D 23.3 4d ⁶ 5p (³ H) ² I + 18.9 4d ⁶ 5p (³ G) ⁴ F + 11.7 4d ⁶ 5p (³ F) ⁴ G 33 4d ⁶ 5p (³ G) ⁴ H + 21 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ F) ⁴ G 33 4d ⁶ 5p (³ G) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 34 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ G) ⁴ H + 5.7 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ² G + 9.5 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ G) ⁴ H + 12.5 4d ⁶ 5p (³ H) ² G + 9.5 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ G) ⁴ H + 12.4 4d ⁶ 5p (³ G) ⁴ G + 18.7 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ² G + 9.5 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ² G + 9.5 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ G) ² H + 12.5 4d ⁶ 5p (³ G) ⁴ G + 18.7 4d ⁶ 5p (³ G) ⁴ H 18.6 4d ⁶ 5
$\begin{array}{r} 235915\\ 236915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\\ 237958.5\\ 238116.8\\ 238944.8\\ 239288.9\\ 239519.2\\ 239754.7\\ 239856.5\\ 239997.5\\ 2409754.7\\ 2404625.4\\ 240655.4\\ 240655.4\\ 240655.4\\ 240665.4\\ 24065.4\\ 2$	235662 235662 235674 235905 236132 236068 237183 237745 237745 237823 237745 238087 238112 238935 239651 239419 239770 240014 240085 240380 240337 240859 240572 240575 240603 241086 241008	$\begin{array}{c} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ -362.1\\ 100.2\\ -15.3\\ -157.5\\ -87.5\\ -87.5\\ -61.3\\ 110.9\\ -233.6\\ 83.4\\ 98.9\\ 78.8\\ -110.6\\ -1.1\\ 0 \\ 0 \\ 0 \end{array}$	6.5 2.5 4.5 3.5 5.5 1.5 2.5 1.5 2.5 4.5 1.5 2.5 4.5 3.5 4.5 2.5 4.5 3.5 4.5 2.5 4.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 4.5 5.5 4.5 3.5 4.5 5.5 4.5 3.5 4.5 5.5 4.5 3.5 4.5 5.5 2.5 4.5 5.5 4.5 5.5 4.5 5.5 4.5 5.5 4.5 5.5 2.5 4.5 5.5 2.5 5.5 2.5 5.5 2.5 5.5 2.5 5.5 2.5 5.5 2.5 5.5 2.5 5.5 2.5 5.5 2.5 5.5 2.5 5.5 2.5 5.5 2.5 5.5 2.5 5.5 2.5 5.5 2.5 5.5 2.5 5.5	33.3 4d ⁵ 5p (³ G) ⁴ G + 14.4 4d ⁵ 5p (³ F) ⁴ D + 8 4d ⁵ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁶ 5p (³ G) ⁴ G + 14.9 4d ⁶ 5p (³ F) ⁴ G + 8.6 4d ⁶ 5p (³ H) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ G) ² H + 11.9 4d ⁶ 5p (¹ I) ² H 25.7 4d ⁶ 5p (³ F) ⁴ D + 14.2 4d ⁶ 5p (⁵ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 25.7 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ D 21.5 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ D 21.5 4d ⁶ 5p (³ G) ⁴ F + 23.3 4d ⁶ 5p (³ G) ⁴ F + 12.8 4d ⁶ 5p (³ G) ⁴ G 24.7 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ G) ⁴ G 24.7 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ² F 46 16.9 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ F 16.9 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ D) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ F 21.7 4d ⁶ 5p (³ B) ⁴ H + 23.4 4d ⁶ 5p (³ D) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ S 21.7 4d ⁶ 5p (³ G) ⁴ H + 23.4 4d ⁶ 5p (³ D) ² P + 12.9 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ D) ⁴ F + 18.5 4d ⁶ 5p (³ D) ² P + 12.9 4d ⁶ 5p (³ P) ⁴ D 23.3 4d ⁶ 5p (³ H) ² G + 13.4 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ P) ⁴ D 73.8 4d ⁶ 5p (¹ D) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ P) ⁴ D 73.8 4d ⁶ 5p (³ H) ⁴ G + 12.4 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ P) ⁴ D 73.8 4d ⁶ 5p (³ H) ⁴ G + 12.4 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ P) ⁴ D 73.8 4d ⁶ 5p (³ H) ⁴ G + 12.4 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ P) ⁴ D 73.8 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ P) ⁴ D 73.8 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ F) ² G + 12.3 4d ⁶ 5p (³ H) ² G + 9.5 4d ⁶ 5p (³ F) ² G 19.6 4d ⁶ 5p (³ G) ⁴ H + 12.5 4d ⁶ 5p (³ H) ² G + 9.5 4d ⁶ 5p (³ G) ⁴ G 11.7 4d ⁶ 5p (³ G) ⁴ H + 12.4 4d ⁶ 5p (³ G) ⁴ G + 12.1 4d ⁶ 5p (³ G) ⁴ G 11.7 4d ⁶ 5p (³ G) ⁴ H + 12.3 4d ⁶ 5p (³ H) ² H + 16.7 4d ⁶ 5p (³ H)
235915 235915 236095.4 237217.6 237351.1 237665.2 237757.5 237864 237958.5 238116.8 238944.8 239288.9 239519.2 239754.7 239856.5 239997.5 240318.7 240427.9 240625.4 240655.4 240655.4 240657.4 240673.9 240627.4	235662 235662 235674 235905 236132 236068 237183 237243 237745 237823 237715 238087 238112 238935 239651 239419 239770 240014 240085 240085 240085 2400572 240572 240572 240572 240572 240572 240572	$\begin{array}{c} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ -362.1\\ 100.2\\ -15.3\\ -157.5\\ -87.5\\ -61.3\\ 110.9\\ -233.6\\ 83.4\\ 98.9\\ 78.8\\ -38.4\\ 98.9\\ 78.8\\ -110.6\\ -1.1\\ 39.8\\ -10.6\\ -1.1\\ 39.8\\ -10.6\\ -1.1\\ 39.8\\ -10.6\\ -1.1\\ -1.2\\ -1$	6.5 2.5 4.5 3.5 1.5 0.5 3.5 1.55 2.5 4.5 1.55 2.5 4.5 1.55 2.5 4.5 5.5 2.5 4.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 2.5 3.5 2.5 4.5 2.5 3.5 2.5 4.5 2.5 3.5 4.5 2.5 2.5 3.5 2.5 2.5 3.5 2.5 2.5 2.5 3.5 2.5 2.5 2.5 2.5 3.5 2.5 3.5 2.5 2.5 3.5 2.5 3.5 2.5 3.5	33.3 $4d^5p$ (³ G) ⁴ G + 14.4 $4d^5p$ (³ F) ⁴ D + 8 $4d^5p$ (³ G) ⁴ G + 15.6 $4d^65p$ (³ F) ⁴ G + 11.1 $4d^65p$ (³ F) ² G 36.3 $4d^65p$ (³ G) ⁴ G + 14.9 $4d^65p$ (³ F) ⁴ G + 8.6 $4d^65p$ (³ H) ² G 36.6 $4d^65p$ (³ H) ⁴ H + 25.2 $4d^65p$ (³ D) ⁴ D + 7.5 $4d^65p$ (³ P) ⁴ D 25.7 $4d^65p$ (³ F) ⁴ D + 14.2 $4d^65p$ (³ D) ⁴ D + 7.5 $4d^65p$ (³ P) ⁴ D 25.7 $4d^65p$ (³ F) ⁴ D + 13.6 $4d^65p$ (³ D) ⁴ D + 11.6 $4d^65p$ (³ P) ⁴ D 34.6 $4d^65p$ (³ G) ⁴ F + 14.4 $4d^65p$ (³ F) ² D + 14.7 $4d^65p$ (³ P) ⁴ D 21.5 $4d^65p$ (³ G) ⁴ F + 12.3 $4d^65p$ (³ H) ² I + 19.9 $4d^65p$ (³ P) ⁴ D 21.5 $4d^65p$ (³ H) ⁴ G + 21.8 $4d^65p$ (³ H) ² I + 19.9 $4d^65p$ (³ G) ⁴ G 24.7 $4d^65p$ (³ H) ⁴ G + 21.8 $4d^65p$ (³ G) ² H + 13.1 $4d^65p$ (³ F) ⁴ F 4.5 $4d^65p$ (³ H) ² G + 25.8 $4d^65p$ (³ D) ² P + 10.9 $4d^65p$ (³ F) ⁴ F 4.5 $4d^65p$ (³ G) ⁴ H + 23.4 $4d^65p$ (³ D) ² P + 10.9 $4d^65p$ (³ F) ⁴ F 321.7 $4d^65p$ (³ D) ⁴ F + 18.5 $4d^65p$ (³ D) ² P + 10.9 $4d^65p$ (³ F) ⁴ G 23.3 $4d^65p$ (³ D) ⁴ F + 18.5 $4d^65p$ (³ D) ² P + 12.9 $4d^65p$ (³ F) ⁴ G 33 $4d^65p$ (³ D) ⁴ F + 18.5 $4d^65p$ (³ H) ⁴ G + 11.6 $4d^65p$ (³ P) ⁴ D 17.9 $4d^65p$ (³ D) ⁴ F + 18.5 $4d^65p$ (³ H) ⁴ G + 11.6 $4d^65p$ (³ P) ⁴ D 33 $4d^65p$ (¹ D) ² F + 14.3 $4d^65p$ (³ H) ⁴ G + 11.6 $4d^65p$ (³ P) ⁴ D 34 $4d^65p$ (³ H) ² G + 12.3 $4d^65p$ (³ H) ⁴ G + 10.2 $4d^65p$ (³ P) ⁴ D 34 $4d^65p$ (³ H) ² G + 12.3 $4d^65p$ (³ H) ⁴ G + 10.2 $4d^65p$ (³ P) ⁴ D 34 $4d^65p$ (³ H) ² H + 12.4 $4d^65p$ (³ G) ⁴ F + 9.5 $4d^65p$ (³ P) ⁴ D 38.5 $4d^65p$ (³ H) ² G + 12.3 $4d^65p$ (³ G) ⁴ G + 8.5 $4d^65p$ (³ H) ⁴ H 41.6 $4d^65p$ (³ H) ² H + 12.5 $4d^65p$ (³ G) ⁴ G + 12.1 $4d^65p$ (³ G) ⁴ G 11.7 $4d^65p$ (³ G) ⁴ H + 12.1 $3d^65p$ (³ G) ⁴ G + 12.1 $4d^65p$ (³ D) ⁴ F 38.8 $4d^65p$ (³ G) ⁴ H + 12.3 $4d^65p$ (³ G) ⁴ G + 12.1 $4d^65p$ (³ D) ⁴ F 38.8 $4d^65p$ (³ G) ⁴ H + 12.5 $4d^65p$ (³ G) ⁴ G + 12.1 $4d^65p$ (³ D) ⁴ F 38.8 $4d^65p$ (³ G) ⁴ H + 12.5 $4d^6$
$\begin{array}{r} 2350361.3\\ 235915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\\ 237958.5\\ 238116.8\\ 239288.9\\ 239519.2\\ 239519.2\\ 239519.2\\ 239519.2\\ 239519.2\\ 239519.2\\ 23955.5\\ 240318.7\\ 240625.4\\ 240655.4\\ 240655.4\\ 240655.4\\ 240655.4\\ 240655.4\\ 240655.4\\ 240651.8\\ 240673.9\\ 240681.8\\ 240975.4\\ 240681.8\\ 240975.4\\ 240661.8\\ 241006.9\\ 241149.8\\ 241220.5\\ 241405.5\\ 24165.5\\ 24155.5\\ 24155.5\\ 24155.5\\ 24155.5\\ 24155.$	235662 235662 235674 235905 236132 236068 237183 237243 237745 237823 237715 238087 238112 238935 239651 239419 239770 240014 240085 240037 2400572 240575 240603 240575 240603 240085 240086 241008 241100 241124	$\begin{array}{c} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -38.3\\ 49.9\\ 78.8\\ -10.6\\ 83.4\\ 98.9\\ 78.8\\ -10.6\\ -1.1\\ 39.8\\ -10.5\\ 290.5\\ 200.5\\ 2$	6.5 2.5 4.5 3.5 5.5 1.5 0.5 3.5 1.55 2.5 4.5 1.55 2.5 4.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 3.5 2.5 4.5 3.5 3.5 3.5 4.5 3.5 3.5 3.5 3.5 3.5 4.5 3.5 3.5 4.5 3.5 3.5 4.5 3.5 4.5 3.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 3.5 4.5 3.5 3.5 4.5 3.5 3.5 4.5 3.5 3.5 3.5 4.5 3.5	33.3 $4d^5p$ (³ G) ⁴ G + 14.4 $4d^5p$ (³ F) ⁴ D + 8 $4d^5p$ (³ G) ⁴ F + 29.6 $4d^6p$ (³ G) ⁴ G + 15.6 $4d^6p$ (³ F) ⁴ G + 11.1 $4d^6p$ (³ F) ² G 36.3 $4d^6p$ (³ G) ⁴ G + 14.9 $4d^6p$ (³ G) ² H + 11.9 $4d^6p$ (³ H) ² G 36.6 $4d^6p$ (³ H) ⁴ H + 25.2 $4d^6p$ (³ D) ⁴ D + 7.5 $4d^6p$ (³ P) ⁴ D 25.7 $4d^6p$ (³ F) ⁴ D + 14.2 $4d^6p$ (³ D) ⁴ D + 7.5 $4d^6p$ (³ P) ⁴ D 25.7 $4d^6p$ (³ F) ⁴ D + 14.2 $4d^6p$ (³ D) ⁴ D + 7.5 $4d^6p$ (³ P) ⁴ D 34.6 $4d^6p$ (³ G) ⁴ F + 14.4 $4d^6p$ (³ F) ⁴ D + 11.6 $4d^6p$ (³ P) ⁴ D 34.6 $4d^6p$ (³ G) ⁴ F + 12.3 $4d^6p$ (³ F) ² D + 14.7 $4d^6p$ (³ P) ⁴ D 21.5 $4d^6p$ (³ D) ⁴ F + 23.3 $4d^6p$ (³ G) ² H + 12.8 $4d^6p$ (³ P) ⁴ D 21.5 $4d^6p$ (³ H) ⁴ G + 14.8 $4d^6p$ (³ G) ² H + 12.8 $4d^6p$ (³ F) ⁴ F 4.5 $4d^6p$ (³ H) ⁴ G + 14.8 $4d^6p$ (³ G) ² H + 13.1 $4d^6p$ (³ F) ⁴ F 4.5 $4d^6p$ (³ H) ² G + 25.8 $4d^6p$ (³ D) ² P + 10.9 $4d^6p$ (³ F) ⁴ F 321.7 $4d^6p$ (³ G) ⁴ H + 23.4 $4d^6p$ (³ D) ² P + 12.9 $4d^6p$ (³ F) ⁴ G 23.3 $4d^6p$ (³ D) ⁴ D + 13.7 $4d^6p$ (³ D) ² P + 12.9 $4d^6p$ (³ F) ⁴ G 23.3 $4d^6p$ (³ D) ² F + 18.5 $4d^6p$ (³ D) ² P + 12.9 $4d^6p$ (³ F) ⁴ G 23.3 $4d^6p$ (³ D) ² F + 18.9 $4d^6p$ (³ H) ⁴ G + 10.2 $4d^6p$ (³ F) ⁴ G 33 $4d^6p$ (³ D) ⁴ H + 21.4 $4d^6p$ (³ H) ⁴ G + 10.2 $4d^6p$ (³ F) ⁴ G 33 $4d^6p$ (³ D) ² F + 12.3 $4d^6p$ (³ D) ⁴ F + 9.5 $4d^6p$ (³ F) ⁴ G 13.4 $4d^6p$ (³ D) ⁴ H + 12.4 $4d^6p$ (³ D) ⁴ F + 9.5 $4d^6p$ (³ F) ⁴ G 38.5 $4d^6p$ (³ H) ² G + 12.3 $4d^6p$ (³ G) ⁴ G + 8.4 $4d^6p$ (³ F) ⁴ G 11.7 $4d^6p$ (³ G) ⁴ H + 12.3 $4d^6p$ (³ G) ⁴ G + 12.1 $4d^6p$ (³ F) ⁴ G 11.7 $4d^6p$ (³ G) ⁴ H + 12.3 $4d^6p$ (³ G) ⁴ G + 12.1 $4d^6p$ (³ F) ⁴ F + 10.3 $4d^6p$ (³ F) ⁴ G 11.7 $4d^6p$ (³ F) (² F + 11.8 $4d^6p$ (³ G) (³ G + 12.1 $4d^6p$ (³ G) (³ G + 11.7 $4d^6p$ (³ F) (³ F) ⁴ G 11.7 $4d^6p$ (³ G) ⁴ H + 16.7 $4d^6p$ (³ G) (⁴ G + 12.1 $4d^6p$ (³ G) (³ G + 11.7 $4d^6p$ (³ G) (³ G + 11.7 $4d^6p$ (³ G) (³ G + 11.2 $4d^6p$ (³ G) (³ G + 11.2 $4d^$
$\begin{array}{r} 235915\\ 236915\\ 236915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\\ 237958.5\\ 238116.8\\ 239288.9\\ 239519.2\\ 239754.7\\ 239856.5\\ 239975.4\\ 239856.5\\ 239975.2\\ 240318.7\\ 2404625.4\\ 240665.4\\ 24065.4\\ 24$	235662 235662 235674 235905 236132 236068 237183 237243 237745 237823 237745 238087 238112 238935 239651 239651 239419 239770 240014 240085 240380 240085 240380 240575 240603 241086 241008 241100 241324 241566	$\begin{array}{c} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -362.1\\ 100.2\\ -362.1\\ 39.8\\ -100.6\\ -1.1\\ 39.8\\ -103.5\\ 229.7\\ 229.7\\ 16.0\\ -220.2\\ -20.2$	6.5 2.5 4.5 3.5 1.5 0.5 1.5 2.5 4.5 1.5 2.5 4.5 2.5 2.5 4.5 2.5 2.5 3.5 2.5 2.5 3.5 2.5 2.5 3.5 2.5 3.5 2.5 3.5 2.5 3.5 2.5 3.5 2.5 3.5 2.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 5.5 3.5 3.5 3.5 5.5 3.5 5.5 3.5 5.5 3.5 5.5	33.3 4d ⁵ 5p (³ G) ⁴ G + 14.4 4d ⁵ 5p (³ F) ⁴ D + 8 4d ⁵ 5p (³ G) ⁴ F) ² G 29.6 4d ⁶ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ G) ² H + 11.9 4d ⁶ 5p (¹ H) ² H 25.7 4d ⁶ 5p (³ F) ⁴ D + 13.2 4d ⁶ 5p (⁵ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 25.7 4d ⁶ 5p (³ F) ⁴ D + 13.6 4d ⁶ 5p (⁵ D) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ F 16.6 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ² C + 8.4 4d ⁶ 5p (³ P) ⁴ F 16.6 4d ⁶ 5p (³ G) ⁴ F + 13.4 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ F 16.6 4d ⁶ 5p (³ G) ⁴ F + 23.3 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ G) ⁴ G 24.7 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 16.9 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 16.9 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² P + 10.9 4d ⁶ 5p (³ F) ⁴ G 16.9 4d ⁶ 5p (³ G) ⁴ H + 23.4 4d ⁶ 5p (³ G) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ D) ² S + 13.4 4d ⁶ 5p (³ G) ² P + 12.9 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ D) ² F + 14.3 4d ⁶ 5p (³ G) ² P + 11.7 4d ⁶ 5p (³ P) ⁴ D 7.7 4d ⁶ 5p (³ G) ⁴ H + 21 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ F) ⁴ G 33 4d ⁶ 5p (³ G) ⁴ H + 21 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 38.4 d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ G) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ² G + 9.5 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 16.7 4d ⁶ 5p (³ G) ⁴ F + 9.5 4d ⁶ 5p (³ F) ⁴ G 19.6 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ G) ⁴ G + 12.1 4d ⁶ 5p (³ G) ⁴ G 11.7 4d ⁶ 5p (³ G) ⁴ H + 12.5 4d ⁶ 5p (³ G) ⁴ G + 12.1 4d ⁶ 5p (³ G) ⁴ G 11.7 4d ⁶ 5p (³ G) ⁴ H + 14.5 4d ⁶ 5p (³ G) ⁴ F + 10.3 4d ⁶ 5p (³ F) ⁴ F 54.3 4d ⁶ 5p (³ H) ² G + 17.8 4d ⁶ 5p (³ H) ⁴ H
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235915 235915 236095.4 237217.6 237351.1 237665.2 237757.5 237864 237958.5 238116.8 238944.8 239288.9 239519.2 239754.7 239856.5 239997.5 240318.7 240625.4 240655.4 240655.4 240655.4 240655.4 240657.5 241485.7 241445.7 241549.2 24185.7 241549.2 241934	235662 235662 235674 238905 236132 236068 237183 237243 237745 237823 237745 238087 238112 238935 239651 239419 239770 240014 240085 240085 240085 240085 240575 240603 241086 241008 241100 241324 241256 241566 241807	$\begin{array}{c} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -362.1\\ 10$	$egin{array}{c} 6.5\\ 2.5\\ 4.5\\ 3.5\\ 5.5\\ 1.5\\ 0.5\\ 3.5\\ 1.5\\ 2.5\\ 4.5\\ 1.5\\ 2.5\\ 4.5\\ 2.5\\ 4.5\\ 2.5\\ 6.5\\ 3.5\\ 2.5\\ 6.5\\ 3.5\\ 2.5\\ 6.5\\ 1.5\\ 2.5\\ 3.5\\ 4.5\\ 1.5\\ 2.5\\ 3.5\\ 1.5\\ 2.5\\ 3.5\\ 1.5\\ 2.5\\ 3.5\\ 1.5\\ 2.5\\ 3.5\\ 3.5\\ 1.5\\ 2.5\\ 3.5\\ 3.5\\ 3.5\\ 3.5\\ 3.5\\ 3.5\\ 3.5\\ 3$	33.3 $4d^5p$ (³ G) ⁴ G + 14.4 $4d^5p$ (³ F) ⁴ D + 8 $4d^5p$ (³ G) (³ G) ² G 29.6 $4d^6p$ (³ G) ⁴ G + 14.9 $4d^6p$ (³ F) ⁴ G + 11.1 $4d^6p$ (³ F) ² G 36.3 $4d^6p$ (³ H) ⁴ H + 25.2 $4d^6p$ (³ G) ² H + 11.9 $4d^6p$ (¹ H) ² H 25.8 $4d^6p$ (³ F) ⁴ D + 14.2 $4d^6p$ (³ D) ⁴ D + 7.5 $4d^6p$ (³ P) ⁴ D 25.7 $4d^6p$ (³ F) ⁴ D + 13.6 $4d^6p$ (³ D) ⁴ D + 7.5 $4d^6p$ (³ P) ⁴ D 34.6 $4d^6p$ (³ G) ⁴ F + 14.4 $4d^6p$ (³ F) ⁴ D + 11.6 $4d^6p$ (³ P) ⁴ D 34.6 $4d^6p$ (³ G) ⁴ F + 12.3 $4d^6p$ (³ F) ² D + 14.7 $4d^6p$ (³ P) ⁴ D 21.5 $4d^6p$ (³ F) ⁴ G + 21.8 $4d^6p$ (³ H) ² I + 19.9 $4d^6p$ (³ G) ⁴ G 24.7 $4d^6p$ (³ H) ⁴ G + 14.8 $4d^6p$ (³ G) ² H + 13.1 $4d^6p$ (³ F) ⁴ F 4.5 $4d^6p$ (³ H) ² G + 25.8 $4d^6p$ (³ G) ² H + 13.1 $4d^6p$ (³ F) ⁴ F 4.5 $4d^6p$ (³ H) ² G + 25.8 $4d^6p$ (³ D) ² P + 10.9 $4d^6p$ (³ F) ⁴ S 21.7 $4d^6p$ (³ H) ⁴ G + 13.7 $4d^6p$ (³ D) ² P + 10.9 $4d^6p$ (³ F) ⁴ S 21.7 $4d^6p$ (³ D) ⁴ H + 23.4 $4d^6p$ (³ D) ² P + 10.9 $4d^6p$ (³ F) ⁴ G 33 $4d^6p$ (³ H) ² S + 13.4 $4d^6p$ (³ D) ² P + 12.9 $4d^6p$ (³ F) ⁴ G 33 $4d^6p$ (³ D) ⁴ H + 21.4 $4d^6p$ (³ H) ⁴ H + 19.4 d^6p (³ F) ⁴ G 33 $4d^6p$ (³ G) ⁴ H + 21.4 $4d^6p$ (³ H) ⁴ G + 11.6 $4d^6p$ (³ P) ⁴ D 17.9 $4d^6p$ (³ D) ⁴ F + 18.5 $4d^6p$ (³ H) ⁴ G + 11.6 $4d^6p$ (³ P) ⁴ D 13.8 $4d^6p$ (³ H) ² I + 18.9 $4d^6p$ (³ H) ⁴ G + 10.2 $4d^6p$ (³ P) ⁴ D 34.2 $4d^6p$ (³ H) ² I + 18.9 $4d^6p$ (³ G) ⁴ H + 5.7 $4d^6p$ (³ F) ⁴ G 34.4 d^6p (³ H) ² I + 12.4 $4d^6p$ (³ G) ⁴ G + 19.5 $4d^6p$ (³ G) ³ G ⁴ G 11.7 $4d^6p$ (³ G) ⁴ H + 21.3 $4d^6p$ (³ G) ³ G ⁴ G + 8.8 $4d^6p$ (³ G) ³ G ⁴ G 11.7 $4d^6p$ (³ H) ² H + 12.5 $4d^6p$ (³ G) ³ G ⁴ G + 12.1 $4d^6p$ (³ G) ⁴ G 11.7 $4d^6p$ (³ F) ² F + 21.8 $4d^6p$ (³ G) ³ G ⁴ G + 12.1 $4d^6p$ (³ G) ⁴ G 11.7 $4d^6p$ (³ G) ⁴ H + 12.3 $4d^6p$ (³ G) ³ G ⁴ G + 12.1 $4d^6p$ (³ G) ⁴ G 11.7 $4d^6p$ (³ G) ³ H + 14.16.7 $4d^6p$ (³ G) ³ G ⁴ G + 12.1 $4d^6p$ (³ G) ³ G ⁴ G 11.7 $4d^6p$ (³ G) ³ H + 14.16.7 4
$\begin{array}{r} 2350361.3\\ 235915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\\ 237958.5\\ 238116.8\\ 239288.9\\ 239519.2\\ 239519.2\\ 239519.2\\ 239519.2\\ 239519.2\\ 239519.2\\ 23955.7\\ 240318.7\\ 240625.4\\ 240655.4\\ 240$	235662 235662 235674 235905 236132 236068 237183 237243 237745 237823 237715 238087 238112 238935 239651 239651 239419 239770 240014 240085 240380 240387 240859 240575 240603 241086 241088 241088 241100 241324 2411256 241566 241807 242571 242571	$\begin{array}{c} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ -362.$	6.5 2.5 4.5 3.5 1.5 0.5 3.5 1.5 2.5 4.5 2.5 4.5 2.5 4.5 2.5 4.5 2.5 4.5 2.5 4.5 2.5 4.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 2.5 4.5 3.5 4.5 2.5 4.5 3.5 4.5 2.5 4.5 3.5 4.5 2.5 4.5 2.5 4.5 2.5 4.5 2.5 4.5 2.5 4.5 2.5 3.5 4.5 2.5 3.5 4.5 2.5 3.5 4.5 2.5 3.5 4.5 2.5 3.5 4.5 2.5 3.5 3.5 4.5 3.5 3.5 4.5 3.5 3.5 4.5 3.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 4.5 3.5 5.5 3.5 4.5 3.5 5.5 5.5 3.5 5.5 3.5 5.5	33.3 4d ⁵ 5p (³ G) ⁴ G + 14.4 4d ⁵ 5p (³ F) ⁴ D + 8 4d ⁵ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.3 4d ⁶ 5p (³ G) ⁴ G + 14.9 4d ⁶ 5p (³ F) ⁴ G + 8.6 4d ⁶ 5p (³ H) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 25.7 4d ⁶ 5p (³ F) ⁴ D + 13.2 4d ⁶ 5p (⁵ D) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ F 16.6 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ F 16.6 4d ⁶ 5p (³ G) ⁴ F + 13.4 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ F 16.6 4d ⁶ 5p (³ G) ⁴ F + 23.3 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ G) ⁴ G 24.7 4d ⁶ 5p (³ H) ⁴ G + 21.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ G 16.9 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ G 16.9 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ D) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ H) ² G + 13.4 4d ⁶ 5p (³ D) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ D) ⁴ F + 18.5 4d ⁶ 5p (³ D) ² P + 12.9 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ D) ² F + 14.3 4d ⁶ 5p (³ D) ² P + 11.7 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ D) ² F + 14.3 4d ⁶ 5p (³ D) ⁴ F + 11.7 4d ⁶ 5p (³ P) ⁴ D 17.8 4d ⁶ 5p (³ H) ² L + 18.9 4d ⁶ 5p (³ D) ⁴ F + 9.5 4d ⁶ 5p (³ P) ⁴ D 17.8 4d ⁶ 5p (³ H) ² H + 12.4 4d ⁶ 5p (³ D) ⁴ F + 9.5 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² H + 12.4 4d ⁶ 5p (³ D) ⁴ F + 9.5 4d ⁶ 5p (³ F) ⁴ G 18.5 4d ⁶ 5p (³ H) ² H + 12.5 4d ⁶ 5p (³ D) ⁴ F + 9.5 4d ⁶ 5p (³ F) ⁴ G 19.6 4d ⁶ 5p (³ H) ² H + 12.5 4d ⁶ 5p (³ D) ⁴ D + 15.3 4d ⁶ 5p (³ F) ⁴ G 19.6 4d ⁶ 5p (³ H) ² H + 12.5 4d ⁶ 5p (³ D) ⁴ D + 15.3 4d ⁶ 5p (³) ⁴ G 17.7 4d ⁶ 5p (³ D) ² F + 12.3 4d ⁶ 5p (³ D) ⁴ D + 15.3 4d ⁶ 5p (³ D) ⁴ F 19.4 4d ⁶ 5p (³ H) ² H + 12.5 4d ⁶ 5p (³ D) ⁴ D + 15.3 4d ⁶ 5p (³ D) ⁴ F 19.4 4d ⁶ 5p (³ H) ² H + 12.5 4d ⁶ 5p (³ D) ⁴ D + 15.3 4d ⁶ 5p (³ D) ⁴ F 19.4 4d ⁶ 5p (³ H) ² H + 12.5 4d ⁶ 5p (³ D) ⁴ D + 15.3 4d ⁶ 5p (³ D) ⁴ F 19.4 4d ⁶ 5p (³ H) ² H + 12.5 4d ⁶ 5p (³ D) ⁴ D + 15.3 4d ⁶ 5p (³ D) ⁴ D 1
$\begin{array}{r} 235915\\ 236915\\ 236995\\ 236915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\\ 237958.5\\ 23816.8\\ 238944.8\\ 239928.9\\ 239519.2\\ 239754.7\\ 239856.5\\ 239997.5\\ 240318.7\\ 24047.9\\ 240655.4\\ 240655.4\\ 240655.4\\ 240655.4\\ 240655.4\\ 240655.4\\ 240655.4\\ 240655.4\\ 241066.9\\ 241149.8\\ 241220.5\\ 241485.7\\ 241549.2\\ 241934\\ 242472.5\\ 242570.4\\ 241934\\ 242472.5\\ 242570.4\\ 24106.9\\ 2411934\\ 242472.5\\ 242570.4\\ 24106.9\\ 2411934\\ 242472.5\\ 242570.4\\ 24106.9\\ 2411934\\ 242472.5\\ 242570.4\\ 24106.9\\ 2411934\\ 242472.5\\ 242570.4\\ 24106.9\\ 2411934\\ 242472.5\\ 242570.4\\ 24106.9\\ 2411934\\ 242472.5\\ 242570.4\\ 24106.9\\ 2411934\\ 242472.5\\ 242570.4\\ 24106.9\\ 2411934\\ 242472.5\\ 242570.4\\ 24106.9\\ 2411934\\ 242472.5\\ 242570.4\\ 24106.9\\ 2411934\\ 242472.5\\ 242570.4\\ 24106.9\\ 241106.9\\ 241149.8\\ 242472.5\\ 2422570.4\\ 24106.9\\ 241149.8\\ 242472.5\\ 2422570.4\\ 24106.9\\ 241149.8\\ 242472.5\\ 2422570.4\\ 24106.9\\ 241149.8\\ 242472.5\\ 2422570.4\\ 24106.9\\ 241149.8\\ 242472.5\\ 2422570.4\\ 24106.9\\ 241149.8\\ 242472.5\\ 2422570.4\\ 24106.9\\ 241149.8\\ 242472.5\\ 2422570.4\\ 24106.9\\ 241149.8\\ 242472.5\\ 2422570.4\\ 241106.9\\ 241149.8\\ 242472.5\\ 2422570.4\\ 241106.9\\ 241149.8\\ 242472.5\\ 2422570.4\\ 241106.9\\ 241149.8\\ 242472.5\\ 2422570.4\\ 241106.9\\ 241149.8\\ 242472.5\\ 2422570.4\\ 241106.9\\ 241149.8\\ 242472.5\\ 2424570.4\\ 241106.9\\ 241149.8\\ 242472.5\\ 2424570.4\\ 242472.5\\ 242570.4\\ 242472.5\\ 242570.4\\ 242472.5\\ 242570.4\\ 242472.5\\ 242570.4\\ 242472.5\\ 242570.4\\ 242472.5\\ 242470.5\\ 24270.5\\ 24270.5\\ 24270.5\\ 24$	235662 235662 235674 235905 236132 236068 237183 237745 237823 237745 237823 237715 238087 238112 238935 239651 239651 239419 239770 240014 240085 240380 240337 240859 240575 240603 241086 241008 241008 241008 241008 24102575 240603 241086 241100 241324 241256 241566 241807 242571 242607	$\begin{array}{r} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ -362.1\\ 100.2\\ -15.3\\ -157.5\\ -87.5\\ -61.3\\ 110.9\\ -233.6\\ 83.4\\ 98.9\\ 78.8\\ -110.6\\ -1.1\\ 39.8\\ -103.5\\ 229.7\\ -16.8\\ -103.5\\ 229.7\\ -16.8\\ -36.6\\ -36.$	$egin{array}{c} 6.5\\ 2.5\\ 3.5\\ 5.5\\ 1.5\\ 0.5\\ 3.5\\ 1.5\\ 5.5\\ 2.5\\ 4.5\\ 1.5\\ 2.5\\ 4.5\\ 2.5\\ 4.5\\ 2.5\\ 4.5\\ 2.5\\ 3.5\\ 2.5\\ 6.5\\ 1.5\\ 2.5\\ 3.5\\ 2.5\\ 1.5\\ 2.5\\ 3.5\\ 1.5\\ 2.5\\ 1.5\\ 1.5\\ 2.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1$	33.3 $4d^5p$ (°G) ⁴ G + 14.4 $4d^5p$ (°F) ⁴ D + 8 $4d^5p$ (°G) ⁷ F) ² G 29.6 $4d^65p$ (3G) ⁴ G + 15.6 $4d^65p$ (3F) ⁴ G + 11.1 $4d^65p$ (3F) ² G 36.3 $4d^5p$ (3G) ⁴ G + 14.9 $4d^5p$ (3F) ⁴ G + 8.6 $4d^65p$ (3H) ² G 36.6 $4d^65p$ (3H) ⁴ H + 25.2 $4d^65p$ (3D) ⁴ D + 7.5 $4d^65p$ (3P) ⁴ D 25.7 $4d^65p$ (3F) ⁴ D + 13.2 $4d^65p$ (3D) ⁴ D + 7.5 $4d^65p$ (3P) ⁴ D 25.7 $4d^65p$ (3G) ⁴ F + 14.4 $4d^65p$ (3F) ⁴ D + 11.6 $4d^65p$ (3P) ⁴ D 24.6 $4d^65p$ (3G) ⁴ F + 14.4 $4d^65p$ (3F) ² D + 14.7 $4d^65p$ (3P) ⁴ D 21.5 $4d^65p$ (3F) ⁴ G + 21.8 $4d^65p$ (3H) ² I + 19.9 $4d^65p$ (3G) ⁴ G 24.7 $4d^65p$ (3H) ⁴ G + 12.8 $4d^65p$ (3G) ⁴ F + 12.8 $4d^65p$ (3F) ⁴ G 15.9 $4d^65p$ (3H) ² G + 25.8 $4d^65p$ (3G) ² H + 13.1 $4d^65p$ (3F) ⁴ F 16.9 $4d^65p$ (3H) ² G + 25.8 $4d^65p$ (3D) ² P + 10.9 $4d^65p$ (3F) ⁴ G 16.9 $4d^65p$ (3D) ⁴ H + 23.4 $4d^65p$ (3D) ² P + 10.9 $4d^65p$ (3P) ⁴ S 21.7 $4d^65p$ (3D) ⁴ H + 23.4 $4d^65p$ (3D) ² P + 12.9 $4d^65p$ (3P) ⁴ D 17.9 $4d^65p$ (3D) ⁴ F + 18.5 $4d^65p$ (3D) ² P + 12.9 $4d^65p$ (3F) ⁴ G 23.3 $4d^65p$ (3D) ⁴ F + 18.5 $4d^65p$ (3H) ⁴ G + 11.6 $4d^65p$ (3F) ⁴ G 23.3 $4d^65p$ (3G) ⁴ H + 21.4 $4d^65p$ (3H) ⁴ G + 10.2 $4d^65p$ (3F) ⁴ G 33 $4d^65p$ (3G) ⁴ H + 21.4 $4d^65p$ (3H) ⁴ G + 10.2 $4d^65p$ (3F) ⁴ G 38.5 $4d^65p$ (3H) ² G + 12.3 $4d^65p$ (3D) ⁴ F + 9.5 $4d^65p$ (3F) ⁴ G 38.5 $4d^65p$ (3H) ² G + 12.3 $4d^65p$ (3D) ⁴ F + 9.5 $4d^65p$ (3F) ⁴ G 38.5 $4d^65p$ (3H) ² H + 12.5 $4d^65p$ (3D) ⁴ F + 9.5 $4d^65p$ (3F) ⁴ G 38.5 $4d^65p$ (3D) ⁴ H + 21.3 $4d^65p$ (3H) ⁴ G + 10.3 $4d^65p$ (3F) ⁴ G 11.7 $4d^65p$ (3G) ⁴ H + 21.3 $4d^65p$ (3H) ⁴ G + 12.1 $4d^65p$ (3F) ⁴ G 38.5 $4d^65p$ (3H) ² H + 12.5 $4d^65p$ (3H) ⁴ G + 12.1 $4d^65p$ (3F) ⁴ G 11.7 $4d^65p$ (3G) ⁴ H + 12.5 $4d^65p$ (3H) ² I + 8.5 $4d^65p$ (3H) ⁴ H 16.6 $4d^65p$ (3D) ⁴ P + 14.5 $4d^65p$ (3H) ⁴ F + 10.3 $4d^65p$ (3H) ⁴ H 17.8 $4d^65p$ (3D) ⁴ P + 14.5 $4d^65p$ (3H) ⁴ F + 10.3 $4d^65p$ (3F) ⁴ D 19.4 $4d^65p$ (3D) ⁴ P + 14.5 $4d^65p$ (3H) ⁴ G + 14.4 d^65p (3G) ⁴ G 17.5
$\begin{array}{r} 235915\\ 236915\\ 236915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\\ 237757.5\\ 237864\\ 239285.9\\ 239519.2\\ 239754.7\\ 239856.5\\ 239997.5\\ 240975.4\\ 240655.4\\ 240655.4\\ 240655.4\\ 240655.4\\ 240655.4\\ 240665.4\\ 240665.4\\ 240665.4\\ 240665.4\\ 240665.4\\ 240665.4\\ 240665.4\\ 240665.4\\ 240665.4\\ 240655.4\\ 240655.4\\ 24120.5\\ 241485.7\\ 241549.2\\ 241934\\ 242472.5\\ 241934\\ 242472.5\\ 242570.4\\ 243101.5\\ 24151.5\\ 242570.4\\ 243101.5\\ 24151.5\\ 24151.5\\ 24151.5\\ 242570.4\\ 243101.5\\ 24151.5\\ 2$	235662 235662 235674 235905 236132 236068 237183 237243 237745 237823 237745 238087 238112 238935 239651 239419 239770 240014 240085 240085 240085 2400575 240603 241086 241008 241110 241324 241256 241566 241566 241807 242571 242607 242571	$\begin{array}{r} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ -362.1\\ 100.2\\ -15.3\\ -157.5\\ -87.5\\ -61.3\\ 110.9\\ -233.6\\ 83.4\\ -98.9\\ -233.6\\ 83.4\\ -98.9\\ -10.6\\ -1.1\\ 39.8\\ -110.6\\ -1.1\\ 39.8\\ -103.5\\ 229.7\\ -16.8\\ 127\\ -98.5\\ -36.6\\ 182.5\\ -36.6\\ 182.5\\ -36.6\\ -182.5\\ -36.6\\ $	$egin{array}{c} 6.5\\ 2.5\\ 3.5\\ 5.5\\ 1.5\\ 5.5\\ 1.5\\ 2.5\\ 4.5\\ 1.5\\ 5.5\\ 2.5\\ 4.5\\ 2.5\\ 4.5\\ 2.5\\ 2.5\\ 3.5\\ 2.5\\ 2.5\\ 3.5\\ 2.5\\ 3.5\\ 2.5\\ 3.5\\ 2.5\\ 3.5\\ 2.5\\ 3.5\\ 1.5\\ 2.5\\ 3.5\\ 1.5\\ 2.5\\ 3.5\\ 1.5\\ 3.5\\ 1.5\\ 3.5\\ 3.5\\ 3.5\\ 3.5\\ 3.5\\ 3.5\\ 3.5\\ 3$	33.3 $4d^5p$ (°G) ⁴ G + 14.4 $4d^5p$ (°F) ⁴ D + 8 $4d^5p$ (°G) ⁴ F) ² G 29.6 $4d^6p$ (°G) ⁴ G + 15.6 $4d^6p$ (°F) ⁴ G + 11.1 $4d^6p$ (°F) ² G 36.3 $4d^5p$ (°G) ⁴ G + 14.9 $4d^5p$ (°F) ⁴ G + 8.6 $4d^6p$ (°F) ⁴ F) ² G 36.6 $4d^6p$ (°F) ⁴ D + 14.2 $4d^6p$ (°F) ⁴ D + 7.5 $4d^6p$ (°F) ⁴ D 25.7 $4d^6p$ (°F) ⁴ D + 13.2 $4d^6p$ (°F) ⁴ D + 11.6 $4d^6p$ (°F) ⁴ P 25.7 $4d^6p$ (°F) ⁴ D + 13.2 $4d^6p$ (°F) ⁴ D + 11.6 $4d^6p$ (°F) ⁴ P 34.6 $4d^6p$ (°F) (°F) ⁴ F + 13.4 $4d^6p$ (°F) ⁴ D + 11.6 $4d^6p$ (°F) ⁴ F 16.6 $4d^6p$ (°F) ³ D ⁴ F + 23.3 $4d^6p$ (°F) ² D + 14.7 $4d^6p$ (°F) ⁴ P 21.5 $4d^6p$ (°F) ³ F) ⁴ G + 21.8 $4d^6p$ (°F) ² D + 14.7 $4d^6p$ (°F) ³ F) ⁴ G 24.7 $4d^6p$ (°F) ³ H) ² G + 25.8 $4d^6p$ (°G) ² H + 13.1 $4d^6p$ (°F) (°F) ⁴ F 16.9 $4d^6p$ (°F) ³ D) ⁴ F + 13.7 $4d^6p$ (°G) ² H + 13.1 $4d^6p$ (°F) (°F) ⁴ F 16.9 $4d^6p$ (°F) ³ D) ⁴ F + 13.7 $4d^6p$ (°G) ² P + 10.9 $4d^6p$ (°F) ³ P) ⁴ D 17.9 $4d^6p$ (°G) ⁴ H + 23.4 $4d^6p$ (°G) ² P + 12.9 $4d^6p$ (°F) ⁴ F) ⁴ G 23.3 $4d^6p$ (°G) ⁴ H + 21.4 $4d^6p$ (°G) ⁴ H + 11.7 $4d^6p$ (°F) ³ F) ⁴ G 33 $4d^6p$ (°G) ⁴ H + 21.4 $4d^6p$ (°G) ⁴ H + 11.7 $4d^6p$ (°F) ³ P) ⁴ D 17.9 $4d^6p$ (°G) ⁴ H + 21.4 $4d^6p$ (°G) ⁴ H + 10.2 $4d^6p$ (°F) ⁴ P) ⁴ D 17.9 $4d^6p$ (°G) ⁴ H + 21.4 $4d^6p$ (°G) ⁴ H + 5.7 $4d^6p$ (°F) ⁴ F) ⁴ G 33 $4d^6p$ (°G) ⁴ H + 21.4 $4d^6p$ (°G) ⁴ H + 5.7 $4d^6p$ (°F) ⁴ P) ² G 7.7 $4d^6p$ (°G) ⁴ H + 12.4 $4d^6p$ (°G) ⁴ H + 5.7 $4d^6p$ (°F) ⁴ P) ² G 3.8 $4d^6p$ (°G) ⁴ H + 12.4 $4d^6p$ (°G) ⁴ H + 16.7 $4d^6p$ (°G) ⁴ G + 12.4 $4d^6p$ (°F) ⁴ F) ⁴ G 38.5 $4d^6p$ (°G) ⁴ H + 12.4 $4d^6p$ (°G) ³ H) ⁴ G + 10.2 $4d^6p$ (°G) ⁴ H + 16.7 $4d^6p$ (°G) ⁴ F) ⁴ F 3.8 $4d^6p$ (°G) ⁴ H + 12.4 $4d^6p$ (°G) ⁴ G + 12.4 $4d^6p$ (°G) ⁴ H + 16.7 $4d^6p$ (°G) ³ F) ² G 19.6 $4d^6p$ (°G) ⁴ H + 12.4 $4d^6p$ (°G) ⁴ G + 12.4 $4d^6p$ (°G) ⁴ H + 16.7 $4d^6p$ (°G) ⁴ G + 12.4 $4d^6p$ (°G) ⁴ G + 12.4 $4d^6p$ (°G) ⁴ H + 16.7 $4d^6p$ (°G) ⁴ F) ⁴ F 3.8 $4d^6p$ (°G) ⁴ H + 12.8 $4d^6p$ (°G) ⁴ G + 12.4 $4d^6p$ (°G)
$\begin{array}{r} 2350315\\ 236915\\ 236915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\\ 237958.5\\ 238116.8\\ 238944.8\\ 239288.9\\ 239519.2\\ 239754.7\\ 239856.5\\ 239997.5\\ 240318.7\\ 240625.4\\ 240655.4\\ 240655.4\\ 240655.4\\ 240655.4\\ 240657.4\\ 240657.4\\ 241066.9\\ 241149.8\\ 241220.5\\ 241485.7\\ 241549.2\\ 241934\\ 242472.5\\ 241934\\ 242472.5\\ 242570.4\\ 243101.5\\ 243373.6\\ \end{array}$	235662 235662 235674 235905 236132 236068 237183 237243 237745 237823 237745 238087 238112 238935 239651 239419 239770 240014 240085 2400575 2406572 240575 240603 241086 241008 241100 241324 241256 241566 241807 242571 242572 242575 24192 241575 24192 242571 245	$\begin{array}{r} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -38.4\\ 9.8\\ -362.1\\ 100.2\\ -15.3\\ -366.8\\ -1.1\\ 39.8\\ -100.6\\ 83.4\\ 98.9\\ 78.8\\ -101.6\\ 83.4\\ 98.9\\ 78.8\\ -103.5\\ 229.7\\ -16.8\\ 127\\ -98.5\\ -366.6\\ 182.5\\ -366.4\\ 127\\ -98.5\\ -366.6\\ 182.5\\ -66.4\\ \end{array}$	$egin{array}{c} 6.5\\ 2.5\\ 3.5\\ 5.5\\ 3.5\\ 1.5\\ 0.5\\ 3.5\\ 1.5\\ 5.5\\ 2.5\\ 4.5\\ 1.5\\ 2.5\\ 4.5\\ 2.5\\ 4.5\\ 2.5\\ 6.5\\ 3.5\\ 4.5\\ 2.5\\ 6.5\\ 3.5\\ 4.5\\ 2.5\\ 3.5\\ 4.5\\ 2.5\\ 3.5\\ 1.5\\ 2.5\\ 1.5\\ 1.5\\ 2.5\\ 1.5\\ 1.5\\ 2.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1$	33.3 $4d^5p$ (³ G) ⁴ G + 14.4 $4d^5p$ (³ F) ⁴ D + 8 $4d^5p$ (³ G) ⁴ G + 12.4 $4d^5p$ (³ F) ² G 36.3 $4d^5p$ (³ G) ⁴ G + 14.9 $4d^5p$ (³ F) ⁴ G + 8.6 $4d^6p$ (³ F) ² G 36.6 $4d^6p$ (³ H) ⁴ H + 25.2 $4d^6p$ (³ D) ⁴ D + 7.5 $4d^6p$ (³ P) ⁴ D 25.7 $4d^6p$ (³ F) ⁴ D + 14.2 $4d^6p$ (³ D) ⁴ D + 7.5 $4d^6p$ (³ P) ⁴ D 34.6 $4d^6p$ (³ G) ⁴ F + 14.4 $4d^6p$ (³ D) ⁴ D + 11.6 $4d^6p$ (³ P) ⁴ D 24.6 $4d^6p$ (³ G) ⁴ F + 14.4 $4d^6p$ (³ F) ² D + 14.7 $4d^6p$ (³ P) ⁴ D 21.5 $4d^6p$ (³ G) ⁴ F + 23.3 $4d^6p$ (³ F) ² D + 14.7 $4d^6p$ (³ P) ⁴ D 21.5 $4d^6p$ (³ H) ⁴ G + 21.8 $4d^6p$ (³ G) ² H + 13.1 $4d^6p$ (³ F) ⁴ F 4.5 $4d^6p$ (³ H) ² G + 25.8 $4d^6p$ (³ G) ² H + 13.1 $4d^6p$ (³ F) ⁴ F 4.5 $4d^6p$ (³ H) ² G + 25.8 $4d^6p$ (³ D) ² P + 10.9 $4d^6p$ (³ F) ⁴ F 21.7 $4d^6p$ (³ H) ⁴ G + 11.8 $4d^6p$ (³ D) ² P + 10.9 $4d^6p$ (³ F) ⁴ F 21.7 $4d^6p$ (³ G) ⁴ H + 23.4 $4d^6p$ (³ D) ² P + 10.9 $4d^6p$ (³ F) ⁴ F 23.3 $4d^6p$ (³ D) ⁴ F + 18.5 $4d^6p$ (³ D) ² P + 12.9 $4d^6p$ (³ F) ⁴ F 33.4 d^6p (³ D) ⁴ F + 18.5 $4d^6p$ (³ D) ⁴ F + 11.7 $4d^6p$ (³ P) ⁴ D 17.9 $4d^6p$ (³ D) ⁴ H + 21.4 $4d^6p$ (³ H) ⁴ G + 11.6 $4d^6p$ (³ P) ⁴ D 17.9 $4d^6p$ (³ D) ⁴ H + 12.4 $4d^6p$ (³ H) ⁴ G + 11.6 $4d^6p$ (³ P) ⁴ D 17.9 $4d^6p$ (³ D) ⁴ H + 12.4 $4d^6p$ (³ H) ⁴ G + 10.2 $4d^6p$ (³ P) ⁴ D 17.8 $4d^6p$ (³ D) ² F + 14.3 $4d^6p$ (³ G) ⁴ H + 5.7 $4d^6p$ (³ P) ⁴ D 38.5 $4d^6p$ (³ H) ² G + 12.3 $4d^6p$ (³ G) ⁴ G + 8.4 $4d^6p$ (³ G) ⁴ G 11.7 $4d^6p$ (³ D) ² F + 21.8 $4d^6p$ (³ G) ⁴ G + 12.1 $4d^6p$ (³ D) ⁴ G 11.7 $4d^6p$ (³ D) ² F + 12.8 $4d^6p$ (³ D) ⁴ F + 10.3 $4d^6p$ (³ D) ⁴ G 11.7 $4d^6p$ (³ B) ² D + 10.5 $4d^6p$ (³ D) ⁴ F + 10.3 $4d^6p$ (³ D) ⁴ G 11.7 $4d^6p$ (³ D) ² F + 12.8 $4d^6p$ (³ D) ⁴ F + 10.3 $4d^6p$ (³ D) ⁴ G 11.7 $4d^6p$ (³ D) ² F + 12.8 $4d^6p$ (³ D) ⁴ F + 10.3 $4d^6p$ (³ D) ⁴ G 11.7 $4d^6p$ (³ D) ² F + 12.8 $4d^6p$ (³ D) ² F + 12.1 $4d^6p$ (³ D) ⁴ G 11.7 $4d^6p$ (³ D) ² P + 14
$\begin{array}{r} 235915\\ 236915\\ 236915\\ 236095.4\\ 237217.6\\ 237351.1\\ 237665.2\\ 237757.5\\ 237864\\ 237958.5\\ 238116.8\\ 239288.9\\ 239519.2\\ 239519.2\\ 239519.2\\ 239519.2\\ 239519.2\\ 239519.2\\ 23955.7\\ 240318.7\\ 240625.4\\ 240655.4$	235662 235662 235674 235905 236132 236068 237183 237243 237745 237823 237745 238087 238112 238935 239651 239651 239419 239770 240014 240085 240380 240387 240859 240572 240575 240603 241086 241008 241100 241324 241256 241566 241807 242571 242607 242571 242607	$\begin{array}{r} -119.7\\ 7.8\\ 58.5\\ -23.1\\ -217\\ 27.4\\ 34.6\\ 108.1\\ -79.8\\ -65.5\\ 149\\ -128.5\\ 4.8\\ 9.8\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -15.3\\ -362.1\\ 100.2\\ -33.4\\ 98.9\\ 78.8\\ -110.6\\ 83.4\\ 98.9\\ 78.8\\ -110.5\\ 229.7\\ -16.8\\ 127\\ -98.5\\ -36.6\\ 182.5\\ -66.4\\ 205.8\\ \end{array}$	$egin{array}{c} 6.5\\ 2.5\\ 3.5\\ 5.5\\ 1.5\\ 0.5\\ 3.5\\ 1.5\\ 5.5\\ 2.5\\ 4.5\\ 1.5\\ 2.5\\ 4.5\\ 2.5\\ 4.5\\ 2.5\\ 4.5\\ 2.5\\ 3.5\\ 2.5\\ 3.5\\ 2.5\\ 3.5\\ 2.5\\ 3.5\\ 2.5\\ 3.5\\ 1.5\\ 2.5\\ 1.5\\ 1.5\\ 2.5\\ 1.5\\ 1.5\\ 2.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1.5\\ 1$	33.3 4d ⁵ 5p (³ G) ⁴ G + 14.4 4d ⁵ 5p (³ F) ⁴ D + 8 4d ⁵ 5p (³ G) ⁴ F) ² G 28.6 4d ⁶ 5p (³ G) ⁴ G + 15.6 4d ⁶ 5p (³ F) ⁴ G + 11.1 4d ⁶ 5p (³ F) ² G 36.6 4d ⁶ 5p (³ H) ⁴ H + 25.2 4d ⁶ 5p (³ G) ² H + 11.9 4d ⁶ 5p (¹ H) ² H 25.7 4d ⁶ 5p (³ F) ⁴ D + 13.2 4d ⁶ 5p (⁵ D) ⁴ D + 7.5 4d ⁶ 5p (³ P) ⁴ D 25.7 4d ⁶ 5p (³ F) ⁴ D + 13.6 4d ⁶ 5p (⁵ D) ⁴ D + 11.6 4d ⁶ 5p (³ P) ⁴ F 16.6 4d ⁶ 5p (³ G) ⁴ F + 14.4 4d ⁶ 5p (³ F) ² D + 14.7 4d ⁶ 5p (³ P) ⁴ F 16.6 4d ⁶ 5p (³ G) ⁴ F + 23.3 4d ⁶ 5p (³ G) ² H + 13.9 4d ⁶ 5p (³ G) ⁴ G 24.7 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ F 4.5 4d ⁶ 5p (³ H) ² G + 25.8 4d ⁶ 5p (³ G) ² H + 13.1 4d ⁶ 5p (³ F) ⁴ G 16.9 4d ⁶ 5p (³ B) ⁴ D + 13.7 4d ⁶ 5p (³ D) ² P + 10.9 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ D) ² F + 13.4 4d ⁶ 5p (³ D) ² P + 12.9 4d ⁶ 5p (³ P) ⁴ D 17.9 4d ⁶ 5p (³ D) ² F + 13.4 4d ⁶ 5p (³ D) ² P + 12.9 4d ⁶ 5p (³ P) ⁴ D 7.7 4d ⁶ 5p (³ D) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ F) ⁴ G 33 4d ⁶ 5p (³ G) ⁴ H + 21 4d ⁶ 5p (³ H) ⁴ G + 11.6 4d ⁶ 5p (³ F) ⁴ G 33 4d ⁶ 5p (³ G) ² F + 14.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 10.2 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 16.7 4d ⁶ 5p (³ F) ⁴ G 38.5 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ G + 16.7 4d ⁶ 5p (³ F) ⁴ G 19.6 4d ⁶ 5p (³ H) ² G + 12.3 4d ⁶ 5p (³ H) ⁴ H + 15.8 4d ⁶ 5p (³ G) ⁴ G 11.7 4d ⁶ 5p (³ G) ⁴ H + 21.3 4d ⁶ 5p (³ H) ⁴ H + 15.8 4d ⁶ 5p (³ G) ⁴ G 11.7 4d ⁶ 5p (³ G) ² F + 21.8 4d ⁶ 5p (³ H) ² H + 16.7 4d ⁶ 5p (³ G) ⁴ G 11.7 4d ⁶ 5p (³ G) ² F + 12.8 4d ⁶ 5p (³ H) ⁴ H + 15.8 4d ⁶ 5p (³ G) ⁴ G 11.7 4d ⁶ 5p (³ H) ² G + 17.8 4d ⁶ 5p (³ H) ² H + 15.3 4d ⁶ 5p (³ G) ⁴ G 11.7 4d ⁶ 5p (³ G) ⁴ H + 14.5 4d ⁶ 5p (³ H) ² H + 15.3 4d ⁶ 5p (³ H) ²

			Т	able A37: Continued
E^a_{exp}	E^b_{calc}	ΔE	J	Leading components (in $\%$) in LS Coupling ^c
244815.5	244836	-20.5	5.5	$50.5 4d^{6}5p (^{3}H) ^{2}H + 37.3 4d^{6}5p (^{1}I) ^{2}H$
245016.1 245073-3	244841 245094	-20.7	0.5	$26 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}D + 33.9 \ 4d^{\circ}5p \ (^{\circ}F) \ ^{\circ}D + 17 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}P$ $28 \ 9 \ 4d^{6}5p \ (^{3}C) \ ^{2}C + 12 \ 4d^{6}5p \ (^{3}C) \ ^{2}F + 10 \ 7 \ 4d^{6}5p \ (^{1}C) \ ^{2}F$
245179.9	245051	128.9	5.5	$38.5 4d^{6}5p (^{3}G) ^{2}H + 15.3 4d^{6}5p (^{3}G) ^{4}H + 11 4d^{6}5p (^{1}I) ^{2}I$
245878.2	245960	-81.8	7.5	94.4 $4d^{6}5p(^{1}I)^{2}K + 5.3 4d^{6}5p(^{3}H)^{4}I$
246010.1	245916	94.1	1.5	$37.8 \ 4d^{0}5p \ (^{3}G) \ ^{4}F + 11.9 \ 4d^{0}5p \ (^{3}D) \ ^{4}F + 10.1 \ 4d^{0}5p \ (^{3}D) \ ^{2}P$
246376.2 246420.2	246356 246533	20.2 -112.8	4.5 1.5	$33.8 \ 4d^{\circ}5p \ (^{\circ}G)^{-}H + 18 \ 4d^{\circ}5p \ (^{\circ}G)^{-}G + 12.2 \ 4d^{\circ}5p \ (^{\circ}H)^{-}H$ $31.3 \ 4d^{6}5p \ (^{3}D)^{-}4D + 10.4 \ 4d^{6}5p \ (^{3}F)^{-}4D + 8.6 \ 4d^{6}5p \ (^{1}D)^{-}2P$
246450.7	246496	-45.3	0.5	$33.6 \ 4d^65p \ (^3D) \ ^4P + 10.3 \ 4d^65p \ (^3P) \ ^2P + 8 \ 4d^65p \ (^3P) \ ^4P$
246935.2	246771	164.2	2.5	49.5 4d ⁶ ₆ 5p (³ ₂ D) ⁴ ₂ D + 20.6 4d ⁶ ₆ 5p (³ ₁ F) ⁴ ₂ D + 6.5 4d ⁶ ₅ 5p (³ ₂ D) ⁴ P
246978.2	246857	121.2	3.5	$10.4 \ 4d^{0}5p \ (^{3}G) \ ^{2}F + 16.1 \ 4d^{0}5p \ (^{1}G) \ ^{2}G + 14.7 \ 4d^{0}5p \ (^{3}G) \ ^{4}F$
247257.8	247104 247214	88.8	$\frac{3.5}{2.5}$	26.4 4 d 5p (D) D + 20.2 4 d 5p (D) F + 8.4 4 d 5p (G) G $34.1 4d^{6}5p (^{3}G) ^{4}F + 29.6 4d^{6}5p (^{3}D) ^{4}F + 7.9 4d^{6}5p (^{3}G) ^{2}F$
247444.2	247358	86.2	1.5	$36.3 \ 4d^{6}5p \ (^{3}D) \ ^{2}P + 13.9 \ 4d^{6}5p \ (^{3}G) \ ^{4}F + 6.5 \ 4d^{6}5p \ (^{3}P) \ ^{2}D$
247525.9	247376	149.9	4.5	$35.4 \ 4d_{0}^{6}5p \ ({}^{3}D) \ {}^{4}F + 15.4 \ 4d_{0}^{6}5p \ ({}^{3}G) \ {}^{2}G + 8.3 \ 4d_{0}^{6}5p \ ({}^{3}H) \ {}^{2}G$
247919.3	248060	-140.7	0.5	11.5 $4d^{0}5p$ (³ P) ² P + 16.6 $4d^{0}5p$ (³ D) ⁴ P + 14.7 $4d^{0}5p$ (³ D) ⁴ D
248496.3 248566.7	248438 248749	58.3 -182.3	1.5	44.9 4d°5p (°D) ^{-}D + 9.6 4d°5p (°D) ^{-}D + 6.9 4d°5p (°D) ^{-}F 21.2 4d ⁶ 5p (¹ F) ^{2}D + 12.8 4d ⁶ 5p (¹ D) ^{2}D + 10.9 4d ⁶ 5p (³ D) ^{2}F
248656.6	248522	134.6	3.5	21.2 4d $^{6}5p$ (^{1}G) ^{2}F + 18 4d $^{6}5p$ (^{1}F) ^{2}G + 12.2 4d $^{6}5p$ (^{3}F) ^{2}F
248732.1	248605	127.1	4.5	22.5 $4d^{6}5p$ (³ G) ² G + 31.6 $4d^{6}5p$ (³ D) ⁴ F + 11.9 $4d^{6}5p$ (³ H) ² H
249209.7	249196	13.7	2.5	$33.3 \ 4d^65p \ (^3D) \ ^2D + 27.2 \ 4d^65p \ (^3D) \ ^2F + 5 \ 4d^65p \ (^3D) \ ^4P$
249480.9	249252	228.9	3.5	$35.3 \ 4d^{6}5p \ (^{1}G) \ ^{2}G + 10.3 \ 4d^{6}5p \ (^{3}D) \ ^{4}F + 7.2 \ 4d^{6}5p \ (^{1}D) \ ^{2}F$
250353.6	250252	-198.4	1.5 5.5	22.1 4d 5p (D) D + 19.9 4d 5p (D) P + 8.6 4d 5p (F) D 59.8 4d ⁶ 5p (¹ I) ² I + 17.2 4d ⁶ 5p (¹ G) ² H + 5.5 4d ⁶ 5p (³ H) ² H
250411	250372	39	4.5	$44 \ 4d^{6}5p \ (^{1}I) \ ^{2}H + 15.2 \ 4d^{6}5p \ (^{3}G) \ ^{2}H + 12.5 \ 4d^{6}5p \ (^{1}G) \ ^{2}H$
250439.6	250534	-94.4	2.5	21.8 $4d^{6}5p$ (${}^{3}G$) ${}^{2}F$ + 19.9 $4d^{6}5p$ (${}^{3}F$) ${}^{2}F$ + 12.4 $4d^{6}5p$ (${}^{1}D$) ${}^{2}F$
250483.9	250435	48.9	3.5	$37.3 \ 4d^{6}5p \ (^{3}D) \ ^{2}F + 23.3 \ 4d^{6}5p \ (^{3}D) \ ^{4}D + 6.8 \ 4d^{6}5p \ (^{1}D) \ ^{2}F$
250486.7	250589	-102.3	6.5 4 5	$87.9 \ 4d^{6}5p \ (^{1}I) \ ^{2}I + 8.6 \ 4d^{6}5p \ (^{1}I) \ ^{2}K + 2.8 \ 4d^{6}5p \ (^{3}H) \ ^{2}H + 10.4 \ 4d^{6}5p \ (^{1}I) \ ^{2}H$
251797.6	251328	254.9 469.6	4.5 5.5	$36.5 \ 4d^{6}5p \ (^{1}G)^{2}H + 25 \ 4d^{6}5p \ (^{1}G)^{2}H + 15.5 \ 4d^{6}5p \ (^{1}I)^{2}I$
252246.3	252233	13.3	2.5	$0.8 \ 4d^{6}5p \ (^{3}P) \ ^{4}P + 22.8 \ 4d^{6}5p \ (^{3}D) \ ^{2}D + 18 \ 4d^{6}5p \ (^{1}D) \ ^{2}F$
252985.8	252813	172.8	1.5	19 4d ⁶ 5p (¹ S) ² P + 13.9 4d ⁶ 5p (³ D) ² D + 11.5 4d ⁶ 5p (¹ D) ² D
253412.1	253058	354.1	0.5	$33 \ 4d^{0}5p \ (^{3}D) \ ^{2}P + 21 \ 4d^{0}5p \ (^{1}S) \ ^{2}P + 11.7 \ 4d^{0}5p \ (^{3}D) \ ^{4}D$
254041.7	255544	-00 3	3.5	$31.2 \ 4d^{\circ} \text{5p} (^{\circ} \text{F}) \ ^{\circ} \text{G} + 22.2 \ 4d^{\circ} \text{5p} (^{\circ} \text{G}) \ ^{\circ} \text{G} + 9.8 \ 4d^{\circ} \text{5p} (^{\circ} \text{H}) \ ^{\circ} \text{G}$ $35.2 \ 4d^{\circ} \text{5p} (^{3} \text{F}) \ ^{4} \text{D} + 14.7 \ 4d^{\circ} \text{5p} (^{3} \text{P}) \ ^{4} \text{D} + 10.6 \ 4d^{\circ} \text{5p} (^{3} \text{G}) \ ^{2} \text{F}$
255608.3	255392	216.3	0.5	$42.4 \ 4d^{6}5p \ (^{3}P) \ ^{4}D + 17.7 \ 4d^{6}5p \ (^{3}F) \ ^{4}D + 12.9 \ 4d^{6}5p \ (^{1}S) \ ^{2}P$
255752.6	255496	256.6	2.5	$32.5 \ 4d^{6}5p \ (^{1}G) \ ^{2}F + 16.7 \ 4d^{6}5p \ (^{3}D) \ ^{2}F + 15.2 \ 4d^{6}5p \ (^{1}G) \ ^{2}F$
256377.2	256598	-220.8	1.5	29.2 $4d^{6}5p$ (³ P) ⁴ D + 18.3 $4d^{6}5p$ (¹ D) ² D + 12.6 $4d^{6}5p$ (³ F) ⁴ D
256402.5	256757	-354.5	0.5	$40.8 \ 4d^{6}\text{5p} \ (^{1}\text{D}) \ ^{2}\text{P} + 18.4 \ 4d^{6}\text{5p} \ (^{3}\text{P}) \ ^{2}\text{P} + 13.4 \ 4d^{6}\text{5p} \ (^{1}\text{D}) \ ^{2}\text{P}$
257015.9	257052 257178	-162.1	2.5	$31.1 \ 4d^{6}5p \ (^{3}P) \ ^{4}D + 34.1 \ 4d^{6}5p \ (^{3}F) \ ^{4}D + 7.1 \ 4d^{6}5p \ (^{3}P) \ ^{4}D$
257568.4	257274	294.4	1.5	$13.4 \ 4d^{6}5p \ (^{1}D) \ ^{2}P + 23.5 \ 4d^{6}5p \ (^{1}S) \ ^{2}P + 9.6 \ 4d^{6}5p \ (^{3}P) \ ^{2}D$
258005.8	258178	-172.2	3.5	$35.1 \ 4d_{0}^{6}5p \ (^{1}D) \ ^{2}F + 24.5 \ 4d_{0}^{6}5p \ (^{3}F) \ ^{4}D + 7.2 \ 4d_{0}^{6}5p \ (^{1}G) \ ^{2}F$
258708.7	259045	-336.3	2.5	$37.2 \ 4d^{0}5p \ (^{1}D) \ ^{2}D + 11.1 \ 4d^{0}5p \ (^{1}D) \ ^{2}F + 7.7 \ 4d^{0}5p \ (^{1}F) \ ^{2}D$
260126.4	260199	-12.0	2.5 1.5	41 4d ^o 5p (^{1}F) ^{2}G + 25 4d ^o 5p (^{1}F) ^{2}F + 9.6 4d ^o 5p (^{1}F) ^{2}D 54 1 4d ⁶ 5p (^{1}F) ^{2}D + 6.3 4d ⁶ 5p (^{1}D) ^{2}D + 5.7 4d ⁶ 5p (^{3}P) ^{2}D
260437.3	260576	-138.7	3.5	$58 \ 4d^65p \ (^1F) \ ^2F + 6.1 \ 4d^65p \ (^1G) \ ^2F + 5.9 \ 4d^65p \ (^1F) \ ^2G$
261991.2	262063	-71.8	2.5	$32.3 \ 4d^{6}5p \ (^{1}F) \ ^{2}F + 29.2 \ 4d^{6}5p \ (^{3}F) \ ^{4}G + 7.8 \ 4d^{6}5p \ (^{1}G) \ ^{2}F$
262557.3	262539	18.3	4.5	$27.9 \ 4d^{6}5p \ (^{3}F) \ ^{2}G + 25 \ 4d^{6}5p \ (^{3}F) \ ^{4}G + 15.9 \ 4d^{6}5p \ (^{1}F) \ ^{2}G$
262987 265034-4	262965 264978	22 56.4	3.5	$59.7 \ 4d^{\circ}5p \ (^{\circ}F) \ ^{\circ}G + 8.6 \ 4d^{\circ}5p \ (^{\circ}F) \ ^{\circ}G + 7.3 \ 4d^{\circ}5p \ (^{\circ}F) \ ^{\circ}G$ 11.8 $4d^{6}5p \ (^{3}F) \ ^{2}D + 14.6 \ 4d^{6}5p \ (^{3}P) \ ^{4}S + 13.5 \ 4d^{6}5p \ (^{3}F) \ ^{4}D$
265241.5	265105	136.5	5.5	$75.6 \ 4d^{6}5p \ (^{3}F) \ ^{4}G + 15.4 \ 4d^{6}5p \ (^{3}F) \ ^{4}G$
265642.1	265517	125.1	1.5	$38.4 \ 4d^{6}5p \ (^{3}P) \ ^{4}S + 22.9 \ 4d^{6}5p \ (^{3}F) \ ^{2}D + 6.7 \ 4d^{6}5p \ (^{3}P) \ ^{4}S$
266306.3	266216	90.3	1.5	$36.5 \ 4d^{6}5p \ (^{3}P) \ ^{4}P + 20 \ 4d^{6}5p \ (^{3}P) \ ^{4}P + 10.2 \ 4d^{6}5p \ (^{3}P) \ ^{4}S$
267191.2	267166	25.2 00.5	4.5	$35.8 \text{ 4d}^{\circ}5p ({}^{\circ}F) {}^{\circ}G + 20.8 \text{ 4d}^{\circ}5p ({}^{\circ}F) {}^{\circ}G + 9.8 \text{ 4d}^{\circ}5p ({}^{\circ}G) {}^{\circ}G$
267320.3 267493.2	267227	99.5 118.2	2.5 0.5	21.4 4 d 5 p (F) F + 10.9 4 d 5 p (F) D + 12.4 4 d 5 p (F) D $62.3 4 d^{6}5 p (^{3}F) ^{4}D + 9.2 4 d^{6}5 p (^{3}P) ^{4}D + 6.9 4 d^{6}5 p (^{3}F) ^{4}D$
268208.4	268253	-44.6	2.5	29 4d ⁶ 5p (³ P) ² D + 13.7 4d ⁶ 5p (³ P) ² D + 13.2 4d ⁶ 5p (³ P) ⁴ P
268262.7	268212	50.7	3.5	$37.6 \ 4d^{6}5p \ (^{3}F) \ ^{4}F + 12.2 \ 4d^{6}5p \ (^{3}F) \ ^{2}G + 12 \ 4d^{6}5p \ (^{3}F) \ ^{4}F$
268610.3	268660	-49.7	1.5	24.1 4d ⁶ 5p (³ P) ² D + 26.5 4d ⁶ 5p (³ F) ⁴ F + 10.4 4d ⁶ 5p (³ P) ² D 21.7 4d ⁶ 5 (³ F) ⁴ D + 12.0 4d ⁶ 5 (³ F) ² D + 11.0 4d ⁶ 5 (³ P) ² D
269889 7	269949	-59.3	1.5 3.5	51.7 40 5p(F) D + 13.9 40 5p(F) D + 11.9 40 5p(F) D $54.9 4d^{6}5p(^{3}F) ^{2}G + 10.9 4d^{6}5p(^{1}G) ^{2}F + 8.8 4d^{6}5p(^{3}F) ^{2}G$
270214.4	270284	-69.6	2.5	$33.9 \ 4d^65p \ (^{3}F) \ ^{2}D + 18.8 \ 4d^65p \ (^{3}F) \ ^{4}F + 15.5 \ 4d^65p \ (^{3}P) \ ^{4}P$
270353.3	270385	-31.7	4.5	$37.4 \ 4d^{6}5p \ (^{1}G) \ ^{2}H + 23 \ 4d^{6}5p \ (^{3}F) \ ^{4}F + 18.8 \ 4d^{6}5p \ (^{1}G) \ ^{2}H$
270766.2	270842	-75.8	3.5	$16.1 \ 4d^{0}5p \ (^{3}F) \ ^{2}F + 20.7 \ 4d^{0}5p \ (^{1}G) \ ^{2}F + 15.4 \ 4d^{0}5p \ (^{3}P) \ ^{4}D$
271217.8	271171 271541	46.8	2.5	24.1 4d ⁶ 5p (³ F) ⁴ D + 21.5 4d ⁵ 5p (³ F) ² D + 7.9 4d ⁶ 5p (³ F) ⁴ F 29.1 4d ⁶ 5p (³ F) ⁴ F + 24.9 4d ⁶ 5p (³ F) ² D + 7.9 4d ⁶ 5p (³ F) ⁴ F
271792.5	271738	54.5	4.5	$33.6 \ 4d^{6}5p \ (^{3}F) \ ^{4}F + 27 \ 4d^{6}5p \ (^{3}F) \ ^{2}G + 11.8 \ 4d^{6}5p \ (^{3}F) \ ^{4}F$
273408.9	273446	-37.1	3.5	$16.5 \ 4d^{6}5p \ (^{3}P) \ ^{4}D + 17.7 \ 4d^{6}5p \ (^{3}F) \ ^{2}F + 14.9 \ 4d^{6}5p \ (^{3}F) \ ^{4}D$
273965.5	274237	-271.5	2.5	$16.6 \ 4d^{6}5p \ (^{3}P) \ ^{2}D + 23.8 \ 4d^{6}5p \ (^{3}P) \ ^{2}D + 14.2 \ 4d^{6}5p \ (^{3}P) \ ^{4}P$
274684.2 274707 =	274884	-199.8 7 F	2.5 2 F	$60.7 \ 4d^{\circ}5p \ (^{\circ}F) \ ^{4}F + 19.8 \ 4d^{\circ}5p \ (^{\circ}F) \ ^{4}F$ $4.5 \ 4d^{6}5p \ (^{3}F) \ ^{4}F + 35.7 \ 4d^{6}5p \ (^{1}C) \ ^{2}C + 19.6 \ 4d^{6}5p \ (^{3}E) \ ^{4}F$
∠14191.5 275204.8	274790 275354	1.0 -149.2	э.э 5.5	$4d^{6}5p$ (¹ G) ² H + 30.2 4d ⁶ 5p (¹ G) ² H
275971.8	276197	-225.2	1.5	$34 4d^{6}5p (^{3}P) ^{2}P + 22.3 4d^{6}5p (^{3}P) ^{2}P + 7.4 4d^{6}5p (^{3}P) ^{2}D$
276014.8	276142	-127.2	2.5	$45.9 \ 4d^{6}5p \ (^{1}G) \ ^{2}F + 12.7 \ 4d^{6}5p \ (^{1}G) \ ^{2}F + 11.9 \ 4d^{6}5p \ (^{1}F) \ ^{2}F$
277850.2	277950	-99.8	4.5	59.4 $4d^{0}5p$ (¹ G) ² G + 18.2 $4d^{0}5p$ (¹ G) ² G + 6.7 $4d^{6}5p$ (¹ G) ² H
279626.8	279731 285026	-104.2 106 1	3.5 1.5	22.0 4a ^o op (^a G) ^a G + 18.4 4d ^o op (^a F) ^a F + 16.1 4d ^o op (^a G) ^a F 69.1 4d ⁶ op (¹ D) ² D + 9.5 4d ⁶ op (¹ D) ² D \pm 8.3 4d ⁶ op (¹ D) ² D
287725.2	287653	72.2	2.5	$62.6 \ 4d^{6}5p \ (^{1}D) \ ^{2}D + 11.3 \ 4d^{6}5p \ (^{1}D) \ ^{2}F + 8.3 \ 4d^{6}5p \ (^{1}D) \ ^{2}D$
293238.9	293171	67.9	2.5	$52.2 \ 4d^{6}5p \ (^{1}D) \ ^{2}F + 18.3 \ 4d^{6}5p \ (^{1}D) \ ^{2}D + 14.4 \ 4d^{6}5p \ (^{1}D) \ ^{2}F$
294884.3	294728	156.3	1.5	51.6 $4d^{6}5p$ (¹ D) ² P + 20.4 $4d^{6}5p$ (¹ D) ² P + 10.5 $4d^{6}5p$ (¹ D) ² D
295024.7 296253.4	294942 296106	82.7 147 4	0.5 3.5	2 24.9 4d ⁵ 5p (¹ D) ² F + 22.4 4d ⁶ 5p (¹ D) ² F + 17.4 4d ⁶ 5p (¹ S) ² P 70.1 4d ⁶ 5p (¹ D) ² F + 19.8 4d ⁶ 5p (¹ D) ² F + 5.2 4d ⁶ 5p (¹ C) ² F
			0.0	

a: From Van Kleef [30] and Kildiyarova [42] b: This work c: Only the component ≥ 5% are given

Labic 1		putted osen	lator	Surcinguits	and 0	1 411510.	ion probe		5 118
	Wavelength	Lower Level ^a	J_{Low}	Upper level ^a	J_{Up}	log gf	gA	CF	
	Å	cm^{-1}		cm^{-1}			s^{-1}		
	391.668	22532	5.5	277850	4.5	-0.38	1.83E + 10	-0.323	
	394.853	26368	4.5	279627	3.5	-0.47	$1.46E \pm 10$	-0.225	
	307 762	14800	2.5	266306	1.5	0.96	4 50E+00	0.172	
	207 777	24625	2.5	200300	1.5	-0.30	$4.09D \pm 0.09$	0.172	
	397.777	34635	2.5	286032	1.5	-0.6	1.06E + 10	0.394	
	398.198	36594	3.5	287725	2.5	-0.52	1.28E + 10	0.307	
	398.815	14899	2.5	265642	1.5	-0.87	5.65E + 09	0.305	
	401.187	22532	5.5	271793	4.5	-0.37	1.76E + 10	0.337	
	402.528	26368	4.5	274798	3.5	-0.63	9.71E + 09	-0.231	
	403 279	17067	0.5	265034	1.5	-0.94	$4.70E \pm 0.09$	0.199	
	404 701	26269	4.5	272400	2.5	0.97	5.52E+00	0.155	
	404.791	20308	4.5	273409	3.5	-0.87	$0.02E \pm 10$	0.215	
	410.641	26368	4.5	269890	3.5	-0.23	2.33E + 10	0.339	1
	410.907	14204	1.5	257568	1.5	-0.93	4.66E + 09	-0.178	
	411.343	14899	2.5	258006	3.5	-0.76	6.86E + 09	0.418	
	412.084	14899	2.5	257568	1.5	-0.96	4.35E + 09	0.376	
	414.284	34635	2.5	276015	2.5	-0.86	$5.38E \pm 0.09$	0.085	
	414 407	36504	3.5	277850	4.5	0.42	$1.48E \pm 10$	0.528	
	415 700	14000	0.5	211030	4.0	-0.42	1.400+10	0.520	
	415.722	14899	2.5	255445	3.5	-0.39	1.59E+10	0.444	
	416.384	34635	2.5	274798	3.5	-0.9	4.89E + 09	0.187	
	416.581	34635	2.5	274684	2.5	-0.77	6.50E + 09	-0.145	
	416.623	22532	5.5	262557	4.5	-0.08	3.19E + 10	0.586	
	416.695	55041	1.5	295025	0.5	-0.46	1.34E + 10	-0.643	
	417 093	0	4 5	239755	5.5	-0.86	$5.26E \pm 0.9$	-0.088	
	417 556	20124	1.5	260622	1.5	0.72	7 12E 00	0.200	
	417.550	50154	1.5	209023	1.5	-0.75	7.13E+09	0.209	
	418.563	7097	1.5	246010	1.5	-0.78	6.30E+09	-0.191	
	419.97	56772	2.5	294884	1.5	-0.16	2.59E + 10	-0.576	
	420.241	0	4.5	237959	4.5	-0.76	6.62E + 09	0.241	
	420.53	3691	3.5	241486	4.5	-0.81	5.85E + 09	0.119	
	420.95	5816	2.5	243374	2.5	-0.86	5.16E + 0.9	-0.273	
	421.28	36594	35	273066	2.0	-0.85	$5.32E \pm 0.0$	_0.007	
	400.07	96504	0.0 9 E	273/00	2.0 9 =	0.00	5 491 - 00	0.097	
	422.21	30394	3.5	213409	3.5	-0.84	J.43E+09	-0.214	
	422.62	26368	4.5	262987	3.5	-0.69	7.63E+09	0.502	
	422.892	56772	2.5	293239	2.5	-1	3.71E + 09	-0.183	
	423.431	3691	3.5	239857	4.5	-1	3.70E + 09	-0.416	
	423.592	24361	2.5	260437	3.5	-0.77	6.34E + 09	0.147	
	424.037	3691	3 5	239519	2.5	-0.7	$7.37E \pm 0.9$	-0.408	
	424 476	14800	2.5	250494	2.5	0.66	8 19E 00	0.442	
	424.470	14099	2.0	250484	3.5	-0.00	0.12E+09	0.442	
	424.727	21571	1.5	257016	2.5	-0.6	9.33E+09	-0.37	
	424.97	20442	3.5	255753	2.5	-0.35	1.64E + 10	0.276	
	425.172	36594	3.5	271793	4.5	-0.95	4.13E + 09	-0.376	
	425.549	0	4.5	234991	4.5	0.04	4.02E + 10	-0.583	
	425.553	34635	2.5	269623	1.5	-0.95	$4.09E \pm 09$	-0.261	
	425.78	0	4.5	234863	3.5	0.00	$2.07E \pm 10$	0.682	
	426.100	5916	9.5	234003	2.5	-0.03	1.70E + 10	0.205	
	420.199	3810	2.5	240448	3.5	-0.33	1.70E+10	-0.305	
	426.419	16875	4.5	251386	4.5	-0.66	7.95E+09	0.067	
	426.49	0	4.5	234472	5.5	-0.5	1.16E + 10	0.489	
	426.572	22532	5.5	256959	4.5	-0.06	3.17E + 10	0.55	
	426.69	14204	1.5	248567	2.5	-0.99	3.79E + 09	-0.174	
	427 036	36594	3.5	270766	3.5	-0.46	$1.29E \pm 10$	0.257	
	427 255	7007	1.5	241150	2.5	0.96	$4.06E \pm 0.00$	0.341	
	427.205	24625	1.5	241130	2.5	-0.90	4.00E+09	0.341	
	427.395	34635	2.5	268610	1.5	-0.82	5.58E+09	0.216	
	427.463	0	4.5	233938	3.5	-0.79	5.94E + 09	0.223	
	427.516	7097	1.5	241007	1.5	-0.83	5.41E + 09	0.333	
	427.892	5816	2.5	239519	2.5	-0.76	6.34E + 09	-0.153	
	427.919	0	4.5	233689	4.5	-0.96	$4.04E \pm 0.09$	-0.102	
	427 971	3691	3.5	237351	3.5	0.06	4.13E + 10	-0.603	
	429.065	16975	4.5	250484	2.5	0.00	9.41E + 10	0.225	
	428.005	10075	4.5	250484	3.5	-0.18	2.415+10	0.323	
	428.199	16875	4.5	250411	4.5	-0.97	3.90E + 09	0.054	
	429.681	14204	1.5	246935	2.5	-0.84	5.23E + 09	0.149	
	430.252	7097	1.5	239519	2.5	-0.42	1.36E + 10	0.497	
	430.476	5816	2.5	238117	1.5	-0.69	7.41E + 09	-0.405	
	430.634	14204	1.5	246420	1.5	-0.67	$7.75E \pm 0.09$	0.29	
	430.945	5816	2.5	237864	2.5	0.3	$1.80E \pm 10$	0.484	
	430.056	2601	2.0	201004	1 5	_0.94	1.63E.10	-0.466	
	430.930	3091	3.5	233733	4.5	-0.34	1.03E+10	-0.400	
	430.968	14899	2.5	246935	2.5	-0.47	1.22E + 10	0.5	
	431.073	3691	3.5	235670	2.5	-0.84	5.21E + 09	-0.363	
	431.399	20442	3.5	252246	2.5	-0.34	1.63E + 10	0.419	
	431.4	24599	0.5	256402	0.5	-0.69	7.37E + 09	0.382	
	431.44	16875	4.5	248657	3.5	-0.04	3.24E + 10	0.364	
	431,645	34635	2.5	266306	1.5	-1	$3.56E \pm 0.9$	0.414	
	431 752	36594	3.5	268208	2.5	-0.06	$3.13E \pm 10$	-0.516	
	431 900	5816	0.0 0.5	200200	2.0 9 K	0.05	4.025 + 00	0.197	
	401.099	0100	2.0	20/001	3.5	-0.90	4.02E+09	0.137	
	432.339	3691	3.5	234991	4.5	-0.68	(.53E+09	0.426	
	432.462	3691	3.5	234925	2.5	-0.32	1.70E + 10	0.413	
	432.744	24361	2.5	255445	3.5	-0.98	3.76E + 09	0.127	
	432.887	34635	2.5	265642	1.5	-0.67	7.58E + 09	-0.402	
	432.917	55041	1.5	286032	1.5	-0.35	1.59E + 10	-0.44	
	432 088	56772	2.5	287725	2.5	-0.32	$1.72E \pm 10$	_0.207	
	499 100	00112	4.0 1 E	201120	2.0 9 =	0.32	1 20 - 10	0.201	
	433.180	5005	4.5	230848	3.5	-0.41	1.395+10	-0.362	
	433.712	7097	1.5	237665	1.5	-0.44	1.29E + 10	0.557	
	434.254	5816	2.5	236095	1.5	-0.23	2.08E+10	0.593	
	434.443	30134	1.5	260314	1.5	-0.47	1.19E + 10	0.255	
	434.555	7097	1.5	237218	0.5	-0.48	1.18E + 10	0.554	
	434.657	5816	2.5	235882	3.5	-0.33	1.65E + 10	-0.518	
	434 785	3601	35	233680	4 5	-0.65	7 85E+00	_0.282	
	404.700	00442	0.0	200009	4.0	-0.05	1.00E+09	-0.202	
	434.787	20442	3.5	250440	2.5	-0.01	3.43E+10	0.425	
	434.841	20442	3.5	250411	4.5	-0.56	9.72E + 09	-0.167	
	435.727	16875	4.5	246376	4.5	-0.55	9.84E + 09	0.122	
	435.85	14899	2.5	244336	1.5	-0.92	4.22E + 09	0.337	
	436.175	22532	5.5	251798	5.5	-0.47	1.19E + 10	0.27	
	436 474	5816	25	234025	25	_0.81	5 49E+00	_0.21	
	400.474	06260	4.0 1 E	204920	2.0 9 =	0.01	6.355-00	0.22	
	430.334	20308	4.0	200440	3.0	-0.74	1 502 10	-0.231	
	436.607	20442	3.5	249481	3.5	-0.37	1.50E + 10	0.272	
	436.762	3691	3.5	232648	4.5	-0.43	1.29E + 10	-0.518	
	437.038	24599	0.5	253412	0.5	-0.96	3.82E + 09	0.356	
	437.096	21571	1.5	250354	1.5	-0.84	5.02E + 09	-0.094	
	437.125	20442	3.5	249210	2.5	-0.84	5.11E + 0.9	-0.142	1

Table A38: Computed oscillator strengths and transition probabilities Ag V.

Table A38: Continued

abs.r.g. 2020 30191 3.5 232379 3.5 -0.03 4.1354-00 -0.112 457.498 7007 1.5 232670 2.5 -0.51 1.0054-10 -0.417 457.498 7007 1.5 232670 2.5 -0.51 1.0054-10 -0.428 438.101 1.167.10 4.5 242180 5.5 -0.428 1.0054-10 -0.428 438.104 0 4.5 24280 3.5 -0.428 3.5381-10 0.448 438.018 1.045.5 241061-06 5.5 -0.75 3.5381-10 0.448 438.025 1.0570-05 245016 0.5 -0.17 2.1051-10 0.042 438.045 24301 2.5 20246 2.5 -0.16 2.3884-10 0.348 439.23 14899 2.5 242670 1.5 -0.67 5.4667-00 0.324 439.33 14389 2.5 242670 1.5 -0.67 5.4667-00 0.324	Wavelength	Lower Level	JLow	Upper level	JUP	log gf	gA	CF
447.485 30134 1.5 258709 2.5 -0.77 5.887±00 -0.417 437.486 14014 1.5 242570 1.5 -0.8 5.505±00 0.232 433.01 16571 4.5 244557 3.5 -0.92 1.082±00 0.232 448.141 12042 1.5 24857 3.5 -0.92 1.082±00 0.323 448.201 0 4.5 22047 3.5 -0.92 3.081±00 0.432 438.01 1.489 2.5 22047 3.5 -0.92 3.081±00 0.443 438.025 1.7067 0.5 22741 2.5 0.17 5.385±10 0.378 438.035 2038 4.5 22741 2.5 0.17 5.385±10 0.324 439.33 30434 1.5 24767 1.5 -0.85 4.005±00 0.324 440.035 31071 1.3 2443973 1.5 0.4032 4.004±00 0.324 <tr< td=""><td>437.275 437.398</td><td>3691 24361</td><td>$\frac{3.5}{2.5}$</td><td>232379 252986</td><td>3.5 1.5</td><td>-0.93 -0.42</td><td>4.13E+09 1.32E+10</td><td>-0.122 -0.414</td></tr<>	437.275 437.398	3691 24361	$\frac{3.5}{2.5}$	232379 252986	3.5 1.5	-0.93 -0.42	4.13E+09 1.32E+10	-0.122 -0.414
447.488 7097 1.5 235870 2.5 -0.51 1.007±10 -0.428 447.584 14204 1.5 242473 5.5 -0.88 5.507±00 -0.258 448.184 12044 1.5 244673 5.5 -0.98 1.002±10 -0.129 448.201 0 4.5 228206 4.5 -0.142 3.53 -0.042 3.35 -0.06 -0.423 438.058 1255 5.5 5.50477 5.5 -0.12 5.161±10 -0.618 438.058 12057 5.5 5.50477 5.46±0.0 -0.42 3.48 -0.42 3.48 -0.42 3.48 -0.42 3.48 -0.42 3.48 -0.42 3.48 -0.42 3.48 -0.42 3.48 -0.42 3.48 -0.42 -0.44 -0.43 3.48 -0.42 -0.44 -0.43 -0.44 -0.43 -0.44 -0.43 -0.44 -0.43 -0.44 -0.43 -0.44 -0.43 -0.44	437.495	30134	1.5	258709	2.5	-0.77	5.89E+09	-0.147
$\begin{array}{c} 1, 1, 2, -1, 1, -1, -1, -1, -1, -1, -1, -1, -1,$	437.498	7097	1.5	235670	2.5	-0.51	1.09E+10	-0.427
438.881 14204 1.5 242473 2.5 -0.92 3.022+09 0.191 438.801 0 4.5 222305 4.5 -0.14 2.332+10 -0.161 438.803 12657 5.5 220407 6.5 -0.12 1.232+10 -0.163 438.605 12572 5.5 250487 6.5 -0.11 2.752+10 0.605 438.605 1207 5.5 252404 2.5 -0.17 2.352+10 0.473 439.255 23388 4.5 242470 1.5 -0.85 4.062+09 0.322 439.083 31343 1.5 275764 1.5 -0.77 5.542+09 0.323 440.033 11567 4.5 243973 4.5 -0.02 3.252+09 0.323 440.033 11571 1.5 244967 2.5 -0.73 5.44290 0.232 441.377 816 2.5 23379 3.5 -0.08 7.122+09 0.208 441.431 0314 1.5 2434967 2.5 -0.77 6.676+0	437.894 438.01	$14204 \\ 16875$	1.5 4.5	242570 245180	1.5 5.5	-0.8 -0.42	1.32E+10	$0.258 \\ 0.323$
438.181 202 1.0 248657 3.0 -1.034 4.108+09 0.1129 438.205 14899 2.5 244073 3.5 -0.02 1.055+10 -0.152 438.205 12057 4.5 224016 0.5 -0.78 5.805+09 -0.448 438.608 17007 0.5 24016 0.5 -0.78 5.805+09 -0.448 439.225 26568 4.5 254042 3.5 -0.07 5.545+09 -0.449 439.235 14899 2.5 24570 1.5 -0.79 5.545+09 -0.285 440.071 17007 0.5 244338 1.5 -0.79 5.545+10 -0.33 440.338 213571 1.5 244373 4.5 -0.73 3.055+10 -0.33 440.338 213571 1.5 244567 2.5 -0.68 7.125+09 -0.235 441.375 26457 1.5 -0.73 3.055+09 -0.33 4.055+10 -0.37 441.375 26452 232373 3.5 -0.44 3.105+10<	438.081	14204	1.5	242473	2.5	-0.95	3.92E + 09	-0.191
418.216 14899 2.5 243102 3.5 -0.68 3.638+09 -0.468 438.265 16875 4.5 24073 3.5 -0.22 1.657+00 -0.163 438.668 22532 5.5 250487 6.5 -0.17 5.35E+10 -0.53 439.252 23586 4.5 224412 5.5 -0.17 5.35E+10 -0.53 439.084 30134 5.5 245768 1.5 -0.37 5.44+09 0.133 430.881 30134 1.5 257568 1.5 -0.67 5.654+09 -0.23 440.338 1.6875 4.5 243973 4.5 -0.63 7.969+09 -0.231 441.337 5.16 2.5 23379 3.5 -0.63 7.989+09 -0.232 441.33 20462 2.5 -0.63 7.125+09 -0.238 441.341 20442 3.5 243738 3.5 -0.63 7.989+09 -0.237 441.377	438.184	20442	$\frac{3.5}{4.5}$	248657 228206	3.5 4.5	-0.92 -0.14	4.16E+09 2.53E+10	-0.129 -0.618
448.215 18675 4.5 246073 3.5 -0.52 1.05E+10 0.0132 438.683 24561 0.5 235246 0.5 0.16 2381E+10 0.0375 438.922 0 4.5 225414 5.5 0.047 4.55E+10 -0.583 439.235 1.4899 1.5 22471 1.5 0.455 4.465+10 -0.533 439.33 314931 1.5 2241370 1.5 0.455 4.165+10 -0.533 440.070 1.707 0.5 244336 1.5 -0.37 4.55E+09 0.33 440.035 21671 1.5 244496 1.5 -0.57 6.13E+09 -0.215 441.377 2816 2.5 22379 3.5 -0.68 7.12F+09 0.131 441.377 2816 2.5 22379 3.5 -0.68 7.12F+09 0.131 441.376 2461 3.5 241302 3.5 -0.57 6.157 0.68	438.208	14899	2.5	243102	3.5	-0.98	3.63E+10	-0.468
438.862 24361 0.3 244636 0.3 1.0.8 5.4687+00 0.442 438.818 24361 2.5 222246 2.5 0.016 23887+10 0.376 439.225 236388 4.5 242470 1.5 -0.85 4.002+00 0.3224 439.235 14899 2.5 242470 1.5 -0.36 4.002+00 0.3224 439.838 1.4204 1.5 241599 0.5 -0.79 5.557+09 0.33 440.033 1.4704 1.5 241570 2.5 -0.73 3.298+10 -0.33 440.073 21571 1.5 244966 1.5 -0.75 6.175+09 0.208 441.377 5864 2.5 232379 3.5 -0.68 7.125+09 -0.208 441.431 3014 3.5 265377 1.5 -0.44 6456+09 -0.51 441.766 21571 1.5 2453372 1.5 -0.44 4025+69 -0.135	438.215	16875	4.5	245073	3.5	-0.52	1.05E+10	-0.152
438.818 2436 2.5 -0.16 2.38E+10 0.0376 439.225 26368 4.5 22541 5.5 0.077 4.09E+10 0.481 439.235 14899 5.5 24578 1.5 0.077 4.09E+10 0.481 439.888 34635 2.5 24578 1.5 0.027 1.76E+10 0.529 440.038 14204 1.5 244374 1.5 0.023 1.76E+10 0.285 440.033 21571 1.5 24496 1.5 0.023 7.63E+09 0.237 441.079 20442 3.5 247333 2.5 -0.57 6.3E+09 -0.234 441.1709 26594 3.5 240778 3.5 -0.68 7.124F+00 -0.344 441.161 21424 3.5 240779 3.5 -0.74 6.32E+09 -0.15 441.1709 26594 3.5 264392 -0.5 -0.53 4.00E+10 -0.294 441.1515	438.695	22532 17067	0.5	250487 245016	0.5 0.5	-0.1	2.77E+10 5.80E+09	$0.605 \\ 0.442$
448.902 0 4.5 227841 5.5 0.17 5.158+10 0.083 439.225 23388 10134 1.5 227568 1.5 0.07 4.091410 0.134 439.838 10134 1.5 247568 1.5 0.079 5.458+00 0.034 440.037 1.10641 1.5 241540 0.5 -0.79 5.558+09 0.033 440.033 1.8757 4.5 243973 4.5 -0.027 3.2958+10 -0.333 440.033 21671 1.5 244966 1.5 -0.75 6.178+09 -0.208 441.737 5816 2.5 232379 3.5 -0.64 4.078+09 -0.33 441.766 21571 1.5 247919 0.5 -0.33 4.0028+09 -0.35 441.984 31349 2.5 241150 2.5 -0.51 1.0668+10 -0.335 441.984 14899 2.5 244732 2.5 -0.53 1.128+10	438.818	24361	2.5	252246	2.5	-0.16	2.38E + 10	0.376
$\begin{array}{c} 139.233 \\ 149.688 \\ 30134 \\ 1.5 \\ 1.5 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2.5 \\ 2.6191 \\ 2.5 \\ 2$	438.902	0	4.5	227841 254042	5.5	0.17 0.07	5.15E+10	-0.583
	439.225	14899	2.5	242570	1.5	-0.85	4.09E+10 4.90E+09	0.322
439 8.83 44333 2.5 20.1991 2.4 3.9 1.76E+10 0.235 440.038 16875 4.5 243973 4.5 -0.02 3.29E+10 -0.335 440.536 21571 1.5 2445677 2.5 -0.63 -0.77 6.13E+09 -0.213 440.635 12424 1.5 244967 3.5 -0.077 6.66E+09 -0.231 441.631 24244 1.5 2440678 3.5 -0.077 6.66E+09 -0.231 441.612 3691 3.5 203134 4.5 -0.87 4.57E+09 -0.284 441.612 3691 3.5 203134 4.5 -0.87 4.57E+00 -0.284 441.709 30594 3.5 265402 0.5 -0.33 4.06E+09 -0.135 441.940 30134 1.5 256402 0.35 -0.74 6.26E+09 -0.135 442.063 30134 1.5 256472 3.5 -0.43 1.27E+10 0.753 442.064 30134 1.5 256472	439.688	30134	1.5	257568	1.5	-0.79	5.54E + 09	0.134
	439.838	$34635 \\ 14204$	2.5 1.5	261991 241549	2.5 0.5	-0.29 -0.79	1.76E+10 5.55E+09	0.529 0.33
440.388 16875 4.5 243973 4.5 -0.02 3.20E+10 -0.301 440.635 14201 1.5 244567 2.5 -0.63 7.75 6.13E+40 -0.01 441.777 5816 2.5 243733 3.5 -0.66 7.12E+00 -0.231 441.431 20442 3.5 24078 3.5 -0.68 7.12E+00 -0.238 441.612 3661 3.5 203134 4.5 -0.68 7.12E+00 -0.248 441.612 3661 3.5 203134 4.5 -0.68 7.12E+00 -0.248 441.944 30134 1.5 256402 0.5 -0.51 1.00E+10 -0.299 442.003 30314 1.5 256471 1.5 -0.83 5.12E+00 0.75 442.034 16875 4.5 243102 3.5 -0.17 2.28E+10 0.475 442.034 16875 4.5 243102 2.5 -0.437 2.6 -0.438 5.12E+00 0.128 442.034 24511 2.5 <td< td=""><td>440.007</td><td>17067</td><td>0.5</td><td>244336</td><td>1.5</td><td>-0.87</td><td>4.65E+09</td><td>-0.285</td></td<>	440.007	17067	0.5	244336	1.5	-0.87	4.65E+09	-0.285
$\begin{array}{c} + 440 \ ef{a} & 2164 \ ef{a} & 24100 \ ef{a} & 25 \ ef{a} & -0.73 \ ef{a} & -0.76 \ ef{$	440.338	16875	4.5	243973	4.5	-0.02	3.29E+10	-0.393
	440.635	14204	1.5	248567 241150	2.5	-0.03	6.13E+09	-0.201
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	440.673	21571	1.5	248496	1.5	-0.75	6.17E + 09	0.163
$\begin{array}{c} +44.431 \\ +44.1431 \\ +2442 \\ +41.55 \\ +441.55 \\ +441.55 \\ +441.56 \\ +41.56 \\ +41.766 \\ +41.766 \\ +41.766 \\ +41.766 \\ +41.766 \\ +41.766 \\ +41.766 \\ +41.766 \\ +41.766 \\ +41.766 \\ +41.766 \\ +41.988 \\ +41.998 \\ +41.988 \\ +41.998 \\ +42.93 \\ +41.988 \\ +42.93 \\ +42.93 \\ +42.93 \\ +41.988 \\ +42.93 \\ +42.93 \\ +42.93 \\ +42.93 \\ +42.93 \\ +42.93 \\ +42.93 \\ +42.93 \\ +42.93 \\ +42.93 \\ +42.93 \\ +44.2431 \\ +2.5 \\ +2.55 \\ +45.72 \\ +42.94 \\ +42.93 \\ +42.943 \\ +44.2431 \\ +2.5 \\ +2.55 \\ +45.72 \\ +45. \\ +42.94 \\ +44.27 \\ +44.27 \\ +44.27 \\ +44.27 \\ +44.243 \\ +44.27 \\ +44.243 \\ +44.27 \\ +44.243 \\ +44.243 \\ +44.25 \\ +44.243 \\ $	440.799 441.377	20442 5816	3.5 2.5	247303 232379	2.5	-0.97	3.69E+09 7 12E+09	0.237
	441.431	20442	3.5	246978	3.5	-0.04	3.10E+10	0.51
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	441.545	14204	1.5	240682	2.5	-0.87	4.57E+09	-0.269
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	441.612	3691 36594	3.5 3.5	230134 262987	4.5 3.5	-0.86	4.69E+09 6.26E+09	-0.218
	441.796	21571	1.5	247919	0.5	-0.93	4.00E + 09	-0.135
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	441.954	30134	1.5	256402	0.5	-0.51	1.06E + 10	-0.335
	442.003	30134	$^{2.0}_{1.5}$	241150 256377	2.5 1.5	-0.5 -0.84	4.92E+09	0.299 0.168
	442.034	16875	4.5	243102	3.5	-0.17	2.28E + 10	0.275
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	442.086	22532 24361	5.5	248732 250440	4.5	-0.26	1.87E+10 5.12E-00	0.475
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	442.493	24361	$2.5 \\ 2.5$	250440 250354	$^{2.0}_{1.5}$	-0.83	6.38E+09	0.152
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	442.607	20442	3.5	246376	4.5	-0.61	8.42E + 09	0.268
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	442.904	14899 24599	2.5	240682 250354	2.5	-0.79	5.51E+09 1.70E+10	0.281
	442.333	30134	1.5	255753	2.5	-0.43	1.27E+10 1.27E+10	-0.253
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	443.331	0	4.5	225565	3.5	-0.65	7.67E + 09	0.29
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	444.205 444.208	$3691 \\ 24361$	$\frac{3.5}{2.5}$	$228812 \\ 249481$	3.5 3.5	-0.82 -0.78	5.10E+09 5.57E+09	-0.244 -0.229
	444.278	14204	1.5	239289	0.5	-0.95	3.80E+09	0.209
$ \begin{array}{ccccccccccccccccccccccccccccccccccc$	444.408	26368	4.5	251386	4.5	0.25	5.94E + 10	-0.523
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	444.456 444.682	22532 21571	5.5 1.5	247526 246451	4.5	-0.25	1.91E+10 4.24E+09	-0.378
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	444.744	24361	2.5	249210	2.5	-0.88	4.47E+09	0.092
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	445.174	20442	3.5	245073	3.5	-0.73	6.24E + 09	0.146
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	445.225	3691 3691	3.5 3.5	228296 228206	$\frac{2.5}{4.5}$	-0.46 -0.82	1.18E+10 5.05E+09	-0.383 -0.128
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	445.555	21571	1.5	246010	1.5	-0.93	3.97E + 0.09	-0.122
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	445.74	16875	4.5	241221	3.5	-0.56	9.21E+09	0.187
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	445.841 446.342	24361 26368	2.5 4.5	248657 250411	3.5 4.5	-0.69	$4.10E \pm 10$	-0.142 0.412
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	446.447	26368	4.5	250358	5.5	0	3.32E + 10	0.575
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	446.549	17067	0.5	241007	1.5	-0.86	4.65E+09	0.33
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	446.741	36594	3.5	260437	3.5	-0.40	1.56E+10 1.56E+10	0.322
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	446.829	16875	4.5	240674	5.5	-0.21	2.05E+10	0.601
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	447.366 447.873	20442 30134	3.5 1.5	243973 253412	4.5 0.5	-0.4 -0.51	1.32E+10 1.03E+10	$0.345 \\ 0.37$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	448.146	5816	2.5	228957	2.5	-0.92	3.96E + 09	-0.192
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	448.264	24361	2.5	247444	1.5	-0.49	1.09E+10	0.317
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	448.438	16875	2.5 4.5	239755	5.5 5.5	-0.94	7.72E+09	-0.114 0.294
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	448.722	56772	2.5	279627	3.5	-0.06	2.91E + 10	-0.508
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	449.116	20442	3.5	243102 246978	3.5	-0.98	3.48E+09 4.84E+09	0.119 0.203
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	449.712	26368	4.5	248732	4.5	-0.86	4.55E+09	0.073
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	449.865	26368	4.5	248657	3.5	-0.72	6.32E + 09	-0.136
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	449.876 450.217	22532 36594	5.5 3.5	244816 258709	$\frac{5.5}{2.5}$	0.54 -0.85	1.14E+11 4.62E+09	0.651 0.101
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	450.331	24361	2.5	246420	1.5	-0.93	3.86E + 09	0.16
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	450.389	20442	3.5	242473	2.5	-0.96	3.63E+09	0.136
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	450.851	24599 21571	1.5	240451 243374	2.5	-0.95	8.32E+09	-0.18
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	451.588	22532	5.5	243973	4.5	-0.86	4.51E + 09	-0.12
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	451.647	36594 34635	3.5	258006 255752	3.5	-0.35	1.47E+10 9.85E-00	0.322 0.172
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	452.317	16875	$\frac{2.5}{4.5}$	237959	$\frac{2.5}{4.5}$	-0.52	2.06E+10	-0.322
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	452.489	21571	1.5	242570	1.5	-0.92	3.93E + 09	0.128
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	452.543 452.943	$55041 \\ 20442$	1.5 3.5	276015 241221	2.5 3.5	-0.25 -0.64	1.86E+10 7.45E+09	-0.392 0.252
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	453.062	14204	1.5	234925	2.5	-1	3.27E+09	0.114
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	454.105	20442	3.5	240655	4.5	-0.83	4.78E+09	0.156
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	404.172 455.284	55041	$^{4.0}_{1.5}$	220181 274684	3.5 2.5	-0.63 -0.55	7.55E+09 9.03E+09	-0.387
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	455.417	21571	1.5	241150	2.5	-0.9	4.07E + 09	0.144
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	455.774	$34635 \\ 56772$	2.5	254042 276015	$\frac{3.5}{2.5}$	-0.52	9.79E+09 4.13E±00	0.23
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	456.205	56772	2.5	275972	$\frac{2.5}{1.5}$	-0.68	6.65E+09	-0.127
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	456.29	36594	3.5	255753	2.5	-0.9	4.05E + 09	0.176
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	456.537	16875 14800	4.5 2.5	235915	5.5 3.5	-0.87 -0.92	4.31E+09 3.89E±09	-0.141
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	456.595	24361	2.5	243374	2.5	-0.79	5.18E + 09	-0.13
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	456.918	16875	4.5	235733	4.5	-0.35	1.44E + 10	-0.285
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	456.932 457.163	36594 24361	3.5 2.5	255445 243102	3.5 3.5	-0.37 -0.54	1.38E+10 9.12E+09	-0.408 0.249
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	457.784	22532	5.5	240975	6.5	-0.62	7.73E + 09	0.71
L 900,004 00772 2.0 274798 3.5 -0.71 6.938-100 0.359	458.276	24361	2.5	242570	1.5	-0.84	4.63E+09	-0.189
459.309 21571 1.5 239289 0.5 -0.58 $8.38E+09$ 0.307	459.309	21571	2.5 1.5	∠(4(98 239289	3.5 0.5	-0.71 -0.58	0.23E+09 8.38E+09	$0.352 \\ 0.307$
244			~	244				

Table A38: Continued

Wavelength	Lower Level	June	Upper level	Ju	log gf	σA	CF
459 534	34635	2.5	252246	25^{0}	-0.85	$4.45E \pm 0.9$	-0.108
459 749	0	4.5	217510	4.5	-0.45	$1.13E \pm 10$	-0.313
460 357	22532	5.5	239755	5.5	-0.40	$5.09E \pm 09$	0.198
400.337	22002	4.5	217208	2.5	-0.15	0.09 ± 10	0.138
400.389	20124	4.0	217208	0.0	-0.10	2.20E+10	-0.312
460.472	30134	1.5	247303	2.5	-0.84	4.58E + 09	0.295
461.128	24361	2.5	241221	3.5	-0.71	6.08E+09	-0.341
461.602	56772	2.5	273409	3.5	-0.99	3.22E + 09	-0.173
461.914	3691	3.5	220181	3.5	-0.78	5.23E + 09	-0.141
462.212	55041	1.5	271392	1.5	-0.77	5.34E + 09	0.183
463.073	14899	2.5	230848	3.5	-0.9	3.95E + 09	-0.145
463.382	34635	2.5	250440	2.5	-0.51	9.72E + 09	-0.141
463.449	16875	4.5	232648	4.5	-0.95	$3.49E \pm 0.09$	0.051
463 658	5816	2.5	221492	2.5	-0.84	$4.52E \pm 0.9$	-0.168
463 744	24361	2.5	230008	2.5	0.02	$3.72E \pm 0.0$	0.14
403.744	24301	1.5	200000	1.5	-0.32	$3.12D \pm 0.03$	-0.14
403.842	7097	1.0	222000	1.5	-0.9	3.94E+09	-0.188
464.534	3691	3.5	218960	2.5	-0.51	9.49E+09	-0.279
464.742	55041	1.5	270214	2.5	-0.97	3.33E+09	0.368
465.298	0	4.5	214916	3.5	-0.98	3.19E + 09	0.239
466.023	55041	1.5	269623	1.5	-0.78	5.12E + 09	-0.253
466.662	26368	4.5	240655	4.5	-0.78	5.05E + 09	0.069
467.481	3691	3.5	217603	2.5	-0.68	6.31E + 09	0.284
467.592	34635	2.5	248496	1.5	-0.88	4.02E + 09	0.246
467.978	5816	2.5	219501	1.5	-0.47	$1.04E \pm 10$	-0.305
468.347	3691	3.5	217208	3.5	-0.79	$4.89E \pm 0.09$	0.249
468 51	56772	2.5	270214	2.5	-0.31	$1.48E \pm 10$	-0.35
469 614	7097	1.5	220038	0.5	-0.6	$7.57E \pm 0.09$	-0.319
470 216	24625	2.5	247258	2.5	0.08	2.17E+00	0.227
470.010	7007	1.5	247200	1.5	-0.98	$3.17E \pm 0.0$	0.237
470.802	1091	1.5	219301	1.0	-0.98	3.17E+09	0.275
470.894	0	4.5	212302	4.5	-0.83	4.48E+09	-0.305
470.947	30134	1.5	242473	2.5	-0.66	6.55E+09	0.235
471.391	36594	3.5	248732	4.5	-0.41	1.18E + 10	0.495
472.955	56772	2.5	268208	2.5	-0.28	1.58E + 10	-0.318
472.96	22532	5.5	233966	6.5	-0.66	6.47E + 09	0.661
473.191	16875	4.5	228206	4.5	-0.95	3.37E + 09	-0.095
473.421	14899	2.5	226128	1.5	-0.67	6.45E + 09	-0.205
473.851	0	4.5	211037	3.5	-0.55	8.35E + 09	-0.29
474.086	36594	3.5	247526	4.5	-0.52	8.86E + 0.9	-0.307
474 542	14204	1.5	224934	0.5	-0.62	$7.11E \pm 0.0$	-0.44
474 832	55041	1.5	265642	1.5	-0.47	9.95E±00	-0 494
474.032	56779	1.5	205042	1.5	-0.47	5.55D+05	0.997
474.930	50772	2.0	207327	2.5	-0.71	5.70E+09	-0.387
470.200	005041	1.5	203034	1.5	-1	2.97E+09	0.215
476.684	36594	3.5	246376	4.5	-0.72	5.64E + 09	-0.261
478.606	14899	2.5	223840	1.5	-0.97	3.14E + 09	-0.116
481.302	14204	1.5	221974	2.5	-0.93	3.43E + 09	0.162
481.426	3691	3.5	211407	2.5	-0.91	3.56E + 09	-0.19
482.917	14899	2.5	221974	2.5	-0.26	1.58E + 10	-0.34
483.623	17067	0.5	223840	1.5	-0.89	3.64E + 09	0.168
485.459	34635	2.5	240625	3.5	-0.43	$1.06E \pm 10$	-0.369
488.387	14204	1.5	218960	2.5	-0.94	3.23E + 0.9	-0.241
491 974	36594	3.5	239857	4.5	-0.82	$4.20E \pm 0.09$	-0.34
404 206	1/800	2.5	217208	3.5	0.82	4.20E + 0.00	0.303
434.230	171520	2.5 C E	217200	5.5	-0.82	4.14D + 0.00	-0.303
904.550	171550	0.5	275205	5.5	-0.89	9.236+08	-0.344
1017.47	172070	5.5	270353	4.5	-0.92	7.82E+08	-0.423
1021.198	198329	4.5	296253	3.5	-0.85	8.95E+08	0.369
1061.668	199048	3.5	293239	2.5	-0.99	6.09E + 08	0.335
1062.212	181872	2.5	276015	2.5	-0.91	7.35E + 08	-0.189
1127.294	165334	4.5	254042	3.5	-0.81	8.20E + 08	-0.221
1127.679	199048	3.5	287725	2.5	-0.81	8.20E + 08	-0.552
1146.242	161491	5.5	248732	4.5	-0.45	1.81E + 09	0.494
1147.564	170865	4.5	258006	3.5	-0.74	9.17E + 08	0.516
1150.248	135036	3.5	221974	2.5	-0.88	6.72E + 08	-0.434
1150.581	160023	3.5	246935	2.5	-0.88	$6.58E \pm 08$	-0.259
1154 414	181639	3.5	268263	3 5	-0.88	$6.63E \pm 08$	-0.229
1157 492	189621	2.5	276015	2.5	-0.7	$9.92E \pm 08$	-0.511
1157 597	191972	2.5	268262	2.5	0.87	6.70E+08	0.281
1161 516	170865	2.5	208203	3.5	-0.87	5.10E+08	0.281
1101.010	101000	4.5	200909	4.5	-0.98	5.19E+08	-0.269
1108.873	181639	3.5	267191	4.5	-0.78	8.09E+08	0.168
1173.91	188224	4.5	273409	3.5	-0.69	9.82E + 08	-0.192
1174.034	189621	2.5	274798	3.5	-0.6	1.21E + 09	-0.588
1174.473	135036	3.5	220181	3.5	-0.69	9.92E + 08	0.557
1177.442	186288	1.5	271218	2.5	-0.94	5.53E + 08	0.25
1178.5	189944	3.5	274798	3.5	-0.71	9.34E + 08	0.132
1179.735	132745	4.5	217510	4.5	-0.65	1.08E + 09	0.76
1180.806	156798	5.5	241486	4.5	-0.82	7.24E + 08	0.134
1182.313	170865	4.5	255445	3.5	-0.65	1.07E + 09	-0.359
1183.957	132745	4.5	217208	3.5	-0.28	2.50E + 09	-0.592
1185.812	156645	6.5	240975	6.5	-0.35	2.14E + 09	0.726
1186.064	160704	1.5	245016	0.5	-0.89	$6.12E \pm 0.08$	-0.313
1186.34	156155	4.5	240448	3.5	-1	$4.75E \pm 0.8$	-0.079
1187 964	156798	5.5	240975	6.5	-0.98	$5.00E \pm 0.8$	-0.05
1100.99	166467	9.5 9.5	250484	9.5 9.5	_0.80	6 10 - 00	0.00
1101 56	195096	0.0 2 K	218060	0.0 0 K	_0.09	0.1017-00	-0.25
1102.00	156700	0.0 5 F	210900	4.0 5 F	-0.7	5.50E+00	-0.204
1102 404	106401	0.0	240074	0.0 1 E	-0.91	J.19E+U8	0.212
1192.484	130401	2.5	220200	1.0	-0.99	4.795+08	-0.10
1193.602	136401	2.5	220181	3.5	-0.72	8.94E+08	0.372
1196.174	196027	3.5	279627	3.5	-0.93	5.50E + 08	0.052
1196.616	188224	4.5	271793	4.5	0.13	6.30E + 09	0.723
1198.107	189944	3.5	273409	3.5	-0.1	3.67E + 09	0.639
1198.347	164078	4.5	247526	4.5	-0.93	5.40E + 08	-0.147
1198.861	164032	2.5	247444	1.5	-0.96	5.12E + 08	0.249
1199.064	165334	4.5	248732	4.5	-1	4.68E + 08	0.065
1199.975	186288	1.5	269623	1.5	-0.96	5.12E + 08	0.241
1200.12	161491	5.5	244816	5.5	-0.92	5.64E + 08	-0.106
1200.897	190694	2.5	273966	2.5	-0.34	2.12E + 09	0.574
1202.227	159923	2.5	243102	3.5	-0.94	5.25E + 08	0.269
1202.271	175533	3.5	258709	2.5	-0.85	$6.65E \pm 0.8$	-0.563
1203 229	156645	6.5	239755	5.5	-0.43	$1.69E \pm 00$	-0.301
1205 445	156798	5.5	239755	5.5	-0.9	$5.79E \pm 0.8$	0.105
1205.440	156009	0.0 2 K	233133	0.0 1 K	-0.9	1 12E - 00	-0.200
1200.470	1750902	0.0 1 F	203001	4.J 9 F	-0.01	5 800 109	0.202
1203.970	127250	4.0	200000	3.0	-0.9	0.09E+U8	-0.230
1206.129	164070	1.0	220200	1.0	-0.32	2.17E+09	0.089
1200.204	104078	4.5	240978	3.0	-0.44	1.075+09	-0.423
1206.292	188494	1.5	271392	1.5	-0.37	1.98E+09	0.659
1208.836	188494	1.5	271218	2.5	-0.74	8.34E+08	-0.651
1208.978	190694	2.5	273409	3.5	-0.2	2.84E + 09	0.634
1210.397	164685	3.5	247303	2.5	-0.37	1.92E + 09	-0.364

Table A38: Continued

Wavelength	Lower Level	JLow	Upper level	J _{Un}	log gf	gA	CF
1211.146	135036	3.5	217603	2.5°	-0.79	7.29E + 08	-0.114
1211.255	136401	2.5	218960	2.5	-0.29	2.33E + 09	0.671
1212.512	135036	3.5	217510	4.5	-0.2	2.86E + 09	0.499
1212.518	163052	3.5	258006	3.0 1.5	-0.9	$5.80E \pm 08$ 7.60E \pm 08	0.528
1212.394	160125	1.5	240420	1.5	-0.78	5.70E+08	-0.341 0.243
1214.391	137914	0.5	220260	1.5	-0.51	1.40E+09	-0.518
1216.973	135036	3.5	217208	3.5	-0.61	1.10E + 09	0.469
1216.974	132745	4.5	214916	3.5	-0.53	1.33E + 09	-0.141
1217.106	168322	3.5	250484	3.5	-0.36	1.97E + 09	0.451
1217.585	188224	4.5	270353	4.5	-0.21	2.79E + 09	-0.449
1218.869	156902	3.5	238945	3.5	-0.58	1.19E + 09	0.176
1219.341	159923	2.5	241934	1.5	-0.87	6.10E + 08	-0.397
1219.834	167527	2.5	240010	1.0	-0.50	$1.22E \pm 09$ 5.20E \pm 08	-0.334
1220.536	165595	5.5	247526	4.5	-0.61	1.11E+09	0.349
1220.696	186288	1.5	268208	2.5	-0.42	1.70E + 09	0.715
1222.146	196027	3.5	277850	4.5	-0.36	1.97E + 09	0.678
1222.959	160704	1.5	242473	2.5	-0.79	7.20E + 08	0.366
1223.679	188494	1.5	270214	2.5	-0.99	4.54E + 08	0.607
1224.059	164685	3.5	254042	3.3 4 5	-0.29	2.28E+09 6.10E+08	-0.474
1224.127	188224	4.5	269890	3.5	-0.99	$4.56E \pm 08$	0.102
1225.54	189621	2.5	271218	2.5	-0.12	3.35E+09	0.569
1225.682	137914	0.5	219501	1.5	-0.55	1.25E + 09	0.678
1227.128	178946	2.5	260437	3.5	-0.96	4.86E + 08	0.243
1230.049	198329	4.5	279627	3.5	-0.5	1.41E + 09	-0.31
1230.407	189944	3.5	271218	2.5	-0.86	6.06E + 08	-0.105
1230.418	150226	2.5	250440	2.5	-0.79	1.10E + 08 1.76E + 00	0.192
1231.197	136401	2.5	217603	2.5	-0.4	$5.93E \pm 08$	0.094
1231.559	160023	3.5	241221	3.5	-0.72	8.48E + 08	-0.244
1231.586	156155	4.5	237351	3.5	-0.64	1.00E + 09	-0.227
1232.123	156798	5.5	237959	4.5	-0.76	7.58E + 08	0.37
1232.588	167527	2.5	248657	3.5	-0.88	5.82E + 08	0.361
1232.632	160023	3.5	241150	2.5	-0.79	7.13E + 08	0.499
1233.011	164078	4.5	245180	5.5 4 E	-0.55	1.24E + 09 2.12E + 00	0.192
1233.92	186288	4.5	240370	4.5 2.5	-0.31	2.13E+09 2.42E+09	-0.667
1235.14	156902	3.5	237864	2.5	-0.18	2.42E + 0.00 2.87E + 0.00	-0.493
1235.591	170865	4.5	251798	5.5	-0.63	1.01E + 09	0.299
1235.81	181639	3.5	262557	4.5	-0.77	7.47E + 08	-0.096
1236.002	156445	2.5	237351	3.5	-0.72	8.34E + 08	0.56
1236.364	160125	1.5	241007	1.5	-0.79	6.99E + 08	0.221
1237.907	165595	5.5	246376	4.5	-0.77	7.46E + 08	0.365
1239.393	150226	0.5	200300	1.5	-0.25	$2.47E \pm 09$ $2.30E \pm 09$	-0.092
1240.227	160023	4.5 3.5	240625	4.5 3.5	-0.28	$6.22E \pm 08$	0.362
1240.798	189621	2.5	270214	2.5	-0.85	6.19E + 08	-0.236
1241.014	199048	3.5	279627	3.5	0.18	6.63E + 09	0.715
1241.795	159226	4.5	239755	5.5	-0.53	1.26E + 09	0.208
1242.056	166467	3.5	246978	3.5	-0.87	5.81E + 08	0.131
1242.068	175242	1.5	255753	2.5	-0.56	1.20E+09 1.15E+00	-0.485
1243.014	160704	1.5	241150	2.5	-0.97	$4.58E \pm 08$	-0.18
1243.39	160023	3.5	240448	3.5	-0.54	1.26E + 09	0.467
1243.622	168322	3.5	248732	4.5	-0.12	3.25E + 09	-0.518
1243.636	189944	3.5	270353	4.5	-0.46	1.49E + 09	0.609
1244.791	168322	3.5	248657	3.5	-0.72	8.25E + 08	-0.269
1245.20	164032	2.5	244330	1.0	-0.98	4.54E + 08 8 75E + 00	0.27
1245.788	189944	3.5	270214	2.5	-0.78	$7.19E \pm 08$	-0.482
1245.836	171530	6.5	251798	5.5	-0.54	1.22E + 09	-0.393
1246.058	137350	1.5	217603	2.5	-0.09	3.47E + 09	-0.729
1246.575	175533	3.5	255753	2.5	0	4.30E + 09	-0.656
1247.373	132745	4.5	212914	5.5	0.54	1.48E + 10	-0.855
1248.134	181872	2.5	261991	2.5	-0.31	2.10E + 09	0.415
1248.179	190694	2.5	270766	3.5	-0.25	$2.41E \pm 09$	0.09
1249.388	188224	4.5	268263	3.5	-0.74	7.75E+08	0.473
1249.713	186288	1.5	266306	1.5	-0.6	1.06E + 09	0.477
1249.97	189621	2.5	269623	1.5	-0.53	1.27E + 09	-0.401
1250.075	161491	5.5	241486	4.5	-0.6	1.07E + 09	-0.271
1250.189	196027	3.5	276015	2.5	-0.81	6.60E + 08	0.199
1250.541	167527	1.0 2.5	240082 247444	2.0 1.5	-0.02	1.02E+09 5.49E+08	-0.408
1251.378	175533	3.5	255445	3.5	-0.92	5.14E+08	-0.403
1251.413	166467	3.5	246376	4.5	-0.96	4.71E + 08	0.106
1251.884	135036	3.5	214916	3.5	-0.65	9.57E + 08	0.096
1251.989	160125	1.5	239998	2.5	-0.82	6.45E + 08	-0.206
1252.408	165334	4.5	245180	5.5	-0.9	5.36E + 08	-0.085
1253.722	178946	2.5	258709	2.5	-0.21	$2.58E \pm 09$	0.381
1253.701	165334	4.5	245073	3.5	-0.13	$5.21E \pm 0.09$ $5.02E \pm 0.08$	0.341
1254.213	167527	2.5	247258	3.5	0.04	4.62E + 09	-0.746
1254.276	172070	5.5	251798	5.5	-0.24	2.42E + 09	0.679
1255.978	170865	4.5	250484	3.5	-0.84	6.13E + 08	0.36
1256.333	159923	2.5	239519	2.5	-0.47	1.42E + 09	-0.538
1256.515	165595	5.5 ₄ ⊑	245180	5.5 4 E	-0.05	3.72E+09	0.621
1257 590	108330	4.0 4.5	2007030 277850	4.5	-0.92	0.12E+08 8.30E⊥00	0.093
1257.545	190694	2.5	270214	2.5	-0.39	1.71E + 0.9	0.634
1258.101	161491	5.5	240975	6.5	0.02	4.41E + 09	-0.244
1258.389	179242	1.5	258709	2.5	-0.37	1.78E + 09	-0.533
1258.626	167527	2.5	246978	3.5	-0.84	6.13E+08	0.226
1259.308	167527	2.5	246935	2.5	-0.26	2.29E+09	0.419
1209.032	167079	1.0	239319 247302	2.0 2.5	-0.3 K	4.19E+08 1 90E-00	-0.123
1260.043	172070	1.0 5.5	251386	4.5	-0.33	$1.91E \pm 09$	0.029 0.733
1262.295	165595	5.5	244816	5.5	0.14	5.72E + 0.09	0.571
1262.561	168322	3.5	247526	4.5	0.1	5.23E + 09	-0.715
1262.701	190694	2.5	269890	3.5	-0.77	7.03E + 08	-0.545
1263.948	156798	5.5	235915	5.5	-0.05	3.71E+09	0.554
1264.705	164032	2.5	243102	3.5 9 E	-0.66	9.18E+08	0.562
1265.466	159923	2.5	238945	3.5	-0.68	8.68E+08	0.518
Table A38: Continued

Wavelength 1265.791	Lower Level 216023	J _{Low} 1.5	Upper level 295025	J_{Up} 0.5	log gf -0.37	gA 1.80E+09	CF -0.719
1265.829	188494	1.5	267493	0.5	-0.41	1.61E + 09	-0.749
1266.137 1266.512	156902 167978	$\frac{3.5}{1.5}$	235882 246935	$\frac{3.5}{2.5}$	-0.92 -0.42	5.03E+08 1.60E+09	0.129 -0.674
1266.52	171530	6.5	250487	6.5	0.52	1.37E + 10	0.711
1266.849	168322	3.5	234042 247258	3.5 3.5	-0.68	8.77E+08	0.384 0.121
1266.968 1267.193	190694 215970	2.5 2.5	269623 294884	1.5 1.5	-0.77 -0.28	6.98E+08 2.17E+09	0.587 -0.409
1268.044	216023	1.5	294884	1.5	-0.35	1.84E + 09	0.774
$1268.464 \\ 1268.536$	$156155 \\ 156902$	$\frac{4.5}{3.5}$	$234991 \\ 235733$	$\frac{4.5}{4.5}$	-0.24 -0.8	2.39E+09 6.59E+08	$0.311 \\ -0.144$
1268.582	161491	5.5	240319	6.5	-0.56	1.16E + 09	-0.178
1268.992 1269.058	181639	3.5 3.5	260437	$^{4.5}_{3.5}$	-0.56	5.07E+09	-0.334 0.566
1269.509 1269.546	196027 156902	3.5	274798 235670	3.5	0.08	4.97E+09 6.86E+08	-0.647
1270.498	156645	6.5	235354	6.5	-0.15	2.94E+09	0.307
$1271.352 \\ 1271.592$	$168322 \\ 189621$	$\frac{3.5}{2.5}$	$246978 \\ 268263$	3.5 3.5	-0.71 -0.32	8.10E+08 1.99E+09	$0.246 \\ -0.505$
1271.632	165334	4.5	243973	4.5	-0.73	7.58E + 08	-0.55
1271.905 1272.155	166467	2.5	257568 245073	1.5 3.5	-0.72	1.66E+09	-0.311
1272.82	181872 156798	2.5	260437 235354	3.5 6.5	-0.62	9.95E + 08 1.09E + 10	-0.393
1273.376	159226	4.5	237758	5.5	-0.14	2.96E+09	0.439
1273.642 1274.332	$136401 \\ 167978$	2.5 1.5	214916 246451	$3.5 \\ 0.5$	$0.15 \\ -0.65$	5.76E+09 9.18E+08	-0.821 -0.618
1274.821	181872	2.5	260314	1.5	-0.14	2.99E+09	-0.744
1274.827 1274.847	$167978 \\ 164032$	$\frac{1.5}{2.5}$	$246420 \\ 242473$	$1.5 \\ 2.5$	-0.47 -0.5	1.40E+09 1.32E+09	$0.505 \\ -0.535$
1275.222	156445	2.5	234863	3.5	0.17	6.06E+09	-0.752
1275.245 1275.247	164685	3.5	243102	3.5	-0.23	2.43E+09 8.97E+08	-0.832
1275.867 1276.476	$165595 \\ 172070$	5.5 5.5	243973 250411	$4.5 \\ 4.5$	-0.98 0.12	4.30E+08 5.33E+09	0.439
1276.709	179242	1.5	257568	1.5	-0.72	7.60E + 08	-0.471
1276.833 1276.86	$189944 \\ 156155$	$\frac{3.5}{4.5}$	$268263 \\ 234472$	$3.5 \\ 5.5$	-0.29 0.12	2.10E+09 5.35E+09	$0.327 \\ 0.757$
1277.273	132745	4.5	211037	3.5	-0.84	5.84E + 08	0.217
1277.335 1277.723	161491	5.5 5.5	250358 239755	5.5 5.5	-0.03	9.62E+09 3.83E+09	-0.598
1277.877	181872	2.5	260126	2.5	-0.2	2.61E+09	0.629
1279.813	169166	2.5	247303	2.5	-0.78	6.78E + 08	0.41
1280.52 1280.59	$172346 \\ 156902$	3.5 3.5	250440 234991	2.5 4.5	-0.36 -0.54	1.80E+09 1.17E+09	-0.526 -0.407
1280.989	172346	3.5	250411	4.5	-0.78	6.71E + 0.08	0.115
$1282.354 \\ 1283.051$	$163952 \\ 198033$	$0.5 \\ 1.5$	$241934 \\ 275972$	$1.5 \\ 1.5$	-0.84 -0.06	5.85E+08 3.55E+09	$0.386 \\ 0.708$
1283.061	196027	3.5	273966	2.5	-0.48	1.35E+09	0.599
1283.106 1284.234	170865	3.5 4.5	237959 248732	4.5 4.5	-0.14	2.92E+09 3.99E+09	-0.746
1284.663	160023	3.5	237864	2.5	-0.96	4.41E+08	-0.132
1284.899	156155	4.5	233938	3.5	-0.88	5.38E+08	0.499 0.176
1285.863 1286.349	$169166 \\ 160125$	2.5 1.5	246935 237864	2.5 2.5	-0.95 -0.51	4.53E+08 1.24E+09	$0.34 \\ 0.621$
1286.912	189621	2.5	267327	2.5	-0.94	4.63E + 08	0.107
1287.634 1288.713	197022 163952	2.5	$274684 \\ 241549$	$2.5 \\ 0.5$	0.14 -1	4.06E+08	$0.732 \\ 0.34$
1289.186	190694	2.5	268263	3.5	-0.61	9.83E+08	-0.568
1289.755 1290.09	190694	2.5	268208	$\frac{4.5}{2.5}$	-0.73	1.07E+08 1.07E+09	-0.402
1291.512 1291.854	159923 164078	2.5 4 5	237351 241486	3.5	-0.57 -0.38	1.07E+09 1.65E+09	0.35 0.257
1292.28	189944	3.5	267327	2.5	-0.28	2.11E + 09	0.526
1292.29 1293.233	196027 135036	$3.5 \\ 3.5$	273409 212362	$\frac{3.5}{4.5}$	-0.47 0.35	1.37E+09 8.80E+09	0.282 -0.857
1293.308	156645	6.5	233966	6.5	0.03	4.28E+09	0.766
1294.177 1294.544	189944	2.5	293239 267191	4.5	-0.98	4.20E+08 3.70E+09	-0.425
1295.065 1295.525	216023 164032	1.5 2.5	293239 241221	2.5 3.5	0.13	5.38E+09 4 18E+08	-0.763 0.176
1295.681	156445	2.5	233625	2.5	-0.28	2.06E+09	-0.555
$1296 \\ 1296.425$	$179242 \\ 179242$	$1.5 \\ 1.5$	$256402 \\ 256377$	$0.5 \\ 1.5$	-0.54 -0.6	1.14E+09 9.91E+08	-0.601 -0.41
1297.522	181639	3.5	258709	2.5	-0.73	7.41E + 08	-0.484
1298.398 1299.253	199048	4.5	276015	2.5	-0.06	3.42E+09	-0.836
1299.349 1300.27	160704 166467	1.5 3.5	237665 243374	1.5 2.5	-0.87 -0.27	5.30E+08 2.14E+09	0.338
1300.537	156798	5.5	233689	4.5	-0.52	1.20E+09	-0.247
1300.803 1301.343	198329 169166	$\frac{4.5}{2.5}$	275205 246010	5.5 1.5	0.5 - 0.59	1.26E+10 1.01E+09	-0.834 -0.513
1301.892	156155	4.5	232966	5.5	-0.65	8.91E+08	-0.105
1301.919 1302.077	167527 164685	$\frac{2.5}{3.5}$	244336 241486	$1.5 \\ 4.5$	-0.67 0.11	8.38E+08 5.02E+09	-0.395 -0.734
1303.574 1304.441	175085 170865	4.5	251798 247526	5.5 4.5	0.33	8.32E+09 3.00E+09	-0.782 0.652
1304.592	156645	6.5	233297	7.5	0.66	1.78E+10	-0.899
$1305.066 \\ 1305.546$	$175622 \\ 164078$	$2.5 \\ 4.5$	$252246 \\ 240674$	$2.5 \\ 5.5$	-0.61 0.32	9.60E+08 8.23E+09	0.232 -0.852
1305.861	164078	4.5	240655	4.5	-0.17	2.64E + 09	-0.449
1306.588 1306.95	164685 160704	$3.5 \\ 1.5$	241221 237218	$\frac{3.5}{0.5}$	-0.31 -0.64	1.91E+09 8.90E+08	0.361 -0.515
1307.215	178946	2.5	255445	3.5	-0.32	1.87E+09	0.647
1308.023 1309.132	104032 197022	2.5 2.5	240448 273409	3.5 3.5	-0.43 -0.64	1.45E+09 8.86E+08	-0.697
1309.144	172346 164078	3.5 4 5	248732 240448	4.5	-0.86	5.39E + 08 9.80E ± 08	-0.254 0.274
1309.706	167021	4.5	243374	2.5	-0.41	1.50E+08 1.50E+09	-0.586
1310.439 1310.607	$172346 \\ 175085$	$3.5 \\ 4.5$	248657 251386	$3.5 \\ 4.5$	-0.9 0.27	4.92E+08 7.25E+09	$0.309 \\ 0.669$
$1311.183 \\ 1311.918$	$161491 \\ 156155$	$5.5 \\ 4.5$	$237758 \\ 232379$	5.5 3.5	0.13 -0.36	5.27E+09 1.69E+09	$0.671 \\ -0.479$

Table A38: Continued

Wavelength	Lower Level	JLow	Upper level	J_{Un}	log gf	gA	CF
1312.234	171713	0.5	247919	0.5^{-1}	-0.76	6.80E + 08	-0.609
1312.803	159923	2.5	236095	1.5	-0.73	7.20E + 08	-0.36
1312.879	156798	5.5	232966	5.5	-0.31	1.90E+09	0.276
1313.103	100334	4.5	241480	4.0	-0.76	0.07E+08 $4.59E\pm08$	0.313 0.177
1315 783	135036	3.5	211037	3.5	-0.92	3.01E+09	-0.177
1316.295	160125	1.5	236095	1.5	-0.45	1.37E + 0.9	0.475
1316.493	159923	2.5	235882	3.5	-0.77	6.59E + 08	0.187
1316.93	156445	2.5	232379	3.5	-0.54	1.10E + 09	-0.606
1316.952	198033	1.5	273966	2.5	-0.15	2.72E + 09	-0.653
1317.403	169166	2.5	245073	3.5	-0.59	9.78E+08	0.448
1317.752	105334	4.5	241221	3.5	-0.9	4.89E+08	-0.153
1318 385	156798	5.5	231580	4.5	-0.03	$1.64E \pm 09$	-0.598
1319.86	196027	3.5	271793	4.5	-0.5	1.04E+0.9 1.22E+0.9	-0.179
1319.881	159226	4.5	234991	4.5	-0.89	4.91E + 08	-0.083
1319.994	146216	3.5	221974	2.5	-0.04	3.55E + 09	-0.558
1320.132	199048	3.5	274798	3.5	-0.47	1.31E + 09	0.174
1320.831	160023	3.5	235733	4.5	-0.22	2.29E + 09	0.568
1321.404	164078	4.5	239755	5.5	-0.85	5.40E + 08	0.257
1323.63	167021	1.5	242570	1.5	-0.67	8.03E+08	0.374
1320.020	165505	2.5	265034	1.5	-0.45	$1.30E \pm 0.00$	-0.611
1327 639	165334	4.5	240975	4.5	-0.07	$3.18E \pm 09$	-0.304 0.625
1327.662	181639	3.5	256959	4.5	0.34	8.34E+09	-0.789
1328.168	165334	4.5	240625	3.5	-0.6	9.54E + 08	0.402
1328.499	175085	4.5	250358	5.5	-0.05	3.40E + 09	0.756
1328.974	159226	4.5	234472	5.5	-0.2	2.37E + 09	-0.34
1329.824	175242	1.5	250440	2.5	-0.72	7.16E + 08	0.463
1330.277	148667	2.5	223840	1.5	-0.35	1.67E + 09	-0.543
1330.297	164685	3.5	239857	4.5	-0.59	9.76E+08	-0.154
1330.321	165505	2.0	244330	1.0	-0.79	$0.13E \pm 0.00$	-0.277
1332 255	165595	5.5	240674	4.5	-0.74	$6.86E \pm 08$	0.342
1332.413	168322	3.5	243374	2.5	-0.88	4.99E + 08	0.328
1332.553	167527	2.5	242570	1.5	-0.76	6.51E + 08	-0.333
1333.234	136401	2.5	211407	2.5	-0.21	2.28E + 09	-0.565
1333.298	159923	2.5	234925	2.5	-0.76	6.57E + 08	0.278
1333.904	160023	3.5	234991	4.5	-0.57	1.01E + 09	0.351
1334.107	172346	3.5	247303	2.5	-0.91	4.60E + 08	-0.351
1334.264	190694	2.5	265642	1.5	-0.4	1.48E + 09 7.40E + 08	-0.75
1334.390	159925	2.5	234803	0.5	-0.7	$7.49E \pm 08$ 8 75E ± 08	0.557
1334.015	167021	1.5	241934	1.5	-0.03	$3.90E \pm 08$	0.186
1334.88	164032	2.5	238945	3.5	-0.32	1.78E + 09	-0.481
1334.909	172346	3.5	247258	3.5	-0.75	6.64E + 08	0.341
1335.08	160023	3.5	234925	2.5	-0.49	1.21E + 09	-0.337
1335.502	175533	3.5	250411	4.5	-0.06	3.29E + 09	-0.706
1335.789	175622	2.5	250484	3.5	0.05	4.17E + 09	-0.738
1336.18	160023	3.5	234863	3.5	-0.73	6.90E + 08	-0.373
1330.293	104080	3.5	239519	2.5	-0.5	1.18E+09	-0.393
1337 261	168322	2.5	243102	2.5	-0.91	$4.08E \pm 08$ 5.62E \pm 08	-0.377
1337.721	166467	3.5	241221	3.5	-0.82	$5.69E \pm 08$	0.123
1337.984	196027	3.5	270766	3.5	-0.68	7.72E + 08	-0.182
1338.258	165595	5.5	240319	6.5	-0.35	1.67E + 09	-0.322
1338.566	171713	0.5	246420	1.5	-0.77	6.41E + 08	0.414
1338.815	156155	4.5	230848	3.5	-0.81	5.73E + 08	-0.145
1339.84	136401	2.5	211037	3.5	-0.25	2.06E+09	-0.447
1339.91	172346	3.5	246978	3.5	-0.33	1.75E+09	0.5
1340.023	159226	1.5	242570	1.5	-0.83	$3.32E \pm 0.00$ $3.48E \pm 0.00$	0.233
1343.707	165334	4.5	239755	5.5	-0.07	3.15E+09	-0.492
1344.63	197022	2.5	271392	1.5	-0.51	1.14E + 09	0.637
1344.854	137350	1.5	211707	1.5	-0.28	1.92E + 09	-0.729
1345.026	171530	6.5	245878	7.5	0.65	1.65E + 10	-0.908
1345.171	190694	2.5	265034	1.5	-0.53	1.09E + 09	-0.408
1345.283	188224	4.5	262557	4.5	-0.24	2.15E+09	-0.731
1343.02	165505	4.0	243180	0.0 4 5	0.19	$1.27E \pm 0.00$	-0.71
1346 629	164685	3.5	238945	3.5	-0.94	4.21E+08	-0.1
1346.946	161491	5.5	235733	4.5	-0.76	6.42E + 08	0.178
1347.553	170865	4.5	245073	3.5	-0.72	7.01E + 08	0.256
1347.911	166467	3.5	240655	4.5	-0.69	7.50E + 08	0.166
1347.936	196027	3.5	270214	2.5	-0.29	1.91E + 09	-0.612
1348.356	163952	0.5	238117	1.5	-0.23	2.17E + 09	-0.796
1348.430	167021	3.5	240625	3.0	-0.75	0.58E+08	-0.248
1349.275	181639	3.5	255753	2.5	-0.47	$3.61E \pm 08$	0.547
1350.176	150869	0.5	224934	0.5	-0.61	9.03E + 08	0.719
1350.313	137350	1.5	211407	2.5	-0.22	2.21E + 09	-0.576
1350.806	172346	3.5	246376	4.5	0.16	5.25E + 09	-0.766
1351.061	159923	2.5	233938	3.5	-0.54	1.07E + 09	-0.597
1351.602	167021	1.5	241007	1.5	-0.76	6.30E + 08	-0.419
1351.742	156155	4.5	230134	4.5	-0.62	8.85E+08	0.192
1351.930	175533	1.0	249210	2.0	-0.91	$4.51E \pm 0.0$ $4.25E \pm 0.0$	0.115
1352.331	156902	3.5	230848	3.5	-0.55	1.04E+09	0.195
1352.538	169166	2.5	243102	3.5	-0.8	5.70E + 08	-0.206
1352.891	160023	3.5	233938	3.5	-0.49	1.18E + 09	0.333
1353.53	164078	4.5	237959	4.5	-0.51	1.14E + 09	-0.345
1354.39	150006	1.5	223840	1.5	-0.67	7.73E+08	0.411
1354.619	137914	0.5	211735	0.5	-0.4	1.44E + 09	-0.833
1355.135	137914	0.5	211707	1.5	-0.46	1.24E+09	-0.656
1356 119	150226	1.0 4 K	292986 232066	1.0 5.5	-0.46	1.24ビ+U9 4 20EJ 00	0.004
1357.469	160023	4.5	233689	4.5	-0.56	$9.84E \pm 08$	-0.402
1357.779	171530	6.5	245180	5.5	-0.82	5.41E + 08	0.598
1358.078	164032	2.5	237665	1.5	-0.55	1.02E + 09	0.598
1358.491	165334	4.5	238945	3.5	-0.81	5.61E + 08	0.631
1358.919	175622	2.5	249210	2.5	-0.02	3.50E + 09	0.693
1359.228	175085	4.5	248657	3.5	-0.08	3.02E+09	-0.731
1359.971	161407	3.5 5 F	239998	2.5 4 F	-0.44	1.335+09	-0.586
1360.544	160125	5.5 1.5	233625 233625	4.0 2.5	-0.27	$4.72E \pm 0.08$	-0.402
1360.589	188494	1.5	261991	2.5	-0.27	1.96E + 09	0.788

Table A38: Continued

Wavelength	Lower Level	JLow	Upper level	J _{Up}	log gf	gA	CF
1361.988	159226	4.5	232648	4.5	-0.85	5.09E + 08	0.159
1362.583	166467	3.5	239857	4.5	-0.01	3.54E+09	-0.671
1363.031	189621	2.5	262987	3.5	0.07	4.22E+09 6.05E+08	-0.556
1363.896	164032	2.5	237351	3.5	-0.78	5.53E+08	0.280
1364.13	148667	2.5	221974	2.5	-0.62	8.68E+08	0.369
1364.53	171530	6.5	244816	5.5	0.1	4.49E + 09	-0.795
1364.75	164078	4.5	237351	3.5	-0.23	2.10E + 09	-0.455
1365.068	156902	3.5	230158	2.5	-0.32	1.71E + 09	-0.569
1365.102	175242	1.5	248496	1.5	-0.33	1.68E + 09	0.624
1365.521	156902	3.5	230134	4.5	-0.12	2.75E+09 5.27E+08	-0.416
1366 518	164685	3.5	246752	4.5 2.5	-0.83	$5.57E \pm 0.08$	-0.388
1366.794	168322	3.5	241486	4.5	-0.72	$6.81E \pm 0.08$	-0.369
1366.994	159226	4.5	232379	3.5	-0.42	1.35E + 09	-0.459
1367.544	175533	3.5	248657	3.5	-0.94	4.16E + 08	-0.181
1367.809	172070	5.5	245180	5.5	-0.99	3.64E + 08	0.108
1368.875	166467	3.5	239519	2.5	-0.91	4.42E + 08	-0.246
1369.055	189944	3.5	262987	3.5	-0.35	1.59E+09	-0.643
1369 782	179242	1.5	252246	2.5	-0.23	$2.06E \pm 0.09$	0.663
1370.208	161491	5.5	234472	5.5	-0.96	3.86E + 08	-0.194
1370.297	167021	1.5	239998	2.5	-0.95	4.02E + 08	0.197
1370.419	150869	0.5	223840	1.5	-0.99	3.66E + 08	-0.654
1371.34	167527	2.5	240448	3.5	-0.7	7.14E + 08	0.31
1371.347	160704	1.5	233625	2.5	-0.44	1.29E+09	-0.515
1371.707	108322	3.5	241221 248496	3.5	-0.83	$5.34E \pm 08$ $4.77E \pm 08$	-0.35
1372.358	197022	2.5	269890	3.5	0.14	4.92E+09	-0.77
1373.098	168322	3.5	241150	2.5	-0.34	1.61E + 09	-0.516
1373.166	148667	2.5	221492	2.5	-0.34	1.62E + 09	-0.791
1374.661	172070	5.5	244816	5.5	-0.62	8.53E + 08	-0.327
1374.665	199048	3.5	271793	4.5	-0.04	3.20E + 09	-0.698
1374.689	146216	3.5	218960	2.5	-0.28	1.88E+09	0.762
1375 853	150006	1.5	222688	1.5	-0.44	$1.29E \pm 09$ 1.16E \pm 09	-0.765
1376.332	156155	4.5	228812	3.5	-0.9	4.50E + 08	-0.201
1376.94	165334	4.5	237959	4.5	-0.4	1.40E + 09	-0.396
1377.156	189944	3.5	262557	4.5	0.09	4.30E + 09	-0.54
1377.399	197022	2.5	269623	1.5	-0.63	8.21E+08	-0.775
1378.995	160125	1.5	232641	1.5	-0.79	5.71E + 08	0.26
1379.337	167021	1.0	239519	2.5	-0.82	$5.24E \pm 08$ $1.00E \pm 00$	0.351
1379.775	161491	5.5	233966	6.5	0.35	$7.76E \pm 09$	0.20
1379.862	167527	2.5	239998	2.5	-0.88	4.67E + 08	0.319
1380.51	198329	4.5	270766	3.5	-0.1	2.75E + 09	-0.734
1380.762	165334	4.5	237758	5.5	-0.02	3.33E+09	-0.649
1381.158	181639	3.5	254042	3.5	-0.74	6.40E+08	-0.564
1381.079	168322	2.0	201991 240682	2.5	-0.66	$9.54E \pm 08$	0.348
1383.733	167021	1.5	239289	0.5	-0.55	9.96E + 08	-0.498
1384.336	170865	4.5	243102	3.5	-0.56	9.47E + 08	-0.424
1384.378	160125	1.5	232359	0.5	-0.45	1.24E + 09	0.755
1385.397	196027	3.5	268208	2.5	-0.72	6.60E + 08	-0.552
1385.612	199048	3.5	271218	2.5	-0.74	6.35E + 08	-0.62
1385.015	181872	2.5	254042 241221	3.5	-0.09	$2.80E \pm 09$ 4.55E \pm 08	-0.66
1388.424	198329	4.5	270353	4.5	-0.68	7.23E+08	-0.655
1388.517	167978	1.5	239998	2.5	-0.83	5.17E + 08	0.436
1389.497	150006	1.5	221974	2.5	-0.76	6.03E + 08	-0.725
1390.094	160704	1.5	232641	1.5	-0.42	1.31E + 09	-0.626
1390.019	150902	3.0 5.5	228812	3.3 4.5	-0.49	1.13E+09 1.37E+09	0.477
1390.96	175085	4.5	246978	3.5	-0.4	5.23E+08	0.389
1391.767	156445	2.5	228296	2.5	-0.17	2.33E + 09	-0.689
1391.972	169166	2.5	241007	1.5	-0.9	4.29E + 08	0.428
1392.033	164078	4.5	235915	5.5	-0.94	3.98E + 08	-0.1
1392.323	175622	2.5	247444	1.5	-0.39	1.40E + 09	-0.595
1392.397	150869	0.5	222688	1.5	-0.18	$2.25E \pm 09$	-0.74
1392.074	215970	4.5 2.5	233882	2.5	-0.57	$4.62E \pm 09$	0.327
1394.214	175533	3.5	247258	3.5	-1	3.42E + 0.08	-0.343
1394.336	199048	3.5	270766	3.5	-0.67	7.39E + 08	-0.276
1394.971	156155	4.5	227841	5.5	-0.34	1.56E + 09	0.468
1395.578	164078	4.5	235733	4.5	-0.49	1.11E+09	0.207
1395.905	164032	2.5	233070	2.5	-0.22	2.09E+09 1.85E+09	0.503
1396.223	159226	4.5	230848	3.5	-0.17	2.33E+09	-0.503 0.647
1396.8	148667	2.5	220260	1.5	-0.72	6.43E + 08	0.77
1397.419	198329	4.5	269890	3.5	-0.57	9.09E + 08	-0.549
1397.8	167978	1.5	239519	2.5	-0.8	5.46E + 08	-0.293
1398.3	169166	2.5	240682	2.5	-0.35	1.53E + 09	0.471
1398.335	148667	2.5	220181	3.5	0.2	5.41E+09	-0.825
1398.751	166467	2.5	237959	4.5	-0.38	1.30E+09	0.428
1398.873	150006	1.5	221492	2.5	-0.03	3.21E + 09	-0.704
1399.075	161491	5.5	232966	5.5	-0.5	1.07E + 09	0.171
1399.404	169166	2.5	240625	3.5	0.05	3.82E + 09	-0.657
1399.67	175533	3.5	246978	3.5	-0.73	6.34E + 08	0.192
1400.401	178946	2.5	250354	4.5 1.5	-0.26	1.84E+09	0.686
1402.41	199048	3.5	270353	4.5	0.09	4.16E + 09	-0.708
1402.438	156902	3.5	228206	4.5	-0.82	5.18E + 08	0.42
1402.532	196027	3.5	267327	2.5	-0.96	3.71E+08	-0.35
1402.652	146216	3.5	217510	4.5 2 E	0.26	6.12E + 09	-0.828
1403.7	179242	2.5 1.5	208203 250440	$\frac{3.5}{2.5}$	-0.03	$4.05E \pm 08$	0.48
1404.561	164685	3.5	235882	3.5	-0.13	2.49E + 0.09	0.516
1404.571	156645	6.5	227841	5.5	0.28	6.40E + 09	-0.835
1405.199	196027	3.5	267191	4.5	0.05	3.79E + 09	0.707
1405.329	161491	5.5	232648	4.5	-0.24	1.96E+09	0.705
1406.189	161872	2.0 1.5	202980 238117	1.5 1.5	-0.94	3.87世+08 4.86日上08	0.403
1407.592	156798	5.5	227841	5.5	-0.39	1.38E+09	0.622
1407.897	159923	2.5	230950	1.5	-0.52	1.02E + 09	0.685
1407.973	156645	6.5	227669	6.5	0.2	5.26E + 09	-0.855

Table A38: Continued

Wavelength	Lower Level	JLow	Upper level	J_{Up}	log gf	gA	CF
1408.26	132745	4.5	203755	4.5	0.4	8.48E + 09	0.88
1408.625	146216	3.5	217208	3.5	0.11	4.36E + 09	0.727
1408.758	104080	3.0 4.5	235670	2.0	-0.71	$0.01E \pm 0.000$	0.277
1410.181	164078	4.5	234991	4.5	-0.65	7.54E+08	-0.197
1410.288	159226	4.5	230134	4.5	-0.52	1.02E+09	-0.343
1410.58	164032	2.5	234925	2.5	-0.73	6.21E + 08	0.503
1411.008	156798	5.5	227669	6.5	0.05	3.79E + 09	-0.5
1411.293	171713	0.5	242570	1.5	-0.9	4.25E+08	-0.368
1411.759	148007	2.5	219501	1.5 2.5	-0.58	8.73E+08 3.54E+08	-0.172
1411.915	160125	1.5	230950	1.5	-0.86	4.59E + 08	0.231
1411.925	160023	3.5	230848	3.5	-0.59	8.58E + 08	0.177
1413.1	156155	4.5	226921	5.5	-0.3	1.69E + 09	-0.283
1413.32	185622	0.5	256377	1.5	-0.67	7.19E + 08	-0.637
1413.867	186288	1.5	257016	2.5	-0.4	1.34E+09	-0.612
1415.969	168322	3.5	238945	3.5	-0.73	$6.29E \pm 08$	-0.483
1416.278	181639	3.5	252246	2.5	-0.54	9.49E + 08	-0.59
1417.742	178946	2.5	249481	3.5	-0.56	8.99E + 08	0.541
1420.479	165334	4.5	235733	4.5	-0.9	4.16E + 08	-0.247
1420.691	175622	2.5	246010	1.5	-0.72	6.29E + 08	-0.535
1421.547 1422.064	165595	4.5	235915	5.5 5.5	-0.4	$9.04E \pm 08$	-0.361
1422.625	148667	2.5	218960	2.5	-0.6	8.36E + 08	0.294
1422.953	156645	6.5	226921	5.5	-0.22	1.97E + 09	-0.825
1423.082	163952	0.5	234222	0.5	-0.56	8.96E + 08	0.745
1423.552	160704	1.5	230950	1.5	-0.58	8.68E+08	0.487
1423.783	159923	2.5	230158	2.5	-0.86	$4.51E \pm 08$ $3.23E \pm 08$	0.108
1424.794	135036	3.5	205222	2.5	0.04	3.61E+09	0.829
1424.993	198033	1.5	268208	2.5	-0.26	1.83E + 09	-0.547
1425.765	165595	5.5	235733	4.5	-0.33	1.52E + 09	0.591
1425.816	160023	3.5	230158	2.5	-0.7	6.59E + 08	0.23
1426.001	172346	3.5 5 F	242473	2.5 5 F	-0.5	1.05E+09	-0.644
1420.055	160023	3.5	220921	0.0 4.5	-0.25	4.11E+09 1.83E+09	-0.007
1426.751	186288	1.5	256377	1.5	-0.61	8.03E + 08	-0.607
1427.299	215970	2.5	286032	1.5	-0.41	1.28E + 09	0.769
1427.892	160125	1.5	230158	2.5	-0.7	6.56E + 08	-0.323
1427.911	150006	1.5	220038	0.5	-0.63	7.62E + 08	0.801
1428.38	216023	1.5	286032	1.5	-0.24	1.88E+09	0.49
1428.818	175085	4.5	245073 255608	3.5 0.5	-0.61	$8.08E \pm 08$ $8.54E \pm 08$	0.549
1429.231	179242	1.5	249210	2.5	-0.95	3.65E+08	-0.208
1429.93	198329	4.5	268263	3.5	-0.99	3.35E + 08	-0.365
1430.478	164032	2.5	233938	3.5	-0.64	7.47E + 08	0.322
1430.777	156155	4.5	226047	4.5	0.16	4.74E + 09	-0.761
1431.418	164078	4.5	233938	3.5	-0.81	5.09E+08	-0.366
1432.418	136401	2.5	241549	0.5	-0.9	4.11E+08 2.74E+09	0.351
1433.028	188224	4.5	258006	3.5	-0.27	1.77E + 0.09	-0.667
1433.494	165595	5.5	235354	6.5	-0.23	1.92E + 09	0.408
1434.101	175085	4.5	244816	5.5	-0.8	5.25E + 08	0.551
1435.07	156445	2.5	226128	1.5	-0.08	2.73E+09	0.802
1436.359	164078	2.5 4.5	248007	2.0 4.5	-0.5	1.02E+09 9.12E+08	-0.417
1436.569	137350	1.5	206960	0.5	-0.35	1.47E+00	0.864
1437.075	159226	4.5	228812	3.5	-0.98	3.40E + 08	-0.164
1438.946	150006	1.5	219501	1.5	-0.48	1.06E + 09	0.711
1440.71	156155	4.5	225565	3.5	-0.2	2.03E+09	0.771
1441.009	105595	5.5 1.5	234991	4.5	-0.38	1.32E+09	-0.778
1442.577	171713	0.5	235008 241007	1.5	-0.63	7.58E+08	-0.741 -0.474
1443.71	166467	3.5	235733	4.5	-0.37	1.38E + 09	0.398
1445.739	150869	0.5	220038	0.5	-0.72	6.15E + 08	0.702
1446.224	156902	3.5	226047	4.5	-0.05	2.81E + 09	-0.38
1446.263	171530	6.5 4.5	240674 224472	5.5	-0.24	1.83E+09 2.77E+00	0.804
1440.574	159923	4.5 2.5	228957	2.5	-0.25	1.81E+09	-0.531
1449.196	164685	3.5	233689	4.5	-0.94	3.69E + 08	0.111
1449.7	159226	4.5	228206	4.5	-0.42	1.22E + 09	-0.328
1450.633	148667	2.5	217603	2.5	-0.38	1.33E+09	-0.757
1450.646	160023	3.5 5 F	228957	2.5	-0.57	8.60E+08	-0.683
1451 589	170865	5.5 4.5	239755	5.5	-0.19	2.04E+09 9.70E+08	0.04
1451.602	159923	2.5	228812	3.5	-0.2	2.00E + 0.09	-0.388
1451.617	164078	4.5	232966	5.5	-0.38	1.31E + 09	0.266
1451.644	175085	4.5	243973	4.5	-0.31	1.55E + 09	-0.529
1451.855	165595	5.5 4 E	234472	5.5 4 E	-0.99	3.20E + 08	-0.379
1452.18	198329	4.5	267191 250484	4.0	-0.43	1.18E+09 4.05E+08	-0.506
1452.796	160125	1.5	228957	2.5	-0.93	3.71E+08	-0.1
1453.045	136401	2.5	205222	2.5	-0.56	8.66E + 08	0.303
1453.714	160023	3.5	228812	3.5	-0.36	1.38E + 09	-0.496
1453.731	171530	6.5	240319	6.5	-0.36	1.37E + 09	-0.829
1400.01	135036	3.5 3.5	214910 203718	э.э 35	-0.50	0.00凸+08 2.37E±00	-0.031
1456.085	179242	1.5	247919	0.5	-0.99	3.18E+08	-0.37
1456.374	156902	3.5	225565	3.5	-0.11	2.46E + 09	0.486
1456.811	161491	5.5	230134	4.5	-0.36	1.38E + 09	0.75
1457.053	150869	0.5	219501	1.5	-0.91	3.87E+08	-0.406
1457.507	197022	2.5 2.5	∠00042 232641	1.5 1.5	-0.77	0.27E+08 4.16E±08	-0.437 0.689
1457.626	165334	4.5	233938	3.5	-0.64	7.27E + 0.08	0.458
1458.387	167527	2.5	236095	1.5	-0.86	4.34E + 08	-0.445
1459.88	169166	2.5	237665	1.5	-0.86	4.32E + 08	-0.233
1461.134	175533	3.5	243973	4.5 6 5	0.08	3.73E+09	-0.609
1463 109	164032	5.5 2.5	232379 232379	0.0 3.5	-0.29 -0.56	1.50E+09 8.51E+08	-0.18
1463.368	172346	3.5	240682	2.5	-0.76	5.43E + 08	0.478
1463.934	172346	3.5	240655	4.5	-0.53	9.23E + 08	0.526
1464.146	137914	0.5	206213	1.5	-0.77	5.34E + 08	-0.229
1465.12	160704	1.5	228957	2.5	-0.43	1.14E+09	-0.334
1465.749	171530	5.5 6.5	240319 239755	0.5 5.5	-0.83	$4.61E \pm 08$	-0.765

		Table	A38: COL	unue	a		
Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA	CF
1466.887	160125	1.5	228296	2.5	-0.4	$1.22E \pm 09$ $3.69E \pm 08$	-0.33
1408.038 1470.24	175085	4.5	243102	3.5	-0.93	4.37E+08	0.283
1471.391	164685	3.5	232648	4.5	-0.26	1.72E + 09	-0.654
1473.355	137350	1.5	205222	2.5	-0.74	5.67E + 08	-0.149
1477.207	159226	4.5	226921	5.5	-0.37	1.31E + 09	-0.319
1481.258	172346	3.5	239857	4.5	-0.99	3.11E + 08 1.25E + 00	-0.401
1481.927	167527	2.5	243102	3.5	-0.30	1.35E+09 1.01E+09	-0.534
1484.305	165595	5.5	232966	5.5	-0.43	$6.48E \pm 08$	0.246
1485.518	136401	2.5	203718	3.5	-0.92	3.64E + 08	-0.088
1485.632	190694	2.5	258006	3.5	-0.65	6.74E + 08	-0.682
1487.414	175242	1.5	242473	2.5	-0.44	1.10E + 09	-0.652
1487.626	188224	4.5	255445	3.5	-0.03	2.83E+09	-0.801
1489.024	166467	3.5	233625	2.5	-0.82	4.61E+08 2.03E+09	-0.461
1491 346	165595	5.5	232648	4.5	-0.56	2.03E+09 8.31E+08	-0.239
1491.522	165334	4.5	232379	3.5	-0.93	3.54E + 08	-0.318
1494.143	181639	3.5	248567	2.5	-0.32	1.43E + 09	-0.711
1496.643	164032	2.5	230848	3.5	-0.97	3.23E + 08	0.287
1497.342	181872	2.5	248657	3.5	-0.51	9.23E + 08	-0.513
1497.99	189621	2.5	256377	1.5	-0.65	6.67E + 08	-0.656
1498.902	175242	2.5	235882 241934	3.0 1.5	-0.79	4.78E+08 5.12E+08	0.304
1501.411	167021	1.5	233625	2.5	-0.73	$5.49E \pm 0.08$	0.193
1501.441	168322	3.5	234925	2.5	-0.92	3.54E + 08	-0.36
1503.072	196027	3.5	262557	4.5	-0.29	1.50E + 09	-0.311
1507.145	161491	5.5	227841	5.5	-0.52	8.89E + 08	0.31
1507.807	190694	2.5	257016	2.5	-0.6	7.30E + 08	-0.6
1508.018	171530	2.5	241934 237758	1.5 5.5	-0.89	3.77E+08 3.58E+08	-0.228
1511.062	161491	5.5	227669	6.5	-0.5	$9.21E \pm 08$	0.162
1511.814	146216	3.5	212362	4.5	-0.3	1.45E + 09	-0.489
1515.965	197022	2.5	262987	3.5	-0.81	4.55E + 08	-0.652
1517.156	166467	3.5	232379	3.5	-0.61	7.09E + 08	-0.342
1517.722	172070	5.5	237959	4.5	-0.62	6.96E + 08	-0.648
1522.355	175533	3.5	241221	3.5	-0.81	4.50E + 08 1.07E + 00	-0.382
1524.003 1524.107	172346	3.5	237959	4.5	-0.43	5.57E+08	-0.471
1526.387	165334	4.5	230848	3.5	-0.77	4.89E + 08	-0.322
1529.375	181872	2.5	247258	3.5	-0.96	3.13E + 08	-0.379
1529.817	168322	3.5	233689	4.5	-0.51	8.89E + 08	-0.566
1535.752	167527	2.5	232641	1.5	-0.94	3.24E + 08	0.491
1537.272	170865	4.5	235915	5.5	-0.15	2.00E+09	-0.556
1542 722	146216	4.5	233882	3.5	-0.58	$6.44E \pm 08$	0 294
1543.212	165334	4.5	230134	4.5	-0.84	4.01E + 08	0.347
1544.263	175242	1.5	239998	2.5	-0.79	4.56E + 08	0.363
1544.394	190694	2.5	255445	3.5	-0.63	6.49E + 08	-0.316
1544.776	164078	4.5	228812	3.5	-0.91	3.42E + 08	0.364
1553.162	171530	6.5	235915	5.5	-0.41	1.08E+09	-0.731
1558 718	100407	3.5	230848	3.0	-1	$2.80E \pm 08$ 5.38E \pm 08	0.191
1565.94	175085	4.5	238945	3.5	-0.87	3.75E+08	0.508
1579.193	172346	3.5	235670	2.5	-0.69	5.52E + 08	-0.714
1582.236	181872	2.5	245073	3.5	-0.92	3.16E + 08	-0.325
1597.158	165595	5.5	228206	4.5	-0.54	7.60E + 08	0.258
1603.35	148667	2.5	211037	3.5	-0.51	7.91E + 08	-0.611
1603.968	165467	3.5	228812	3.5	-0.84	3.74E + 08	0.296
1610.096	107978	4.5	250158	2.0	-0.8	$4.08E \pm 08$ 7.46E \pm 08	-0.582
1610.264	170865	4.5	232966	5.5	-0.68	5.38E+08	0.523
1610.97	165595	5.5	227669	6.5	-0.24	1.47E + 09	-0.286
1618.555	170865	4.5	232648	4.5	-0.54	7.30E + 08	0.353
1623.701	165334	4.5	226921	5.5	-0.84	3.68E+08	-0.324
1628.641	150006	1.5	211407	2.5	-0.66	5.50E + 08	-0.621
1660 261	165334	1.5 4.5	228290 225565	2.0 3.5	-0.70	4.34E+08 5.98E±08	-0.149
1666.886	216023	1.5	276015	2.5	-0.84	3.49E + 08	-0.502
1692.085	166467	3.5	225565	3.5	-0.98	2.47E + 08	-0.105
1737.973	146216	3.5	203755	4.5	-0.82	3.35E + 08	0.569
1946.908	199048	3.5	250411	4.5	-0.92	2.11E + 08	0.183

Table	$\Delta 38 \cdot$	Continue	1
	A . B (x)		

 $\begin{array}{ccccc} 3.5 & 203755 & 4.5 \\ 3.5 & 250411 & 4.5 \\ a: \ \mbox{Energy Levels from [42]} \end{array}$

Ag VI

Energy Levels

/	0			
E^a_{exp}	E^{b}_{calc}	Δ E	J	Leading components (in %) in LS Coupling c
0	-60	60	4	96.2 $4d^6$ (⁵ D) ⁵ D
2692.5	2696	-3.5	3	$98 \text{ 4d}^6 (^5\text{D}) ^5\text{D}$
3953	3979	-26	2	$94.7 4d^6 (^5D) ^5D$
4941	4995	-54	1	$95.3 \text{ 4d}^6 ({}^5\text{D}) {}^5\text{D}$
5380	5442	-62	0	$95.1 \ 4d^6 \ (^5D) \ ^5D$
20494.5	20345	149.5	4	$20.8 4d^{6} (^{3}\text{F}) ^{3}\text{F} + 34.2 4d^{6} (^{3}\text{H}) ^{3}\text{H} + 22.5 4d^{6} (^{3}\text{G}) ^{3}\text{G}$
21041.5	21191	-149.5	2	56.4 4d ⁶ (³ P) ³ P + 31.5 4d ⁶ (³ P) ³ P
21512.5	21565	-52.5	6	94.3 4d ⁶ (³ H) ³ H + 5.5 4d ⁶ (¹ I) ¹ I
21812	21817	-5	5	$69.7 \text{ 4d}^6 ({}^{3}\text{H}) {}^{3}\text{H} + 30.1 \text{ 4d}^6 ({}^{3}\text{G}) {}^{3}\text{G}$
24441	24422	19	3	57.4 4d ⁶ (³ F) ³ F + 24.9 4d ⁶ (³ G) ³ G + 14.9 4d ⁶ (³ F) ³ F
25144.5	25221	-76.5	4	$52.4 \text{ 4d}^6 (^{3}\text{H}) ^{3}\text{H} + 34.6 \text{ 4d}^6 (^{3}\text{F}) ^{3}\text{F} + 10.2 \text{ 4d}^6 (^{3}\text{F}) ^{3}\text{F}$
25306.5	25374	-67.5	2	$81.2 \text{ 4d}^6 ({}^{3}\text{F}) {}^{3}\text{F} + 11.8 \text{ 4d}^6 ({}^{3}\text{F}) {}^{3}\text{F}$
27958.5	27989	-30.5	5	$69.7 4d^6 ({}^{3}\text{G}) {}^{3}\text{G} + 30.1 4d^6 ({}^{3}\text{H}) {}^{3}\text{H}$
28232	28491	-259	1	$58.5 \text{ 4d}^{6} (^{3}\text{P}) ^{3}\text{P} + 22.3 \text{ 4d}^{6} (^{3}\text{P}) ^{3}\text{P} + 14.9 \text{ 4d}^{6} (^{3}\text{D}) ^{3}\text{D}$
29659.5	29638	21.5	4	74.4 4d ⁶ (³ G) ³ G + 12.1 4d ⁶ (³ F) ³ F + 5.1 4d ⁶ (¹ G) ¹ G
30361	30409	-48	3	$72.5 \text{ 4d}^6 ({}^3\text{G}) {}^3\text{G} + 23.6 \text{ 4d}^6 ({}^3\text{F}) {}^3\text{F}$
32650.5	32475	175.5	2	$84.8 \text{ 4d}^6 (^{3}\text{D}) ^{3}\text{D}$
33509	33260	249	3	$94.4 \ 4d^6 \ (^{3}D) \ ^{3}D$
33558	33379	179	1	$83.7 4d^6 (^{3}\text{D}) ^{3}\text{D} + 8 4d^6 (^{3}\text{P}) ^{3}\text{P} + 7.9 4d^6 (^{3}\text{P}) ^{3}\text{P}$
34194.5	34221	-26.5	6	94.3 4d ⁶ (¹ I) ¹ I + 5.5 4d ⁶ (³ H) ³ H
37481	37089	392	4	$60.7 \ 4d^{6} \ (^{1}G) \ ^{1}G + 19.9 \ 4d^{6} \ (^{1}G) \ ^{1}G + 9.4 \ 4d^{6} \ (^{3}F) \ ^{3}F$
41372	42041	-669	2	$67.9 4d^6 (^1\text{D}) ^1\text{D} + 14.7 4d^6 (^1\text{D}) ^1\text{D} + 6.3 4d^6 (^3\text{D}) ^3\text{D}$
41638.5	41140	498.5	0	$45.5 4d^6 (^{1}\text{S}) ^{1}\text{S} + 41.8 4d^6 (^{3}\text{P}) ^{3}\text{P} + 12.1 4d^6 (^{1}\text{S}) ^{1}\text{S}$
44724.5	44864	-139.5	3	$82.9 \ 4d^6 \ (^1F) \ ^1F + 12.5 \ 4d^6 \ (^3F) \ ^3F$
51664.5	51587	77.5	1	$67.1 \ 4d^{6} \ (^{3}P) \ ^{3}P + 31.5 \ 4d^{6} \ (^{3}P) \ ^{3}P$
53990.5	53891	99.5	4	$75.7 \text{ 4d}^6 ({}^3\text{F}) {}^3\text{F} + 18.3 \text{ 4d}^6 ({}^3\text{F}) {}^3\text{F}$
54223	54213	10	2	83.8 4d ⁶ (³ F) ³ F + 13.6 4d ⁶ (³ F) ³ F
55982	56003	-21	3	$69.2 \ 4d^{6} \ ({}^{3}F) \ {}^{3}F + 13.5 \ 4d^{6} \ ({}^{1}F) \ {}^{1}F + 13.2 \ 4d^{6} \ ({}^{3}F) \ {}^{3}F$
56519	56637	-118	2	$60 \ 4d^6 \ ({}^{3}P) \ {}^{3}P + 34.4 \ 4d^6 \ ({}^{3}P) \ {}^{3}P$
61726	61850	-124	4	$66.1 \ 4d^6 \ (^1G) \ ^1G + 27.9 \ 4d^6 \ (^1G) \ ^1G$
			a:	From Kleef [43] and Joshi [44]

Table A39: Comparison between available experimental data and calculated even energy levels (in cm⁻¹) in Ag VI

a: From Kleef [43] and Joshi [44] b: This work c: Only the component ≥ 5% are given

Table A40: Comparison between available experimental data and calculated odd energy levels (in $\rm cm^{-1}$) in Ag VI

Eam	Ebala	ΔE	J	Leading components (in $\%$) in LS Coupling ^{c}
245839.5	245691	148.5	3	$83.4 \ 4d^55p \ (^6S) \ ^7P + 12.8 \ 4d^55p \ (^6S) \ ^5P$
258553	258518	35	3	79.1 $4d^{5}5p$ (⁶ S) ⁵ P + 14.7 $4d^{5}5p$ (⁶ S) ⁷ P
259764.5	259775	-10.5	2	$84.8 \ 4d^55p \ (^6S) \ ^5P + 5.9 \ 4d^55p \ (^6S) \ ^7P$
260687	260702	-15	1	$90.8 \ 4d^55p \ (^6S) \ ^5P$
272741	272797	-56	2	$49.8 \ 4d^55p \ (^4G) \ ^5G + 14.9 \ 4d^55p \ (^4G) \ ^3F + 7.4 \ 4d^55p \ (^2F) \ ^3F$
274565.5	274652	-86.5	5	$49.1 \ 4d^{5}5p \ (^{4}G) \ ^{5}G + 31.3 \ 4d^{5}5p \ (^{4}G) \ ^{5}H + 7.5 \ 4d^{5}5p \ (^{4}G) \ ^{3}H$
275049.5	275078	-28.5	2	$20.4 4 d_{2}^{5}\text{5p} \left({}^{4}\text{D} \right) {}^{5}\text{F} + 24.4 4 d_{2}^{5}\text{5p} \left({}^{4}\text{P} \right) {}^{5}\text{D} + 17.2 4 d_{2}^{5}\text{5p} \left({}^{4}\text{D} \right) {}^{5}\text{D}$
275073.5	275094	-20.5	3	11.7 $4d^{5}5p$ (⁴ G) ³ F + 22.1 $4d^{5}5p$ (⁴ G) ⁵ G + 11.5 $4d^{5}5p$ (⁴ D) ³ F
275162	275233	-71	6	$49.7 \ 4d^{3}5p \ (^{4}G) \ ^{5}G + 25.9 \ 4d^{5}5p \ (^{4}G) \ ^{5}H + 17.5 \ 4d^{5}5p \ (^{4}G) \ ^{5}H$
276281.5	276135	146.5	3	$45.1 \ 4d^{\circ}5p \ (^{\circ}G) \ ^{\circ}H + 11.1 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}F + 9.7 \ 4d^{\circ}5p \ (^{\circ}G) \ ^{\circ}G$
276960	276917	43	4	29.6 4d°5p (°G) °F + 14.2 4d°5p (°G) °H 20.0 $4\sqrt{5}\pi$ (4p) 5π + 17.4 $\sqrt{5}\pi$ (4p) $3p$ + 10.4 $\sqrt{5}\pi$ (4p) $5p$
277162.5	277205	-42.5	2	$23.3 \ 4d^{\circ} \text{5p} (^{\circ} \text{P}) \ ^{\circ} \text{S} + 17.4 \ 4d^{\circ} \text{5p} (^{\circ} \text{P}) \ ^{\circ} \text{P} + 10.4 \ 4d^{\circ} \text{5p} (^{\circ} \text{D}) \ ^{\circ} \text{F}$
2770005 5	2779089	101.5	Э 4	$59.24d^{5}5p(G)^{-1}F + 14.74d^{-5}5p(G)^{-1}H + 8.64d^{-5}5p(G)^{-1}G$ 21.84d ⁵ 5p(4C) $5H + 20.14d^{5}5p(4D)^{-5}F + 12.84d^{5}5p(4C)^{-5}G$
279095.5	210900	107.5 69.5	4	$31.8 4d^{-}5p(-G)^{-}H + 20.1 4d^{-}5p(-D)^{-}F + 13.8 4d^{-}5p(-G)^{-}G$ $28.0 4d^{5}5p(^{4}D)^{-}5p + 16.7 4d^{5}5p(^{4}D)^{-}5p + 0.8 4d^{5}5p(^{4}D)^{-}3p$
281607	280508	61	5	$39.2 \ 4d^{5}5p \ (^{4}G)^{5}H + 36.6 \ 4d^{5}5p \ (^{4}G)^{5}G + 10.4d^{5}5p \ (^{4}G)^{5}F$
282186 5	2811040	81.5	1	$23.9 \ 4d^55n \ (^4P) \ ^3P + 20.7 \ 4d^55n \ (^4P) \ ^5D + 14.2 \ 4d^55n \ (^4P) \ ^5P$
282348 5	282319	29.5	3	$0.6 4d^{5}5p (^{2}D) {}^{3}F + 28.2 4d^{5}5p (^{4}G) {}^{5}F + 16.4 4d^{5}5p (^{4}P) {}^{5}D$
282545.5	282488	57.5	6	$52.3 4d^55\text{p} ({}^4\text{G}) {}^5\text{H} + 40.8 4d^55\text{p} ({}^4\text{G}) {}^5\text{G}$
283032.5	283210	-177.5	2	$33.8 \ 4d^{5}5p \ (^{4}G) \ ^{3}F + 16.2 \ 4d^{5}5p \ (^{4}G) \ ^{5}G + 14.1 \ 4d^{5}5p \ (^{4}P) \ ^{5}S$
283558.5	283448	110.5	4	$43.9 \ 4d^{5}5p \ (^{4}G) \ ^{5}F + 16.4 \ 4d^{5}5p \ (^{4}P) \ ^{5}D + 9.9 \ 4d^{5}5p \ (^{4}D) \ ^{5}D$
284053	284018	35	3	23.3 $4d^{5}5p({}^{4}G){}^{5}F + 11.5 4d^{5}5p({}^{4}G){}^{3}F + 10 4d^{5}5p({}^{4}P){}^{5}P$
284235.5	284186	49.5	2	$14.5 \ 4d^55p \ (^4P) \ ^5P + 18.4 \ 4d^55p \ (^4D) \ ^5P + 11.9 \ 4d^55p \ (^4D) \ ^5D$
284406	284356	50	2	$20.9 \ 4d^55p \ (^4G) \ ^5F + 24 \ 4d^55p \ (^4D) \ ^5P + 13.4 \ 4d^55p \ (^4P) \ ^5S$
284578.5	284639	-60.5	3	22.7 $4d^{5}5p$ (⁴ D) ⁵ F + 23.9 $4d^{5}5p$ (⁴ G) ³ F + 12 $4d^{5}5p$ (⁴ G) ⁵ G
284659.5	284756	-96.5	4	$43.9 \ 4d^55p \ (^4G) \ ^3F + 12 \ 4d^55p \ (^4G) \ ^5G + 8.4 \ 4d^55p \ (^4D) \ ^5F$
284990	285066	-76	1	$46.2 \ 4d^55p \ (^4G) \ ^5F + 17.6 \ 4d^55p \ (^4D) \ ^5F + 15.2 \ 4d^55p \ (^4P) \ ^5P$
285564.5	285611	-46.5	6	$63.9 \ 4d^{5}5p \ (^{4}G) \ ^{3}H + 19.4 \ 4d^{5}5p \ (^{4}G) \ ^{5}H + 5 \ 4d^{5}5p \ (^{2}I) \ ^{3}H$
285714	285803	-89	4	$46.4 \ 4d^{5}5p \ (^{4}G) \ ^{3}H + 11.4 \ 4d^{5}5p \ (^{4}G) \ ^{3}F + 8.6 \ 4d^{5}5p \ (^{4}D) \ ^{3}F$
285791	285707	84	1	$31.8 \ 4d^{5}_{2}5p \ (^{4}P) \ ^{9}_{2}P + 16.2 \ 4d^{5}_{2}5p \ (^{4}D) \ ^{9}_{2}P + 15.1 \ 4d^{5}_{2}5p \ (^{4}G) \ ^{9}_{2}F$
285968	285989	-21	5	$64.4 \ 4d_{2}^{5}5p \ ({}^{4}G) \ {}^{3}H + 13.4 \ 4d_{2}^{5}5p \ ({}^{4}D) \ {}^{5}F + 8.7 \ 4d_{2}^{5}5p \ ({}^{4}G) \ {}^{5}H$
286575.5	286646	-70.5	4	$17.1 \ 4d^{3}5p \ (^{4}P) \ ^{5}D + 17.3 \ 4d^{5}5p \ (^{4}D) \ ^{5}F + 13.3 \ 4d^{5}5p \ (^{4}D) \ ^{5}F$
286636	286635	1	2	$10.9 \ 4d^{5}5p \ (^{4}P) \ ^{5}P + 25.5 \ 4d^{5}5p \ (^{4}G) \ ^{5}F + 15.8 \ 4d^{5}5p \ (^{4}P) \ ^{5}S$
287055.5	286906	149.5	3	$31.3 \ 4d^{3}5p \ (^{4}D) \ ^{5}D \ + \ 15.1 \ 4d^{3}5p \ (^{4}P) \ ^{5}D \ + \ 12.6 \ 4d^{3}5p \ (^{4}G) \ ^{3}F$
287589.5	287536	53.5	4	$34.7 \ 4d^{\circ}5p \ (^{\circ}D) \ ^{\circ}D + 18.5 \ 4d^{\circ}5p \ (^{\circ}P) \ ^{\circ}D + 16.9 \ 4d^{\circ}5p \ (^{\circ}G) \ ^{\circ}H$
288183.5	288170	13.5	5	44.2 4d ^o 5p (⁻ D) F + 10.4 4d ^o 5p (⁻ G) H + 7.5 4d ^o 5p (⁻ I) I
288704	288735	-31	3	$25.5 \ 4d^{\circ} \text{5p} (^{-}\text{P}) \ ^{\circ}\text{D} + 25.2 \ 4d^{\circ} \text{5p} (^{-}\text{D}) \ ^{\circ}\text{F} + 11.9 \ 4d^{\circ} \text{5p} (^{-}\text{P}) \ ^{\circ}\text{D}$
288743	288734	1025	1	$20.6 \ 4d^{-} \text{5p} (D)^{-} D + 19.1 \ 4d^{-} \text{5p} (D)^{-} D + 13.7 \ 4d^{-} \text{5p} (P)^{-} D$ $19.4 \ 4d^{5} \text{5p} (21)^{-} 1 \text{H} + 24.0 \ 4d^{5} \text{5p} (4D)^{-} 5 \text{F} + 10.4 \ d^{5} \text{5p} (21)^{-} 3 \text{I}$
28001.5	288903	-103.5	6	12.4 40 Jp(1) 11 + 24.9 40 Jp(1) 1 + 1940 Jp(1) 1 $60.2 4d^{5}5p(^{2}1) ^{3}K + 21 4d^{5}5p(^{2}1) ^{3}1 + 64 4d^{5}5p(^{2}H) ^{3}1$
289488 5	289453	35.5	3	$46.8 4d^{5}5p ({}^{4}C) {}^{3}C + 9.4d^{5}5p ({}^{4}P) {}^{5}D + 6.3 4d^{5}5p ({}^{4}C) {}^{5}H$
289567	289626	-59	4	$47.6 4d^{5}5p ({}^{4}G) {}^{3}G + 6.2 4d^{5}5p ({}^{4}F) {}^{3}G + 6.4 d^{5}5p ({}^{2}F) {}^{3}G$
290297	290320	-23	1	$(1.3 \text{ 4d } \text{5p} (^4\text{P}) ^5\text{P} + 17.9 \text{ 4d} ^5\text{5p} (^4\text{P}) ^5\text{P} + 7.5 \text{ 4d} ^5\text{5p} (^4\text{P}) ^3\text{P}$
290416	290471	-55	2	$25.8 4d^55p (^4D) ^3F + 12.8 4d^55p (^4P) ^5D + 11.4 4d^55p (^4P) ^3D$
290705	290596	109	3	$34.8 \ 4d^{5}5p \ (^{4}D) \ ^{3}D + 9.7 \ 4d^{5}5p \ (^{4}G) \ ^{3}F + 8.6 \ 4d^{5}5p \ (^{4}D) \ ^{5}D$
291127	291157	-30	7	$50.3 \ 4d^55p \ (^{2}I) \ ^{3}K + 29.2 \ 4d^55p \ (^{2}I) \ ^{3}I + 18.8 \ 4d^55p \ (^{2}I) \ ^{1}K$
291283.5	291338	-54.5	2	$15.2 \ 4d^55p \ (^4D) \ ^3D + 14 \ 4d^55p \ (^4P) \ ^5P + 12.4 \ 4d^55p \ (^4P) \ ^3P$
292117	292062	55	5	$62.2 \ 4d^55p \ (^4G) \ ^3G + 12.8 \ 4d^55p \ (^2I) \ ^3I + 5 \ 4d^55p \ (^2I) \ ^3H$
292500	292681	-181	4	$17.6 \ 4d^55p \ (^4D) \ ^5F + 25.6 \ 4d^55p \ (^4D) \ ^3F + 17.3 \ 4d^55p \ (^4P) \ ^5D$
292607	292593	14	1	22.6 $4d^{5}_{5}$ 5p $\binom{4}{D}^{5}_{D}$ + 19.2 $4d^{5}_{5}$ 5p $\binom{4}{P}^{3}_{P}$ + 14.1 $4d^{5}_{5}$ 5p $\binom{4}{P}^{5}_{D}$
293265	293324	-59	3	14.3 $4d^{5}5p ({}^{4}D) {}^{3}F + 11.3 4d^{5}5p ({}^{4}G) {}^{3}G + 8.7 4d^{5}5p ({}^{4}P) {}^{5}D$
293275	293231	44	2	$14.5 \ 4d_{2}^{5}5p \ \binom{2}{4}D \ \frac{3}{2}F + 21.7 \ 4d_{2}^{5}5p \ \binom{4}{4}D \ \frac{3}{2}D + 14.3 \ 4d_{2}^{5}5p \ \binom{4}{4}D \ \frac{3}{2}F$
293586.5	293554	32.5	2	21.2 $4d^{5}5p ({}^{4}D) {}^{5}P + 15.7 4d^{5}5p ({}^{4}P) {}^{5}P + 12.4 4d^{5}5p ({}^{4}P) {}^{5}S$
293765.5	293681	84.5	3	$26.1 \ 4d^{3}5p \ (^{4}P) \ ^{3}P + 21.1 \ 4d^{3}5p \ (^{4}D) \ ^{3}P + 15.7 \ 4d^{3}5p \ (^{4}D) \ ^{3}F$
293848	293720	128	6	$46.6 \ 4d^{6}5p(^{2}1) \ ^{3}H + 22.7 \ 4d^{6}5p(^{2}1) \ ^{3}I + 12.2 \ 4d^{6}5p(^{2}1) \ ^{3}K$
295023	295165	-142	2	$23.3 \ 4d^{\circ}5p \ (^{2}P) \ ^{\circ}D + 15.6 \ 4d^{\circ}5p \ (^{2}D) \ ^{\circ}P + 11.2 \ 4d^{\circ}5p \ (^{2}G) \ ^{\circ}F$
295372	295402	-30	4	$34.14d^{5}\text{5p}(G)^{-1}\text{H} + 22.54d^{-5}\text{p}(G)^{-1}\text{G} + 10.94d^{-5}\text{p}(1)^{-1}\text{H}$ $28.24d^{5}\text{5p}(4\text{D})^{-3}\text{D} + 254d^{5}\text{5p}(4\text{D})^{-3}\text{G} + 1244d^{5}\text{5p}(4\text{D})^{-3}\text{D}$
295451	295355	175	2	26.3 40 5p(D) $1 + 23 40 5p(T)$ $3 + 12.4 40 5p(T)$ 1
296114 5	295004	201.5	5	$23.9 4d^{5}5n (^{2}C) ^{3}H + 18.3 4d^{5}5n (^{2}C) ^{3}C + 9.2 4d^{5}5n (^{4}F) ^{5}C$
296416.5	296824	-407.5	3	$16.7 \ 4d^{5}5p \ (^{2}F) \ ^{3}D + 11.8 \ 4d^{5}5p \ (^{2}F) \ ^{3}F + 7.8 \ 4d^{5}5p \ (^{2}F) \ ^{3}D$
297076.5	297160	-83.5	5	$30.8 \ 4d^{5}5p \ (^{2}I) \ ^{3}I + 14.7 \ 4d^{5}5p \ (^{2}I) \ ^{1}H + 10.8 \ 4d^{5}5p \ (^{2}H) \ ^{3}I$
297761.5	297626	135.5	4	$10.5 \ 4d^{5}5p \ (^{2}G) \ ^{1}G + 12.3 \ 4d^{5}5p \ (^{2}H) \ ^{1}G + 11.6 \ 4d^{5}5p \ (^{4}D) \ ^{3}F$
297929.5	298101	-171.5	2	$35.6 \ 4d^55p \ ({}^{4}F) \ {}^{5}G + 12 \ 4d^55p \ ({}^{2}F) \ {}^{3}F + 9.6 \ 4d^55p \ ({}^{2}D) \ {}^{3}P$
298069	298244	-175	1	24.3 $4d^{5}5p$ (² D) ³ P + 18.2 $4d^{5}5p$ (⁴ P) ³ S + 9.1 $4d^{5}5p$ (⁴ D) ³ D
298133.5	298128	5.5	6	$33.4 \ 4d^55p \ (^2I) \ ^3I + 24.7 \ 4d^55p \ (^2I) \ ^3H + 16.2 \ 4d^55p \ (^2I) \ ^3K$
298167.5	297975	192.5	4	$16.5 \ 4d^55p \ ({}^{4}F) \ {}^{5}G + 12.9 \ 4d^55p \ ({}^{2}F) \ {}^{3}G + 9.7 \ 4d^55p \ ({}^{2}F) \ {}^{3}G$
298237.5	298354	-116.5	4	$14.5 \ 4d_{2}^{5}5p \ ({}^{2}I) \ {}^{3}H + 15.4 \ 4d_{2}^{5}5p \ ({}^{4}F) \ {}^{5}G + 10.3 \ 4d_{2}^{5}5p \ ({}^{2}G) \ {}^{3}H$
298289	298291	-2	3	$44.2 \ 4d^{3}5p \ (^{4}F) \ ^{5}G + 7.4 \ 4d^{3}5p \ (^{4}G) \ ^{3}G + 6.9 \ 4d^{3}5p \ (^{2}F) \ ^{3}D$
298375.5	298378	-2.5	7	$54.9 \ 4d^{5}5p \ (^{2}I) \ ^{1}K + 29.8 \ 4d^{5}5p \ (^{2}I) \ ^{3}K + 10.3 \ 4d^{5}5p \ (^{2}H) \ ^{3}I$
298421	298681	-260	2	$32.5 \ 4d^{\circ}5p({}^{\circ}D) \ ^{\circ}P + 15.6 \ 4d^{\circ}5p({}^{\circ}P) \ ^{\circ}P + 11.2 \ 4d^{\circ}5p({}^{\circ}F) \ ^{\circ}G$
298870	299014	-144	5	$43.9 \ 4d^{\circ}5p \ (^{-}1) \ ^{\circ}H + 21 \ 4d^{\circ}5p \ (^{-}1) \ ^{-}H + 9.2 \ 4d^{\circ}5p \ (^{-}G) \ ^{-}H$
299164	299220	-00	1	$64.6 \ 4d^{2} \text{ sp}(1)^{-1} + 17.7 \ 4d^{2} \text{ sp}(1)^{-1} \text{ K} + 14.7 \ 4d^{-2} \text{ sp}(1)^{-1} \text{ K}$
299038.3 300101	299027 300001	10	4 0	24.3 40 3p (F) D = 19.3 40 3p (F) F = 11.3 40 3p (F) G 91.6 $Ad^{5}5p$ ($4E$) $5E$ = 11.4 $Ad^{5}5p$ ($4E$) $5D$ = 0.0 $Ad^{5}5p$ ($2E$) $3D$
300460	300091	20/	∠ 3	$21.0 = 4 \text{ op}(\mathbf{r}) \mathbf{r} + 11.4 = 40 \text{ op}(\mathbf{r}) \mathbf{D} + 6.6 = 40 \text{ op}(\mathbf{r}) \mathbf{D}$ $20.5 = 4d^55p(^2F)^3F + 22.0 = 4d^55p(^2F)^3C \pm 11.1 = 4d^55p(^2F)^3F$
300570 5	300597	-26.5	4	$18.4 4d^55p (^2D) \ ^3F + 12.1 \ 4d^55p (^2I) \ ^3H + 10.4 \ 4d^55p (^2F) \ ^3C$
300965.5	301021	-55.5	5	$23.2 \ 4d^55p \ (^4F) \ ^5G + 19.8 \ 4d^55p \ (^2I) \ ^3I + 10.6 \ 4d^55p \ (^2G) \ ^3H$
300975	300868	107	3	19.5 $4d^{5}5p$ (² F) ³ G + 16.4 $4d^{5}5p$ (² D) ³ F + 7.6 $4d^{5}5p$ (² H) ³ G
301167	301055	112	2	10.3 $4d^{5}5p$ (² D) ¹ D + 14.5 $4d^{5}5p$ (⁴ F) ⁵ F + 6.9 $4d^{5}5p$ (² F) ³ F
301314	301237	77	6	41.2 $4d^{5}5p({}^{4}F){}^{5}G + 31.4 4d^{5}5p({}^{2}G){}^{3}H + 9.7 4d^{5}5p({}^{2}I){}^{3}I$
301320	301217	103	3	16.3 $4d^{5}5p$ (² G) ³ G + 14.1 $4d^{5}5p$ (⁴ F) ⁵ F + 10.5 $4d^{5}5p$ (⁴ F) ⁵ D
301607	301604	3	3	23.1 $4d^{5}5p$ (⁴ F) ⁵ F + 14.7 $4d^{5}5p$ (² G) ³ G + 14.3 $4d^{5}5p$ (² F) ³ D
301903.5	301810	93.5	5	21.9 $4d_{5}^{5}5p ({}^{4}F) {}^{5}F + 23.1 4d_{5}^{5}5p ({}^{4}F) {}^{5}G + 12.5 4d_{5}^{5}5p ({}^{2}G) {}^{3}G$
302080.5	302279	-198.5	4	23.4 $4d_{e}^{5}5p$ (² F) $\frac{1}{e}G$ + 12.7 $4d_{e}^{5}5p$ (⁴ F) $\frac{5}{4}G$ + 8 $4d_{e}^{5}5p$ (² I) ³ H
302808.5	302776	32.5	1	$45.6 \ 4d^{5}5p \ ({}^{4}F) \ {}^{5}F + 10.8 \ 4d^{5}5p \ ({}^{2}D) \ {}^{1}P + 9.2 \ 4d^{5}5p \ ({}^{4}F) \ {}^{5}D$
302947.5	303012	-64.5	2	12.3 $4d^{5}5p$ (² F) ¹ D + 17.2 $4d^{5}5p$ (² D) ³ F + 15.4 $4d^{5}5p$ (² D) ³ D
303440	303433	7	1	18.1 4d°5p ("D) °D + 24 4d°5p ("F) °D + 10.7 4d°5p ("F) °D 19.2 415r (21) 311 + 22 44°5p ("F) 56 + 22 7 (27) 17
303558.5	303479	79.5	6	13.3 4a°5p (~H) ~H + 29.4 4d°5p (~F) °G + 23.5 4d°5p (² I) ¹ I
304144	303706	-09.5 017	G A	23.3 40 3P (Π) G + 19 40 3P (Π) 1 + 18.7 40 3P (Γ) F 21.5 4d ⁵ 5p (² F) $^{3}F \pm 0.0$ 4d ⁵ 5p (² F) $^{3}F \pm 7.7$ 4d ⁵ 5p (² F) 10
304144	303927	<i>4</i> ⊥(4	21.0 4u op (r) r ± 3.3 4u op (r) r ± 1.1 4u op (r) G

				Table A40: Continued
E^a_{exp}	E^{b}_{calc}	ΔE	J	Leading components (in %) in LS Coupling ^c
304450 5	304422	28.5	4	$24.4.4d^{5}5n(^{2}G)^{3}G + 14.4.4d^{5}5n(^{2}I)^{3}H + 9.7.4d^{5}5n(^{4}F)^{5}D$
304878 5	305068	180.5	4	$10.1 4d^{5}$ to $({}^{4}$ F) 5 F $\pm 21.6 4d^{5}$ to $({}^{2}$ F) 3 F $\pm 10.6 4d^{5}$ to $({}^{4}$ F) 5 C
304878.3	303008	-189.5	-4 	$19.140 \text{ Jp}(\mathbf{F}) \mathbf{F} + 21.040 \text{ Jp}(\mathbf{F}) \mathbf{F} + 10.040 \text{ Jp}(\mathbf{F}) \mathbf{G}$
304933.3	304914	39.5	1	29.4 40 5p(H) 1 + 29.4 40 5p(H) H + 9.8 40 5p(G) H
305145.5	305122	23.5	1	$19 4d^{\circ} \text{5p} (^{\circ}\text{P}) ^{\circ}\text{S} + 22.5 4d^{\circ}\text{5p} (^{\circ}\text{F}) ^{\circ}\text{D} + 10.9 4d^{\circ}\text{5p} (^{\circ}\text{D}) ^{\circ}\text{P}$
305356.5	305600	-243.5	2	$23 \text{ 4d}^{3}5p ({}^{2}\text{G}) {}^{3}\text{F} + 12.4 \text{ 4d}^{3}5p ({}^{2}\text{F}) {}^{3}\text{F} + 10.3 \text{ 4d}^{3}5p ({}^{4}\text{D}) {}^{3}\text{F}$
305641.5	305588	53.5	6	$46.6 \ 4d^{5}5p \ (^{2}I) \ ^{1}I + 35.7 \ 4d^{5}5p \ (^{2}H) \ ^{3}I$
306147.5	306248	-100.5	5	$64.3 \ 4d^{5}5p \ (^{2}F) \ ^{3}G + 8.5 \ 4d^{5}5p \ (^{4}F) \ ^{5}F$
306210	306261	-51	4	$1.5 4d^55p (^4D) \ ^3F + 26.5 \ 4d^55p (^2G) \ ^3F + 13.5 \ 4d^55p (^2F) \ ^3F$
306474	306508	-34	3	$17.7 \ 4d^55p \ (^2G) \ ^3F + 12.4 \ 4d^55p \ (^4F) \ ^3G + 10.2 \ 4d^55p \ (^2F) \ ^3D$
306715.5	306629	86.5	3	$25.1 \ 4d^55p \ (^2F) \ ^3G + 13 \ 4d^55p \ (^2D) \ ^3F + 8.3 \ 4d^55p \ (^4F) \ ^5F$
306850	306964	-114	2	$17.4 \ 4d^{5}5p \ (^{2}D) \ ^{3}D + 19.4 \ 4d^{5}5p \ (^{4}F) \ ^{5}F + 12.4 \ 4d^{5}5p \ (^{2}F) \ ^{3}D$
307337 5	307112	225.5	4	$17.6 4d^{5}5p (^{2}F) {}^{3}C + 9.4d^{5}5p (^{4}F) {}^{3}C + 7.5 4d^{5}5p (^{2}F) {}^{3}F$
207802	207917	220.0	6	$^{28}6 4d^{5}5p (^{2}H) ^{1}I + ^{22}7 4d^{5}5p (^{2}C) ^{3}H + ^{16}9 4d^{5}5p (^{4}F) ^{5}C$
307892	307817	75	5	38.0 40 5p(H) 1 + 32.7 40 5p(G) H + 10.2 40 5p(F) G
308266	308256	10	5	$39.4 \ 4d^{\circ} \text{5p} (^{-}\text{F}) \ ^{\circ}\text{G} + 12 \ 4d^{\circ} \text{5p} (^{-}\text{F}) \ ^{\circ}\text{G} + 9.8 \ 4d^{\circ} \text{5p} (^{-}\text{F}) \ ^{\circ}\text{F}$
308404.5	308144	260.5	2	$33.4 \ 4d^{\circ}5p({}^{2}F) \ D + 10.1 \ 4d^{\circ}5p({}^{2}F) \ D + 7.8 \ 4d^{\circ}5p({}^{2}F) \ F$
309083	309155	-72	2	$22.2 \ 4d^{5}5p \ (^{4}F) \ ^{5}D + 13.4 \ 4d^{5}5p \ (^{2}F) \ ^{5}D + 11.2 \ 4d^{5}5p \ (^{2}D) \ ^{5}P$
309234	309110	124	1	$53.2 4d^{5}5p (^{2}S) ^{3}P + 9.8 4d^{5}5p (^{2}D) ^{3}P + 7.4 4d^{5}5p (^{4}F) ^{3}D$
309388.5	309281	107.5	5	$34.9 \ 4d^{5}5p \ (^{2}G) \ ^{3}G + 23.7 \ 4d^{5}5p \ (^{2}G) \ ^{3}H + 16.6 \ 4d^{5}5p \ (^{2}F) \ ^{3}G$
309526.5	309596	-69.5	4	$12 \ 4d^55p \ (^4F) \ ^3G + 13.6 \ 4d^55p \ (^4F) \ ^5D + 10.9 \ 4d^55p \ (^2F) \ ^3F$
310253	310198	55	3	$16.2 \ 4d^55p \ (^4F) \ ^3G + 15.9 \ 4d^55p \ (^4F) \ ^3F + 10.6 \ 4d^55p \ (^2F) \ ^1F$
310303	310695	-392	2	$9.7 4d^5 5p (^2F) {}^{3}D + 17.7 4d^5 5p (^4F) {}^{3}D + 14 4d^5 5p (^2D) {}^{1}D$
310335.5	310339	-3.5	6	$35 4d^{5}5p (^{2}H) ^{3}I + 33 4 4d^{5}5p (^{2}H) ^{3}H + 191 4d^{5}5p (^{2}H) ^{1}I$
310470	310490	-20	4	$24.6 4d^{5}5p ({}^{4}F) {}^{3}F + 15.3 4d^{5}5p ({}^{4}F) {}^{3}G + 12.1 4d^{5}5p ({}^{2}H) {}^{3}H$
210672 5	210012	220 5	1	$52.7 4d^{5}$ fp $(^{4}\text{F})^{3}$ D + 11.6 $4d^{5}$ fp $(^{4}\text{D})^{3}$ D + 8.4 $4d^{5}$ fp $(^{2}\text{F})^{3}$ D
310073.5	310912	-238.5	1	32.7 40 5p(F) D + 11.0 40 5p(D) D + 3.4 40 5p(F) D
310967.5	311102	-134.5	4	$27.5 \ 4d^{\circ} \text{5p} (^{-}\text{H}) \ ^{\circ}\text{H} + 20.1 \ 4d^{\circ} \text{5p} (^{-}\text{F}) \ ^{\circ}\text{G} + 11.9 \ 4d^{\circ} \text{5p} (^{-}\text{F}) \ ^{\circ}\text{F}$
311185.5	311184	1.5	7	$82.6 \ 4d^{\circ}_{5p}$ (² H) ³ I + $8.4 \ 4d^{\circ}_{5p}$ (² I) ⁴ K + $4.7 \ 4d^{\circ}_{5p}$ (² I) ⁵ K
311683	311631	52	4	$10.5 \ 4d^{3}5p({}^{2}F) \ {}^{1}G + 17.9 \ 4d^{3}5p({}^{2}G) \ {}^{3}G + 13.5 \ 4d^{3}5p({}^{2}G) \ {}^{1}G$
311962	311852	110	5	23 $4d^{5}5p$ (² H) ³ H + 23 $4d^{5}5p$ (² F) ³ G + 15.3 $4d^{5}5p$ (⁴ F) ³ G
312169	312263	-94	3	$18.6 \ 4d^55p \ (^4F) \ ^3F + 15.9 \ 4d^55p \ (^2F) \ ^1F + 11.3 \ 4d^55p \ (^2G) \ ^1F$
312431.5	312581	-149.5	2	$34.3 \ 4d^55p \ (^4F) \ ^3D + 18.5 \ 4d^55p \ (^2S) \ ^3P + 9.1 \ 4d^55p \ (^2D) \ ^3P$
312636	312440	196	3	$5.4 \ 4d^{5}5p(^{2}F)^{3}D + 22.8 \ 4d^{5}5p(^{4}F)^{3}F + 16.9 \ 4d^{5}5p(^{2}F)^{1}F$
313983 5	313803	180.5	2	$15.4d^{5}5p(^{2}F)^{3}D + 27.84d^{5}5p(^{2}F)^{3}D + 15.14d^{5}5p(^{2}S)^{3}P$
214052.5	21/22/	280.5	2	$16.7 4d^{5}$ Ep (² F) ³ F + 12.2 4d ⁵ Ep (⁴ F) ³ C + 0.1 4d ⁵ Ep (² F) ³ F
314033.3	314334	-280.5	3	10.7 4 d Jp(F) F + 13.2 4 d Jp(F) G + 9.1 4 d Jp(F) F
314172.5	314219	-46.5	4	6.140° p (F) G + 19.840 p (F) G + 15.340 p (F) F
314360	314294	66	1	$24.1 \ 4d^{\circ}5p \ (^{2}F) \ ^{\circ}D + 19.1 \ 4d^{\circ}5p \ (^{2}S) \ ^{\circ}P + 10.7 \ 4d^{\circ}5p \ (^{2}D) \ ^{\circ}P$
314439	314398	41	5	$43.9 \ 4d_{2}^{5}5p \ (^{2}G) \ ^{1}H + 9.9 \ 4d_{2}^{5}5p \ (^{2}H) \ ^{3}H + 9 \ 4d_{2}^{5}5p \ (^{2}G) \ ^{3}H$
314553.5	314736	-182.5	2	$15.9 4d^{5}5p (^{2}F) {}^{3}F + 28.8 4d^{5}5p (^{4}F) {}^{3}F + 9 4d^{5}5p (^{2}F) {}^{1}D$
314675	314565	110	3	11.6 $4d^{5}5p$ (² F) ¹ F + 19.1 $4d^{5}5p$ (² F) ³ G + 16.2 $4d^{5}5p$ (² G) ¹ F
315274	315321	-47	6	$30.7 \ 4d^55p \ (^2G) \ ^3H + 28.5 \ 4d^55p \ (^2H) \ ^3H + 27.5 \ 4d^55p \ (^2H) \ ^1I$
315411.5	315313	98.5	4	$23.6 \ 4d^55p \ (^2F) \ ^3F + 13.6 \ 4d^55p \ (^4F) \ ^3G + 13.4 \ 4d^55p \ (^2F) \ ^1G$
315481.5	315361	120.5	3	$26 \ 4d^5 5p \ (^4F) \ ^3D + 13.1 \ 4d^5 5p \ (^2F) \ ^3D + 12.4 \ 4d^5 5p \ (^2D) \ ^3D$
316355.5	316291	64.5	5	$59.5 4d^{5}5p (^{2}H)^{1}H + 9.4d^{5}5p (^{2}G)^{1}H + 7.7 4d^{5}5p (^{2}G)^{3}G$
317080 5	316085	05.5	3	$34.3.4d^{5}$ 5p (² H) ³ C + 10.1.4d ⁵ 5p (² C) ³ C + 7.0.4d ⁵ 5p (⁴ F) ³ C
217257	217241	16	4	34.340 $3p(11)$ $3p(11)$ $4p(10.140$ $3p(3)$ $3p(17)$ 40 $3p(17)$ $3p($
317337	317341	100 5	4	32 4 d 3p (H) G + 18.1 4 d 3p (F) G + 7.5 4 d 3p (G) G
317484.5	317382	102.5	2	$19.5 \ 4d^{\circ} \text{5p} (-\text{S})^{\circ} \text{P} + 12.9 \ 4d^{\circ} \text{5p} (-\text{F})^{\circ} \text{D} + 12.7 \ 4d^{\circ} \text{5p} (-\text{F})^{\circ} \text{D}$
318262.5	317996	266.5	5	$31.6 \ 4d^{\circ} 5p \ (^{2}F) \ ^{\circ}G + 32.1 \ 4d^{\circ} 5p \ (^{2}H) \ ^{\circ}G + 10.1 \ 4d^{\circ} 5p \ (^{2}H) \ ^{1}H$
320038	320226	-188	4	$39 \ 4d^{3}5p \ (^{2}H) \ ^{1}G + 20.2 \ 4d^{3}5p \ (^{2}G) \ ^{1}G + 8.3 \ 4d^{3}5p \ (^{2}F) \ ^{1}G$
320974	321188	-214	3	$37.4 \ 4d^{5}5p \ (^{2}F) \ ^{1}F + 7.8 \ 4d^{5}5p \ (^{2}F) \ ^{1}F + 6.6 \ 4d^{5}5p \ (^{2}G) \ ^{3}F$
322424.5	322143	281.5	1	$58.5 4d^{5}5p (^{2}D) ^{3}D + 22.4 4d^{5}5p (^{2}S) ^{1}P$
324022	324130	-108	3	$16.6 \ 4d^55p \ (^2D) \ ^1F + 21.8 \ 4d^55p \ (^2D) \ ^3F + 10.7 \ 4d^55p \ (^2F) \ ^1F$
326026	326148	-122	3	$30.2 \ 4d^55p \ (^2D) \ ^3F + 23.2 \ 4d^55p \ (^2D) \ ^1F + 18.1 \ 4d^55p \ (^2G) \ ^1F$
327004	326798	206	3	$51 4d^{5}5p (^{2}D) {}^{3}D + 16.6 4d^{5}5p (^{2}D) {}^{3}F$
327145	327142	3	4	$55.8 4d^{5}5p (^{2}G) {}^{3}F + 13.1 4d^{5}5p (^{2}G) {}^{3}G + 5.6 4d^{5}5p (^{2}D) {}^{3}F$
327517	327459	58	5	$50.8 4d^{5}5p (^{2}C) ^{3}H + 19.1 4d^{5}5p (^{2}C) ^{1}H + 17.2 4d^{5}5p (^{2}C) ^{3}C$
227071 5	229015	42.5	4	$5254d^{5}5p(^{2}C)^{3}H + 1044d^{5}5p(^{2}D)^{3}F + 674d^{5}5p(^{2}C)^{1}C$
321911.3	328013	-43.5	4	52.5 4 d 5 p (G) H + 10.4 4 d 5 p (D) F + 0.7 4 d 5 p (G) G
328307.5	328400	-32.5	4	$69.2 \ 4d^{-}{}$ $5p(-D)^{-}F + 6.5 \ 4d^{-}{}$ $5p(-G)^{-}F + 6.4 \ 4d^{-}{}$ $5p(-G)^{-}H$
329699.5	329674	25.5	3	$34.5 \ 4d^{\circ}5p \ (^{2}G) \ ^{3}G + 20.7 \ 4d^{\circ}5p \ (^{2}G) \ ^{3}F + 15 \ 4d^{\circ}5p \ (^{2}D) \ ^{4}F$
331605.5	331553	52.5	2	$55.9 \text{ 4d}^{5}_{5}_{5}_{2} (^{2}_{2}_{D}) ^{1}_{0}_{1}_{1}_{2}_{2}_{2}_{2}_{3}_{4}_{4}_{3}_{5}_{5}_{5}_{5} (^{2}_{2}_{D}) ^{3}_{2}_{2}_{2}_{2}_{2}_{2}_{2}_{2}_{2}_{2$
332893	332834	59	6	$94.5 \ 4d^{5}5p \ (^{2}G) \ ^{3}H$
333194.5	333237	-42.5	3	$45 \ 4d^55p \ (^2G) \ ^3F + 29.8 \ 4d^55p \ (^2G) \ ^3G + 6.2 \ 4d^55p \ (^2D) \ ^1F$
333270	333347	-77	2	$62.5 \ 4d^55p \ (^2G) \ ^3F + 12.2 \ 4d^55p \ (^2D) \ ^3F + 7.4 \ 4d^55p \ (^2D) \ ^1D$
333800.5	333799	1.5	4	$69.9 \ 4d^55p \ (^2G) \ ^3G + 13.5 \ 4d^55p \ (^2G) \ ^3H + 9.4 \ 4d^55p \ (^2G) \ ^3F$
334948 5	334923	25.5	5	$62 \text{ 4d}^5 \text{5p} (^2 \text{G}) ^3 \text{G} + 27.7 \text{ 4d}^5 \text{5p} (^2 \text{G}) ^3 \text{H}$
336820	336803	-64	4	$79.2 4d^55p (^2\text{G}) ^1\text{G} + 6.4d^55p (^2\text{G}) ^3\text{F}$
337020	337022	- 0-4	-1 K	$72.8 4d^{5}5n (^{2}C) ^{1}H \pm 0.6 4d^{5}5n (^{2}C) ^{3}H \pm 0.1 4d^{5}5n (^{2}C) ^{3}C$
331029 337550	337U32 227714	-0 156	3	12.0 = 40 op (G) = 11 + 3.0 = 40 op (G) = 11 + 3.1 = 40 op (G) = 6 54 1 4d555 (2p) 3p + 92 4d555 (2p) 3p + 71 4d55 (2p) 3p
331338	331114	-100	4	$_{24.14}$ u op (r) r + 25 40 op (⁻ D) r + (.140 op (⁻ P) O
338182.5	338165	17.5	3	$33 4a^{\circ} p ({}^{\circ}G) {}^{+}F + 15.5 4a^{\circ} p ({}^{+}D) {}^{+}F + 9.6 4a^{\circ} 5p ({}^{+}G) {}^{3}G$
341727	341775	-48	2	28.6 4d ^o 5p (² P) $^{\circ}D$ + 26.3 4d ^o 5p (² P) $^{\circ}D$ + 9.6 4d ^o 5p (² D) $^{\circ}P$
342518.5	342556	-37.5	1	76.2 4d ⁵ ₂ 5p (² P) ³ D + 5.4 4d ⁵ ₂ 5p (² F) ³ D + 5.3 4d ⁵ ₂ 5p (² D) ³ D
347274	347237	37	3	$80.6 _{4}\text{d}^{5}5\text{p}$ (² P) ³ D + $8.7 _{4}\text{d}^{5}5\text{p}$ (² D) ³ D + $2.7 _{4}\text{d}^{5}5\text{p}$ (² F) ³ D
347842	347900	-58	2	$0 4d^{5}5p (^{2}F) {}^{3}F + 46 4d^{5}5p (^{2}P) {}^{3}D + 24.5 4d^{5}5p (^{2}P) {}^{1}D$
353721	353650	71	3	$44.3 \ 4d^55p \ (^2D) \ ^3F + 12.8 \ 4d^55p \ (^2D) \ ^3D + 12 \ 4d^55p \ (^2D) \ ^3F$
359642	359622	20	2	$37.7 \ 4d^55p \ (^2D) \ ^3D + 12.5 \ 4d^55p \ (^2D) \ ^3P + 10 \ 4d^55p \ (^2D) \ ^3F$
361475.5	361356	119.5	3	$53.5 \ 4d^55p \ (^2D) \ ^3D + 13.1 \ 4d^55p \ (^2D) \ ^3D + 12.9 \ 4d^55p \ (^2D) \ ^3F$
363436	363364	72	3	$59.1 \ 4d^55p \ (^2D) \ ^1F + 15.5 \ 4d^55p \ (^2D) \ ^1F + 8.9 \ 4d^55p \ (^2D) \ ^3F$
		. —		r r r r r r r r r r

Table A 40. Contir 1

a:a: From Kleef [43] and Joshi [44] b: This work c: Only the component $\geq 5\%$ are given

Transitions

 Wavelength	Lower Level ^a	Jran	Upper level ^a	Jun	log gf	gA	CF	O
Å	cm ⁻¹	• L0w	cm^{-1}	0 <i>U p</i>	108 81	s ⁻¹	01	
319.044	21513	6	334949	5	-0.79	1.07E + 10	0.17	
325.219	53991	4	361476	3	-0.57	1.68E + 10	0.147	
326.966	27959	5	333801	4	-0.67	1.35E + 10	-0.359	
327.916	56519	2	361476	3	-0.92	7.46E + 09	0.251	
329.316	55982	3	359642	2	-0.75	1.10E + 10	0.191	
329.451	29660	4	333195	3	-0.75	1.09E + 10	-0.162	
330.132	30361	3	333270	2	-0.83	9.14E + 09	-0.164	
221 444	54195 61796	4	262426	2	-0.19	$3.91E \pm 10$ $2.47E \pm 10$	-0.305	
336 698	44725	3	341727	2	-0.24	$3.47E \pm 10$ 8.44E \pm 09	-0.166	
336.762	2693	3	299639	4	-1	5.84E + 09	0.13	
340.6	21812	5	315412	4	-0.61	1.41E + 10	-0.145	1
340.922	34195	6	327517	5	-0.83	8.46E + 09	-0.196	
340.967	53991	4	347274	3	-0.13	4.23E + 10	0.5	
341.88	0	4	292500	4	-1	5.65E + 09	-0.152	
342.043	21812	5	314173	4	-0.92	6.89E+09	-0.059	
342.63	55982	3	347842	2	-0.43	2.12E + 10	0.456	
343.272	29000	6	311062	5	-0.97	$0.02E \pm 0.09$ 2.61E \pm 10	0.005	
344 427	25145	4	315482	3	-0.93	$6.61E \pm 09$	0.083	
344.55	41372	2	331606	2	-0.9	7.09E+09	-0.09	
345.057	2693	3	292500	4	-0.83	8.37E + 09	0.284	1
345.217	21513	6	311186	7	-0.73	1.05E + 10	-0.348	1
345.544	27959	5	317357	4	-0.93	6.51E + 09	0.076	
346.13	25145	4	314054	3	-0.4	2.25E + 10	-0.251	
346.233	21513	6	310336	6	-0.71	1.08E + 10	-0.162	
346.259	0	4 5	288802	б л	-0.75	9.81E+09 6.12E+00	-0.277	
346.431	21012	0 9	202607	4	-0.90	0.13E+09 6.88E±00	-0.009	
346.866	54223	2	342519	1	-0.49	$1.80E \pm 10$	0.561	1
347.207	2693	3	290705	3	-0.59	1.41E + 10	0.324	
347.372	21513	6	309389	5	-0.23	3.27E + 10	0.631	
347.718	0	4	287590	4	-0.06	4.84E + 10	-0.721	1
347.734	21812	5	309389	5	-0.6	1.39E + 10	-0.225	
348.049	27959	5	315274	6	-0.46	1.93E + 10	-0.451	
348.365	0	4	287056	3	-0.77	9.44E+09	-0.265	
348.437	30361	3	317357	4	-0.89	$7.16E \pm 09$ $2.22E \pm 10$	-0.134	
348.732	21513	6	308266	5	-0.23	$9.76E \pm 09$	-0.041	
348.948	0	4	286576	4	-0.89	7.08E+09	-0.118	
349.096	21812	5	308266	5	-0.7	1.10E + 10	0.14	
349.187	21513	6	307892	6	-1	5.43E + 09	-0.202	
349.675	20495	4	306474	3	-0.82	8.31E + 09	-0.063	
349.781	51665	1	337558	2	-0.78	9.04E + 09	0.433	
349.962	55982	3	341727	2	-0.92	6.58E + 09	0.123	
350	0	4	285714	4	-0.78	9.05E+09	0.304	
351 004	20140	4	287590	4	-0.91	5.73E+09 5.70E+09	0.007	
351.082	32651	2	317485	2	-0.5	1.71E + 10	-0.157	
351.149	29660	4	314439	5	-0.79	8.75E + 09	0.185	
351.327	21513	6	306148	5	0.02	5.60E + 10	-0.677	
351.478	29660	4	314173	4	-0.52	1.64E + 10	0.116	1
351.62	21812	5	306210	4	-0.72	1.03E + 10	-0.106	
351.64	25145	4	309527	4	-0.95	6.04E + 09	-0.084	
351.663	2693	3	287056	3	-0.86	7.47E+09	-0.153	
352 047	0000	4	284053	3	-0.82	$2.22E \pm 09$ $2.30E \pm 10$	-0.401	
352.047	27959	5	284055	5	-0.37	$1.08E \pm 10$	-0.492	
352.204	33558	1	317485	2	-0.99	5.55E+09	0.116	
352.324	21812	5	305642	6	-0.68	1.12E + 10	0.417	
352.548	20495	4	304144	4	-0.86	7.33E + 09	-0.05	1
352.807	21513	6	304954	5	-0.79	8.71E+09	0.177	
353.18	21812	5	304954	5	-0.27	2.89E + 10	-0.317	
353.229	3993 2603	2	287090 285714	3 1	-0.45	1.08E+10 8.60E-1.00	-0.470	
353 346	27959	5	310968	4	-0.19	3.73E+10	0.473	
353.568	32651	2	315482	3	-0.95	6.02E + 09	-0.084	
353.794	41372	2	324022	3	-0.85	7.42E + 09	0.103	1
353.968	27959	5	310470	4	-0.29	2.72E + 10	0.267	1
354.096	24441	3	306850	2	-0.86	7.38E + 09	-0.1	
354.23	29660	4	311962	5	-0.54	1.54E+10	-0.295	
354.408	34195	6	316356	5	-0.23	3.13E + 10 2.67E + 10	-0.186	
354.508	24441 33500	3	315489	3 3	-0.3	2.07 ± 10 $2.08E\pm10$	-0.17	
354.733	33509	3	315412	4	-0.92	$6.40E \pm 0.09$	-0.108	
354.753	2693	3	284579	3	-0.86	7.38E + 09	0.296	
354.852	30361	3	312169	3	-0.56	1.47E + 10	-0.183	
354.971	2693	3	284406	2	-0.23	3.13E + 10	-0.647	1
354.994	4941	1	286636	2	-0.56	1.47E + 10	-0.404	
355.105	0	4	281607	5	-0.53	1.57E+10	-0.523	
355.151	∠0495 25145	4 1	302081 306716	4	-0.8	0.43E+09 7 06E-00	-0.102	
355 154	20140	4 5	309527	3 4	-0.81	8 20E±09	-0.103	
355.328	27959	5	309389	5	-0.67	1.13E+10	-0.144	
355.416	2693	3	284053	3	-0.91	6.54E + 09	-0.109	
355.789	25145	4	306210	4	-1	5.30E + 09	-0.06	
355.805	41372	2	322425	1	-0.55	1.47E + 10	0.467	
355.823	56519	2	337558	2	-0.52	1.61E + 10	-0.345	
355.925	53991	4	334949	j ∕	-0.42	2.01E+10 5.22E + 10	0.431	
356.042	2095 28232	э 1	⊿oooo9 309083	4 2	-0.62	$1.26E \pm 10$	0.224	
356.112	29660	4	310470	4	-0.88	6.87E+09	0.06	
356.123	33558	1	314360	1	-0.78	8.84E + 09	0.199	1
356.149	37481	4	318263	5	-0.98	5.57E + 09	0.174	1
356.299	33509	3	314173	4	-0.75	9.44E + 09	-0.244	1

Table A41: Computed oscillator strengths and transition probabilities Ag VI.

Table A41: Continued

Wavelength	Lower Level	JLow	Upper level	JUP	log gf	gA 5 76E 00	CF 0.165
356.387	29660	4	310253	3	-0.34	2.42E+10	0.207
356.423	21042	2	301607	3	-0.51	1.61E + 10 7.27E + 00	-0.247
356.531	20495	3 4	300975	3	-0.85	4.41E+10	-0.399
356.539	33509	3	313984	2	-0.27	2.80E+10	-0.425
356.645	21513	6	285791 301904	1 5	-0.43 -0.76	1.95E+10 9.21E+09	-0.613 0.175
356.663	0	4	280377	3	-0.14	3.81E + 10	-0.387
356.751 356.783	27959 3953	5 2	$308266 \\ 284236$	5 2	-0.34 -0.26	2.41E+10 2.87E+10	$0.292 \\ 0.574$
356.788	21042	2	301320	3	-0.78	8.67E + 09	-0.197
356.801	21812 34195	5	302081	4 5	-0.41	2.05E+10 1.43E+11	-0.337
356.983	21042	2	301167	2	-1	5.27E+09	-0.096
357.015	3953	2	284053	3	-0.66	1.16E + 10	-0.196
357.079	25307	2	305357	2	-0.73	9.82E+09	-0.135
357.08	4941	1	284990	1	-0.3	2.65E+10	-0.66
357.131	24441 20495	3 4	300460	4 3	-0.92	1.04E+10	-0.103
357.281	30361	3	310253	3	-0.43	1.96E + 10	0.187
$357.313 \\ 357.385$	$29660 \\ 53991$	4	309527 333801	4	-0.52 -0.49	1.57E+10 1.68E+10	-0.177 0.477
357.422	32651	2	312432	2	-0.99	5.36E + 09	-0.078
357.654 357.758	37481 32651	4	317081	3	-0.2	3.29E+10 6.17E+09	-0.418 0.185
357.827	4941	1	284406	2	-0.56	1.44E+10	-0.357
357.937	27959	5	307338	4	-0.72	1.00E+10	0.104
358.03 358.041	44725	4 3	324022	4 3	-0.2	7.00E+09	-0.066
358.238	20495	4	299639	4	-0.79	8.47E + 09	0.085
358.26 358.3	33509	3	$312636 \\ 279096$	3	-0.76 -0.87	9.14E+09 7 07E+09	-0.104 -0.232
358.363	54223	2	333270	2	-0.17	3.48E + 10	0.453
358.424	25145	4	304144	4	-0.2	3.30E+10	0.36
358.584	37481	3 4	316356	5	-0.58	1.38E+10 1.12E+10	0.25 0.153
358.733	21812	5	300571	4	-0.08	4.35E + 10	0.491
358.78 358.86	30361 33509	3	$309083 \\ 312169$	2	-0.6 -0.98	1.31E+10 5.50E+09	$0.261 \\ 0.149$
358.914	28232	1	306850	2	-0.74	9.42E + 09	-0.157
359.058 359.064	24441 25145	3	302948 303647	2 5	-0.33	2.45E+10 2.28E+10	-0.379
359.201	3953	2	282349	3	-0.38	2.18E+10	-0.323
359.227	20495	4	298870	5	-0.88	6.82E+09	0.084
359.41	3953	2	282187	4	-0.55	1.52E+10 1.11E+10	-0.140 -0.523
359.468	27959	5	306148	5	-0.61	1.27E + 10	-0.253
$359.54 \\ 359.712$	$25307 \\ 37481$	2 4	$303440 \\ 315482$	1 3	-0.65 -0.81	1.15E+10 8.01E+09	-0.29
359.802	37481	4	315412	$\tilde{4}$	-0.39	2.09E + 10	0.268
359.947 360.013	55982 34195	3	333801 311962	4	-0.63	1.21E+10 4 71E+10	0.264 0.669
360.12	0	4	277686	5	0.18	7.85E+10	-0.656
360.122	2693	3	280377	3	-0.24	2.93E+10	0.486
360.162	21513	6	299164	7	-0.08	2.50E+10	-0.354
360.546	21513	6	298870	5	-0.87	6.88E+09	-0.136
360.663	20495	3 4	297762	2 4	-0.73	9.65E+09 5.02E+10	-0.324
360.689	21042	2	298289	3	-0.76	8.94E + 09	0.29
$360.734 \\ 360.758$	$55982 \\ 37481$	3	$333195 \\ 314675$	3	-0.06 0.05	4.51E+10 5.80E+10	$0.474 \\ -0.443$
360.849	28232	1	305357	2	-0.55	1.45E + 10	0.332
360.935 360.938	21812 29660	5 4	298870 306716	5	-0.1 -0.96	4.05E+10 5.62E+09	-0.371 0.1
360.975	21042	2	298069	1	-0.78	8.51E + 09	-0.133
361.017 361.023	27959 34195	5	304954	5	-0.39	2.10E+10 6.39E+09	0.299
361.063	0	4	276960	4	-0.44	1.86E+10	-0.429
361.124	28232	1	305146	1	-0.37	2.17E+10	0.416
361.169	24441	3	301320	3	-0.37	2.16E+0.09	$0.254 \\ 0.259$
361.189	21513	6	298376	7	-0.66	1.13E+10	0.644
361.325	25145 33509	4 3	310253	э З	-0.79	6.61E+09	$0.197 \\ 0.142$
361.413	37481	4	314173	4	0.05	5.68E + 10	-0.476
361.505 361.554	21513 32651	6 2	298134 309234	6 1	-0.28	9.70E+10 2.97E+10	-0.757 0.472
361.598	29660	4	306210	4	-0.6	1.30E + 10	0.112
361.678 361.713	30361 25145	3	306850 301607	2	-0.89 -0.86	6.56E+09 7 07E+09	-0.159 0.143
361.721	61726	4	338183	3	0.1	6.47E + 10	0.482
361.854	30361	3	306716	3	-0.86	7.11E+09 2.75E+10	-0.122
362.075	27959	5	304144	4	-0.56	1.39E+10	-0.197
362.089	25145	4	301320	3	-0.49	1.64E + 10	-0.233
362.149	24441	3	300571	4	-0.78	8.42E+09	0.123
362.171 362.171	30361	3	306474	3	-0.33	2.39E+10	-0.216
362.301	25307	2 2	301320	2 3	-0.58	1.04E+10	-0.204
362.502	25307	2	301167	2	-0.77	8.55E+09	-0.227
362.554 362.701	25145 53991	4 4	300966 329700	5 3	-0.8 -0.86	7.99E+09 7.06E+09	-0.231 -0.238
362.729	27959	5	303647	5	-0.41	1.97E + 10	-0.257
362.818 362.845	20495 27959	4	296115 303559	5	-0.45 -0.35	1.81E+10 2.28E+10	-0.279 0.558
362.892	21513	6	297077	5	-0.62	1.22E + 10	-0.156
363.007 363.141	54223 21042	2	$329700 \\ 296417$	3 3	-0.54 -0.49	1.47E+10 1.65E+10	0.412 0.261
363.222	44725	3	320038	4	-0.53	1.48E+10	0.168
363.236 363.287	61726 21812	4	337029 297077	5 5	-0.47	1.70E+10 3.11E+10	0.39
556.201	21012	0	201011	0	J. 2 I	0.11D F10	0.000

Table A41: Continued

Wavelength	Lower Level	JLow	Upper level	J_{Up}	log gf	gA	CF
363.375 363.432	24441 37481	3	299639 312636	4	-0.96 -0.5	5.57E+09 1.61E+10	$0.169 \\ -0.246$
363.5	61726	4	336829	4	0.23	8.62E + 10	0.554
363.539	0	4	275074	3	-0.6	1.27E+10	0.362
363.642 363.775	30361 33509	3	305357 308405	2	-0.54 -0.84	1.44E+10 7.33E+09	-0.178 -0.277
363.913	29660	4	304451	4	-0.36	2.20E + 10	-0.183
364.307	25145	4	299639	4	-0.59	1.29E+10	0.172
364.324	37481	4	311962	4 5	-0.48	6.87E+09	$0.101 \\ 0.204$
364.445	21042	2	295431	ĩ	-0.43	1.88E + 10	0.267
364.561	21812	5	296115	5	-0.8	7.98E+09	0.125
364.608 364.844	2693	3	276960 304451	4	-0.5	1.58E+10 1.02E+10	-0.241
364.868	34195	6	308266	5	-0.61	1.23E + 10	-0.287
364.988	21042	2	295023	2	-0.48	1.65E + 10	-0.303
364.989	53991 27959	4	327972 301904	4	-0.64	1.16E+10 4 21E+10	-0.345 0.481
365.235	24441	3	298238	4	-0.61	1.22E+10 1.22E+10	-0.208
365.328	24441	3	298168	4	-0.74	9.18E + 09	0.235
365.34	55982 24105	3	329700	3	-0.64	1.14E+10 5.56E+00	-0.133
365.551	21812	5	295372	4	-0.44	1.83E+10	-0.231
365.595	53991	4	327517	5	-0.63	1.18E + 10	-0.427
365.646	24441	3	297930 306850	2	-0.95	5.60E + 09 7 59E + 09	0.147
366.093	53991	4	327145	4	0.06	5.75E+10	0.2
366.107	25145	4	298289	3	-0.75	8.85E + 09	0.153
366.282	53991	4	327004	3	-0.72	9.46E+09	0.128
366.607	37481	4	310253	3	-0.81	1.27E+10	$0.178 \\ 0.138$
366.674	41639	0	314360	1	-0.82	7.51E + 09	0.328
366.702	33509	3	306210	4	-0.58	1.32E + 10	0.258
366.815	25145 29660	4	297762 302081	4	-0.85	$6.98E \pm 10$ 1 59E \pm 10	-0.073
367.165	2693	3	275050	2	-0.94	5.63E + 09	0.202
367.194	21513	6	293848	6	0.16	7.11E + 10	-0.54
367.586	37481	4	309527	4	-0.98	5.17E+09 3.93E+10	-0.081
367.739	25145	4	297077	5	-0.85	7.01E+09	-0.103
368.107	29660	4	301320	3	-0.86	6.79E + 09	-0.117
368.367	61726	4	333195	3	-0.56	1.35E+10	0.418
368.634	$\frac{34195}{25145}$	6 4	305642 296417	3	-0.82	1.16E + 11 7.52E + 09	-0.146
368.782	55982	3	327145	4	-0.39	1.99E + 10	-0.373
368.923	41372	2	312432	2	-0.78	8.09E+09	-0.15
369.124	27959 41372	5	298870 312169	5 3	-0.8	7.72E+09 1.88E+10	0.098
369.429	21812	5	292500	4	-0.55	1.40E+10	-0.225
369.543	21513	6	292117	5	0.22	8.17E+10	0.534
369.574	24441 56519	3	295023 327004	2	-0.49	1.58E+10 1.47E+10	0.215
369.952	21812	5	292117	5	-0.98	5.09E+09	0.063
370.083	30361	3	300571	4	-0.94	5.58E + 09	-0.097
370.084	27959	5	298168	4	-0.74	8.94E+09	0.129
370.438	44725	3	314675	3	-0.53	1.43E+10 1.43E+10	0.125
370.567	37481	4	307338	4	-0.5	1.53E + 10	-0.276
370.641	27959	5	297762	4	-0.65	1.09E+10	0.157
370.833	21042 21513	6	290705 291127	3 7	-0.8	1.76E+09 1.76E+10	0.148 0.555
371.245	34195	6	303559	6	-0.34	2.22E + 10	0.203
371.457	29660	4	298870	5	-0.47	1.63E+10	0.19
371.750	20495 41372	4 2	289489 310303	3 2	-0.25	$2.74E \pm 10$ $2.11E \pm 10$	0.284 0.271
371.977	24441	3	293275	2	-0.73	8.93E+09	-0.123
371.991	24441	3	293265	3	-0.85	6.79E+09	-0.065
372.34	33509 20495	3	288802	4 5	-0.82	7.34E+09 2.88E+10	0.381 0.377
372.843	20495	4	288704	3	-0.5	1.52E+10	0.184
372.967	25145	4	293265	3	-0.67	1.03E + 10	0.137
373.192	25307	2	293265	3	-0.87	6.43E+09 1 84E+10	-0.166
373.4	32651	2	300460	3	-0.8	7.52E+09	0.238
373.476	21812	5	289567	4	-0.26	2.61E+10	0.177
373.537 373.568	41372 20495	2 4	309083 288184	2 5	-0.71 -0.78	9.38E+09 8.00E+09	0.22
373.828	56519	2	324022	3	-0.91	5.92E + 09	0.306
373.953	27959	5	295372	4	-0.82	7.26E + 09	0.135
374.068	21812	5	289143	6	-0.68	9.94E+09	0.296 0.155
374.55	25145	4	292117	5	-0.49	1.55E+10	-0.31
374.59	44725	3	311683	4	-0.52	1.43E + 10	0.327
374.994	21513	6	288184	5	-1	4.72E+09	-0.096
375.593	61726	4	327972	4	-0.58	1.25E+10	0.296
375.757	33509	3	299639	4	-0.99	4.85E + 09	-0.243
375.975	24441	3	290416	2	-0.99	4.79E + 09	0.076
376.537	44725	3	310303	2	-0.5	1.49E+10	-0.208
376.607	44725	3	310253	3	-0.48	1.56E + 10	-0.195
376.977	30361	3	295629	2	-0.9	5.86E+09	-0.109
377.179	20495 24441	4 3	289714 289567	4 4	-0.44 -0.84	1.71E+10 6.75E+09	-0.115
377.343	30361	3	295372	4	-0.66	1.02E + 10	0.158
377.37	55982	3	320974	3	-0.42	1.77E+10	0.181
377.402	34195 33509	ь З	299164 298421	2	-0.56 -0.71	1.28E+10 9.24E+09	0.017
378.056	33558	1	298069	1	-0.93	5.55E + 09	-0.145
378.136	56519	2	320974	3	-0.83	6.96E + 09	0.213
378.183 378.256	25145 33558	4	289567 297930	4	-0.85 -0.99	6.59E+09 4 77E+09	-0.139 0.255
378.295	25145	4	289489	3	-0.9	5.82E + 09	0.07
378.398	53991	4	318263	5	-0.41	1.80E + 10	0.218
378.527	25307	2	289489	3	-0.66	1.03E + 10	-0.325

		Table	A41: Con	tinue	ea		
Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA	CF
378.528	34195	6	298376	7	-0.57	1.25E + 10	0.398
378.561	27959	5	292117	5	-0.69	9.55E + 09	0.103
378.564	21812	5	285968	5	-0.49	1.50E + 10	0.18
378 667	20495	4	284579	3	-0.82	6.98E±09	0.124
279 709	55082	2	204019	4	-0.82	$7.25E \pm 0.0$	0.124
378.708	01510	3	320038	4	-0.8	1.50E+10	0.150
378.713	21513	0	285565	0	-0.47	1.59E + 10	0.158
380.434	54223	2	317081	3	-0.55	1.30E + 10	0.22
380.449	21812	5	284660	4	-0.65	1.05E + 10	0.263
380.669	51665	1	314360	1	-0.96	5.06E + 09	-0.181
381.014	29660	4	292117	5	-0.79	7.49E + 09	-0.178
381.215	51665	1	313984	2	-0.93	5.36E + 09	0.141
381.249	61726	4	324022	3	-0.64	1.05E + 10	-0.102
381.809	25145	4	287056	3	-0.97	4.93E + 09	0.111
382.251	27959	5	289567	4	-0.95	$5.18E \pm 0.09$	-0.057
382 406	55982	3	317485	2	-0.92	5.50E+09	-0.118
382 422	53001	4	315482	3	0.74	$8.21E \pm 0.00$	0.002
282.422	44795	2	206210	4	-0.74	6.08E+00	0.032
302.43	44720	3	300210	4 F	-0.82	1.4011+10	-0.218
382.572	37481	4	298870	5	-0.49	1.48E + 10	0.293
382.592	55982	3	317357	4	-0.72	8.60E + 09	0.121
383.192	56519	2	317485	2	-0.4	1.79E + 10	0.301
383.484	51665	1	312432	2	-0.51	1.42E + 10	-0.439
383.694	32651	2	293275	2	-0.9	5.74E + 09	0.141
384.127	54223	2	314554	2	-0.89	5.84E + 09	0.101
384.346	53991	4	314173	4	-0.99	4.61E + 09	-0.042
385.021	44725	3	304451	4	-0.82	6.78E + 09	-0.226
385.215	37481	4	297077	5	-0.78	7.43E + 09	-0.151
385 334	25145	4	284660	4	-0.74	$8.21E \pm 0.09$	-0.107
385 731	61726	4	320974	3	-0.6	$1.12E \pm 10$	0.147
286.087	51665	1	210674	1	0.00	1.12E 10 4.61E 00	0.155
296 156	51005	1	215492	2	-0.99	$4.01E \pm 10$	-0.133
380.150	55000	2	01462		-0.20	$2.44E \pm 10$	-0.237
386.559	55982	3	314675	3	-0.77	7.56E+09	0.13
386.63	53991	4	312636	3	-0.86	6.20E + 09	0.092
386.71	24441	3	283033	2	-1	4.46E + 09	-0.145
386.768	0	4	258553	3	-0.05	3.99E + 10	-0.454
387.129	61726	4	320038	4	-0.11	3.45E + 10	-0.278
388.19	27959	5	285565	6	-0.58	1.17E + 10	0.418
388.809	33509	3	290705	3	-0.56	1.22E + 10	0.187
388.996	2693	3	259765	2	-0.37	1.90E + 10	-0.352
389.14	53991	4	310968	4	-0.64	1.02E + 10	0.167
389 508	3953	2	260687	1	-0.81	$6.88E \pm 0.9$	-0.297
389 558	27959	5	284660	4	-0.65	$9.92E \pm 0.00$	0.157
280.805	52001	4	210470	-1	0.07	9.32E + 0.00	0.286
280.020	53991	4	210674	1 1	-0.27	$2.34E \pm 10$ 1.20E ± 10	0.280
369.939	54225	2	310074	1	-0.5	1.39E+10	0.31
389.94	55982	3	312432	2	-0.77	7.39E+09	0.131
390.155	29660	4	285968	5	-0.82	6.69E + 09	0.256
390.34	55982	3	312169	3	-0.75	$7.74E \pm 09$	0.091
390.44	21042	2	277163	2	-0.94	4.99E + 09	-0.113
390.838	2693	3	258553	3	-0.64	9.91E + 09	0.425
390.913	3953	2	259765	2	-0.55	1.25E + 10	0.363
391.013	4941	1	260687	1	-0.67	9.37E + 09	0.342
391.615	30361	3	285714	4	-1	4.32E + 09	0.223
392.281	29660	4	284579	3	-0.96	$4.81E \pm 0.9$	0.082
392 727	61726	4	316356	5	-0.29	2.22E+10	-0.329
303 281	55082	3	310253	3	0.80	$5.50E \pm 00$	0.064
305 706	61726	3	314430	5	0.73	7.05E±00	0.004
200 160	22500	4	004660	4	-0.75	F 70E + 00	0.224
398.168	33509	3	284660	4	-0.87	5.72E+09	-0.12
419.945	53991	4	292117	5	-0.93	4.42E + 09	-0.298

Table A41: Continued

a: Energy Levels from [43]

Ag VII

Energy Levels

Ean	E^b_{calc}	Δ E	J	Leading components (in $\%$) in LS Coupling ^{c}
0	-65	65	2.5	$97.5 \ 4d^5 \ (^6S) \ ^6S$
29390	29381	9	2.5	79.5 4d ⁵ (⁴ G) ⁴ G + 8 4d ⁵ (² F) ² F
30378	30381	-3	3.5	$93.1 \ 4d^5 \ (^4G) \ ^4G$
30662	30668	-6	5.5	96.5 $4d^5$ (⁴ G) ⁴ G
30907	30901	6	4.5	$97.4 \ 4d^5 \ (^4G) \ ^4G$
32005	32063	-58	2.5	$44.9 \ 4d^5 \ (^4P) \ ^4P + 35 \ 4d^5 \ (^4D) \ ^4D + 12.3 \ 4d^5 \ (^4G) \ ^4G$
32994	33032	-38	1.5	53.6 4d ⁵ (⁴ P) ⁴ P + 43.6 4d ⁵ (⁴ D) ⁴ D
34605	34634	-29	0.5	$66.7 \ 4d^5 \ (^4P) \ ^4P + 31.9 \ 4d^5 \ (^4D) \ ^4D$
36485	36493	-8	3.5	91.8 $4d^5$ (⁴ D) ⁴ D
38685	38683	2	0.5	$67.8 \text{ 4d}^5 (^4\text{D}) ^4\text{D} + 31.3 \text{ 4d}^5 (^4\text{P}) ^4\text{P}$
39299	39243	56	2.5	54.3 4d ⁵ (⁴ D) ⁴ D + 31.8 4d ⁵ (⁴ P) ⁴ P + 6.9 4d ⁵ (² D) ² D
39788	39757	31	1.5	$53 \text{ 4d}^5 (^4\text{D}) ^4\text{D} + 43.6 \text{ 4d}^5 (^4\text{P}) ^4\text{P}$
44011	44016	-5	5.5	$88.4 4d^5 (^2I) ^2I + 10.4 4d^5 (^2H) ^2H$
45546	45543	3	6.5	99.9 $4d^5$ (² I) ² I
47119	47030	89	2.5	$31.9 4d^5 (^2\text{F}) ^2\text{F} + 30.1 4d^5 (^2\text{D}) ^2\text{D} + 12 4d^5 (^4\text{P}) ^4\text{P}$
48086	48109	-23	1.5	$40.8 4d^5 (^2\text{D}) \ ^2\text{D} + 43.5 \ 4d^5 (^4\text{F}) \ ^4\text{F} + 13.2 \ 4d^5 (^2\text{D}) \ ^2\text{D}$
48712	48950	-238	3.5	$48.8 4\text{d}^5 (^4\text{F}) \ ^4\text{F} + 23.2 4\text{d}^5 (^2\text{F}) \ ^2\text{F} + 15.1 4\text{d}^5 (^2\text{G}) \ ^2\text{G}$
49104	49101	3	4.5	59.8 4d ⁵ (⁴ F) ⁴ F + 32.8 4d ⁵ (² G) ² G + 5.3 4d ⁵ (² H) ² H
51049	51141	-92	2.5	$75.2 4d^5 ({}^4\text{F}) {}^4\text{F} + 11.7 4d^5 ({}^2\text{F}) {}^2\text{F} + 6.8 4d^5 ({}^2\text{F}) {}^2\text{F}$
53353	53174	179	3.5	$50 \ 4d^5 \ (^2F) \ ^2F + 29.4 \ 4d^5 \ (^4F) \ ^4F + 8.8 \ 4d^5 \ (^2G) \ ^2G$
53796	53836	-40	1.5	$53.7 4d^5 ({}^4\text{F}) {}^4\text{F} + 37.3 4d^5 ({}^2\text{D}) {}^2\text{D} + 6.2 4d^5 ({}^2\text{D}) {}^2\text{D}$
53797	53768	29	4.5	$52.3 \text{ 4d}^5 (^2\text{H}) ^2\text{H} + 29 \text{ 4d}^5 (^4\text{F}) ^4\text{F} + 18.5 \text{ 4d}^5 (^2\text{G}) ^2\text{G}$
55773	55969	-196	3.5	73.3 4d ⁵ (² G) ² G + 19.4 4d ⁵ (² F) ² F + 5.6 4d ⁵ (² F) ² F
57413	56937	476	2.5	$48.9 \ 4d^5 \ (^2F) \ ^2F + 20 \ 4d^5 \ (^2D) \ ^2D + 19 \ 4d^5 \ (^2F) \ ^2F$
57962	57884	78	5.5	$86.3 \text{ 4d}^5 (^2\text{H}) ^2\text{H} + 11.3 \text{ 4d}^5 (^2\text{I}) ^2\text{I}$
59223	59186	37	4.5	$47.7 \ 4d^5 \ (^2G) \ ^2G + 41.4 \ 4d^5 \ (^2H) \ ^2H + 9.6 \ 4d^5 \ (^4F) \ ^4F$
59792	59608	184	3.5	$77.3 \ 4d^5 \ (^2F) \ ^2F + 15.8 \ 4d^5 \ (^4F) \ ^4F$
59954	60469	-515	2.5	$17.1 \ 4d^5 \ (^2D) \ ^2D + 34.3 \ 4d^5 \ (^2F) \ ^2F + 28.7 \ 4d^5 \ (^2F) \ ^2F$
71517	71544	-27	1.5	$97.3 \ 4d^5 \ (^2D) \ ^2D$
72934	72951	-17	2.5	90.8 4d ⁵ (² D) ² D + 6.5 4d ⁵ (² F) ² F
79131	79127	4	4.5	$98.8 \text{ 4d}^5 (^2\text{G}) ^2\text{G}$
79705	79729	-24	3.5	96.1 4d ⁵ (² G) ² G
103996	103917	79	2.5	$79.5 \text{ 4d}^5 (^2\text{D}) \ ^2\text{D} + 19.2 \text{ 4d}^5 (^2\text{D}) \ ^2\text{D}$
104821	104832	-11	1.5	$74 \text{ 4d}^5 (^2\text{D}) \ ^2\text{D} + 18.1 \text{ 4d}^5 (^2\text{D}) \ ^2\text{D}$
				a: From Ryabtsev [45]

Table A42: Comparison between available experimental data and calculated even energy levels (in $\rm cm^{-1}$) in Ag VII

a: From Ryabtsev [45] b: This work c: Only the component ≥ 5% are given

Table A43: Comparison between available experimental data and calculated odd energy levels (in cm^{-1}) in Ag VII

E^a_{exp}	E^b_{calc}	Δ E	J	Leading components (in $\%$) in LS Coupling ^{c}
331200	331234	-34	1.5	$39.8 \ 4d^{4}5p \ (^{5}D) \ ^{4}P + 29.8 \ 4d^{4}5p \ (^{5}D) \ ^{6}D + 24.8 \ 4d^{4}5p \ (^{5}D) \ ^{6}P$
333327	333186	141	2.5	$62.5 \ 4d^{4}5p \ (^{5}D) \ ^{6}P + 16.9 \ 4d^{4}5p \ (^{5}D) \ ^{4}P + 15.9 \ 4d^{4}5p \ (^{5}D) \ ^{6}D$
334906	334682	224	3.5	$85.5 \ 4d^45p \ (^5D) \ ^6P + 5.9 \ 4d^45p \ (^5D) \ ^6D$
336333	336133	200	1.5	$69.4 \ 4d^{4}5p \ (^{5}D) \ ^{6}P + 17 \ 4d^{4}5p \ (^{5}D) \ ^{6}D + 6.7 \ 4d^{4}5p \ (^{5}D) \ ^{4}P$
339172	339057	115	2.5	51.3 $4d^{4}5p$ (⁵ D) ⁶ D + 28.1 $4d^{4}5p$ (⁵ D) ⁶ P + 8.8 $4d^{4}5p$ (⁵ D) ⁴ P
341227	341268	-41	0.5	$64.6 \ 4d^{4}5p^{(5}D)^{6}D + 29.8 \ 4d^{4}5p^{(5}D)^{4}P + 1.5 \ 4d^{4}5p^{(1}P)^{1}S$
341458	341405	53	3.5	$61.6 \ 4d^{4}5p \ (^{5}D) \ ^{6}D + 17.1 \ 4d^{4}5p \ (^{5}D) \ ^{4}F + 11 \ 4d^{4}5p \ (^{5}D) \ ^{6}F$
341983	342086	-103	1.5	$30.5 \ 4d^{4}5p \ (^{5}D) \ ^{4}P + 29.7 \ 4d^{4}5p \ (^{5}D) \ ^{6}D +$
342289	342228	61	4.5	$42.6 \ 4d^{4}5p \ (^{5}D) \ ^{6}D + 24.8 \ 4d^{4}5p \ (^{5}D) \ ^{6}F + 24.7 \ 4d^{4}5p \ (^{5}D) \ ^{4}F$
343336	343453	-117	2.5	$_{38.7}^{4} 4d^{4}5p (^{5}D) ^{4}F + 35.8 4d^{4}5p (^{5}D) ^{4}P + 5.3 4d^{4}5p (^{5}D) ^{6}P$
344695	344814	_119	2.5	$27.5 4d^{4}5p ({}^{5}D) {}^{4}P + 35.7 4d^{4}5p ({}^{5}D) {}^{4}F + 25.4 4d^{4}5p ({}^{5}D) {}^{6}D$
346061	346107	136	3.5	$55.9 4d^45p (^5D) 4F + 26.2 4d^45p (^5D) 6D$
248277	248404	-130	4.5	$28.8 4d^{4}5p (^{5}D) 4F + 41.1 4d^{4}5p (^{5}D) 6D + 5.5 4d^{4}5p (^{3}H) 4I$
240047	240120	-117	95	28.840 Jp (D) F + 41.140 Jp (D) D + 5.540 Jp (H) 1 47.54d45p (3H) 4H + 22.54d45p (3C) 4H + 0.24d45p (3H) 2C
349047	349139	-92	3.0	$47.5 40 \text{ sp}(^{-}\text{H}) \text{ H} + 22.5 40 \text{ sp}(^{-}\text{G}) \text{ H} + 9.2 40 \text{ sp}(^{-}\text{H}) \text{ G}$
349721	349800	-79	4.5	0.740 sp(G) + 27.440 sp(H) + 25.040 sp(H) + 27.440 sp
352082	352117	-30	5.5	$38.0 4 \text{d} \text{ sp}(^{-}\text{H}) \text{H} + 31.4 4 \text{d} \text{ sp}(^{-}\text{H}) \text{I} + 17.1 4 \text{d} \text{ sp}(^{-}\text{G}) \text{H}$
352270	352276	-6	0.5	$75.9 \text{ 4d}^{5}\text{p} (^{\circ}\text{D}) ^{1}\text{D} + 9.6 \text{ 4d}^{5}\text{p} (^{\circ}\text{P}) ^{1}\text{D}$
352685	352838	-153	2.5	$25.4 \ 4d^{4}5p \ (^{3}G) \ ^{4}G + 22.7 \ 4d^{4}5p \ (^{3}F) \ ^{4}G + 14 \ 4d^{4}5p \ (^{3}F) \ ^{4}G$
353454	353591	-137	3.5	$17.3 \ 4d^{4}5p \ (^{3}H) \ ^{2}G + 20 \ 4d^{4}5p \ (^{3}G) \ ^{4}H + 9 \ 4d^{4}5p \ (^{3}F) \ ^{4}G$
353549	353519	30	1.5	$44.8 \ 4d^{4}5p \ (^{\circ}D) \ ^{\circ}D + 21.2 \ 4d^{4}5p \ (^{\circ}P) \ ^{\circ}D + 7.5 \ 4d^{4}5p \ (^{\circ}P) \ ^{\circ}D$
354122	354127	-5	4.5	$12.3 \ 4d^{4}5p \ (^{3}H) \ ^{2}G + 29.7 \ 4d^{4}5p \ (^{3}H) \ ^{4}H + 15.7 \ 4d^{4}5p \ (^{3}H) \ ^{4}I$
354235	354195	40	2.5	76 4d ⁴ 5p (⁵ D) ⁴ D + 3.9 4d ⁴ 5p (⁵ D) ⁴ D + 2.5 4d ⁴ 5p (⁵ F) ⁴ F
354719	354727	-8	6.5	47.6 $4d^{4}5p ({}^{3}H) {}^{4}H + 25.3 4d^{4}5p ({}^{3}H) {}^{4}I + 12.8 4d^{4}5p ({}^{3}H) {}^{2}I$
354869	354843	26	3.5	$66.2 4d^45p (^5D) \ ^4D + 6.1 \ 4d^45p (^3F) \ ^4F + 5.2 \ 4d^45p (^3D) \ ^4D$
355790	355539	251	0.5	$32.4 4d^45p (^{1}P) ^{4}P + 14.8 4d^45p (^{1}P) ^{4}P + 12.7 4d^45p (^{1}P) ^{1}S$
356233	356215	18	2.5	$14.2 4d^45p (^{3}\text{F}) ^4\text{D} + 13.4 4d^45p (^{1}\text{P}) ^4\text{D} + 13.1 4d^45p (^{3}\text{F}) ^4\text{G}$
356416	356440	-24	4.5	$31.7 \ 4d^45p \ (^{3}H) \ ^{4}I + 11.2 \ 4d^45p \ (^{3}G) \ ^{4}H + 10.7 \ 4d^45p \ (^{3}G) \ ^{4}G$
356493	356663	-170	3.5	$16.5 \ 4d^45p \ (^{3}F) \ ^{4}D + 11.8 \ 4d^45p \ (^{5}D) \ ^{4}D + 11.1 \ 4d^45p \ (^{3}G) \ ^{4}G$
356993	356957	36	1.5	$19.9 \ 4d^{4}5p \ (^{3}F) \ ^{2}D + 19.1 \ 4d^{4}5p \ (^{3}F) \ ^{4}F + 8.9 \ 4d^{4}5p \ (^{3}F) \ ^{2}D$
357689	357575	114	5.5	$45 \ 4d^{4}5p \ (^{3}H) \ ^{4}G + 12.8 \ 4d^{4}5p \ (^{3}H) \ ^{2}H + 12.2 \ 4d^{4}5p \ (^{3}H) \ ^{4}H$
358392	358321	71	2.5	$21.4 4d^{4}5p ({}^{3}F) {}^{4}G + 11.5 4d^{4}5p ({}^{3}G) {}^{2}F + 9.5 4d^{4}5p ({}^{1}P) {}^{4}D$
359687	359756	-69	3.5	$6.3 4d^{4}5p ({}^{3}F) {}^{2}G + 17.7 4d^{4}5p ({}^{3}G) {}^{4}G + 13.2 4d^{4}5p ({}^{3}H) {}^{4}G$
360092	360121	-29	1.5	$37.9 \ 4d^{4}5n \ (^{1}P) \ ^{4}P + 14.3 \ 4d^{4}5n \ (^{1}P) \ ^{4}P + 10.3 \ 4d^{4}5n \ (^{3}D) \ ^{4}D$
360481	360323	158	5.5	50.6 $4d^{4}5p$ (³ H) ⁴ I + 14.8 $4d^{4}5p$ (³ G) ⁴ G + 14 $4d^{4}5p$ (³ H) ⁴ H
360482	360532	50	4.5	$17.6 \ 4d^{4}5p \ (^{3}F) \ ^{4}C \ + \ 13.5 \ 4d^{4}5p \ (^{3}C) \ ^{4}F \ + \ 12.3 \ 4d^{4}5p \ (^{3}F) \ ^{4}F$
261172	261025	120	9.5	$40.2 \ 4d^{4}5p^{-}(^{3}F)^{4}C^{-} + 12.6 \ 4d^{4}5p^{-}(^{3}H)^{4}C^{-} + 10.1 \ 4d^{4}5p^{-}(^{3}C)^{4}H^{-}$
301173	301035	106	3.0 9.5	40.240 Sp (F) G + 15.040 Sp (H) G + 10.140 Sp (G) H $27.143^{4}\epsilon_{-}$ (^{3}E) ^{4}E + 10.4 $^{4}\epsilon_{-}$ (^{3}E) ^{2}D + 0 ϵ 4 $^{4}\epsilon_{-}$ (^{3}C) ^{4}E
361296	361402	-106	2.5	$27.14d \text{ sp}(^{-}\text{F}) \text{ F} + 104d \text{ sp}(^{-}\text{F}) \text{ D} + 9.54d \text{ sp}(^{-}\text{G}) \text{ F}$
361593	361784	-191	3.5	$25.4 \ 4d^{-5}p(^{\circ}G) \ F + 19.1 \ 4d^{-5}p(^{\circ}D) \ F + 8.9 \ 4d^{-5}p(^{\circ}D) \ F$
361650	361610	40	4.5	$32.1 \text{ 4d}^{-5}\text{p} (^{\circ}\text{H})^{-1}\text{G} + 23.1 \text{ 4d}^{-5}\text{p} (^{\circ}\text{G})^{-1}\text{G} + 11.2 \text{ 4d}^{-5}\text{p} (^{\circ}\text{F})^{-2}\text{G}$
362381	362524	-143	2.5	$4.5 \ 4d^{4}5p \ (^{1}D) \ ^{2}F + 18.1 \ 4d^{4}5p \ (^{3}H) \ ^{4}G + 12.2 \ 4d^{4}5p \ (^{3}D) \ ^{2}F$
362447	362541	-94	4.5	22.3 4d ⁺ 5p (³ H) ⁴ H + 27.4 4d ⁺ 5p (³ G) ⁴ F + 7.8 4d ⁺ 5p (³ G) ⁴ H
362535	362582	-47	5.5	$34.8 \ 4d^{4}5p \ (^{3}H) \ ^{2}I + 16.3 \ 4d^{4}5p \ (^{3}F) \ ^{4}G + 10.8 \ 4d^{4}5p \ (^{3}G) \ ^{2}H$
362942	363039	-97	3.5	$25.2 \ 4d^{4}5p \ (^{3}G) \ ^{4}H + 24.4 \ 4d^{4}5p \ (^{3}H) \ ^{4}H + 9.5 \ 4d^{4}5p \ (^{3}H) \ ^{2}G$
362975	362853	122	2.5	23.8 $4d^{4}5p$ (¹ P) ⁴ D + 18.6 $4d^{4}5p$ (³ G) ⁴ F + 12.1 $4d^{4}5p$ (¹ P) ⁴ D
363454	363574	-120	1.5	$32.2 \ 4d^45p \ (^{3}D) \ ^{4}F + 31.4 \ 4d^45p \ (^{3}G) \ ^{4}F + 10.8 \ 4d^45p \ (^{1}P) \ ^{4}P$
363614	363422	192	6.5	53.1 $4d^{4}5p$ (³ H) ⁴ I + 37.1 $4d^{4}5p$ (³ H) ⁴ H
364025	364158	-133	2.5	$15.1 \text{ 4d}^45 \text{p} (^3\text{D}) ^4\text{P} + 17.6 \text{ 4d}^45 \text{p} (^3\text{D}) ^2\text{D} + 8 \text{ 4d}^45 \text{p} (^3\text{F}) ^2\text{D}$
364518	364445	73	6.5	$35.8 4d^45p (^{3}\text{H}) ^{2}\text{I} + 23.6 4d^45p (^{3}\text{G}) ^{4}\text{H} + 14.7 4d^45p (^{3}\text{H}) ^{4}\text{I}$
364772	364791	-19	4.5	$18.9 \ 4d^45p \ (^{3}G) \ ^{4}F + 16.9 \ 4d^45p \ (^{3}F) \ ^{4}G + 12.7 \ 4d^45p \ (^{3}H) \ ^{2}G$
364877	364893	-16	2.5	$0.2 \ 4d^{4}5p \ (^{3}F) \ ^{2}D + 19.2 \ 4d^{4}5p \ (^{1}P) \ ^{4}P + 13 \ 4d^{4}5p \ (^{1}P) \ ^{4}P$
365017	365102	-85	5.5	$21.5 \ 4d^{4}5p(^{3}G)^{4}H + 28.1 \ 4d^{4}5p(^{3}H)^{4}H + 17.5 \ 4d^{4}5p(^{3}G)^{2}H$
365569	365533	36	4.5	$43.6 \ 4d^{4}5p \ ({}^{3}F) \ {}^{4}F + 9.3 \ 4d^{4}5p \ ({}^{3}G) \ {}^{2}H + 7.7 \ 4d^{4}5p \ ({}^{3}H) \ {}^{2}H$
365842	366094	-252	3.5	$19.8 \text{ 4d}^4 \text{ 5p} ({}^3\text{F}) {}^4\text{F} + 14 \text{ 4d}^4 \text{ 5p} ({}^3\text{F}) {}^2\text{G} + 13.6 \text{ 4d}^4 \text{ 5p} ({}^3\text{D}) {}^2\text{F}$
366078	365947	131	1.5	$16.7 4d^{4}5p (^{1}P) ^{4}S + 15.1 4d^{4}5p (^{1}P) ^{4}S + 14.2 4d^{4}5p (^{3}F) ^{4}F$
366573	366477	96	1.5	$27.2 4d^{4}5p (^{3}\text{F}) ^{4}\text{F} + 13.5 4d^{4}5p (^{3}\text{F}) ^{4}\text{D} + 10.7 4d^{4}5p (^{3}\text{F}) ^{2}\text{D}$
366693	366575	118	2.5	9.1 dd^45p (³ G) ⁴ F + 13.5 dd^45p (³ F) ⁴ D + 12 dd^45p (³ D) ⁴ D
366806	366568	228	3.5	9.7
367483	367392	91	5.5	$40.3 4d^{4}5p ({}^{3}F) {}^{4}G + 21.2 4d^{4}5p ({}^{3}H) {}^{2}I + 9.7 4d^{4}5p ({}^{3}G) {}^{4}H$
367010	367657	262	2.5	$10.0 \text{ 4d}^{4}\text{5p}$ (¹ P) ⁴ P + 25.6 4d ⁴ 5p (³ D) ⁴ P + 0.4 4d ⁴ 5p (³ C) ⁴ C
268420	269257	202	4.5	$^{26} 4d^{4}5p (^{3}C) ^{4}H + 15.6 4d^{4}5p (^{3}F) ^{4}C + 12.6 4d^{4}5p (^{3}H) ^{2}H$
268560	268582	14	4.5	204d 5p(3p) 4D + 0.24d 5p(7) 4E + 7.24d 5p(11) 4D
308309	308383	-14	1.0	2540.5p(T) D + 9.540.5p(D) T + 7.240.5p(D) D
308908	308933	13 E0	1.5	(1.140 Jp(17) F + 20.740 Jp(17) D + 12.140 Jp(17) D
260579	260476	109	1.5	$0.240 \text{ Jp}(D) = 29.240 \text{ Jp}(D) = 7 \pm 20.940 \text{ Jp}(D) = 20.4445 \text{ g}(3\text{F})^2 \text{F} \pm 14.4445 \text{ g}(3\text{F}) = 4.4445 \text{ g}(3\text{F})^4 \text{C}$
260654	260608	102	6.5	$20.2 \ 4d^{4}5p(11)^{2}K + 22.0 \ 4d^{4}5p(11)^{2}I + 18.4 \ 4d^{4}5p(3H)^{2}I$
360661	360500	199	5.5	$^{23.7}$ 4d 45 $^{(1)}$ 21 $^{+}$ $^{10.4}$ 40 $^{(1)}$ 11 $^{-10.4}$ 40 $^{(1)}$ 11 11 21 $^{-11}$ $^{-11}$ $^{$
369870	369528	100	0.0	35.740 $3p(1)$ $1 + 19.940$ $3p(1)$ $1 + 15.940$ $3p(1)$ 1
309879	309737	122	3.J E E	23.44 d 5p (1) D + 12.74 d 5p (1) F + 9.24 d 5p (1) G
370488	370344	-00	0.0	17.4 4 d 3 p (G) H + 21.1 4 d 3 p (G) H + 19 4 d 3 p (G) G
370501	370601	-100	4.5	$12.0 \ 4d \ 5p(^{-}H) \ H + 11.1 \ 4d \ 5p(^{-}G) \ G + 9.0 \ 4d \ 5p(^{-}F) \ G$
370993	371099	-106	3.5	$25.3 4d^{-}5p(^{\circ}G)^{-}F + 30 4d^{-}5p(^{\circ}F)^{-}F + 10 4d^{-}5p(^{\circ}G)^{-}G$
371061	371084	-23	4.5	$23.8 \text{ 4d}^{-5}\text{p} (^{\circ}\text{G})^{-2}\text{H} + 17 \text{ 4d}^{-5}\text{p} (^{\circ}\text{H})^{-2}\text{H} + 11.3 \text{ 4d}^{-5}\text{p} (^{\circ}\text{H})^{-2}\text{G}$
371408.6	371168	240.6	1.5	$25.4 \ 4d^{5} \text{ 5p} (^{1} \text{P})^{2} \text{D} + 14.7 \ 4d^{5} \text{5p} (^{1} \text{P})^{2} \text{P} + 12.7 \ 4d^{5} \text{5p} (^{1} \text{P})^{2} \text{D}$
371673	371750	-77	3.5	21.4 4d ⁴ 5p (³ G) ^{4}G + 20.9 4d ⁴ 5p (¹ G) ^{2}F + 8 4d ⁴ 5p (³ F) ^{2}G
372051	372060	-9	2.5	21.6 4d ⁴ 5p (³ H) ${}^{4}G$ + 18.5 4d ⁴ 5p (³ F) ${}^{2}F$ + 17.6 4d ⁴ 5p (³ G) ${}^{4}G$
372676	372533	143	5.5	46.4 4d ⁺⁵ p ('H) 'H + 16.1 4d ⁺⁵ p ('I) 'H + 12.4 4d ⁺⁵ p ('I) 'I
372822	372804	18	6.5	51.1 4d ⁺ 5p (°G) ^{+}H + 29.2 4d ⁺ 5p (°H) ^{-}I + 7.9 4d ⁺ 5p (°H) ^{4}H
373120	373163	-43	4.5	21 4d ⁺ 5p (³ G) ⁴ G + 14.2 4d ⁺ 5p (³ H) ² H + 11.1 4d ⁴ 5p (³ G) ² H
373577	373728	-151	3.5	4.1 4d ⁺⁵ 5p (¹ F) ² G + 13.2 4d ⁺⁵ 5p (³ F) ⁴ D + 12.6 4d ⁺⁵ 5p (³ D) ⁴ D
374236	374163	73	1.5	28.8 4d ⁴ 5p (³ D) ⁴ P + 14.4 4d ⁴ 5p (³ G) ⁴ F + 6.2 4d ⁴ 5p (³ D) ⁴ F
374426	374536	-110	2.5	10.7 4d ⁴ 5p (¹ P) 2 D + 14.3 4d ⁴ 5p (³ G) 4 F + 10.5 4d ⁴ 5p (¹ G) 2 F
374810	374945	-135	0.5	13.5 4d ⁴ 5p (¹ S) ² P + 24.9 4d ⁴ 5p (³ D) ⁴ P + 21.7 4d ⁴ 5p (¹ P) ² P
374839	374990	-151	3.5	16.1 $4d^{4}5p$ (¹ G) ² F + 12.2 $4d^{4}5p$ (³ H) ⁴ G + 11.3 $4d^{4}5p$ (³ G) ² G
374938	375158	-220	1.5	13.1 $4d^{4}5p$ (³ G) ${}^{4}F$ + 23.2 $4d^{4}5p$ (³ D) ${}^{2}P$ + 13.6 $4d^{4}5p$ (³ D) ${}^{4}F$
975965		-87	3.5	$34.1 \ 4d^45p \ (^3G) \ ^2G + 9.6 \ 4d^45p \ (^3D) \ ^4D + 8.5 \ 4d^45p \ (^3D) \ ^2F$
373305	375452	-01		$(1 - 1)^{-1} (1 $
375365 375489	$375452 \\ 375543$	-54	0.5	$46.2 \ 4d^{4}5p \ (^{\circ}D) \ ^{4}P + 12.3 \ 4d^{4}5p \ (^{\circ}P) \ ^{2}P + 11.4 \ 4d^{4}5p \ (^{\circ}D) \ ^{4}D$
375365 375489 375593	$375452 \\ 375543 \\ 375771$	-54 -178	$0.5 \\ 4.5$	$ \begin{array}{c} 46.2 \ 4d^{2}5p \ (^{3}D) \ ^{4}P + 12.3 \ 4d^{4}5p \ (^{3}P) \ ^{2}P + 11.4 \ 4d^{4}5p \ (^{3}D) \ ^{4}D \\ 53.1 \ 4d^{4}5p \ (^{3}D) \ ^{4}F + 15.6 \ 4d^{4}5p \ (^{3}G) \ ^{2}G + 8.7 \ 4d^{4}5p \ (^{3}H) \ ^{2}G \end{array} $
375365 375489 375593 375706	375452 375543 375771 375782	-54 -178 -76	$0.5 \\ 4.5 \\ 1.5$	$\begin{array}{c} 46.2 \ 4d^{+}5p\ (^{0}D)\ ^{+}P + 12.3 \ 4d^{+}5p\ (^{+}P)\ ^{-}P + 11.4 \ 4d^{+}5p\ (^{0}D)\ ^{+}D \\ 53.1 \ 4d^{+}5p\ (^{3}D)\ ^{4}F + 15.6 \ 4d^{+}5p\ (^{3}G)\ ^{2}G + 8.7 \ 4d^{+}5p\ (^{3}H)\ ^{2}G \\ 30.9 \ 4d^{+}5p\ (^{3}D)\ ^{4}D + 11.3 \ 4d^{+}5p\ (^{3}D)\ ^{4}F + 10.5 \ 4d^{+}5p\ (^{1}D)\ ^{2}D \end{array}$
375365 375489 375593 375706 376414	375452 375543 375771 375782 376391	-54 -178 -76 23	$0.5 \\ 4.5 \\ 1.5 \\ 5.5$	$ \begin{array}{c} 46.2 \ 4d^{+}5p \ (^{0}D) \ ^{0}P + 12.3 \ 4d^{+}5p \ (^{+}P) \ ^{-}P + 11.4 \ 4d^{+}5p \ (^{0}D) \ ^{0}D \\ 53.1 \ 4d^{+}5p \ (^{3}D) \ ^{4}F + 15.6 \ 4d^{+}5p \ (^{3}G) \ ^{2}G + 8.7 \ 4d^{+}5p \ (^{3}H) \ ^{2}G \\ 30.9 \ 4d^{+}5p \ (^{3}D) \ ^{4}D + 11.3 \ 4d^{+}5p \ (^{3}D) \ ^{4}F + 10.5 \ 4d^{+}5p \ (^{1}D) \ ^{2}D \\ 30.7 \ 4d^{+}5p \ (^{3}G) \ ^{4}G + 23.3 \ 4d^{+}5p \ (^{3}G) \ ^{2}H + 17.8 \ 4d^{+}5p \ (^{3}H) \ ^{4}G \end{array} $
375365 375489 375593 375706 376414 376419	375452 375543 375771 375782 376391 376319	-54 -178 -76 23 100	$0.5 \\ 4.5 \\ 1.5 \\ 5.5 \\ 6.5$	$\begin{array}{l} 46.2 \ 4d^{+}5p \ (^{+}D) \ ^{+}P + 12.3 \ 4d^{+}5p \ (^{+}P) \ ^{+}P + 11.4 \ 4d^{+}5p \ (^{+}D) \ ^{+}D \\ 53.1 \ 4d^{+}5p \ (^{3}D) \ ^{4}F + 15.6 \ 4d^{+}5p \ (^{3}G) \ ^{2}G + 8.7 \ 4d^{+}5p \ (^{3}H) \ ^{2}G \\ 30.9 \ 4d^{+}5p \ (^{3}D) \ ^{4}D + 11.3 \ 4d^{+}5p \ (^{3}D) \ ^{4}F + 10.5 \ 4d^{+}5p \ (^{1}D) \ ^{2}D \\ 30.7 \ 4d^{+}5p \ (^{3}G) \ ^{4}G + 23.3 \ 4d^{+}5p \ (^{3}G) \ ^{2}H + 17.8 \ 4d^{+}5p \ (^{3}H) \ ^{4}G \\ 54.5 \ 4d^{+}5p \ (^{1}I) \ ^{2}I + 38.4 \ 4d^{+}5p \ (^{1}I) \ ^{2}K \end{array}$
375365 375489 375593 375706 376414 376419 376543	375452 375543 375771 375782 376391 376319 376660	-54 -178 -76 23 100 -117	$0.5 \\ 4.5 \\ 1.5 \\ 5.5 \\ 6.5 \\ 2.5$	$\begin{array}{l} 46.2 \ 4d^{5} 5p \ (^{5} D) \ ^{4} P + 12.3 \ 4d^{5} 5p \ (^{4} P) \ ^{4} P + 11.4 \ 4d^{5} 5p \ (^{5} D) \ ^{4} D \\ 53.1 \ 4d^{4} 5p \ (^{3} D) \ ^{4} F + 15.6 \ 4d^{4} 5p \ (^{3} G) \ ^{2} G + 8.7 \ 4d^{4} 5p \ (^{3} H) \ ^{2} G \\ 30.9 \ 4d^{4} 5p \ (^{3} D) \ ^{4} D + 11.3 \ 4d^{4} 5p \ (^{3} D) \ ^{4} F + 10.5 \ 4d^{4} 5p \ (^{1} D) \ ^{2} D \\ 30.7 \ 4d^{4} 5p \ (^{3} G) \ ^{4} G + 23.3 \ 4d^{4} 5p \ (^{3} D) \ ^{4} F + 17.8 \ 4d^{4} 5p \ (^{3} H) \ ^{4} G \\ 54.5 \ 4d^{4} 5p \ (^{1} I) \ ^{2} I + 38.4 \ 4d^{4} 5p \ (^{1} I) \ ^{2} K \\ 21.9 \ 4d^{4} 5p \ (^{3} D) \ ^{4} F + 16.6 \ 4d^{4} 5p \ (^{3} D) \ ^{4} D + 10 \ 4d^{4} 5p \ (^{1} F) \ ^{2} F \end{array}$
375365 375489 375593 375706 376414 376419 376543 377163	375452 375543 375771 375782 376391 376319 376660 377194	-54 -178 -76 23 100 -117 -31	0.5 4.5 1.5 5.5 6.5 2.5 3.5	46.2 4d ⁺ 5p (³ D) ⁴ P + 12.3 4d ⁺ 5p (⁴ P) ⁴ P + 11.4 4d ⁺ 5p (³ D) ⁴ D 53.1 4d ⁴ 5p (³ D) ⁴ F + 15.6 4d ⁴ 5p (³ G) ² G + 8.7 4d ⁴ 5p (³ H) ² G 30.9 4d ⁴ 5p (³ D) ⁴ D + 11.3 4d ⁴ 5p (³ D) ⁴ F + 10.5 4d ⁴ 5p (¹ D) ² D 30.7 4d ⁴ 5p (³ G) ⁴ G + 23.3 4d ⁴ 5p (³ G) ² H + 17.8 4d ⁴ 5p (³ H) ⁴ G 54.5 4d ⁴ 5p (¹ D) ² I + 38.4 4d ⁴ 5p (¹ D) ² L 21.9 4d ⁴ 5p (³ D) ⁴ F + 16.6 4d ⁴ 5p (³ D) ⁴ D + 10 4d ⁴ 5p (¹ F) ² F 27.6 4d ⁴ 5p (³ D) ⁴ F + 17.9 4d ⁴ 5p (³ D) ⁴ D + 17.1 4d ⁴ 5p (³ G) ⁴ F

E^{a}_{ern}	E^{b}_{calc}	ΔE	J	Leading components (in $\%$) in LS Coupling ^{c}
377717	377724	-7	5.5	$24.6 \ 4d^{4}5p \ (^{1}I) \ ^{2}H + 36.1 \ 4d^{4}5p \ (^{1}G) \ ^{2}H + 15.4 \ 4d^{4}5p \ (^{3}G) \ ^{2}H$
377910	377954	-44	1.5	$20.6 \ 4d^{4}5p \ (^{3}D) \ ^{2}P + 18.8 \ 4d^{4}5p \ (^{1}S) \ ^{2}P + 16 \ 4d^{4}5p \ (^{1}D) \ ^{2}P$
378355	378275	80	7.5	93.7 $4d^{4}5p(^{1}I)^{2}K + 6.1 4d^{4}5p(^{3}H)^{4}I$
379061	379296	-235	3.5	$0.1 \ 4d^{4}5p \ (^{3}D) \ ^{4}D + 21.8 \ 4d^{4}5p \ (^{1}F) \ ^{2}F + 18 \ 4d^{4}5p \ (^{1}G) \ ^{2}G$
379077	378813	264	2.5	$15.4 \ 4d^{4}5p \ (^{1}F) \ ^{2}F + 23.8 \ 4d^{4}5p \ (^{1}P) \ ^{2}D + 13.7 \ 4d^{4}5p \ (^{1}D) \ ^{2}D$
379226	379363	-137	4.5	21.8 4d ⁴ 5p (³ G) ² G + 12.2 4d ⁴ 5p (³ G) ⁴ F + 11 4d ⁴ 5p (¹ G) ² H
379478	379137	341	2.5	$26.1 \ 4d^{4}5p \ (^{3}G) \ ^{2}F + 22.2 \ 4d^{4}5p \ (^{1}D) \ ^{2}F + 17.7 \ 4d^{4}5p \ (^{1}F) \ ^{2}F$
380468	380499	-31	3.5	$12.4 \ 4d^{4}5p \ (^{3}D) \ ^{2}F + 18.6 \ 4d^{4}5p \ (^{3}G) \ ^{2}G + 15.5 \ 4d^{4}5p \ (^{1}F) \ ^{2}F$
380891	381139	-248	2.5	$31.3 \ 4d^{4}5p \ (^{1}G) \ ^{2}F + 21 \ 4d^{4}5p \ (^{3}D) \ ^{2}D + 8.2 \ 4d^{4}5p \ (^{3}F) \ ^{2}F$
382377	382360	17	4.5	$53.2 \ 4d^{4}5p \ (^{1}I)^{2}H + 11.5 \ 4d^{4}5p \ (^{3}G)^{2}H + 9.1 \ 4d^{4}5p \ (^{1}G)^{2}H$
382720	383056	-336	4.5	$34.1 \ 4d^{4}5p(^{1}G) \ ^{2}G + 20.8 \ 4d^{4}5p(^{1}G) \ ^{2}G + 12.2 \ 4d^{4}5p(^{3}G) \ ^{2}G$
383109	383073	36	2.5	$24.2 \ 4d^{4}5p \ (^{3}D) \ ^{2}F + 9 \ 4d^{4}5p \ (^{1}F) \ ^{2}F + 7.2 \ 4d^{4}5p \ (^{1}D) \ ^{2}F$
383280	383295	-15	1.5	$42.7 \ 4d^{4}5p(^{3}D) \ ^{2}D + 18.1 \ 4d^{4}5p(^{3}F) \ ^{2}D + 10.8 \ 4d^{4}5p(^{1}D) \ ^{2}D$
383539	383678	-139	5.5	$23.5 \ 4d^{4}5p(^{1}G)^{2}H + 22.3 \ 4d^{4}5p(^{1}I)^{2}H + 17.3 \ 4d^{4}5p(^{1}G)^{2}H$
384772	384719	53	3.5	$27.9 \ 4d^45p \ (^1D) \ ^2F + 17.2 \ 4d^45p \ (^1G) \ ^2G + 8.8 \ 4d^45p \ (^3F) \ ^2F$
385962	385733	229	2.5	$19.3 \ 4d^{4}5p(^{1}D) \ ^{2}D + 14.3 \ 4d^{4}5p(^{3}D) \ ^{2}F + 9.8 \ 4d^{4}5p(^{1}D) \ ^{2}F$
386268	386031	237	2.5	$16.6 \ 4d^{4}5p(^{3}D)^{2}D + 14.1 \ 4d^{4}5p(^{3}F)^{2}D + 10.7 \ 4d^{4}5p(^{3}D)^{2}F$
386582	386882	-300	1.5	$4.7 \ 4d^{4}5p \ (^{1}P) \ ^{4}P + 19 \ 4d^{4}5p \ (^{1}S) \ ^{2}P + 9.9 \ 4d^{4}5p \ (^{3}F) \ ^{4}F$
386615	386397	218	3.5	$23.4 \ 4d^{4}5p \ (^{1}F) \ ^{2}F + 23.7 \ 4d^{4}5p \ (^{1}F) \ ^{2}G + 5.6 \ 4d^{4}5p \ (^{3}F) \ ^{4}F$
388163	387921	242	3.5	$9.8 \ 4d^45p \ (^1G) \ ^2G + 25.4 \ 4d^45p \ (^1F) \ ^2G + 16.5 \ 4d^45p \ (^3D) \ ^2F$
389293	389304	-11	1.5	$46.9 \ 4d^45p \ (^3F) \ ^4F + 7.9 \ 4d^45p \ (^1P) \ ^4D + 6.3 \ 4d^45p \ (^3F) \ ^4D$
390060	390159	-99	2.5	$37.1 \ 4d^45p \ (^3F) \ ^4F + 12.3 \ 4d^45p \ (^1P) \ ^4D + 6.5 \ 4d^45p \ (^3F) \ ^4D$
390759	390631	128	4.5	$46.5 \ 4d^45p \ (^1F) \ ^2G + 29.4 \ 4d^45p \ (^3F) \ ^4F + 5 \ 4d^45p \ (^3F) \ ^2G$
391338	391254	84	3.5	$45.5 \ 4d^45p \ (^{3}F) \ ^{4}F + 11 \ 4d^45p \ (^{1}D) \ ^{2}F + 10.2 \ 4d^45p \ (^{3}F) \ ^{4}G$
391396	391582	-186	2.5	$31.1 \ 4d^45p \ (^3F) \ ^4G + 11.7 \ 4d^45p \ (^3F) \ ^4G + 10.9 \ 4d^45p \ (^3F) \ ^2F$
391553	391584	-31	1.5	$19.8 4d^45p (^{1}P) ^{4}D + 13.8 4d^45p (^{1}P) ^{4}D + 12.7 4d^45p (^{3}F) ^{2}D$
392424	392447	-23	0.5	$38.1 \ 4d^45p \ (^1P) \ ^4D + 20.9 \ 4d^45p \ (^1P) \ ^4D + 10.2 \ 4d^45p \ (^1P) \ ^4P$
392486	392444	42	4.5	$28.3 \ 4d^45p \ (^3F) \ ^4G + 19.8 \ 4d^45p \ (^1F) \ ^2G + 18.5 \ 4d^45p \ (^3F) \ ^4F$
393295	393268	27	3.5	$15.9 \ 4d^45p \ (^3F) \ ^4D + 22.8 \ 4d^45p \ (^3F) \ ^4G + 12.2 \ 4d^45p \ (^3F) \ ^2F$
393610	393485	125	1.5	19.9 $4d^{4}5p$ (¹ D) ² P + 15.1 $4d^{4}5p$ (¹ P) ⁴ P + 9.1 $4d^{4}5p$ (¹ S) ² P
394049	393914	135	2.5	11.9 $4d^{4}5p$ (¹ P) ⁴ D + 29 $4d^{4}5p$ (³ F) ⁴ F + 20.8 $4d^{4}5p$ (¹ F) ² D
396241	396260	-19	3.5	$31.4 \ 4d^45p \ (^1P) \ ^4D + 20.5 \ 4d^45p \ (^3F) \ ^2F + 13.8 \ 4d^45p \ (^1P) \ ^4D$
397858	397829	29	3.5	$25.5 4d^{4}5p (^{3}\text{F}) \ ^{4}\text{G} + 22.3 \ 4d^{4}5p (^{3}\text{F}) \ ^{4}\text{F} + 9.1 \ 4d^{4}5p (^{3}\text{F}) \ ^{4}\text{G}$
398431	398374	57	4.5	$37.2 \ 4d^45p \ ({}^3F) \ {}^4F + 24.8 \ 4d^45p \ ({}^3F) \ {}^4G + 7.8 \ 4d^45p \ ({}^1G) \ {}^2H$
398662	398784	-122	2.5	$28.6 4d^{4}5p (^{3}\text{F}) \ ^{2}\text{F} + 20.5 \ 4d^{4}5p (^{3}\text{F}) \ ^{4}\text{G} + 7.1 \ 4d^{4}5p (^{3}\text{F}) \ ^{4}\text{G}$
399022	399065	-43	5.5	77.6 $4d^{4}5p(^{3}F)^{4}G + 14.1 4d^{4}5p(^{3}F)^{4}G$
399850	399834	16	1.5	9.4 $4d^{4}5p$ (¹ P) ² D + 40.4 $4d^{4}5p$ (¹ F) ² D + 13.7 $4d^{4}5p$ (³ F) ² D
400637	400577	60	2.5	$24.2 \ 4d^{4}5p ({}^{1}F) \ {}^{2}D + 14.3 \ 4d^{4}5p ({}^{3}F) \ {}^{2}F + 9.5 \ 4d^{4}5p ({}^{1}P) \ {}^{4}D$
401561	401542	19	4.5	$33 \ 4d^{4}5p \ (^{1}G) \ ^{2}H + 13.7 \ 4d^{4}5p \ (^{1}G) \ ^{2}G + 13.6 \ 4d^{4}5p \ (^{1}G) \ ^{2}H$
403133	402978	155	3.5	19.7 $4d^{4}5p$ (¹ G) ² G + 20.8 $4d^{4}5p$ (³ F) ⁴ D + 9.6 $4d^{4}5p$ (¹ P) ⁴ D
403942	404038	-96	4.5	$50.5 \ 4d^45p \ ({}^3F) \ {}^2G + 11.7 \ 4d^45p \ ({}^3F) \ {}^2G + 10.3 \ 4d^45p \ ({}^3F) \ {}^4G$
404117	404172	-55	3.5	$27.5 \ 4d^45p \ ({}^3F) \ {}^2F + 22.3 \ 4d^45p \ ({}^3F) \ {}^4D + 6.8 \ 4d^45p \ ({}^1G) \ {}^2G$
406495	406657	-162	3.5	$46.4 \ 4d^{4}5p \ (^{3}F) \ ^{2}G + 17 \ 4d^{4}5p \ (^{3}F) \ ^{2}G + 12.3 \ 4d^{4}5p \ (^{1}G) \ ^{2}G$
406673	406743	-70	0.5	$35.7 \ 4d^{4}5p \ (^{3}F) \ ^{4}D + 18.4 \ 4d^{4}5p \ (^{3}F) \ ^{4}D + 14.8 \ 4d^{4}5p \ (^{1}P) \ ^{2}P$
409186	409360	-174	2.5	$51.4 \text{ 4d}^{4}\text{5p} ({}^{1}\text{G}) {}^{2}\text{F} + 19.4 \text{ 4d}^{4}\text{5p} ({}^{1}\text{D}) {}^{2}\text{F} + 7.6 \text{ 4d}^{4}\text{5p} ({}^{3}\text{F}) {}^{2}\text{F}$
409441	409324	117	5.5	$64.4 \ 4d^{4}5p ({}^{1}G) \ {}^{2}H + 25.2 \ 4d^{4}5p ({}^{1}G) \ {}^{2}H + 5.3 \ 4d^{4}5p ({}^{1}I) \ {}^{2}H$
409779	409465	314	4.5	$34 \ 4d^{+}5p \ (^{+}G)^{-2}G + 16.7 \ 4d^{+}5p \ (^{+}G)^{-2}G + 16.5 \ 4d^{+}5p \ (^{+}G)^{-2}H$
409889	409800	89	3.5	$40.4 \ 4d^{-5}p(^{+}G)^{-2}F + 12.6 \ 4d^{+5}p(^{+}G)^{-2}G + 9.3 \ 4d^{+5}p(^{3}F)^{-2}G$
414230	414194	36	2.5	$47 4d^{+}5p (^{\circ}F) ^{2}D + 16.5 4d^{+}5p (^{\circ}F) ^{2}D + 13 4d^{+}5p (^{1}P) ^{2}D$
422985	422971	14	2.5	$43.8 \ 4d^{-5}p({}^{+}D) \ ^{2}F + 16.1 \ 4d^{+5}p({}^{+}G) \ ^{2}F + 12.6 \ 4d^{+5}p({}^{+}G) \ ^{2}F$
428522	428612	-90	3.5	$70.1 \ 4d^{+}5p \ (^{+}D) \ ^{2}F \ + \ 15.5 \ 4d^{+}5p \ (^{+}D) \ ^{2}F \ + \ 6.7 \ 4d^{+}5p \ (^{+}G) \ ^{2}F$

Table A43: Continued

 $\frac{10.144}{\text{From Ryabtsev [45]}}$ b: This work
c: Only the component $\geq 5\%$ are given

Transitions

10001011		1 10 10 10 10 10 10 10 10 10 10 10 10 10	1	11 10 1 10	101 010	1 6	<u></u>	CD	0
	wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gi	gA	CF	
	A	$\rm cm^{-1}$		cm ⁻¹			s^{-1}		
	284.239	57962	5.5	409779	4.5	-0.17	5.60E + 10	-0.218	
	284.512	57962	5.5	409441	5.5	-0.93	9.72E + 09	-0.088	
	285.172	59223	4.5	409889	3.5	-0.44	2.96E + 10	0.251	
	285 725	59792	3.5	409779	4.5	-0.75	$1.47E \pm 10$	-0.287	
	200.120	70121	3.5 4 E	409119	9.5	-0.75	$1.47D \pm 10$ $4.19E \pm 10$	0.201	
	200.212	79131	4.5	426022	3.5	-0.3	4.12E + 10	0.281	
	286.257	53797	4.5	403133	3.5	-0.65	1.82E + 10	-0.101	
	286.265	49104	4.5	398431	4.5	-1	8.12E + 09	-0.059	
	286.735	49104	4.5	397858	3.5	-0.79	1.32E + 10	-0.171	
	287.949	53353	3.5	400637	2.5	-0.92	$9.73E \pm 0.09$	0.063	
	288.071	49104	4.5	306241	3.5	0.01	0 80E+00	0.076	
	280.071	57062	4.0 5 5	402042	4.5	-0.91	9.00E+09	0.070	
	289.034	07902	0.0	403942	4.5	-0.90	0.71E+09	0.031	
	289.572	48712	3.5	394049	2.5	-0.86	1.10E + 10	-0.096	
	289.913	30662	5.5	375593	4.5	-0.87	1.08E + 10	-0.112	
	289.944	59223	4.5	404117	3.5	-0.88	1.06E + 10	-0.086	
	290.163	53797	4.5	398431	4.5	-0.37	3.41E + 10	-0.313	
	290.536	49104	4.5	393295	3.5	-0.76	$1.37E \pm 10$	0.111	
	201.207	70705	2.5	422085	2.5	0.78	1.20E 10	0.112	
	291.307	19705	3.5	422960	2.5	-0.78	1.30E+10	0.112	
	291.814	48712	3.5	391396	2.5	-0.95	8.83E+09	0.101	
	291.863	48712	3.5	391338	3.5	-0.65	1.77E + 10	-0.117	
	291.919	51049	2.5	393610	1.5	-0.77	1.34E + 10	0.275	
	292.019	53797	4.5	396241	3.5	-0.3	3.89E + 10	0.354	
	292.261	30662	5.5	372822	6.5	-0.52	$2.36E \pm 10$	0.45	
	292 693	49104	4.5	390759	4.5	-0.22	$4.69E \pm 10$	-0.332	
	202.000	40006	1.0	280202	1.0	0.22	1.00E+10	0.125	
	293.011	48080	1.5	309293	1.5	-0.88	$1.02E \pm 10$	-0.135	
	293.388	59792	3.5	400637	2.5	-0.56	2.11E + 10	0.162	
	293.517	53353	3.5	394049	2.5	-0.6	1.96E + 10	-0.192	
	293.682	51049	2.5	391553	1.5	-0.72	1.47E + 10	0.178	
	293.712	57962	5.5	398431	4.5	-0.6	1.94E + 10	0.351	
	293.868	51049	2.5	391338	3.5	-0.85	$1.08E \pm 10$	0.194	
	204.000	50054	2.5	300050	1 5	0.72	1.45E + 10	0 109	
	294.200	53304	4.0	333000	1.0	-0.73	1.400+10	0.102	
	294.553	03/9/	4.5	393295	3.5	-0.71	1.50E+10	0.181	
	294.804	59223	4.5	398431	4.5	-0.81	1.19E + 10	-0.141	
	294.836	0	2.5	339172	2.5	-0.37	3.25E + 10	-0.71	
	294.87	53353	3.5	392486	4.5	-0.55	2.15E + 10	-0.259	
	294 934	49104	4.5	388163	3.5	-0.94	$8.85E \pm 0.9$	-0.067	
	204.076	51049	2.5	300060	2.5	0.52	$2.30E \pm 10$	0.169	
	234.310	20000	2.0	330000	2.0	-0.52	2.30 ± 10	-0.105	
	294.986	30662	5.5	369661	5.5	-0.75	1.37E+10	0.191	
	295.303	59223	4.5	397858	3.5	-0.56	2.11E+10	-0.303	
	295.309	53796	1.5	392424	0.5	-0.65	1.72E + 10	0.486	
	295.538	44011	5.5	382377	4.5	-0.06	6.61E + 10	0.331	
	295.977	39299	2.5	377163	3.5	-0.99	$7.75E \pm 0.09$	-0.074	
	206 575	20300	2.5	366573	1.5	0.88	0.00E+00	0.135	
	290.575	29390	2.5	200073	1.5	-0.88	9.99E+09	0.135	
	296.72	59223	4.5	396241	3.5	-0.84	1.09E + 10	0.107	
	296.776	72934	2.5	409889	3.5	-0.79	1.23E+10	0.153	
	296.894	30662	5.5	367483	5.5	-0.71	1.49E + 10	0.344	
	296.952	39788	1.5	376543	2.5	-0.89	9.78E + 09	-0.13	
	297.217	32994	1.5	369448	1.5	-0.62	$1.82E \pm 10$	-0.265	
	297 324	0	2.5	336333	1.5	-0.14	$5.53E \pm 10$	-0.807	
	207 508	29695	0.5	274910	0.5	0.02	0.14E+00	0.454	
	297.008	38085	0.5	374810	0.5	-0.92	9.146+09	-0.434	
	297.695	32005	2.5	367919	2.5	-0.83	1.10E + 10	-0.094	
	297.884	39788	1.5	375489	0.5	-0.75	1.35E+10	0.313	
	297.913	49104	4.5	384772	3.5	-0.4	2.99E + 10	0.21	
	297.953	55773	3.5	391396	2.5	-0.78	1.26E + 10	-0.132	
	298 065	53796	1.5	389293	1.5	-0.4	$2.99E \pm 10$	-0.394	
	208.316	44011	5.5	370226	4.5	0.22	$4.51E \pm 10$	0.288	
	298.310	20200	0.0	379220	4.5	-0.22	$4.51E \pm 10$ $1.99E \pm 10$	-0.288	
	298.394	39299	2.5	374420	2.5	-0.79	1.22E+10	-0.099	
	298.488	39788	1.5	374810	0.5	-0.91	9.27E + 09	0.263	
	298.564	39299	2.5	374236	1.5	-0.4	2.98E + 10	0.337	
	298.565	30907	4.5	365842	3.5	-0.48	2.46E + 10	0.419	
	298.59	30662	5.5	365569	4.5	-0.04	$6.91E \pm 10$	0.641	
	298 591	0	2.5	334906	3.5	0.28	$1.43E \pm 11$	-0.899	
	208.647	34605	0.5	360449	1 5	0.01	0.16E L00	0.202	
	290.04/	54000	0.5	509448	1.0	-0.91	9.10E+09	0.202	
	298.931	79705	3.5	414230	2.5	-0.88	9.83E + 09	0.42	
	299.046	48712	3.5	383109	2.5	-0.46	2.61E+10	0.139	
	299.083	30662	5.5	365017	5.5	-0.6	1.88E + 10	-0.293	
	299.303	30907	4.5	365017	5.5	-0.51	2.32E+10	-0.29	
	299.303	30662	5.5	364772	4.5	-0.81	1.14E + 10	0.153	
	299.331	48086	1.5	382164	0.5	-0.76	1.27E + 10	0.393	
	299 336	32005	2.5	366078	1.5	-0.72	$1.43E \pm 10$	-0 187	
	200.244	20200	2.5	2624=4	1 5	0.66	1.64E 10	0.10	
	299.344	29390	2.0	303434	1.0	-0.00	1.046+10	-0.19	
	299.394	48712	3.5	382720	4.5	-0.84	1.08E + 10	0.122	
	299.433	34605	0.5	368569	1.5	-0.74	1.37E + 10	-0.239	
	299.522	30907	4.5	364772	4.5	-0.23	4.43E + 10	-0.551	
	299.718	30378	3.5	364025	2.5	-0.28	3.89E + 10	-0.538	
	299.746	49104	4.5	382720	4 5	-0.55	2.10E + 10	-0.175	
	200.774	20200	9.5	262075	9.5	0.06	2.10E 10 8.19E 00	0.000	
	200.000	23330	2.0	302313	2.0	-0.90	7.805.00	-0.099	
	299.803	29390	2.5	362942	3.5	-0.97	1.89E+09	0.094	
	299.847	59792	3.5	393295	3.5	-0.91	9.14E + 09	-0.161	
	299.945	36485	3.5	369879	3.5	-0.65	1.68E + 10	-0.241	
	299.986	47119	2.5	380468	3.5	-0.94	8.48E + 09	-0.076	
	300.006	0	2.5	333327	2.5	0.04	$8.18E \pm 10$	-0.882	
	300.062	50222	4.5	303496	15	0.56	2 02E 10	0.214	
	200.003	53440	4.0	092400	4.J	-0.00	1.0000 1.10	0.214	
	300.064	03303	3.5	386615	3.5	-0.76	1.29E+10	-0.071	
	300.216	36485	3.5	369578	2.5	-0.69	1.50E + 10	0.267	
	300.225	32994	1.5	366078	1.5	-0.78	1.22E + 10	0.169	
	300.308	29390	2.5	362381	2.5	-0.5	2.37E + 10	-0.197	
	300.344	30662	5.5	363614	6.5	-0.41	$2.86E \pm 10$	-0.538	
	300.479	45546	65	378255	7 5	_0 42	2 73E-10	0.679	
	200.473	57060	0.0	200750	1.0	-0.43	2.13E+10 6.76E - 10	0.010	
	300.483	0/902	0.0	390759	4.5	-0.04	0.70E+10	-0.555	
	300.694	30378	3.5	362942	3.5	-0.66	1.62E + 10	0.234	
	300.767	36485	3.5	368968	3.5	-0.46	2.57E + 10	-0.344	
	300.851	55773	3.5	388163	3.5	-0.76	1.28E + 10	0.089	
	300.995	51049	2.5	383280	1.5	-0.95	8.31E+09	0.128	
	301.05	45546	6.5	377717	5.5	0.45	$2.07E \pm 11$	0.03	
	301.054	53706	1 5	385069	0.5	-0 02	8.61E-100	0 102	
	001.004	00190	1.0	000002	⊿.0	-0.90	0.010 ± 09	0.139	1

Table A44: Computed oscillator strengths and transition probabilities Ag VII.

Table A44: Continued

Wavelength 301.101	Lower Level 59223	J _{Low} 4.5	Upper level 391338	$\frac{J_{Up}}{3.5}$	log gf -0.83	gA 1.09E+10	CF 0.126
301.142	30378	3.5	362447	4.5	-0.67	1.59E + 10	0.23
301.173 301.187	30907 32005	$\frac{4.5}{2.5}$	362942 364025	$\frac{3.5}{2.5}$	-0.68 -0.58	1.52E+10 1.92E+10	$0.37 \\ 0.151$
301.243 301.256	47119	2.5	379077	2.5	-0.7	1.47E+10 1.31E+10	-0.098
301.29	29390	2.5	361296	2.5	-0.63	1.72E+10 1.72E+10	-0.198
301.32 301.4	$30662 \\ 30662$	5.5 5.5	362535 362447	$5.5 \\ 4.5$	-0.1 -0.02	5.88E+10 6.97E+10	$0.712 \\ 0.624$
301.402	29390	2.5	361173	3.5	-0.91	9.03E+09	-0.231
301.549 301.585	$39788 \\ 44011$	1.5 5.5	371409 375593	$1.5 \\ 4.5$	-0.89 -0.69	9.41E+09 1.51E+10	$0.196 \\ 0.302$
301.617	59792	3.5	391338	3.5	-0.21	4.56E + 10	-0.505
301.706	36485	2.5 3.5	363454 367919	$^{1.5}_{2.5}$	-0.51	2.26E + 10 3.46E + 10	$0.302 \\ 0.359$
301.919	30378	3.5	361593	3.5	-0.51	2.24E+10 2.35E+10	-0.32
302.19	30378	3.5	361296	2.5	0	7.24E+10	0.519
302.231 302.235	$45546 \\ 45546$	6.5 6.5	$376419 \\ 376414$	$6.5 \\ 5.5$	$0.03 \\ -0.24$	7.88E+10 4.19E+10	$0.56 \\ -0.371$
302.302	30378	3.5	361173	3.5	-0.08	6.03E+10	0.594
302.306	48712	2.5 3.5	379478	$^{1.5}_{2.5}$	-0.6	1.83E+10 2.34E+10	-0.198 -0.176
302.336 302.343	$79131 \\ 57413$	4.5	409889 388163	3.5	-0.04 -0.81	6.72E+10 1 14E+10	-0.545
302.345	30907	4.5	361650	4.5	0.19	1.13E+10 1.13E+11	-0.687
302.402 302.436	$30907 \\ 79131$	$4.5 \\ 4.5$	$361593 \\ 409779$	$3.5 \\ 4.5$	$0.14 \\ -0.63$	1.01E+11 1.70E+10	0.63 - 0.113
302.576	55773	3.5	386268	2.5	-0.37	3.11E+10	0.204
302.685 302.736	32005 36485	$\frac{2.5}{3.5}$	362381 366806	$\frac{2.5}{3.5}$	-0.86 -0.63	1.01E+10 1.70E+10	$0.145 \\ 0.17$
302.746	79131	4.5	409441	5.5	-0.52	2.20E+10 1.07E+10	-0.495
302.839	36485	3.5	366693	2.5	-0.28	3.80E+10	0.127 0.455
302.857 302.933	55773 59954	$3.5 \\ 2.5$	$385962 \\ 390060$	$2.5 \\ 2.5$	-0.9 -0.44	9.14E+09 2.64E+10	0.057 -0.211
302.935	30378	3.5	360482	4.5	-0.68	1.51E + 10	-0.518
303.048 303.07	$32994 \\ 49104$	$1.5 \\ 4.5$	$362975 \\ 379061$	$2.5 \\ 3.5$	-0.37 -0.2	3.10E+10 4.62E+10	$0.395 \\ -0.529$
303.192	48086	1.5	377910	1.5	-0.89	9.31E+09	0.24
303.197 303.255	53353	5.5 3.5	383109	2.5	-0.28	3.83E+10 7.49E+09	-0.543 -0.045
303.343	39788 30907	1.5	369448	1.5	-0.67	1.54E+10 3.14E+10	-0.22
303.508	79705	3.5	409186	2.5	0.1	9.10E+10	-0.642
303.56 303.622	47119 36485	2.5 3.5	$376543 \\ 365842$	2.5 3.5	-0.99 -0.97	7.50E+09 7.85E+09	0.081 - 0.157
303.666	30378	3.5	359687	3.5	-0.21	4.42E + 10	0.416
303.683 303.795	32005 57413	$2.5 \\ 2.5$	361296 386582	$\frac{2.5}{1.5}$	-0.94 -0.33	8.37E+09 3.37E+10	-0.09
303.841	71517	1.5	400637	2.5	-0.97	7.76E+09	0.208
303.95	29390	2.5	358392	2.5	-0.36	4.02E+10	$0.143 \\ 0.341$
303.952 304.155	55773 30907	3.5	384772 359687	3.5	-0.29	3.73E+10 1 10E+10	0.267
304.261	44011	5.5	372676	5.5	-0.29	3.71E+10	0.239
304.303 304.34	$39299 \\ 53797$	$2.5 \\ 4.5$	$367919 \\ 382377$	$2.5 \\ 4.5$	-0.49 -0.26	2.32E+10 3.95E+10	-0.22 -0.263
304.369	57413	2.5	385962	2.5	-0.47	2.44E+10	0.122
304.514 304.536	36485 53796	3.5 1.5	364877 382164	$2.5 \\ 0.5$	-0.79	1.17E+10 1.24E+10	-0.125 -0.447
304.569 304.612	71517	1.5	399850 364772	1.5	-0.49	2.34E+10 1.99E+10	-0.33
304.684	59954	2.5	388163	3.5	-0.76	1.24E+10 1.24E+10	-0.314
304.797 304.865	32005 30378	2.5 3.5	360092 358392	$\frac{1.5}{2.5}$	-0.38 -0.79	3.01E+10 1 17E+10	-0.305 0.232
305.035	48712	3.5	376543	2.5	-0.83	1.07E+10	0.123
305.046 305.154	47119 72934	$2.5 \\ 2.5$	374938 400637	$1.5 \\ 2.5$	-0.69 -0.47	1.47E+10 2.41E+10	-0.154
305.174	32005	2.5	359687	3.5	-0.55	2.02E+10	-0.259
305.337	39299	2.5	366806	3.5	-0.25	4.25E+10 3.99E+10	0.334
305.434 305.442	$48086 \\ 39299$	$1.5 \\ 2.5$	375489 366693	$0.5 \\ 2.5$	-0.94 -0.55	8.23E+09 2.04E+10	$0.35 \\ 0.151$
305.443	38685	0.5	366078	1.5	-0.82	1.09E + 10	0.271
305.444 305.47	59223 79131	$4.5 \\ 4.5$	406495	$3.5 \\ 3.5$	-0.1 -0.79	1.17E+10	-0.3
305.521 305.524	49104	4.5	376414	5.5	-0.69	1.47E + 10 1.19E + 10	0.137
305.553	45546	6.5	372822	6.5	0.11	9.30E+10	0.891
$305.554 \\ 305.689$	$39299 \\ 45546$	2.5 6.5	366573 372676	$1.5 \\ 5.5$	-0.83 0.39	1.07E+10 1.76E+11	0.261
305.701	47119	2.5	374236	1.5	-0.79	1.15E + 10	0.167
305.785 305.889	$30662 \\ 72934$	$5.5 \\ 2.5$	$357689 \\ 399850$	$5.5 \\ 1.5$	0.17 -0.68	1.06E+11 1.48E+10	-0.581 -0.389
305.899	39788	1.5	366693	2.5	-0.69	1.45E+10	0.144
305.976	29390 59792	⊿.ə 3.5	386615	⊿.ə 3.5	-0.36	3.12E+10	0.249 0.192
306.007 306.012	79705 39788	3.5 1.5	406495 366573	3.5 1.5	0.15 -0.47	1.00E+11 2.39E+10	-0.572 0.4
306.014	30907	4.5	357689	5.5	-0.24	4.08E + 10	0.686
306.069 306.159	$48086 \\ 59954$	$1.5 \\ 2.5$	$374810 \\ 386582$	$0.5 \\ 1.5$	-0.86 -0.3	9.77E+09 3.58E+10	-0.354 0.23
306.181	55773	3.5	382377	4.5	-0.9	8.98E+09	0.078
306.288	44011 49104	э.э 4.5	375593	$^{4.0}_{4.5}$	0.36 -0.55	2.00E+10	-0.732 0.231
306.301	59792 47110	3.5 2 F	386268 373577	2.5	-0.33	3.30E+10	-0.18
306.453	59954	2.5	386268	2.5	-0.34	3.20E+10	0.143
306.476 306.589	39788 59792	$1.5 \\ 3.5$	$366078 \\ 385962$	$1.5 \\ 2.5$	-0.7 -0.67	1.41E+10 1.52E+10	-0.207 0.171
306.631	53353	3.5	379478	2.5	-0.87	9.55E+09	0.086
306.784 306.846	$36485 \\ 36485$	$3.5 \\ 3.5$	$362447 \\ 362381$	$\frac{4.5}{2.5}$	-0.33 -0.99	3.30E+10 7.25E+09	-0.363 0.234
306.868	53353	3.5	379226	4.5	-0.87	9.61E + 09	0.11
000.014	01410	4.0	000200	1.0	-0.10	3.1213 + 10	-0.209

Table A44: Continued

Wavelength	Lower Level	JLow	Upper level	JUp	log gf	gA 4.56E+10	CF
306.98	$30662 \\ 72934$	$\frac{5.5}{2.5}$	356416 398662	$\frac{4.5}{2.5}$	-0.19	4.56E+10 1.54E+10	-0.577
307.008	53353	3.5	379077	2.5	-0.01	6.96E + 10	0.411
307.023	53353	3.5	379061	3.5	-0.69	1.44E+10	-0.12
307.035	57413 44011	2.5 5.5	383109 369661	2.5 5.5	-0.98	7.48E+09 1.84E+11	0.032
307.085	44011	5.5	369654	6.5	-0.52	2.14E + 10	0.448
307.146	39299	2.5	364877	2.5	-0.58	1.87E + 10	0.159
307.147	57962	5.5 4.5	383539	5.5	0.39	1.73E+11 6.09E+10	0.76
307.232	34605	0.5	360092	1.5	-0.57	1.89E + 10	0.366
307.287	53797	4.5	379226	4.5	-0.62	1.71E + 10	0.113
307.316	32994 53707	1.5	358392	2.5	-0.97	7.60E+09 6.21E+10	-0.225
307.581	55773	3.5	380891	2.5	-0.00	5.66E+10	0.309 0.494
307.608	39788	1.5	364877	2.5	-0.95	7.99E + 09	-0.155
307.706	79131	4.5	404117	3.5	-0.14	5.10E + 10	-0.52
307.805	79131	2.5 4.5	403942	$\frac{3.5}{4.5}$	0.19	1.18E+10 1.09E+11	-0.125
307.911	38685	0.5	363454	1.5	-0.53	2.07E + 10	0.38
307.922	57962	5.5	382720	4.5	0.09	8.66E+10	0.606
307.981	55773 51049	3.5 2.5	380468	3.5 1.5	-0.26	$1.06E \pm 10$	0.166 0.206
308.115	47119	2.5	371673	3.5	-0.93	8.33E + 09	0.085
308.142	103996	2.5	428522	3.5	-0.72	1.34E+10	0.438
308.178	32005 49104	2.5 4.5	373577	3.5 3.5	-0.2	$4.42E \pm 10$ 8 45E \pm 09	-0.355
308.244	44011	5.5	368429	4.5	-0.51	2.16E + 10	0.228
308.254	48712	3.5	373120	4.5	-0.67	1.50E + 10	0.165
308.366	47119 45546	2.5 6.5	371409 369661	1.5 5.5	-0.64	1.62E+10 1.47E+10	0.123 0.122
308.539	45546	6.5	369654	6.5	0.22	1.16E + 11	-0.791
308.581	29390	2.5	353454	3.5	-0.55	1.97E + 10	0.358
308.588	30662 70131	5.5 4 K	354719	6.5 3 F	-0.24	4.03E+10 1.01E-10	-0.545 0.275
308.645	36485	4.5 3.5	360482	$\frac{3.5}{4.5}$	-0.34	3.19E+10	-0.535
308.823	53353	3.5	377163	3.5	-0.63	1.66E + 10	0.16
308.842	51049	2.5	374839	3.5	-0.78	1.17E + 10	-0.139
308.923	55773	3.5	379478	$\frac{4.5}{2.5}$	-0.42	4.02E+10	0.202
309.027	53797	4.5	377393	4.5	-0.67	$1.49E{+}10$	0.1
309.122	59223	4.5	382720	4.5	-0.9	8.77E+09	0.05
309.157 309.188	30662 79705	э.э 3.5	403133	$^{4.5}_{3.5}$	-0.36	1.03E+10	-0.146
309.237	51049	2.5	374426	2.5	-0.47	2.36E + 10	0.261
309.247	53797	4.5	377163	3.5	-0.66	1.52E + 10	0.29
309.285	59954 72934	2.5 2.5	383280 396241	1.5 3.5	-0.5 -0.85	2.22E+10 9.86E+09	-0.127 0.224
309.369	32994	1.5	356233	2.5	-0.52	2.10E + 10	-0.322
309.418	39788	1.5	362975	2.5	-0.56	1.93E + 10	0.243
309.45	59223 48712	4.5	382377 371673	4.5 3.5	0.01	7.20E+10 5.75E+10	0.443 0.43
309.728	32005	2.5	354869	3.5	-0.69	1.43E+10	0.198
309.793	32994	1.5	355790	0.5	-0.55	1.94E + 10	-0.412
309.965	53797 30907	4.5 4.5	376414 353454	5.5 3.5	-0.66	1.52E+10 1.57E+10	0.212
310.117	47119	2.5	369578	2.5	-0.6	1.76E + 10	0.133
310.145	79131	4.5	401561	4.5	-0.38	2.87E+10	0.45
310.223	48712	3.5	371061 369448	4.5 1.5	-0.8	1.09E+10 1.30E+10	-0.137
310.263	30378	3.5	352685	2.5	-0.83	1.02E+10 1.02E+10	0.228
310.276	39299	2.5	361593	3.5	-0.61	1.70E+10	-0.174
310.337	32005 53353	2.5	354235 375365	2.5	-0.93	8.07E+09 7.93E+09	0.089
310.6	49104	4.5	371061	4.5	-0.37	2.93E+10	-0.369
310.666	49104	4.5	370993	3.5	-0.27	3.71E+10	0.306
310.698	79705	3.5	401561 368968	4.5 3.5	-0.54	2.00E+10 9.88E+09	-0.428
310.763	48712	3.5	370501	4.5	-0.85	9.83E + 09	0.099
310.883	57413	2.5	379077	2.5	-0.41	2.66E + 10	0.164
310.926	55773 53797	3.5 4.5	377393 375365	4.5 3.5	-0.95	7.80E+09 2 19E+10	-0.092 0.184
310.986	44011	5.5	365569	4.5	-0.43	2.55E+10	0.2
311.05	48086	1.5	369578	2.5	-0.79	1.13E + 10	0.191
311.056	53353 49104	3.5 4 5	374839 370488	3.5 5.5	-0.03	0.41E+10 2.57E+10	-0.37
311.27	57962	5.5	379226	4.5	-0.08	5.68E + 10	0.386
311.347	34605	0.5	355790	0.5	-0.85	9.82E+09	0.367
311.357 311.389	30907 53796	4.5 1.5	352082 374938	э.5 1.5	-0.58 -0.79	$1.82E \pm 10$ $1.11E \pm 10$	-0.285 0.25
311.415	72934	2.5	394049	2.5	-0.51	2.14E + 10	-0.388
311.43	59792	3.5	380891	2.5	-0.93	8.06E + 09	-0.093
311.456	53353 53797	$3.5 \\ 4.5$	374426 374839	2.5 3.5	-0.83 -0.74	1.01E+10 1.27E+10	-0.084 -0.115
311.525	51049	2.5	372051	2.5	-0.28	3.60E + 10	0.443
311.588	59954	2.5	380891	2.5	-0.14	5.02E + 10	-0.265
311.592	79705 79934	3.5	400637	2.5 1.5	-0.53 -0.61	2.01E+10 1.68E+10	0.32
311.886	53796	$^{2.3}_{1.5}$	374426	2.5	-0.72	1.30E+10 1.30E+10	-0.333
311.959	32994	1.5	353549	1.5	-0.6	1.74E + 10	0.274
311.999	59954 44011	2.5 5.5	380468 364518	3.5 6.5	-0.94	7.86E + 09 8 45E + 09	0.059
312.029	48086	1.5	368569	1.5	-0.77	1.17E+10	0.247
312.148	72934	2.5	393295	3.5	-0.96	7.49E + 09	-0.18
312.465	71517	1.5 4 5	391553 370226	1.5 4 F	-0.63	1.59E+10 4 44E 10	0.366
312.663	48086	4.0 1.5	367919	4.5 2.5	-0.19	4.44E + 10 1.18E + 10	-0.301
312.676	55773	3.5	375593	4.5	-0.86	9.46E + 09	0.196
312.715	53797 57962	4.5	373577	3.5 5 5	-0.77	1.17E + 10 2.06E - 10	-0.08
312.807	59792	э.э 3.5	379478	2.5	-0.52 -0.67	1.47E+10	0.173
312.835	29390	2.5	349047	3.5	-0.42	2.59E + 10	-0.32
312.899	55773	3.5	375365	3.5 5 F	-0.28	3.61E + 10	0.198
313.017	43546 47119	$\frac{0.5}{2.5}$	366573	$0.0 \\ 1.5$	-0.42 -0.97	2.02E+10 7.26E+09	-0.094
313.057	57962	5.5	377393	4.5	-0.1	5.37E + 10	-0.256
			264				

Table A44: Continued

Wavelength	Lower Level	JLow	Upper level	J_{Up}	log gf	gA	CF
313.143	30378	3.5	349721	4.5	-0.77	1.16E + 10	0.23
313.163	53797	4.5	373120	4.5	-0.47	2.28E + 10	0.196
313.2	59792	3.5	379077	2.5	-0.49	2.18E+10	-0.188
313.209	32994	1.5	352270	0.5	-0.87	9.16E + 09 8.86E + 00	0.325 0.153
313.359	59954	2.5	379077	$\frac{2.5}{2.5}$	-0.88	$7.89E \pm 09$	-0.133
313.375	59954	2.5	379061	3.5	-0.5	2.15E + 10	-0.197
313.422	30662	5.5	349721	4.5	-0.56	1.88E + 10	0.359
313.507	45546	6.5	364518	6.5	-0.9	8.50E + 09	-0.061
313.522	79705	3.5	398662	2.5	-0.73	1.27E + 10	-0.16
313.599	53797	4.5	372676	5.5	-0.97	7.30E + 09	-0.123
313.647	51049	2.5	369879	3.5 5.5	-0.81	1.04E + 10 1.02E + 10	0.186
313.948	59223	4.5	377717	5.5	-0.82	$1.03E \pm 10$ 1.36E ± 10	0.177
313 985	48086	1.5	366573	1.5	-0.58	$1.30E \pm 10$ $1.77E \pm 10$	-0.286
314.014	57962	5.5	376419	6.5	-0.31	3.34E + 10	-0.597
314.035	44011	5.5	362447	4.5	-0.74	1.24E + 10	-0.172
314.086	36485	3.5	354869	3.5	-0.63	1.57E + 10	0.13
314.213	53796	1.5	372051	2.5	-0.51	2.09E + 10	0.342
314.297	59223	4.5	377393	4.5	-0.49	2.21E+10	-0.12
314.303	104821	1.5	422985	2.5	-0.48	$2.23E \pm 10$ 1.00E ± 10	0.413
314.546	51049	2.5	368968	3.5	-0.6	$1.09E \pm 10$ 1.70E ± 10	-0.287
314.659	55773	3.5	373577	3.5	-1	6.81E + 09	-0.065
314.713	36485	3.5	354235	2.5	-0.88	8.84E + 09	0.134
314.747	30662	5.5	348377	4.5	-0.4	2.66E + 10	0.251
314.754	53353	3.5	371061	4.5	-0.81	1.05E+10	-0.145
314.797	34605	0.5	352270	0.5	-0.76	1.17E + 10	0.411
314.823	44011	5.5	361650	4.5	-0.98	7.04E + 09	0.078
314.849	53790 50702	1.5	371409	1.5	-0.67	$1.44E \pm 10$ $1.70E \pm 10$	-0.394
315.112	55773	3.5	373120	4.5	-0.63	1.57E + 10	0.266
315.262	53797	4.5	370993	3.5	-0.55	1.91E + 10	-0.212
315.267	59223	4.5	376414	5.5	-0.29	3.44E + 10	0.561
315.328	48712	3.5	365842	3.5	-0.45	2.41E+10	0.206
315.332	72934	2.5	390060	2.5	-0.68	1.39E+10	0.357
315.348	79131	4.5	396241	3.5	-0.8	1.06E + 10	0.119
315.551	47119	2.5	364025	2.5	-0.68	1.40E + 10 $1.44E \pm 10$	0.115 0.007
315.765	53797	4.5	370488	5.5	-0.85	9.45E+09	0.14
316.292	57413	2.5	373577	3.5	-0.62	1.60E + 10	0.155
316.374	53797	4.5	369879	3.5	-0.74	1.21E + 10	-0.119
316.543	49104	4.5	365017	5.5	-0.42	2.51E + 10	0.504
316.592	53797	4.5	369661	5.5	-0.78	1.11E + 10	-0.145
316.655	59792	3.5	375593	4.5	-0.69	1.37E+10	-0.298
216 941	49104	4.5	304772	4.5	-0.00	1.44E + 10 2.82E + 10	0.175
316.887	39223	4.5	354869	3.5	-0.57	$2.82E \pm 10$ 1.65E \pm 10	-0.255
317.305	30907	4.5	346061	3.5	-0.2	4.17E+10	0.301
317.413	59792	3.5	374839	3.5	-0.47	2.27E + 10	-0.223
317.597	38685	0.5	353549	1.5	-0.98	6.93E + 09	-0.175
317.735	55773	3.5	370501	4.5	-0.87	8.89E + 09	0.13
317.749	57962	5.5	372676	5.5	-0.43	2.47E+10	-0.108
317.832	53797	4.5	368429	4.5	-0.66	1.45E + 10	0.237
318 113	59223	4.5	373577	2.5 3.5	-0.82	1.00E+10 1.00E+10	-0.287
318.15	30378	3.5	344695	2.5	-0.68	1.39E+10	0.169
318.172	48086	1.5	362381	2.5	-0.72	1.25E + 10	0.232
318.205	48712	3.5	362975	2.5	-0.79	1.07E + 10	-0.128
318.305	79131	4.5	393295	3.5	-0.48	2.17E + 10	-0.255
318.476	57413	2.5	371409	1.5	-0.66	1.46E + 10	-0.117
318.69	59792	3.5	373577	3.5	-0.85	9.36E + 09	0.101
319 127	79131	2.5 4.5	392486	4.5	-0.54	$1.90E \pm 10$ 1.66E ± 10	-0.335
319.139	49104	4.5	362447	4.5	-0.61	1.62E + 10	0.182
319.148	72934	2.5	386268	2.5	-0.64	1.52E + 10	-0.125
319.532	30378	3.5	343336	2.5	-0.39	2.69E + 10	0.305
319.552	48712	3.5	361650	4.5	-0.61	1.60E + 10	0.154
319.61	48712	3.5	361593	3.5	-0.78	1.09E + 10 1.01E + 10	0.08
319.905	29390	2.0	341983	1.5	-0.53	1.91E+10 1.41E+10	0.333
320.343	57413	2.5	369578	2.5	-0.78	$1.08E \pm 10$	0.093
320.624	36485	3.5	348377	4.5	-0.87	8.80E + 09	0.372
320.635	59792	3.5	371673	3.5	-0.86	8.93E + 09	-0.092
320.756	71517	1.5	383280	1.5	-0.41	2.55E+10	-0.35
320.82	32994	1.5	344695	2.5	-0.92	7.73E + 09	0.276
320.822	57962 70705	0.0 2 E	309001	0.0 0.5	-0.82	$9.88E \pm 10$	0.062
320.831	30662	5.5	342289	2.5 4.5	-0.47	$1.88E \pm 10$	-0.288
321.111	53353	3.5	364772	4.5	-0.95	7.34E + 09	0.099
321.202	32005	2.5	343336	2.5	-0.65	1.47E + 10	0.178
321.336	59792	3.5	370993	3.5	-0.9	8.10E + 09	0.107
321.845	59792	3.5	370501	4.5	-0.83	9.58E + 09	0.143
321.909	71517	1.5	382164	0.5	-0.58	1.67E + 10	-0.437
322.008	103996	4.5 2.5	41408	3.3 2.5	-0.81	9.91E+09 6.32E+10	-0.222
322.604	32005	2.5	341983	1.5	-0.92	7.72E+0.9	0.14
322.793	55773	3.5	365569	4.5	-0.93	7.56E + 09	-0.309
322.846	59223	4.5	368968	3.5	-0.96	7.04E + 09	-0.051
323.022	36485	3.5	346061	3.5	-0.88	8.48E + 09	0.362
323.197	104821	1.5	414230	2.5	-0.55	1.81E+10	-0.427
323.591	19131	4.5 1 F	356002	3.5 1 F	-0.64	1.47E+10 0.05E / 00	-0.144
323.122	40000 53797	1.0 4.5	362535	1.0 5.5	-0.85	$1.96E \pm 10$	-0.139
324.06	49104	4.5	357689	5.5	-0.5	2.02E+10	0.223
324.224	57413	2.5	365842	3.5	-0.76	1.10E + 10	-0.135
324.401	59223	4.5	367483	5.5	-0.9	7.89E + 09	-0.314
324.43	32994	1.5	341227	0.5	-1	6.27E + 09	-0.421
324.454	36485	3.5	344695	2.5	-0.86	8.77E+09	-0.194
324.716	71517	1.5 9 F	379478	2.5 2 F	-0.36	2.78E+10 7.27E+00	-0.531
325.107	12934 49104	2.0 4.5	356493	3.5 3.5	-0.94	$1.93E \pm 10$	0.117 0.203
325.891	36485	3.5	343336	2.5	-0.68	1.30E + 10	0.196
326.205	57962	5.5	364518	6.5	-0.67	1.33E + 10	-0.339
326.44	47119	2.5	353454	3.5	-0.67	$1.33E{+}10$	0.175
326.523	79705	3.5	385962	2.5	-0.8	9.98E + 09	0.118

Table	A44	Continued

		rable	A44: U01	umue	ea		
Wavelength	Lower Level	J_{Low}	Upper level	J_{Up}	log gf	gA	CF
326.63	48712	3.5	354869	3.5	-0.76	1.09E + 10	-0.23
326.912	103996	2.5	409889	3.5	-0.26	3.46E + 10	0.466
327.049	49104	4.5	354869	3.5	-0.4	2.50E + 10	0.231
327.181	79131	4.5	384772	3.5	-0.8	9.93E + 09	-0.102
327.308	48712	3.5	354235	2.5	-0.64	1.43E + 10	0.167
327.444	39299	2.5	344695	2.5	-0.64	1.44E + 10	0.301
327.665	103996	2.5	409186	2.5	-0.61	1.53E + 10	0.515
327.89	59792	3.5	364772	4.5	-0.94	7.17E + 09	-0.146
328.506	79131	4.5	383539	5.5	-0.98	6.51E + 09	-0.089
328.553	104821	1.5	409186	2.5	-0.45	2.21E+10	0.263
329.393	79131	4.5	382720	4.5	-0.97	6.61E + 09	-0.055
329.831	51049	2.5	354235	2.5	-0.77	1.04E + 10	-0.169
329.964	53353	3.5	356416	4.5	-0.88	8.13E + 09	0.16
330.017	79705	3.5	382720	4.5	-0.97	6.64E + 09	-0.174
330.391	79705	3.5	382377	4.5	-0.52	1.86E + 10	0.235
332.146	53797	4.5	354869	3.5	-0.97	6.55E + 09	0.109
332.356	53353	3.5	354235	2.5	-0.96	6.61E + 09	0.084
332.481	53353	3.5	354122	4.5	-0.88	7.91E + 09	-0.158
332.488	79705	3.5	380468	3.5	-0.63	1.40E + 10	-0.142
333.199	103996	2.5	404117	3.5	-0.38	2.50E + 10	0.593
333.228	79131	4.5	379226	4.5	-0.82	9.06E + 09	-0.132
334.23	32005	2.5	331200	1.5	-0.84	8.58E + 09	0.251
335.276	79131	4.5	377393	4.5	-0.85	8.46E + 09	-0.077
335.504	72934	2.5	370993	3.5	-0.74	1.07E + 10	0.244
337.311	79131	4.5	375593	4.5	-0.72	1.11E + 10	0.198
338.048	104821	1.5	400637	2.5	-1	5.80E + 09	-0.153
338.226	79705	3.5	375365	3.5	-0.8	9.24E + 09	-0.132
340.663	79131	4.5	372676	5.5	-0.36	2.53E+10	-0.472

 $\begin{array}{cccc} 4.5 & 372676 & 5.5 \\ a: \ Energy \ Levels \ from \ [44, 45] \end{array}$